

# **Wideband FM IF**

The MC13155 is a complete wideband FM detector designed for satellite TV and other wideband data and analog FM applications. This device may be cascaded for higher IF gain and extended Receive Signal Strength Indicator (RSSI) range.

- 12 MHz Video/Baseband Demodulator
- Ideal for Wideband Data and Analog FM Systems
- Limiter Output for Cascade Operation
- Low Drain Current: 7.0 mA
- Low Supply Voltage: 3.0 to 6.0 V
- Operates to 300 MHz

#### **MAXIMUM RATINGS**



**NOTE:** Devices should not be operated at or outside these values. The "Recommended Operating Conditions" provide for actual device operation.



**SEMICONDUCTOR TECHNICAL DATA**



CASE 751B (SO–16)





#### **ORDERING INFORMATION**



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### **RECOMMENDED OPERATING CONDITIONS**



# **DC ELECTRICAL CHARACTERISTICS** (T<sub>A</sub> = 25°C, no input signal.)



# AC ELECTRICAL CHARACTERISTICS (T<sub>A</sub> = 25°C, f<sub>IF</sub> = 70 MHz, V<sub>EE</sub> = – 5.0 Vdc Figure 2, unless otherwise noted.)



**NOTE**: Positive currents are out of the pins of the device.

### **MC13155 CIRCUIT DESCRIPTION**

The MC13155 consists of a wideband three–stage limiting amplifier, a wideband quadrature detector which may be operated up to 200 MHz, and a received signal strength indicator (RSSI) circuit which provides a current output linearly proportional to the IF input signal level for approximately 35 dB range of input level.



**Figure 2. Test Circuit**

### **APPLICATIONS INFORMATION**

#### **Evaluation PC Board**

The evaluation PCB shown in Figures 19 and 20 is very versatile and is designed to cascade two ICs. The center section of the board provides an area for attaching all surface mount components to the circuit side and radial leaded components to the component ground side of the PCB (see Figures 17 and 18). Additionally, the peripheral area surrounding the RF core provides pads to add supporting and interface circuitry as a particular application dictates. This evaluation board will be discussed and referenced in this section.

#### **Limiting Amplifier**

Differential input and output ports interfacing the three stage limiting amplifier provide a differential power gain of typically 46 dB and useable frequency range of 300 MHz. The IF gain flatness may be controlled by decoupling of the internal feedback network at Pins 2 and 15.

Scattering parameter (S–parameter) characterization of the IF as a two port linear amplifier is useful to implement maximum stable power gain, input matching, and stability over a desired bandpass response and to ensure stable operation outside the bandpass as well. The MC13155 is unconditionally stable over most of its useful operating frequency range; however, it can be made unconditionally stable over its entire operating range with the proper decoupling of Pins 2 and 15. Relatively small decoupling capacitors of about 100 pF have a significant effect on the wideband response and stability. This is shown in the scattering parameter tables where S–parameters are shown for various values of C2 and C15 and at  $V_{EE}$  of  $-3.0$  and – 5.0 Vdc.

### **TYPICAL PERFORMANCE AT TEMPERATURE (See Figure 2. Test Circuit)**



**Input Signal Level** 100  $V<sub>EE</sub> = -5.0$ Vdc  $0'$ <sub>dBm</sub> 80  $1_{12}$ , RSSI OUTPUT  $(\mu A)$ RSSI OUTPUT ( A)  $1_{12}$ , RSSI OUTPUT ( $\mu$  $-10$  dBm 60 – 20 dBm 40 – 30 dBm 20  $40'$ dBm 0 10 1.0 2.0 3.0 4.0 5.0 6.0 7.0 8.0 10 100 100 100 1000 1000 1000 f, FREQUENCY (MHz)

**Figure 4. RSSI Output versus Frequency and**

**Figure 5. Total Drain Current versus Ambient Temperature and Supply Voltage**



**Figure 6. Detector Drain Current and Limiter Drain Current versus Ambient Temperature**





**Figure 8. RSSI Output versus Input Signal Voltage** (V<sub>in</sub> at Temperature)





**Figure 10. Differential Limiter Output Voltage versus Ambient Temperature**



**Figure 11A. Differential Detector Output Voltage versus Q of Quadrature LC Tank**



**Figure 12. RSSI Output Voltage versus IF Input**



**Figure 11B. Differential Detector Output Voltage versus Q of Quadrature LC Tank**





IF INPUT (dBm)

In the S–parameters measurements, the IF is treated as a two–port linear class A amplifier. The IF amplifier is measured with a single–ended input and output configuration in which the Pins 16 and 7 are terminated in the series combination of a 47  $\Omega$  resistor and a 10 nF capacitor to V<sub>CC</sub> ground (see Figure 14. S–Parameter Test Circuit).

The S–parameters are in polar form as the magnitude (MAG) and angle (ANG). Also listed in the tables are the calculated values for the stability factor (K) and the Maximum Available Gain (MAG). These terms are related in the following equations:

 $K = (1 - 1S_{11} 1^2 - 1S_{22} 1^2 + 1 \Delta 1^2) / (21S_{12} S_{21} 1)$ where:  $1 \triangle 1 = 1 S_{11} S_{22} - S_{12} S_{21} I$ .

 $MAG = 10 log | S<sub>21</sub> | / | S<sub>12</sub> | + 10 log | K - (K<sup>2</sup> – 1)<sup>1/2</sup> |$ 

where:  $K > 1$ . The necessary and sufficient conditions for unconditional stability are given as  $K > 1$ :

 $B1 = 1 + |S_{11}|^2 - |S_{22}|^2 - |\Delta|^2 > 0$ 



**Figure 14. S–Parameter Test Circuit**



**S-Parameters** ( $V_{EE} = -5.0$  Vdc,  $T_A = 25^{\circ}C$ ,  $C_2$  and  $C_{15} = 0$  pF)

### **S–Parameters** ( $V_{EE} = -5.0$  Vdc,  $T_A = 25^{\circ}C$ ,  $C_2$  and  $C_{15} = 100$  pF)





**S–Parameters** ( $V_{EE} = -5.0$  Vdc,  $T_A = 25^{\circ}$ C, C<sub>2</sub> and C<sub>15</sub> = 680 pF)

### **S–Parameters** ( $V_{EE} = -3.0$  Vdc,  $T_A = 25^{\circ}C$ ,  $C_2$  and  $C_{15} = 0$  pF)





**S-Parameters** ( $V_{EE} = -3.0$  Vdc,  $T_A = 25^{\circ}$ C, C<sub>2</sub> and C<sub>15</sub> = 100 pF)

### **S–Parameters** ( $V_{EE} = -3.0$  Vdc,  $T_A = 25^{\circ}C$ ,  $C_2$  and  $C_{15} = 680$  pF)



#### **DC Biasing Considerations**

The DC biasing scheme utilizes two  $VCC$  connections (Pins 3 and 6) and two  $V_{\text{FE}}$  connections (Pins 14 and 11).  $V$ FF1 (Pin 14) is connected internally to the IF and RSSI circuits' negative supply bus while  $VFF2$  (Pin 11) is connected internally to the quadrature detector's negative bus. Under positive ground operation, this unique configuration offers the ability to bias the RSSI and IF separately from the quadrature detector. When two ICs are cascaded as shown in the 70 MHz application circuit and provided by the PCB (see Figures 17 and 18), the first MC13155 is used without biasing its quadrature detector, thereby saving approximately 3.0 mA. A total current of 7.0 mA is used to fully bias each IC, thus the total current in the application circuit is approximately 11 mA. Both V<sub>CC</sub> pins are biased by the same supply. V<sub>CC</sub>1 (Pin 3) is connected internally to the positive bus of the first half of the IF limiting amplifier, while V<sub>CC</sub>2 is internally connected to the positive bus of the RSSI, the quadrature detector circuit, and the second half of the IF limiting amplifier (see Figure 15). This distribution of the  $VCC$ enhances the stability of the IC.

#### **RSSI Circuitry**

The RSSI circuitry provides typically 35 dB of linear dynamic range and its output voltage swing is adjusted by selection of the resistor from Pin 12 to  $VFF$ . The RSSI slope is typically 2.1 µA/dB ; thus, for a dynamic range of 35 dB, the current output is approximately 74 µA. A 47 k resistor will yield an RSSI output voltage swing of 3.5 Vdc. The RSSI buffer output at Pin 13 is an emitter–follower and needs an external emitter resistor of 10 k to  $VEE$ .

In a cascaded configuration (see circuit application in Figure 16), only one of the RSSI Buffer outputs (Pin 13) is used; the RSSI outputs (Pin 12 of each IC) are tied together and the one closest to the  $V_{EE}$  supply trace is decoupled to  $V_{\text{CC}}$  ground. The two pins are connected to  $V_{\text{EE}}$  through a 47 k resistor. This resistor sources a RSSI current which is proportional to the signal level at the IF input; typically, 1.0 mVrms (– 47 dBm) is required to place the MC13155 into limiting. The measured RSSI output voltage response of the application circuit is shown in Figure 12. Since the RSSI current output is dependent upon the input signal level at the IF input, a careful accounting of filter losses, matching and other losses and gains must be made in the entire receiver system. In the block diagram of the application circuit shown below, an accounting of the signal levels at points throughout the system shows how the RSSI response in Figure 12 is justified.

#### **Block Diagram of 70 MHz Video Receiver Application Circuit**



#### **Cascading Stages**

The limiting IF output is pinned–out differentially, cascading is easily achieved by AC coupling stage to stage. In the evaluation PCB, AC coupling is shown, however, interstage filtering may be desirable in some applications. In which case, the S–parameters provide a means to implement a low loss interstage match and better receiver sensitivity.

Where a linear response of the RSSI output is desired when cascading the ICs, it is necessary to provide at least 10 dB of interstage loss. Figure 12 shows the RSSI response with and without interstage loss. A 15 dB resistive attenuator is an inexpensive way to linearize the RSSI response. This has its drawbacks since it is a wideband noise source that is dependent upon the source and load impedance and the amount of attenuation that it provides. A better, although more costly, solution would be a bandpass filter designed to the desired center frequency and bandpass response while carefully selecting the insertion loss. A network topology shown below may be used to provide a bandpass response with the desired insertion loss.

**Network Topology**



#### **Quadrature Detector**

The quadrature detector is coupled to the IF with internal 2.0 pF capacitors between Pins 7 and 8 and Pins 9 and 10. For wideband data applications, such as FM video and satellite receivers, the drive to the detector can be increased with additional external capacitors between these pins, thus, the recovered video signal level output is increased for a given bandwidth (see Figure 11A and Figure 11B).

The wideband performance of the detector is controlled by the loaded Q of the LC tank circuit. The following equation defines the components which set the detector circuit's bandwidth:

$$
Q = R_T / X_L \tag{1}
$$

where:  $R_T$  is the equivalent shunt resistance across the LC Tank and  $X_L$  is the reactance of the quadrature inductor at the IF frequency  $(X_L = 2\pi fL)$ .

The inductor and capacitor are chosen to form a resonant LC Tank with the PCB and parasitic device capacitance at the desired IF center frequency as predicted by:

$$
fc = (2\pi \sqrt{(LC_p)})^{-1}
$$
 (2)

where: L is the parallel tank inductor and  $C<sub>D</sub>$  is the equivalent parallel capacitance of the parallel resonant tank circuit.

The following is a design example for a wideband detector at 70 MHz and a loaded Q of 5. The loaded Q of the quadrature detector is chosen somewhat less than the Q of the IF bandpass. For an IF frequency of 70 MHz and an IF bandpass of 10.9 MHz, the IF bandpass Q is approximately 6.4.

Example:

Let the external Cext =  $20$  pF. (The minimum value here should be greater than 15 pF making it greater than the internal device and PCB parasitic capacitance, Cint  $\approx$ 3.0 pF).

$$
C_p = Cint + Cext = 23 pF
$$

Rewrite Equation 2 and solve for L:

L =  $(0.159)^2$  /(C<sub>p</sub> fc<sup>2</sup>)

$$
L = 198
$$
 nH, thus, a standard value is chosen.

 $L = 0.22 \mu H$  (tunable shielded inductor).

The value of the total damping resistor to obtain the required loaded Q of 5 can be calculated by rearranging Equation 1:

$$
R_T = Q(2\pi fL)
$$
  

$$
R_T = 5 (2\pi)(70)(0.22) = 483.8 \Omega.
$$

The internal resistance, Rint between the quadrature tank Pins 8 and 9 is approximately 3200  $\Omega$  and is considered in determining the external resistance, Rext which is calculated from:

 $Rext = ((R_T)(Rint))/ (Rint - R_T)$ 

 $Rext = 570$ , thus, choose the standard value.

Rext = 560 Ω.

#### **SAW Filter**

In wideband video data applications, the IF occupied bandwidth may be several MHz wide. A good rule of thumb is to choose the IF frequency about 10 or more times greater than the IF occupied bandwidth. The IF bandpass filter is a SAW filter in video data applications where a very selective response is needed (i.e., very sharp bandpass response). The evaluation PCB is laid out to accommodate two SAW filter package types: 1) A five–leaded plastic SIP package. Recommended part numbers are Siemens X6950M which operates at 70 MHz; 10.4 MHz 3 dB passband, X6951M (X252.8) which operates at 70 MHz; 9.2 MHz 3 dB passband; and X6958M which operates at 70 MHz, 6.3 MHz 3 dB passband, and 2) A four–leaded TO–39 metal can package. Typical insertion loss in a wide bandpass SAW filter is 25 dB.

The above SAW filters require source and load impedances of 50  $\Omega$  to assure stable operation. On the PC board layout, space is provided to add a matching network, such as a 1:4 surface mount transformer between the SAW filter output and the input to the MC13155. A 1:4 transformer, made by Coilcraft and Mini Circuits, provides a suitable interface (see Figures 16, 17 and 18). In the circuit and layout, the SAW filter and the MC13155 are differentially configured with interconnect traces which are equal in length and symmetrical. This balanced feed enhances RF stability, phase linearity, and noise performance.



**Figure 15. Simplified Internal Circuit Schematic**

# **MC13155 Figure 16. 70 MHz Video Receiver Application Circuit**



**Figure 17. Component Placement (Circuit Side)**



**Figure 18. Component Placement (Ground Side)**



**Figure 19. Circuit Side View**



**Figure 20. Ground Side View**



**MOTOROLA ANALOG IC DEVICE DATA 15**

### **OUTLINE DIMENSIONS**



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