

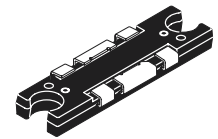
The RF MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

MRF1535T1
MRF1535FT1

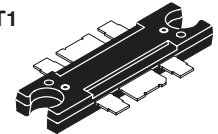
Designed for broadband commercial and industrial applications with frequencies to 520 MHz. The high gain and broadband performance of these devices make them ideal for large-signal, common source amplifier applications in 12.5 volt mobile FM equipment.

- Specified Performance @ 520 MHz, 12.5 Volts
Output Power — 35 Watts
Power Gain — 10.0 dB
Efficiency — 50%
- Capable of Handling 20:1 VSWR, @ 15.6 Vdc, 520 MHz, 2 dB Overdrive
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters
- Broadband-Full Power Across the Band: 135-175 MHz
400-470 MHz
450-520 MHz
- Broadband UHF/VHF Demonstration Amplifier Information Available Upon Request
- In Tape and Reel. T1 Suffix = 500 Units per 44 mm, 13 inch Reel.

520 MHz, 35 W, 12.5 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs



CASE 1264-09, STYLE 1
TO-272
PLASTIC
MRF1535T1



CASE 1264A-02, STYLE 1
TO-272 STRAIGHT LEAD
PLASTIC
MRF1535FT1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V _{DSS}	40	Vdc
Gate-Source Voltage	V _{GS}	±20	Vdc
Drain Current — Continuous	I _D	6	Adc
Total Device Dissipation @ T _C = 25°C (1) Derate above 25°C	P _D	135 0.50	Watts W/°C
Storage Temperature Range	T _{stg}	-65 to +150	°C
Operating Junction Temperature	T _J	175	°C

THERMAL CHARACTERISTICS

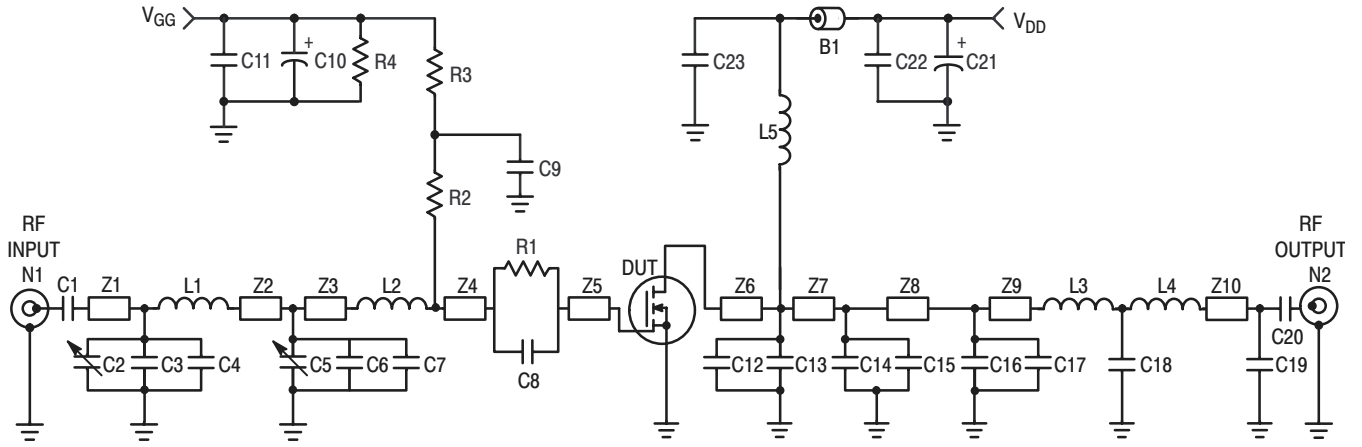
Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	R _{θJC}	0.90	°C/W

(1) Calculated based on the formula $P_D = \frac{T_J - T_C}{R_{\theta JC}}$

NOTE — **CAUTION** — MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ Vdc}$, $I_D = 100\ \mu\text{Adc}$)	$V_{(BR)DSS}$	60	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 60\text{ Vdc}$, $V_{GS} = 0\text{ Vdc}$)	I_{DSS}	—	—	1	μAdc
Gate–Source Leakage Current ($V_{GS} = 10\text{ Vdc}$, $V_{DS} = 0\text{ Vdc}$)	I_{GSS}	—	—	0.3	μAdc
ON CHARACTERISTICS					
Gate Threshold Voltage ($V_{DS} = 12.5\text{ Vdc}$, $I_D = 400\ \mu\text{A}$)	$V_{GS(th)}$	1	—	2.6	Vdc
Drain–Source On–Voltage ($V_{GS} = 5\text{ Vdc}$, $I_D = 0.6\text{ A}$)	$R_{DS(on)}$	—	—	0.7	Ω
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 2.0\text{ Adc}$)	$V_{DS(on)}$	—	—	1	Vdc
DYNAMIC CHARACTERISTICS					
Input Capacitance (Includes Input Matching Capacitance) ($V_{DS} = 12.5\text{ Vdc}$, $V_{GS} = 0\text{ V}$, $f = 1\text{ MHz}$)	C_{iss}	—	—	250	pF
Output Capacitance ($V_{DS} = 12.5\text{ Vdc}$, $V_{GS} = 0\text{ V}$, $f = 1\text{ MHz}$)	C_{oss}	—	—	150	pF
Reverse Transfer Capacitance ($V_{DS} = 12.5\text{ Vdc}$, $V_{GS} = 0\text{ V}$, $f = 1\text{ MHz}$)	C_{rss}	—	—	20	pF
RF CHARACTERISTICS (In Motorola Test Fixture)					
Common–Source Amplifier Power Gain ($V_{DD} = 12.5\text{ Vdc}$, $P_{out} = 35\text{ Watts}$, $I_{DQ} = 500\text{ mA}$) $f = 520\text{ MHz}$	G_{ps}	10	—	—	dB
Drain Efficiency ($V_{DD} = 12.5\text{ Vdc}$, $P_{out} = 35\text{ Watts}$, $I_{DQ} = 500\text{ mA}$) $f = 520\text{ MHz}$	η	50	—	—	%
Load Mismatch ($V_{DD} = 15.6\text{ Vdc}$, $f = 520\text{ MHz}$, 2 dB Input Overdrive, VSWR 20:1 at All Phase Angles)	Ψ	No Degradation in Output Power Before and After Test			



B1	Ferroxcube #VK200	L4	1 Turn, #26 AWG, 0.240" ID
C1, C9, C20, C23	330 pF, 100 mil Chip Capacitors	L5	4 Turn, #24 AWG, 0.180" ID
C2, C5	0 to 20 pF Trimmer Capacitors	N1, N2	Type N Flange Mounts
C3, C15	33 pF, 100 mil Chip Capacitors	R1	6.5 Ω, 1/4 W Chip Resistor
C4, C6, C19	18 pF, 100 mil Chip Capacitors	R2	39 Ω Chip Resistor (0805)
C7	160 pF, 100 mil Chip Capacitor	R3	1.2 kΩ, 1/8 W Chip Resistor
C8	240 pF, 100 mil Chip Capacitor	R4	33 kΩ, 1/4 W Chip Resistor
C10, C21	10 μF, 50 V Electrolytic Capacitors	Z1	0.970" x 0.080" Microstrip
C11, C22	470 pF, 100 mil Chip Capacitors	Z2	0.380" x 0.080" Microstrip
C12, C13	150 pF, 100 mil Chip Capacitors	Z3	0.190" x 0.080" Microstrip
C14	110 pF, 100 mil Chip Capacitor	Z4	0.160" x 0.080" Microstrip
C16	68 pF, 100 mil Chip Capacitor	Z5, Z6	0.110" x 0.200" Microstrip
C17	120 pF, 100 mil Chip Capacitor	Z7	0.490" x 0.080" Microstrip
C18	51 pF, 100 mil Chip Capacitor	Z8	0.250" x 0.080" Microstrip
L1	17.5 nH, Coilcraft #A05T	Z9	0.320" x 0.080" Microstrip
L2	5 nH, Coilcraft #A02T	Z10	0.240" x 0.080" Microstrip
L3	1 Turn, #26 AWG, 0.250" ID	Board	Glass Teflon®, 31 mils

Figure 1. 135 – 175 MHz Broadband Test Circuit

TYPICAL CHARACTERISTICS, 135 – 175 MHz

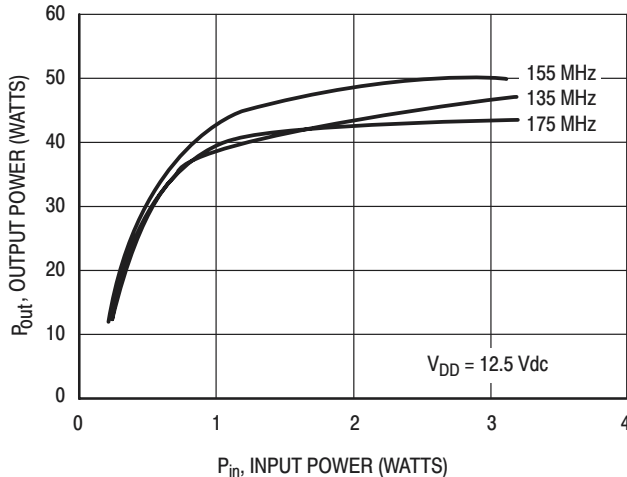


Figure 2. Output Power versus Input Power

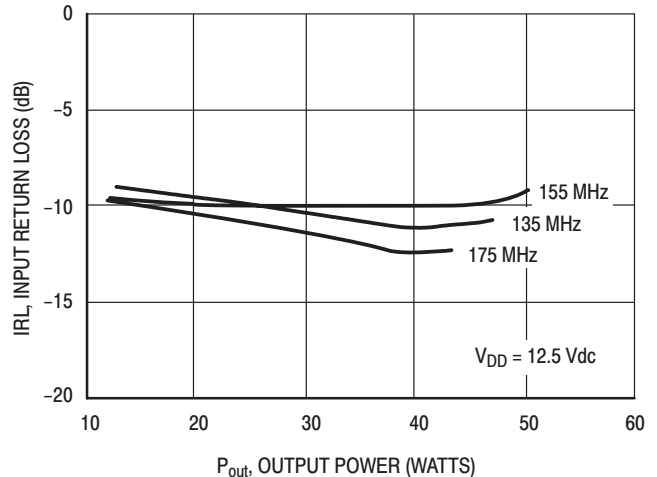


Figure 3. Input Return Loss versus Output Power

TYPICAL CHARACTERISTICS, 135 – 175 MHz

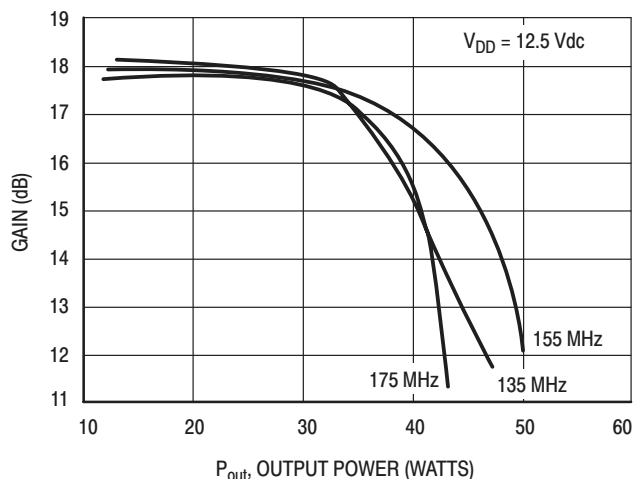


Figure 4. Gain versus Output Power

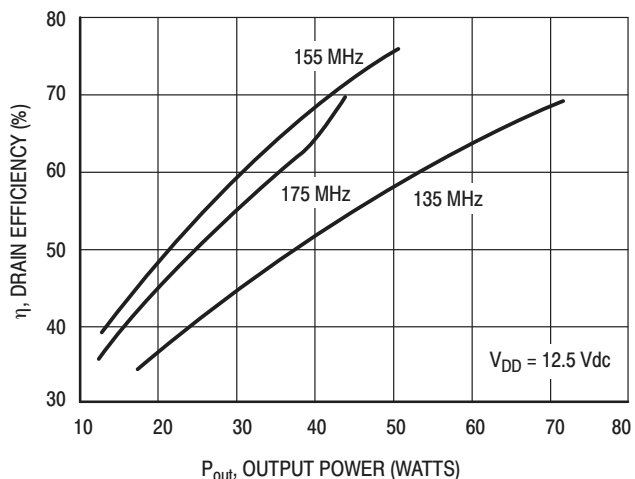


Figure 5. Drain Efficiency versus Output Power

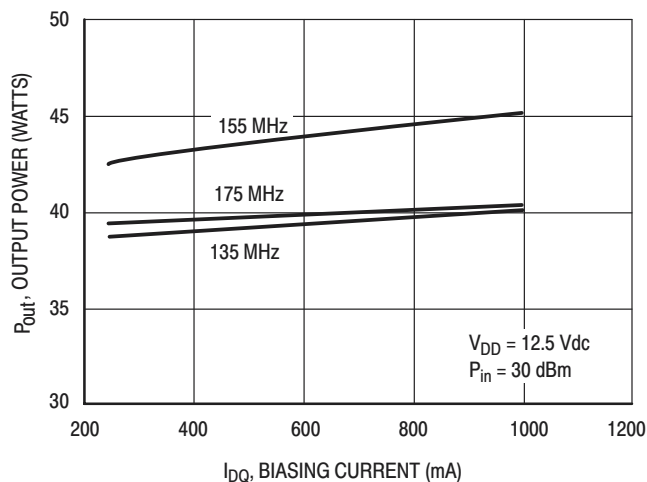


Figure 6. Output Power versus Biasing Current

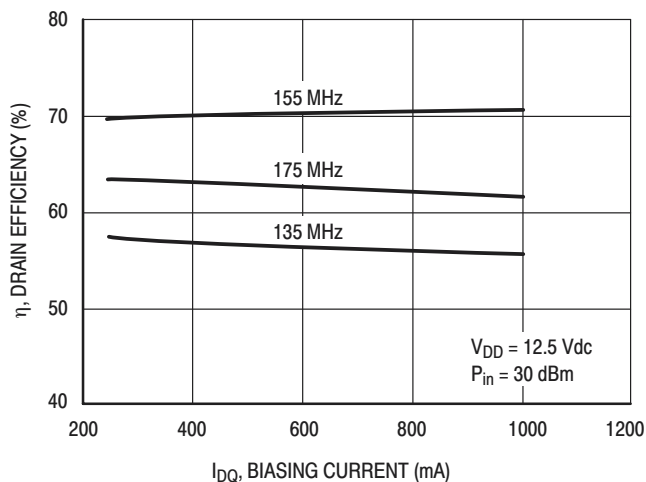


Figure 7. Drain Efficiency versus Biasing Current

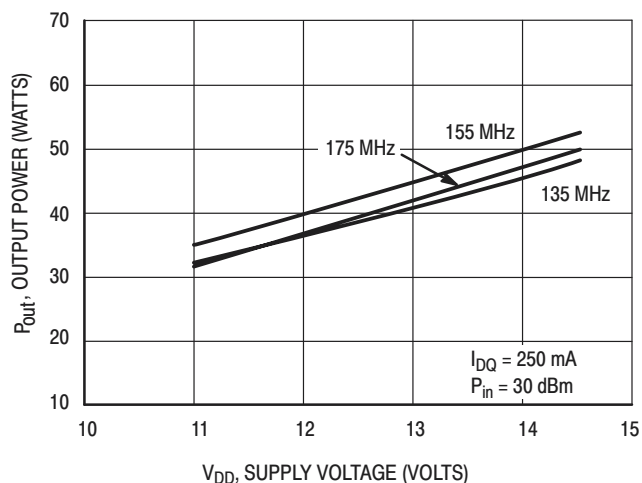


Figure 8. Output Power versus Supply Voltage

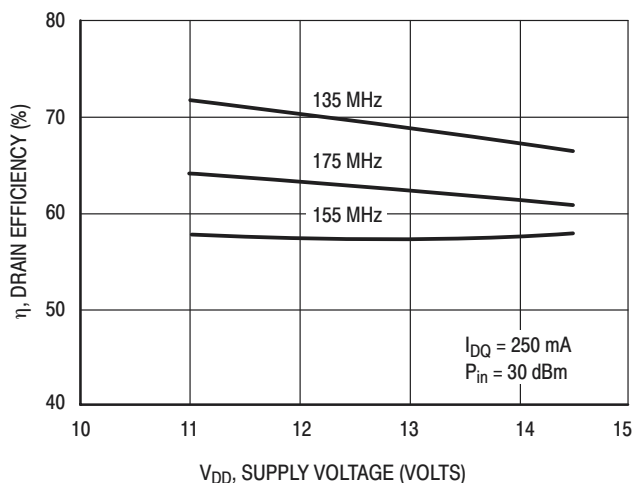
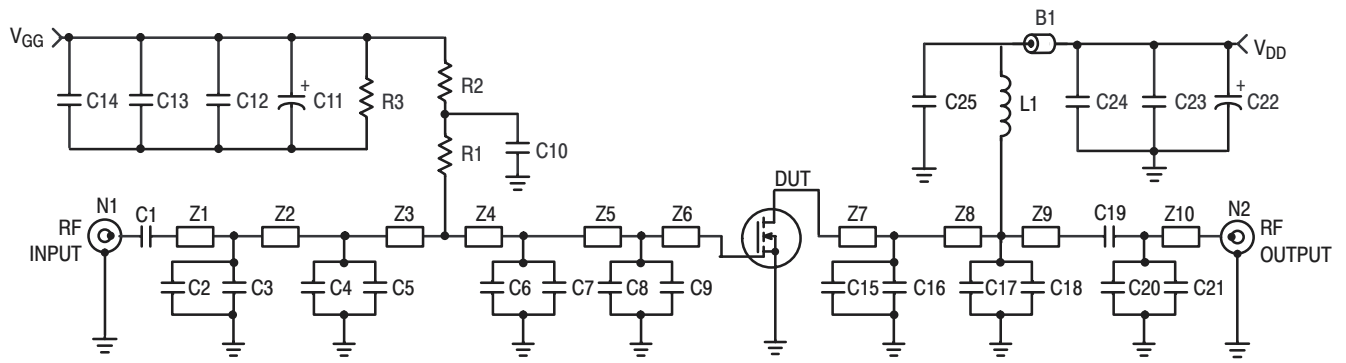


Figure 9. Drain Efficiency versus Supply Voltage



B1	Ferroxcube VK200	C21	1.8 pF, 100 mil Chip Capacitor
C1	160 pF, 100 mil Chip Capacitor	L1	47.5 nH, 5 Turn, Coilcraft
C2	3 pF, 100 mil Chip Capacitor	N1, N2	Type N Flange Mounts
C3	3.6 pF, 100 mil Chip Capacitor	R1	500 Ω Chip Resistor (0805)
C4	2.2 pF, 100 mil Chip Capacitor	R2	1 k Ω Chip Resistor (0805)
C5	10 pF, 100 mil Chip Capacitor	R3	33 k Ω , 1/8 W Chip Resistor
C6, C7	16 pF, 100 mil Chip Capacitors	Z1	0.480" x 0.080" Microstrip
C8, C15, C16	27 pF, 100 mil Chip Capacitors	Z2	1.070" x 0.080" Microstrip
C9	43 pF, 100 mil Chip Capacitor	Z3	0.290" x 0.080" Microstrip
C10, C14, C25	160 pF, 100 mil Chip Capacitors	Z4	0.160" x 0.080" Microstrip
C11, C22	10 μ F, 50 V Electrolytic Capacitors	Z5, Z8	0.120" x 0.080" Microstrip
C12, C24	1,200 pF, 100 mil Chip Capacitors	Z6, Z7	0.120" x 0.223" Microstrip
C13, C23	0.1 μ F, 100 mil Chip Capacitors	Z9	1.380" x 0.080" Microstrip
C17, C18	24 pF, 100 mil Chip Capacitors	Z10	0.625" x 0.080" Microstrip
C19	160 pF, 100 mil Chip Capacitor	Board	Glass Teflon [®] , 31 mils
C20	8.2 pF, 100 mil Chip Capacitor		

Figure 10. 450 – 520 MHz Broadband Test Circuit

TYPICAL CHARACTERISTICS, 450 – 520 MHz

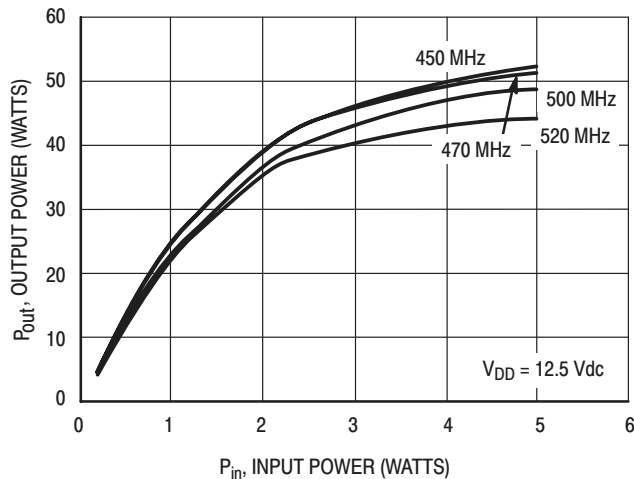


Figure 11. Output Power versus Input Power

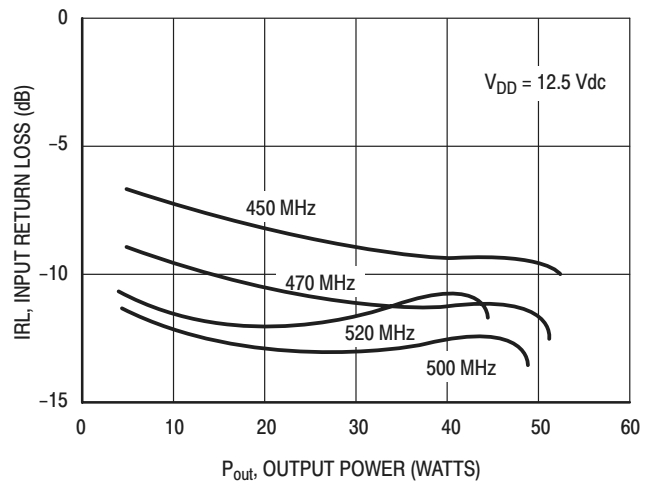


Figure 12. Input Return Loss versus Output Power

TYPICAL CHARACTERISTICS, 450 – 520 MHz

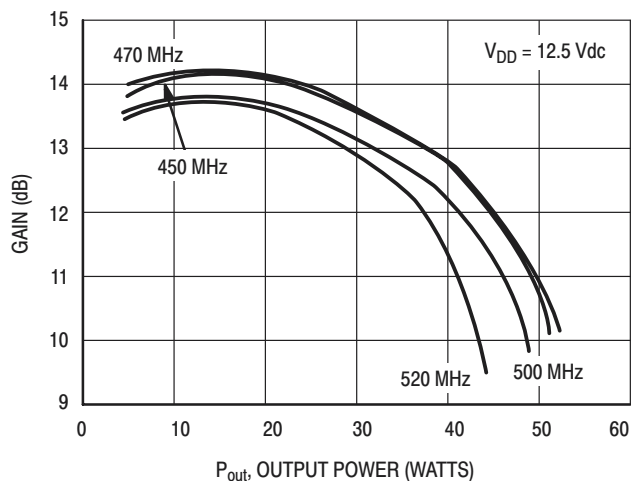


Figure 13. Gain versus Output Power

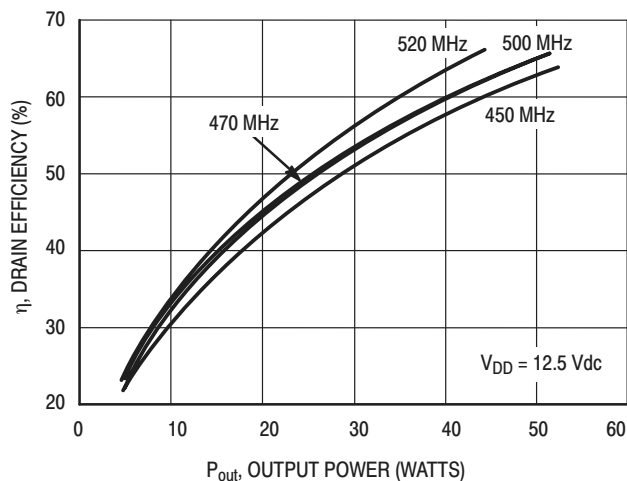


Figure 14. Drain Efficiency versus Output Power

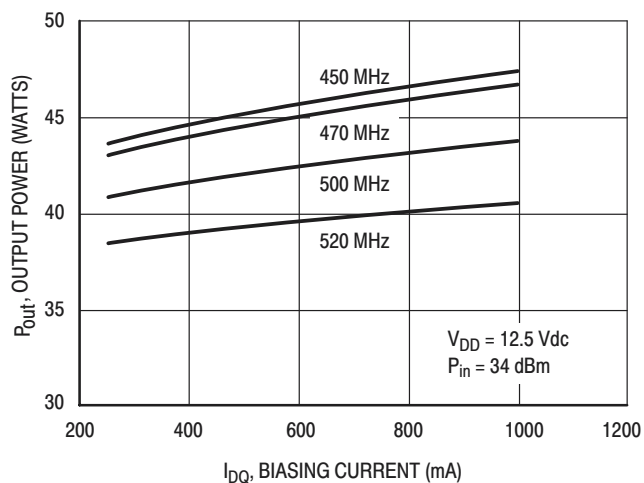


Figure 15. Output Power versus Biasing Current

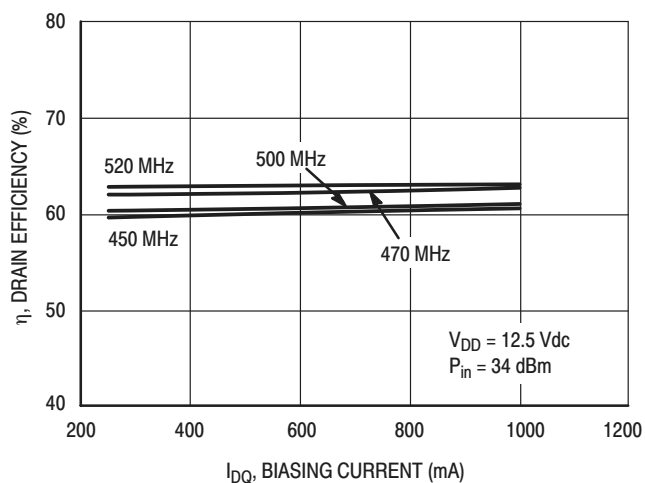


Figure 16. Drain Efficiency versus Biasing Current

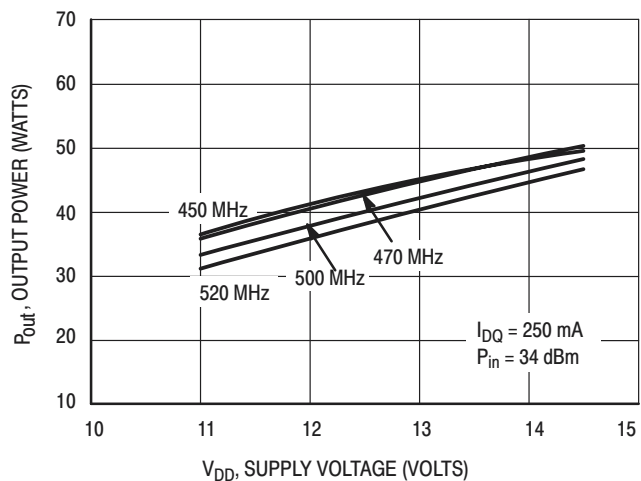


Figure 17. Output Power versus Supply Voltage

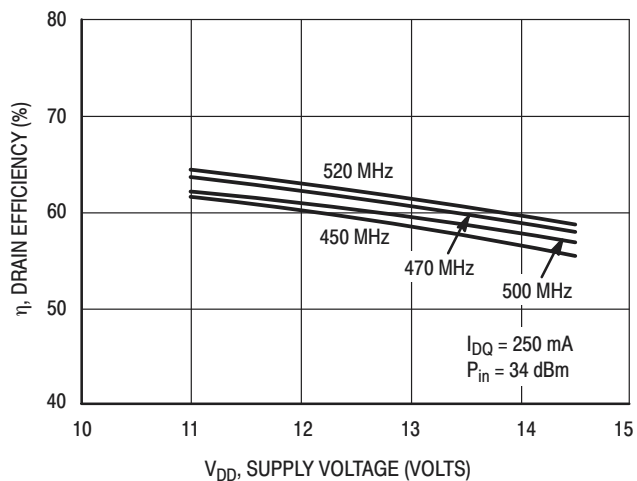
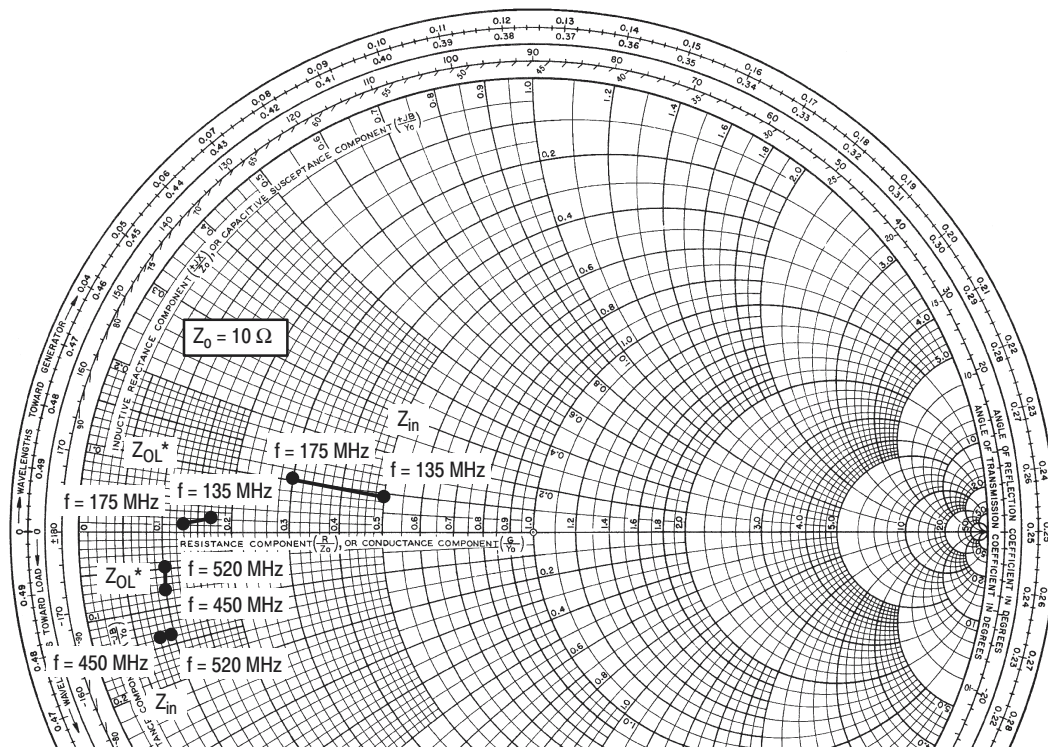


Figure 18. Drain Efficiency versus Supply Voltage



$V_{DD} = 12.5\text{ V}$, $I_{DQ} = 250\text{ mA}$, $P_{out} = 35\text{ W}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
135	$5.0 + j0.9$	$1.7 + j0.2$
155	$5.0 + j0.9$	$1.7 + j0.2$
175	$3.0 + j1.0$	$1.3 + j0.1$

$V_{DD} = 12.5\text{ V}$, $I_{DQ} = 500\text{ mA}$, $P_{out} = 35\text{ W}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
450	$0.8 - j1.4$	$1.0 - j0.8$
470	$0.9 - j1.4$	$1.1 - j0.6$
500	$1.0 - j1.4$	$1.1 - j0.6$
520	$0.9 - j1.4$	$1.1 - j0.5$

Z_{in} = Complex conjugate of source impedance.

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Z_{OL}^* = Complex conjugate of the load impedance at given output power, voltage, frequency, and $\eta_D > 50\%$.

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Note: Z_{OL}^* was chosen based on tradeoffs between gain, drain efficiency, and device stability.

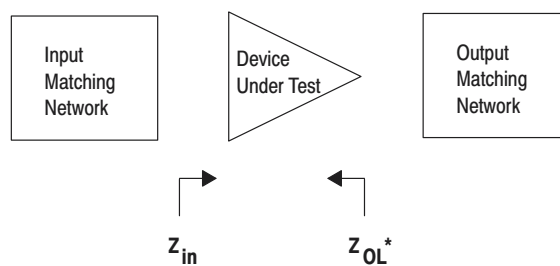


Figure 19. Series Equivalent Input and Output Impedance

Table 1. Common Source Scattering Parameters ($V_{DD} = 12.5$ Vdc)

$I_{DQ} = 250$ mA

f MHz	S_{11}		S_{21}		S_{12}		S_{22}	
	$ S_{11} $	$\angle \phi$	$ S_{21} $	$\angle \phi$	$ S_{12} $	$\angle \phi$	$ S_{22} $	$\angle \phi$
50	0.89	-173	8.496	83	0.014	-26	0.76	-170
100	0.90	-175	3.936	72	0.014	-14	0.79	-170
150	0.91	-175	2.429	63	0.011	-23	0.82	-170
200	0.92	-175	1.627	57	0.010	-44	0.86	-170
250	0.94	-176	1.186	53	0.007	-16	0.88	-170
300	0.95	-176	0.888	49	0.005	-44	0.91	-171
350	0.96	-176	0.686	48	0.005	36	0.92	-170
400	0.96	-176	0.568	44	0.005	-1	0.94	-171
450	0.97	-176	0.457	44	0.004	49	0.94	-172
500	0.97	-176	0.394	44	0.003	-51	0.95	-171
550	0.98	-176	0.332	42	0.001	31	0.95	-173
600	0.98	-177	0.286	41	0.013	99	0.94	-173

$I_{DQ} = 1.0$ A

f MHz	S_{11}		S_{21}		S_{12}		S_{22}	
	$ S_{11} $	$\angle \phi$	$ S_{21} $	$\angle \phi$	$ S_{12} $	$\angle \phi$	$ S_{22} $	$\angle \phi$
50	0.90	-173	8.49	83	0.006	-39	0.86	-176
100	0.90	-175	3.92	72	0.009	-5	0.86	-176
150	0.91	-175	2.44	63	0.006	7	0.87	-176
200	0.92	-175	1.62	57	0.008	21	0.88	-175
250	0.94	-176	1.19	53	0.006	8	0.89	-174
300	0.95	-176	0.89	48	0.008	3	0.89	-174
350	0.96	-176	0.69	48	0.007	48	0.91	-174
400	0.96	-176	0.57	44	0.004	41	0.93	-173
450	0.97	-176	0.46	44	0.004	43	0.93	-173
500	0.97	-176	0.39	44	0.003	57	0.94	-173
550	0.98	-176	0.33	41	0.006	62	0.94	-174
600	0.98	-177	0.28	41	0.009	96	0.93	-173

$I_{DQ} = 2.0$ A

f MHz	S_{11}		S_{21}		S_{12}		S_{22}	
	$ S_{11} $	$\angle \phi$	$ S_{21} $	$\angle \phi$	$ S_{12} $	$\angle \phi$	$ S_{22} $	$\angle \phi$
50	0.94	-176	9.42	88	0.005	-72	0.89	-177
100	0.94	-178	4.56	82	0.005	4	0.89	-177
150	0.94	-178	2.99	78	0.003	7	0.89	-177
200	0.94	-178	2.14	74	0.005	17	0.90	-176
250	0.95	-178	1.67	71	0.004	40	0.90	-175
300	0.95	-178	1.32	67	0.007	35	0.91	-175
350	0.95	-178	1.08	67	0.005	57	0.92	-174
400	0.96	-178	0.93	63	0.003	50	0.93	-173
450	0.96	-178	0.78	62	0.007	68	0.93	-173
500	0.96	-177	0.68	61	0.004	99	0.94	-173
550	0.97	-177	0.59	58	0.008	78	0.93	-175
600	0.97	-178	0.51	57	0.009	92	0.92	-174

APPLICATIONS INFORMATION

DESIGN CONSIDERATIONS

This device is a common-source, RF power, N-Channel enhancement mode, Lateral Metal-Oxide Semiconductor Field-Effect Transistor (MOSFET). Motorola Application Note AN211A, "FETs in Theory and Practice", is suggested reading for those not familiar with the construction and characteristics of FETs.

This surface mount packaged device was designed primarily for VHF and UHF mobile power amplifier applications. Manufacturability is improved by utilizing the tape and reel capability for fully automated pick and placement of parts. However, care should be taken in the design process to insure proper heat sinking of the device.

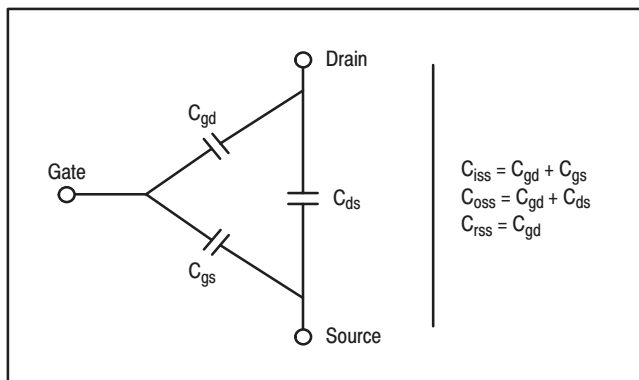
The major advantages of Lateral RF power MOSFETs include high gain, simple bias systems, relative immunity from thermal runaway, and the ability to withstand severely mismatched loads without suffering damage.

MOSFET CAPACITANCES

The physical structure of a MOSFET results in capacitors between all three terminals. The metal oxide gate structure determines the capacitors from gate-to-drain (C_{gd}), and gate-to-source (C_{gs}). The PN junction formed during fabrication of the RF MOSFET results in a junction capacitance from drain-to-source (C_{ds}). These capacitances are characterized as input (C_{iss}), output (C_{oss}) and reverse transfer (C_{rss}) capacitances on data sheets. The relationships between the inter-terminal capacitances and those given on data sheets are shown below. The C_{iss} can be specified in two ways:

1. Drain shorted to source and positive voltage at the gate.
2. Positive voltage of the drain in respect to source and zero volts at the gate.

In the latter case, the numbers are lower. However, neither method represents the actual operating conditions in RF applications.



DRAIN CHARACTERISTICS

One critical figure of merit for a FET is its static resistance in the full-on condition. This on-resistance, $R_{DS(on)}$, occurs in the linear region of the output characteristic and is specified at a specific gate-source voltage and drain current. The

drain-source voltage under these conditions is termed $V_{DS(on)}$. For MOSFETs, $V_{DS(on)}$ has a positive temperature coefficient at high temperatures because it contributes to the power dissipation within the device.

BV_{DSS} values for this device are higher than normally required for typical applications. Measurement of BV_{DSS} is not recommended and may result in possible damage to the device.

GATE CHARACTERISTICS

The gate of the RF MOSFET is a polysilicon material, and is electrically isolated from the source by a layer of oxide. The DC input resistance is very high – on the order of $10^9 \Omega$ – resulting in a leakage current of a few nanoamperes.

Gate control is achieved by applying a positive voltage to the gate greater than the gate-to-source threshold voltage, $V_{GS(th)}$.

Gate Voltage Rating — Never exceed the gate voltage rating. Exceeding the rated V_{GS} can result in permanent damage to the oxide layer in the gate region.

Gate Termination — The gates of these devices are essentially capacitors. Circuits that leave the gate open-circuited or floating should be avoided. These conditions can result in turn-on of the devices due to voltage build-up on the input capacitor due to leakage currents or pickup.

Gate Protection — These devices do not have an internal monolithic zener diode from gate-to-source. If gate protection is required, an external zener diode is recommended. Using a resistor to keep the gate-to-source impedance low also helps dampen transients and serves another important function. Voltage transients on the drain can be coupled to the gate through the parasitic gate-drain capacitance. If the gate-to-source impedance and the rate of voltage change on the drain are both high, then the signal coupled to the gate may be large enough to exceed the gate-threshold voltage and turn the device on.

DC BIAS

Since this device is an enhancement mode FET, drain current flows only when the gate is at a higher potential than the source. RF power FETs operate optimally with a quiescent drain current (I_{DQ}), whose value is application dependent. This device was characterized at $I_{DQ} = 150 \text{ mA}$, which is the suggested value of bias current for typical applications. For special applications such as linear amplification, I_{DQ} may have to be selected to optimize the critical parameters.

The gate is a dc open circuit and draws no current. Therefore, the gate bias circuit may generally be just a simple resistive divider network. Some special applications may require a more elaborate bias system.

GAIN CONTROL

Power output of this device may be controlled to some degree with a low power dc control signal applied to the gate, thus facilitating applications such as manual gain control, ALC/AGC and modulation systems. This characteristic is very dependent on frequency and load line.

MOUNTING

The specified maximum thermal resistance of 0.9°C/W assumes a majority of the 0.170" x 0.608" source contact on the back side of the package is in good contact with an appropriate heat sink. As with all RF power devices, the goal of the thermal design should be to minimize the temperature at the back side of the package. Refer to Motorola Application Note AN4005/D, "Thermal Management and Mounting Method for the PLD-1.5 RF Power Surface Mount Package," and Engineering Bulletin EB209/D, "Mounting Method for RF Power Leadless Surface Mount Transistor" for additional information.

AMPLIFIER DESIGN

Impedance matching networks similar to those used with bipolar transistors are suitable for this device. For examples see Motorola Application Note AN721, "Impedance Matching Networks Applied to RF Power Transistors." Large-signal

impedances are provided, and will yield a good first pass approximation.

Since RF power MOSFETs are triode devices, they are not unilateral. This coupled with the very high gain of this device yields a device capable of self oscillation. Stability may be achieved by techniques such as drain loading, input shunt resistive loading, or output to input feedback. The RF test fixture implements a parallel resistor and capacitor in series with the gate, and has a load line selected for a higher efficiency, lower gain, and more stable operating region.

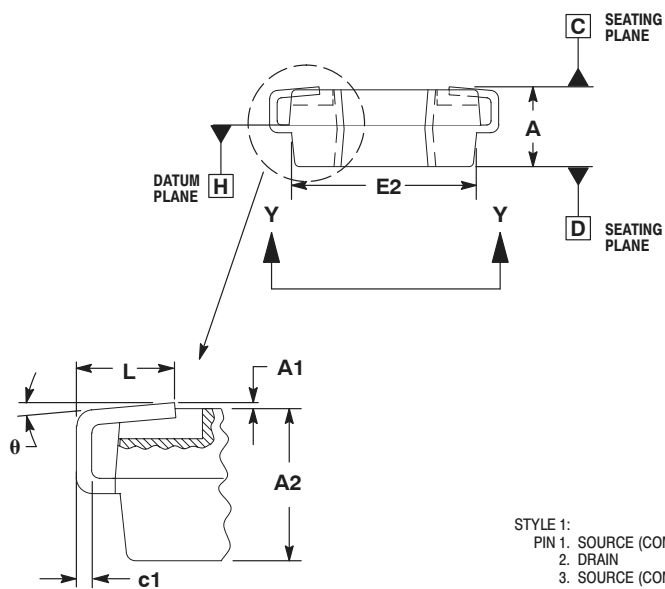
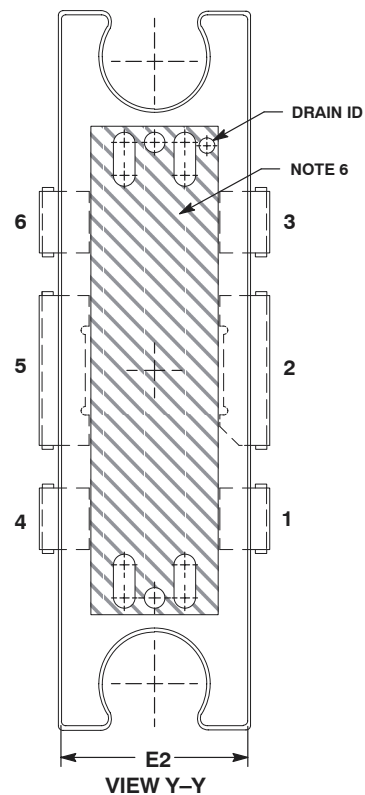
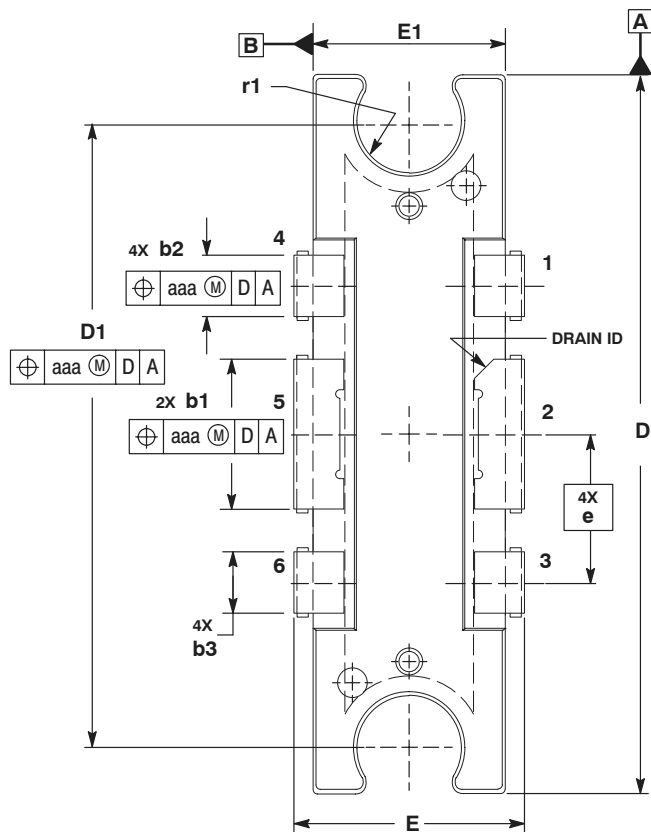
Two-port stability analysis with this device's S-parameters provides a useful tool for selection of loading or feedback circuitry to assure stable operation. See Motorola Application Note AN215A, "RF Small-Signal Design Using Two-Port Parameters" for a discussion of two port network theory and stability.

NOTES

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NOTES

PACKAGE DIMENSIONS



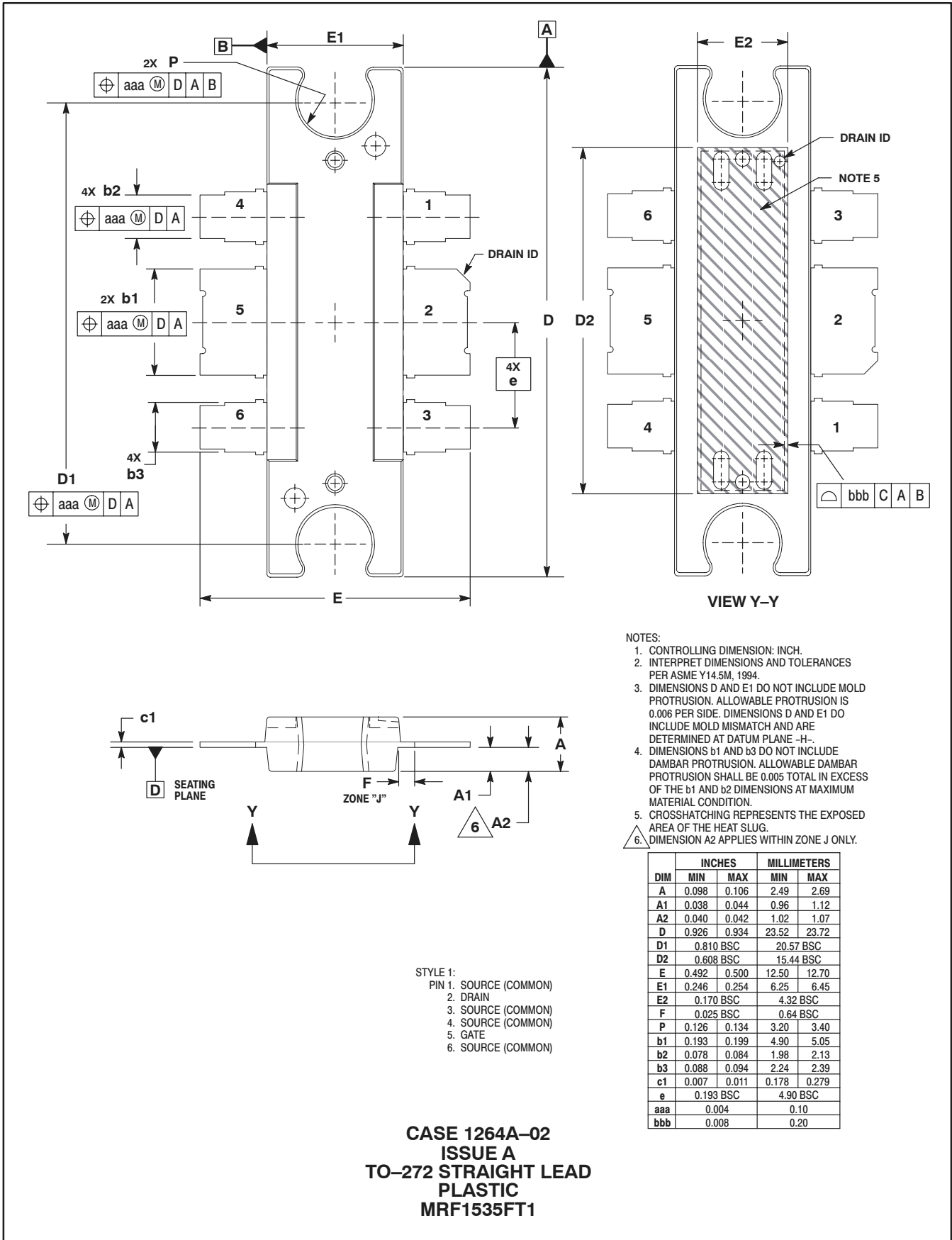
STYLE 1:
 PIN 1. SOURCE (COMMON)
 2. DRAIN
 3. SOURCE (COMMON)
 4. SOURCE (COMMON)
 5. GATE
 6. SOURCE (COMMON)

NOTES:

1. CONTROLLING DIMENSION: INCH.
2. INTERPRET DIMENSIONS AND TOLERANCES PER ASME Y14.5M, 1994.
3. DATUM PLANE -H- IS LOCATED AT TOP OF LEAD AND IS COINCIDENT WITH THE LEAD WHERE THE LEAD EXITS THE PLASTIC BODY AT THE TOP OF THE PARTING LINE.
4. DIMENSION D AND E1 DO NOT INCLUDE MOLD PROTRUSION. ALLOWABLE PROTRUSION IS 0.006 PER SIDE. DIMENSION D AND E1 DO INCLUDE MOLD MISMATCH AND ARE DETERMINED AT DATUM PLANE -H-.
5. DIMENSIONS b1 AND b3 DO NOT INCLUDE DAMBAR PROTRUSION. ALLOWABLE DAMBAR PROTRUSION SHALL BE 0.005 TOTAL IN EXCESS OF THE b1 AND b2 DIMENSIONS AT MAXIMUM MATERIAL CONDITION.
6. CROSSHATCHING REPRESENTS THE EXPOSED AREA OF THE HEAT SLUG.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.098	0.108	2.49	2.74
A1	0.000	0.004	0.00	0.10
A2	0.100	0.104	2.54	2.64
D	0.928	0.932	23.57	23.67
D1	0.806	0.814	20.47	20.68
E	0.296	0.304	7.52	7.72
E1	0.248	0.252	6.30	6.40
E2	0.241	0.245	6.12	6.22
L	0.060	0.070	1.52	1.78
b1	0.193	0.199	4.90	5.05
b2	0.078	0.084	1.98	2.13
b3	0.088	0.094	2.24	2.39
c1	0.007	0.011	0.18	0.28
e	0.193 BSC		4.90 BSC	
r1	0.063	0.068	1.60	1.73
θ	0°	6°	0°	6°
aaa	0.004		0.10	

**CASE 1264-09
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 PLASTIC
 MRF1535T1**



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