## FEATURES

- 8 pin SOIC Switching Controller with HICCUP Current Limiting Reduces Diode Power Dissipation to Less than $1 \%$ of Normal Operation
- Soft Start Capacitor allows for smooth Output Voltage ramp up
- On board MOSFET driver
- Fastest transient response of any controller method. ( 0 to 100\% Duty Cycle in 100 nS )
- $1 \%$ internal voltage reference
- Internal Under Voltage Lockout protects MOSFET during start-up


## APPUCATIONS

Dual supply low voltage processor applications, such as: P55CTN, CYRIX M2 ${ }^{\text {TM }}$, POWER PCTM ${ }^{\text {TM }}$ and AMD K6TM

- Simple 5 V to 3.3 V switcher for Pentium with AGP or Pentium IITM applications


## DESCRIPTION

The US3034 IC provides an 8 pin low cost switching controller with true short circuit protection all in a compact 8 pin surface mount package, providing a low cost switching solution for dual supply processor applications that require switching regulator for the 3.3 V supply such as the applications with AGP on board. Typically in these applications a dual supply regulator converts 5 V to 3.3 V for $\mathrm{I} / \mathrm{O}$ supply and a jumper programmable supply of 1.25 V to 3.5 V for CORE supply . The IC uses an internal regulator generated from the 12 V supply to power the controller as well as the 12 V supply to drive the power MOSFET, allowing a low cost N channel MOSFET to be used. The IC also includes an error comparator for fast transient response, a precise voltage reference for setting the output voltage as well as a direct drive of the MOSFET for the minimum part count.

## TYPICAL APPLCATION



Typical application of US3034
Notes: P55C,Pentium II are trade marks of Intel Corp. K5 \& K6 are trade marks of AMD corp. Cyrix 6X86L,M1,M2 are trade marks of Cyrix Corp. Power PC is trade mark of IBM Corp.

## PACKAGE ORDER INFORMATION

| TA $\left({ }^{\circ} \mathbf{C}\right)$ | 8 PIN PLASTIC <br> SOIC (S) |
| :---: | :---: |
| 0 TO 70 | US3034CS |

## ABSOLUTE MAXMUM RATINGS

| $V_{12}$ Supply Voltages | 20 V |
| :---: | :---: |
| F.B Pin Voltages | -0.3 V to 5V |
| Storage Temperature | $-65 \mathrm{TO} 150^{\circ} \mathrm{C}$ |
| Operating Junction | $0 \mathrm{TO} 150^{\circ} \mathrm{C}$ |

## PACKAGE INFORMATION

| 8 PIN PLASTIC SOIC (S) |  |
| :---: | :---: |
|  |  |
| $\theta_{J A}=160^{\circ} \mathrm{C} / \mathrm{W}$ |  |

## ELECTRICAL SPEOFICATIONS

Unless otherwise specified the following specification applies over $\mathrm{V}_{12}=12 \mathrm{~V}$, and $\mathrm{T}_{\mathrm{A}}=0$ to $70^{\circ} \mathrm{C}$. Low duty cycle pulse testing are used which keeps junction and case temperatures equal to the ambient temperature.

| PARAMETER | SYM | TEST CONDITION | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F.B Voltage Initial Accuracy | $\mathrm{V}_{\text {FB }}$ | $\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}$ | 1.237 | 1.250 | 1.262 | V |
| F.B Voltage Total Variation |  |  | 1.225 | 1.250 | 1.275 | V |
| F.B Voltage Line Regulation |  |  |  | 0.2 |  | \% |
| F.B Input Bias Current | 1 If | $\mathrm{V}_{\mathrm{FB}}=1.25 \mathrm{~V}$ | -1 |  | +1 | UA |
| Min On Time |  | $\mathrm{V}_{\mathrm{FB}}$ is sq wave with 300 ns on time and 2 uS off time |  | 800 |  | nS |
| Min Off Time |  | $\mathrm{V}_{\text {FB }}$ is sq wave with 300 ns off time and 2 uS on time |  | 800 |  | nS |
| Vhyst pin output-HI |  | Isource $=500 \mathrm{uA}, \mathrm{V}_{\text {Fb }}=1.5 \mathrm{~V}$ | 11 |  |  | V |
| Vhyst pin output-LO |  | $1 \mathrm{ISINK}=500 \mathrm{uA}, \mathrm{V}_{\text {FB }}=1 \mathrm{~V}$ |  |  | 1 | V |
| Supply Current | İ2Sw | $\mathrm{V}_{\mathrm{FB}}=1 \mathrm{~V}$ |  | 10 |  | mA |
| Maximum Duty Cycle | Dmax | $\mathrm{V}_{\mathrm{Fb}}=1 \mathrm{~V}$ |  |  | 100 | \% |
| Minimum Duty Cycle | Dmin | $\mathrm{V}_{\mathrm{FB}}=1.5 \mathrm{~V}$ | 0 |  |  | \% |
| Gate Drive Rise/Fall Time | VGate | Load=IRL3303 |  | 70 |  | nS |
| C.L Threshold Current | 1 CL | C.S+, C.S- from 1.3V to 3.7V |  | 20 |  | UA |
| C.S Comp Common Mode |  | $\mathrm{VCS}_{+}=\mathrm{V}_{\text {cs }}$ | 0 |  | 4.5 | V |
| Soft Start Current |  |  |  | 10 |  | uA |

## PIN DESCRIPTIONS

| PIN \# | PIN SYMBOL | PIN DESCRIPTION |
| :---: | :---: | :--- |
| 3 | $V_{\text {FB }}$ | A resistor divider from this pin to the output of the switching regulator and ground sets the <br> Core supply voltage. |
| 6 | C.S- | This pin is connected to the minus side of the external current sense resistor. An internal <br> current source together with an external resistor in series with this pin programs the <br> current limit threshold voltage. This voltage divided by the external current sense resistor <br> sets the current limit threshold. |
| 7 | C.S+ | This pin is connected to the plus side of the external current sense resistor. A resistor in <br> series with this pin and a capacitor connected between this pin and pin 6 provides a high <br> frequency filtering for the noise spikes of turn on and turn off switching. |
| 5 | Gnd | This pin is connected to the IC substrate and must be connected to the lowest potential <br> in the system. |
| 1 | Drv | The PWM output of the switching controller. This pin is a totem pole drive that is con- <br> nected to the gate of the power MOSFET. A resistor may be placed from this pin to the <br> gate in order to reduce switching noise. |
| 4 | $V_{\text {VYYsT }}$ | A resistor and a 10pF capacitor is connected from this pin to the VFB1 pin to set the <br> output ripple voltage for the switching regulator. |
| 2 | $V_{12}$ | This pin supplies the voltage to the PWM drive and hysterises circuitry and it is con- <br> nected to the 12V supply. A 1 uF, high frequency capacitor must be connected from this <br> pin to ground to provide the peak current for charging and discharging of the MOSFET. |
| 8 | S.S | This pin provides the soft start for the regulator during power up. It also sets a long off <br> time when the converter goes into current limiting, providing low duty cycle for the catch <br> diode allowing it to survive during short circuit. |

## BLOCK DIAGRAM



Figure 1 - Simplified block diagram of the US3034

## TYPICAL APPUCATION

## Pentium Core Supply Application (US3034 and US3033 Dual Layout)

## Low Cost 4 Bit VID

** R9 can be eliminated if dual layout with US3033 is not desired.


Figure2- Typical application of US3034 in a flexible motherboard with the 4 bit VID output voltage selection. This circuit is done using a dual layout with the US3033 part. The advantage of this circuit is that it uses a single jumper that programs the output voltage in 16 steps with 0.1 V steps from 2 V to 3.5 V , designed for Intel P55,P54 AMD K5 \& K6 as well as Cyrix M1 and M2 applications.

| JP1 | JP1 | JP1 | JP1 | Output |
| :--- | :--- | :--- | :--- | :--- |
| $1-2$ | $3-4$ | $5-6$ | $7-8$ | Voltage |
| 0 | 0 | 0 | 0 | 3.5 |
| 0 | 0 | 0 | 1 | 3.4 |
| 0 | 0 | 1 | 0 | 3.3 |
| 0 | 0 | 1 | 1 | 3.2 |
| 0 | 1 | 0 | 0 | 3.1 |
| 0 | 1 | 0 | 1 | 3.0 |
| 0 | 1 | 1 | 0 | 2.9 |
| 0 | 1 | 1 | 1 | 2.8 |
| 1 | 0 | 0 | 0 | 2.7 |
| 1 | 0 | 0 | 1 | 2.6 |
| 1 | 0 | 1 | 0 | 2.5 |
| 1 | 0 | 1 | 1 | 2.4 |
| 1 | 1 | 0 | 0 | 2.3 |
| 1 | 1 | 0 | 1 | 2.2 |
| 1 | 1 | 1 | 0 | 2.1 |

## Pentium Core Supply Application Parts List (US3034 and US3033 Dual Layout) Low Cost 4 Bit VID

| Ref Desig | Description | Qty | Part \# | Manufacturer |
| :---: | :---: | :---: | :---: | :---: |
| U1 | LDO/Switcher IC | 1 | US3034CS ( 8 pin SOIC) | Unisem |
| Q2 | MOSFET | 1 | IRL3303 (TO220) IRL3103S (TO263) (note 1) | International Rectifier |
| D1 | Schottky Diode | 1 | MBR1045CT (TO220) MBRB1545CT (TO263) (note1) | Motorola |
| L2 | Inductor | 1 | Core:T50-18,L=4 uH Turns: 10T, 18 AWG | Micro Metal (core) |
| L1 | Inductor | 1 | $\mathrm{L}=2 \mathrm{uH}$ |  |
| R1 | Resistor | 1 | 22 ohm,5\%, SMT 1206 size |  |
| R2 | Resistor | 1 | 10 ohm, 5\%, SMT 1206 size |  |
| R3 | Resistor | 1 | 324 kohm, 1\%, SMT 0805 size |  |
| R4A * | Resistor | 1 | 806 ohm,1\%, SMT 0805 size |  |
| R4B * | Resistor | 1 | 90.9 kohm,1\%, SMT 0805 size |  |
| R5A | Resistor | 1 | 1.24 kohm,1\%, SMT 0805 size |  |
| R5B | Resistor | 1 | 2.49 kohm, 1\%, SMT 0805 size |  |
| R5C | Resistor | 1 | 4.99 kohm, 1\%, SMT 0805 size |  |
| R5D | Resistor | 1 | 10 kohm,1\%, SMT 0805 size |  |
| R5E | Resistor | 1 | 1.30 kohm,1\%, SMT 0805 size |  |
| R6 | Resistor | 1 | 5 miliohm,5\%, 2W |  |
| R7 | Resistor | 1 | 4.99 kohm, $1 \%$, SMT 0805 size |  |
| R8 | Resistor | 1 | 4.7 kohm, $5 \%$ for US3034, open for 3033 |  |
| R9 | Resistor | 1 | open for US3034, 10 ohm for US3033 |  |
| C1 | Capacitor | 1 | 6MV1500GX, 1500uF,6.3V, Elect |  |
| C2 | Capacitor | 1 | 6MV1500GX, 1500uF,6.3V, Elect | Sanyo |
| C3 | Capacitor | 1 | 1 uF,Ceramic, SMT 0805 size |  |
| C4 | Capacitor | 1 | 470 pF,Ceramic, SMT 0805 size | Sanyo |
| C5 | Capacitor | 1 | 10 pF, Ceramic, SMT 0805 size | Sanyo |
| C7 | Capacitor | 4 | 6MV1500GX, 1500uF,6.3V, Elect | Sanyo |
| C8 | Capacitor | 1 | 0.047 uF for 3034, 0.1uf for 3033 |  |
| C6 | Capacitor | 1 | 4700pF for US3034, open for US3033 |  |
| HS1 | Heat Sink | 1 | For MOSFET, 577002 | Aavid |
| HS2 | Heat Sink | 1 | For Schottky Diode , 577002 | Aavid |

* R4 is a parallel combination of R4A and R4B.

Note 1: For the applications where it is desirable to eliminate the heat sink, the IRL3103S for Q2 and MBR1545CT for D2 in TO263 packages with minimum of 1 " square copper pad can be used.

## TYPICAL APPLCATION

5 V to 3.3 V for Pentium Application with AGP or Pentium II Application without ATX power supply Switching mode Operation. (US3034 and US3033 Dual Layout)


Figure4- The circuit in figure 4 is the application of the US3034 which is done using a dual layout with US3033 in a switching mode only. This circuit can be used to generate a low cost 5 V to 3.3 V for either Pentium application with AGP socket or in Pentium II applications where it is desirable to generate an accurate on board 3.3 V supply.

| Ref Desig | Description | Qty | Part \# | Manufacturer |
| :---: | :---: | :---: | :---: | :---: |
| U1 | LDO/Switcher IC | 1 | US3034CS ( 8 pin SOIC) | Unisem |
| Q2 | MOSFET | 1 | IRL3303 (TO220) IRL3103S (TO263) (note 1) | International Rectifier |
| D1 | Schottky Diode | 1 | MBR1045CT (TO220) MBRB1545CT (TO263) (note1) | Motorola |
| L2 | Inductor | 1 | $\begin{aligned} & \text { Core:T50-18,L=4 uH } \\ & \text { Turns: } 10 \mathrm{~T}, 18 \mathrm{AWG} \\ & \hline \end{aligned}$ | Micro Metal (core) |
| L1 | Inductor | 1 | $\mathrm{L}=2 \mathrm{uH}$ |  |
| R1 | Resistor | 1 | 22 ohm,5\%, SMT 1206 size |  |
| R9 | Resistor | 1 | open for US3034, 10 ohm for US3033 |  |
| R2 | Resistor | 1 | 10 ohm, 5\%, SMT 1206 size |  |
| R3 | Resistor | 1 | 249 kohm,1\%, SMT 0805 size |  |
| R4 | Resistor | 1 | 1 kohm,1\%, SMT 0805 size |  |
| R5 | Resistor | 1 | 576 ohm, $1 \%$, SMT 0805 size |  |
| R6 | Resistor | 1 | 5 miliohm,5\%, 2W |  |
| R7 | Resistor | 1 | 4.99 kohm, $1 \%$, SMT 0805 size |  |
| R8 | Resistor | 1 | 4.7 kohm,5\% for US3034, open for 3033 |  |
| C1,2 | Capacitor | 2 | 6MV1500GX, 1500uF,6.3V, Elect | Sanyo |
| C3 | Capacitor | 1 | 1 uF,Ceramic, SMT 0805 size |  |
| C4 | Capacitor | 1 | 470 pF,Ceramic, SMT 0805 size | Sanyo |
| C5 | Capacitor | 1 | 10 pF,Ceramic, SMT 0805 size | Sanyo |
| C6 | Capacitor | 1 | 4700pF for US3034, open for US3033 |  |
| C7 | Capacitor | 2 | 6MV1500GX, 1500uF,6.3V, Elect | Sanyo |
| C8 | Capacitor | 1 | 0.047 uF for 3034, 0.1uf for 3033 |  |
| HS1 | Heat Sink | 1 | For MOSFET, 577002 | Aavid |
| HS2 | Heat Sink | 1 | For Schottky Diode , 577002 | Aavid |

Note 1: For the applications where it is desirable to eliminate the heat sink, the IRL3103S for Q2 and MBR1545CT for D2 in TO263 packages with minimum of 1 " square copper pad can be used.

## TYPICAL APPLCATION

5 V to 3.3 V with lossles short cicuit protection(output UVLO detection).


Figure 5- The circuit in figure 5 is designed to provide lossles output short detection by detecting the dc voltage across the inductor and shutting down the MOSFET and entering HICCUP mode. Note that the current limit point is a function of the inductor resistance and in this application with approximately 8 mil ohm resistance the peak C.L is set at 10A. See application note on how to set the current limiting threshold.

| Ref Desig | Description | Qty | Part \# | Manufacturer |
| :---: | :---: | :---: | :---: | :---: |
| U1 | Switcher IC | 1 | US3034CS ( 8 pin SOIC) | Unisem |
| Q2 | MOSFET | 1 | IRL3303 (TO263) | International Rectifier |
| D1 | Schottky Diode | 1 | PBYR735(Axial Thr Hole pkg) PBYR1035B(SMT, TO263 pkg) | Motorola |
| L2 | Inductor | 1 | Core:T50-18,L=4 uH Turns: $7 \mathrm{~T}, 18 \mathrm{AWG}$ | Micro Metal (core) |
| L1 | Inductor | 1 | $\mathrm{L}=1 \mathrm{uH}$ |  |
| R1,2 | Resistor | 2 | 10 ohm,5\%, SMT |  |
| R3 | Resistor | 1 | 182 kohm,1\%, SMT |  |
| R4 | Resistor | 1 | 1 kohm,1\%, SMT |  |
| R5 | Resistor | 1 | 5760hm,1\%, SMT |  |
| R7 | Resistor | 1 | 3.83 kohm,1\%, SMT |  |
| R6 | Resistor | 1 | $1 \mathrm{kohm}, 1 \%$, SMT |  |
| C1 | Capacitor | 1 | 470uF, Elect |  |
| C2 | Capacitor | 1 | 6MV1000GX, 1000uF,6.3V, Elect | Sanyo |
| C3 | Capacitor | 1 | 1 uF,Ceramic, SMT |  |
| C5 | Capacitor | 1 | 10 pF, Ceramic, SMT | Sanyo |
| C6 | Capacitor | 1 | 0.1 uF |  |
| C7 | Capacitor | 2 | 6MV1000GX, 1000uF,6.3V, Elect | Sanyo |
| C8 | Capacitor | 1 | 0.047 uF |  |

## APPLCATION INFORMATION

## Introduction

The US3034 device is an application specific product designed to provide an on board switching supply for the new generation of microprocessors requiring separate Core and I/O supplies where the load current demand from the I/O supply requires this regulator to also be a switching regulator such as the motherboard applications with AGP slot or the Pentium II with on board 5 V to 3.3 V converter. The US3034 provides an easy and low cost switching regulator solution for Vcore and 3.3V supplies with true short circuit protection.

## Switching Controller Operation

The operation of the switching controller is as follows : after the power is applied, the output drive pin, "Drv" goes to $100 \%$ duty cycle and the the current in the inductor charges the output capacitor causing the output voltage to increase. When output reaches a pre-programmed set point the feedback pin "Vfb" exceeds 1.25 V causing the output drive to switch low and the "Vhyst" pin to switch high which jumps the feedback pin higher than 1.25 V resulting in a fixed output ripple which is given by the following equation:
$\mathrm{dVo}=(\mathrm{Rt} / \mathrm{Rh}) \times 11$
Where:
Rt=Resistor connected from Vout to the Vfb pin of US3034
Rh=Resistor connected from Vfb pin to Vhyst pin.
For example, if $\mathrm{Rt}=1 \mathrm{k}$ and $\mathrm{Rh}=422 \mathrm{k}$, then the output ripple is :
$\mathrm{dVo}=(1 / 422) \times 11=26 \mathrm{mV}$
The advantage of fixed output ripple is that when the output voltage changes from 2 V to 3.5 V , the ripple voltage remains the same which is important in meeting the Intel maximum tolerance specification.

## Soft Start

The soft start capacitor must be selected such that during the start up when the output capacitors are charging up, the peak inductor current does not reach the current limit treshold. A minimum of 0.1 uF capacitor insures this for most applications. During start up the soft start capacitor is charged up to approximately 6 V keeping the output shutdown before an internal 10uA current source start discharging the soft start capacitor which slowly ramps up the inverting input of the PWM comparator, Vfb. This insures the output to ramp up at the same rate as the soft start cap thereby limiting the input current. For example, with 0.1 uF and the 10 uA internal current source the ramp up rate is $(\Delta \mathrm{V} / \Delta \mathrm{t})=I / \mathrm{Css}=10 /$ $0.1=100 \mathrm{~V} /$ Sec or $0.1 \mathrm{~V} / \mathrm{mSec}$. Assuming that the output capacitance is 6000 uF , the peak input current will be: $\operatorname{lin}(\mathrm{pk})=\operatorname{Css}^{*}(\Delta \mathrm{~V} / \Delta \mathrm{t})=6000 \mathrm{uF}{ }^{*}(0.1 \mathrm{~V} / \mathrm{mSec})=0.6 \mathrm{~A}$

The soft start capacitor also provides a delay in the turn on of the output which is given by:
Td=Css*K
Where K=30 ms $/ \mathrm{uF}$
For example for $\mathrm{Css}=0.1 \mathrm{uF}$,
$\mathrm{Td}=0.1^{*} 30=3 \mathrm{~ms}$

## Switcher Current Limit Protection

The US3034 uses an external current sensing resistor and compares the voltage drop across it to a programmed voltage which is set externally via a resistor (RcL) placed between the "CS-" terminal of the IC and Vout. Once the voltage across the sense resistor exceeds the threshold, the soft start capacitor pulls up to 12 V , pulling up the inverting pin of the error comparator higher than non inverting which causes the external MOSFET to shut off. At this point the C.S comparator changes its state and pulls the soft start capacitor to Vcc which is 12 V and shutting the PWM drive. After the output drive is turned off, an internal 10uA current source slowly discharge the soft start capacitor to approximately 5.7 V , before the output starts to turn back on causing a long delay before the MOSFET turns back on. This delay causes the catch diode to cool off between the current limit cycles allowing the converter to survive a short circuit condition. An example is given below as how to select the current limiting components. Assuming the desired current limit point is set to be 20A and the current sense resistor $\mathrm{Rs}=5 \mathrm{~m} \Omega$, then the current limit programming resistor,RcL is calculated as :
Vcs=IcL*Rs=20*0.005=0.1V
$R c L=V c s / l b=(0.1 \mathrm{~V}) /(20 \mathrm{uA})=5 \mathrm{k} \Omega$
Where: $\mathrm{lb}=20 \mathrm{uA}$ is the internal current source of the US3034
The peak power dissipated in the C.S. resistor is :
Ppk=(IcL^2)*Rs=20^2*0.005=2W
However, the average power dissipated is much lower than 2W due to the long off time caused by the hiccup circuit of 3034 . The average power is in fact the short circuit period divided by the short circuit period plus the off time or "hiccup" period. For example, if the short circuit lasts for Tsc=100uSec before the 3034 enters hiccup, the average power is calculated as :
Pave=0.5*Ppk*Dsc
Where:
Dsc=Tsc/ThcP
THCP=Css*M
Where $\mathrm{M}=200 \mathrm{~ms} / \mathrm{uF}$ \& Css, is the soft start capacitor For example for Css=0.1uF \& TsC=500uSec=0.5mS
THCP $=0.1^{*} 200=20 \mathrm{~ms}$
Pave $=0.5^{*} 2^{*}(0.5 / 20)=25 \mathrm{~mW}$
Without "hiccup" technique, the power dissipation of the resistor is 2 W .

## Switcher Output Voltage Setting

The output voltage can be set using the following equations.
Assuming, $\mathrm{Vo}=3.38 \mathrm{~V}$ and the selected output ripple is $\approx 1.3 \%(44 \mathrm{mV})$ of the output voltage, a set of equations are derived that selects the resistor divider and the hysterises resistor.
Assuming, $\mathrm{Rt}=1 \mathrm{k} \Omega, 1 \%$
$\mathrm{Rh}=\left(11^{*} \mathrm{Rt}\right) / \Delta \mathrm{Vo}$
Where:
$\mathrm{Rt}=$ Top resistor of the resistor divider
$\mathrm{Rh}=$ Hysterises resistor connected between pins 3 and 4 of the US3034
$\Delta \mathrm{Vo}=$ Selected output ripple (typically $1 \%$ to $2 \%$ of output voltage)
Assuming, $\Delta \mathrm{Vo}=44 \mathrm{mV}$
$\mathrm{Rh}=(11 * 1000) / 0.044=250 \mathrm{k} \Omega$
Select Rh=249k $\Omega, 1 \%$
The bottom resistor of the divider is then calculated using the following equations:
Rb=Rt/X
Where:
$\mathrm{Rb}=\mathrm{Bottom}$ resistor of the divider
$\mathrm{X}=[(\mathrm{Vo}+(\Delta \mathrm{Vo} / 2)) / \mathrm{Vref}]-1$
Vref=1.25 V typ.
$X=[(3.38+(0.044 / 2)) / 1.25]-1=1.72$
$\mathrm{Rb}=1000 / 1.72=580 \Omega$
Select Rb=576 $\Omega$, 1\%

## Frequency Calculation

The US3034 frequency of operation is calculated using the following formula:
$\mathrm{Fs}=\left[\left(\mathrm{Vo}{ }^{*}(1-\mathrm{D})^{*} \mathrm{ESR}\right) y\left(\mathrm{~L}^{*} \Delta \mathrm{Vo}\right)(\mathrm{MHz})\right.$
Where:
Vo=Output voltage (V)
D=Duty cycle
ESR=Output capacitor ESR (V)
L=Output inductance (uH)
$\Delta \mathrm{V} o=O u t p u t$ ripple voltage (V)
For our example:
$\mathrm{D} \approx(\mathrm{Vo}+\mathrm{Vf}) / \mathrm{Vin}$
Where, $\mathrm{Vf}=$ Forward voltage drop of the Schotky diode $\mathrm{D}=(3.38+0.5) / 5=0.78$
The ESR=18m $\Omega$ for 2 of the Sanyo 1500uF, 6MV1500GX caps. If $L=3.5 u H$ then, $F s$ is calculated as follows:
$\mathrm{Fs}=\left[\left(3.38^{*}(1-0.78)^{*} 0.018\right)\right]\left(3.5^{*} 0.044\right)=0.087 \mathrm{Mhz}=$ 87 kHz

