## PHOTOFLASH CHARGER

## DESCRIPTION

The ZXSC440 is a dedicated photoflash charger, charging an $80 \mu \mathrm{~F}$ photoflash capacitor to 300 V in 3.5 seconds from a 3 V supply.
The flyback conversion efficiency is typically $75 \%$, much higher than the commonly used discrete charging circuits.
The Charge pin enables the circuit to be initiated from the camera's microprocessor, using negligible current when flash is not being used.

## FEATURES

- Charges a $80 \mu \mathrm{~F}$ photoflash capacitor to 300 V in 3.5 seconds from 3 V
- Charges various value photoflash capacitors
- Over 75\% flyback efficiency
- Charge and Ready pins
- Consumes only $4.5 \mu \mathrm{~A}$ when not charging
- Small MSOP8 Iow profile package


## PINOUT



## MSOP8 pin TOP VIEW

The Ready pin signals the microprocessor when the flash is charged and ready to be fired.
A small amount of hysteresis on the voltage feedback shuts down the device as long as the capacitor remains fully charged, again using negligible current.

## APPLICATIONS

- Digital camera flash unit
- Film camera flash unit

TYPICAL APPLICATION CIRCUIT


ORDERING INFORMATION

| DEVICE | DEVICE DESCRIPTION | TEMPERATURE RANGE | PART <br> MARK | TAPING <br> OPTIONS |
| :--- | :--- | :---: | :---: | :---: |
| ZXSC440X8TA | Camera flash charger | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | ZXSC 440 | TA, TC |
| ZXSC440X8TC |  |  |  |  |

- TA reels hold 1000 devices
- TC reels hold 4000 devices


## ZXSC440

ABSOLUTE MAXIMUM RATINGS

| PARAMETER | LIMTT | UNIT |
| :--- | :--- | :---: |
| $\mathrm{V}_{\mathrm{CC}}$ | -0.3 to +10 | V |
| DRIVE | -0.3 to $\mathrm{V}_{\mathrm{CC}}+0.3$ | V |
| READY | -0.3 to $\mathrm{V}_{\mathrm{CC}}+0.3$ | V |
| CHARGE | -0.3 to The lower of $(+5.0)$ or $\left(\mathrm{V}_{\mathrm{CC}}+0.3\right)$ | V |
| $\mathrm{V}_{\mathrm{FB}}$, SENSE | -0.3 to The lower of $(+5.0)$ or $\left(\mathrm{V}_{\mathrm{CC}}+0.3\right)$ | V |
| Operating temperature | -40 to +85 | ${ }^{\circ} \mathrm{C}$ |
| Storage temperature | -55 to +150 | ${ }^{\circ} \mathrm{C}$ |
| Power dissipation at $25^{\circ} \mathrm{C}$ | 450 | mW |

ELECTRICAL CHARACTERISTICS (Test conditions $\mathrm{V}_{\mathrm{CC}}=3 \mathrm{~V}, \mathrm{~T}=25^{\circ} \mathrm{C}$ unless otherwise stated)

| SYMBOL | PARAMETER | CONDITIONS | MIN. | TYP. | MAX. | UNTT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {Cc }}$ | $\mathrm{V}_{\text {CC }}$ range |  | 1.8 |  | 8 | V |
| $1 \mathrm{q}^{(1)}$ | Quiescent current | $\mathrm{V}_{\mathrm{CC}}=8 \mathrm{~V}$ |  |  | 220 | $\mu \mathrm{A}$ |
| ISTDN | Shutdown current |  |  | 4.5 |  | $\mu \mathrm{A}$ |
| Eff ${ }^{(2)}$ | Efficiency |  |  | 85 |  | \% |
| $\mathrm{AcC}_{\text {REF }}$ | Reference tolerance | $1.8 \mathrm{~V}<\mathrm{V}_{\mathrm{CC}}<8 \mathrm{~V}$ | -3.0 |  | 3.0 | \% |
| $\mathrm{TCO}_{\text {REF }}$ | Reference temp co |  |  | 0.005 |  | \%/ ${ }^{\circ} \mathrm{C}$ |
| T ${ }^{\text {DRV }}$ | Discharge pulse width | $1.8 \mathrm{~V}<\mathrm{V}_{\mathrm{CC}}<8 \mathrm{~V}$ |  | 1.7 |  | $\mu \mathrm{S}$ |
| Fosc | Operating frequency |  |  |  | 200 | kHz |
| INPUT PARAMETERS |  |  |  |  |  |  |
| $\mathrm{V}_{\text {SENSE }}$ | Sense voltage |  | 22 | 28 | 34 | mV |
| $\mathrm{I}_{\text {SENSE }}$ | Sense input current | $\mathrm{V}_{\mathrm{FB}}=0 \mathrm{~V} ; \mathrm{V}_{\text {SENSE }}=0 \mathrm{~V}$ | -1 | -7 | -15 | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\mathrm{FB}}$ | Feedback voltage |  | 291 | 300 | 309 | mV |
| $\mathrm{IFB}{ }^{(2)}$ | Feedback input current | $\mathrm{V}_{\mathrm{FB}}=0 \mathrm{~V} ; \mathrm{V}_{\text {SENSE }}=0 \mathrm{~V}$ | -1.2 |  | -4.5 | $\mu \mathrm{A}$ |
| VIH ${ }^{(3)}$ | Shutdown threshold |  | 1.5 |  | $\mathrm{V}_{\mathrm{CC}}$ | V |
| VIL | Shutdown threshold |  | 0 |  | 0.55 | V |
| $\mathrm{dV}_{\mathrm{LN}}$ | Line voltage regulation |  |  | 0.5 |  | \%N |
| OUTPUT PARAMETERS |  |  |  |  |  |  |
| I DRIVE | Transistor drive current | $\mathrm{V}_{\text {DRIVE }}=0.7 \mathrm{~V}$ | 2 | 3.4 | 5 | mA |
| $\mathrm{V}_{\text {DRIVE }}$ | Transistor voltage drive |  | 0 |  | $\mathrm{V}_{\mathrm{CC}}-0.4$ | V |
| $\mathrm{C}_{\text {DRIVE }}$ | Mosfet gate drive cpbty |  |  | 300 |  | pF |
| VOH READY | Ready flag output high | $\mathrm{I}_{\text {EOR }}=-300 \mathrm{nA}, \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 2.5 |  | $\mathrm{V}_{\mathrm{CC}}$ | V |
| VOL ${ }_{\text {READY }}$ | Ready flag output low | $\mathrm{I}_{\text {EOR }}=1 \mathrm{~mA}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 0 |  | 1 | V |
| $\mathrm{T}_{\text {READY }}$ |  | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 195 |  | $\mu \mathrm{S}$ |
| $\mathrm{dl}_{\text {LD }}$ | Load current regulation |  |  |  | 0.01 | \%/mA |

## notes

(1) Excluding gate/base drive current.
(2) IFB is typically half of these at 3 V .
(3) Shutdown pin voltage must not exceed (VCC +0.3 V ) or 5 V , whichever is lower.

ZXSC440

ABSOLUTE MAXIMUM RATINGS

| PIN \# | NAME | DESCRIPTION |
| :---: | :--- | :--- |
| 1 | DRIVE | Drive output for external switching transistor. Connect to base or gate of external <br> switching transistor |
| 2 | $\mathrm{~V}_{\text {FB }}$ | Reference voltage. Internal threshold set to 300mV. Connect external resistor <br> network to set output voltage |
| 3 | SENSE | Inductor current sense input. Internal threshold voltage set to 28mV. Connect <br> external sense resistor |
| 4 | N/C |  |
| 5 | CHARGE | Initiate photoflash capacitor charging |
| 6 | READY | Signal to microprocessor when photoflash capacitor charged |
| 7 | GND | Ground |
| 8 | $\mathrm{~V}_{\mathrm{CC}}$ | Supply voltage, 1.8V to 8 V |

## BLOCK DIAGRAM



## ZXSC440

## DEVICE DESCRIPTION

## Bandgap reference

All threshold voltages and internal currents are derived from a temperature compensated bandgap reference circuit with a reference voltage of 1.22 V nominal. If the REF terminal is used as a reference for external devices, the maximum load should not exceed $\pm 2 \mu \mathrm{~A}$.

## Dynamic drive output

Depending on the input signal, the output is either "LOW" or "HIGH". In the high state a 3.4 mA current source (max drive voltage $=\mathrm{V}_{c c}-0.4 \mathrm{~V}$ ) drives the base or gate of the external transistor. In order to operate the external switching transistor at optimum efficiency, both output states are initiated with a short transient current in order to quickly discharge the base or the gate of the switching transistor.

## Switching circuit

The switching circuit consists of two comparators, Comp1 and Comp2, a gate U1, a monostable and the drive output. Normally the DRIVE output is "HIGH"; the external switching transistor is turned on. Current ramps up in the inductor, the switching transistor and external current sensing resistor. This voltage is sensed by comparator, Comp2, at input SENSE. Once the current sense voltage across the sensing resistor exceeds 28 mV , comparator, Comp2, through gate U1, triggers a re-triggerable monostable and turns off the output drive stage for $1.7 \mu \mathrm{~s}$. The inductor discharges into the reservoir capacitor. After $1.7 \mu$ s a new charge cycle begins, thus ramping the output voltage. When the output voltage reaches the nominal value and $V_{F B}$ gets an input voltage of more than 300 mV , the monostable is forced "on" from Comp1 through gate U 1 , until the feedback voltage falls below 300 mV . The above action continues to maintain regulation, with slight hysteresis on the feedback threshold.

## READY detector

The READY circuit is a re-triggerable $195 \mu \mathrm{~s}$ monostable, which is re-triggered by every down regulating action of comparator Comp1. As long as regulation takes place, output READY is "HIGH" (high impedance, 100 K to $\mathrm{V}_{\text {cc }}$ ). Short dips of the output voltage of less than $195 \mu \mathrm{~s}$ are ignored. If the output voltage falls below the nominal value for more than $195 \mu \mathrm{~s}$, output READY goes "LOW". This can be used to signal to the camera controller that the flash unit has charged fully and is ready to use.

ISSUE 1-J ANUARY 2005

## ZXSC440

TYPICAL OPERATING CHARACTERISTICS
(For typical application circuit at $\mathrm{V}_{\mathrm{IN}}=3 \mathrm{~V}$ and $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless otherwise stated)

|  |  |
| :---: | :---: |
|  |  |

## ZXSC440

## APPLICATIONS

## Switching transistor selection

The choice of switching transistor has a major impact on the converter efficiency. For optimum performance, a bipolar transistor with low $\mathrm{V}_{\text {CE(SAT) }}$ and high gain is required. The $\mathrm{V}_{\text {CEO }}$ of the switching transistor is also an important parameter as this sees typically three times the input voltage when the transistor is switched off. Zetex SuperSOT ${ }^{\text {TM }}$ transistors are an ideal choice for this application. At input voltages above 4 V , suitable Zetex MOSFET transistors will give almost the same performance with a simpler drive circuit, omitting the ZXTD6717 pre-drive stage. Using a MOSFET, the Schottky diode may be omitted, as the body diode of the MOSFET will perform the same function, with justa small loss of efficiency.

## Output rectifier diode selection

The diode should have a fast recovery, as any time spent in reverse conduction removes energy from the reservoir capacitor and dumps it, via the transformer, into the protection diode across the output transistor. This seriously reduces efficiency. Two BAS21 diodes in series have been used, bearing in mind that the reverse voltage across the diode is the sum of the output voltage together with the input voltage multiplied by the step-up ratio of the transformer:
$\mathrm{V}_{\mathrm{R} \text { (DIODE) }}=\mathrm{V}_{\text {OUt(MAX }}+\left(\mathrm{V}_{\text {IN }} \times\right.$ TURNSRAtIO $)$

## Sense resistor

A low value sense resistor is required to set the peak current. Power in this resistor is negligible due to the low sense voltage threshold, $V_{\text {SENSE }}$. Below is a table of recommended sense resistors:

Therefore, with a 300 V output, a supply of 8 volts and a 1:12 step-up transformer, there will be a 396 V across the diode. This occurs during the current ramp-up in the primary, as it transforms the input voltage up by the turns ratio and the polarity at the secondary is such as to add to the output voltage already being held off by the diode.

## Peak current definition

In general, the IPK value must be chosen to ensure that the switching transistor, Q1, is in full saturation with maximum output power conditions, assuming worse-case input voltage and transistor gain under all operating temperature extremes.
Once Ipk is decided the value of Rsense can be determined by:

$$
R_{S E N S E}=\frac{V_{S E N S E}}{I_{P K}}
$$

| Manufacturer | Series | $\mathbf{R}_{\mathbf{D C}}(\boldsymbol{\Omega})$ Range | Size | Tolerance | URL |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Cyntec | RL1220 | $0.022-10$ | 0805 | $\pm 5 \%$ | http://www.cyntec.com |
| IRC | LR1206 | $0.010-1.0$ | 1206 | $\pm 5 \%$ | http://www.irctt.com |

Using a $22 \mathrm{~m} \Omega$ sense resistor results in a peak current of just over 1.2A.

ISSUE 1-J ANUARY 2005

## Transformer parameters

Proprietary transformers are available, for example the Pulse PAO367, Primary inductance: 24 uH , Core: Pulse PAO367, Turns ratio: 1:12, see Bill of Materials below. If designing a transformer, bear in mind that the primary current may be over an amp and, if this flows through 10 turns, the primary flux will be 10 Amp . Turns and small cores will need an air gap to cope with this value without saturation. Secondary winding capacitance should not be too high as this is working at 300 V and could soon cause excessive losses.

## ZXSC440 Transformer specifications

| Part No. | Size <br> $(\mathbf{W x L x H}) \mathbf{m m}$ | $\mathbf{L}_{\text {PRI }}$ <br> $(\mu \mathrm{H})$ | $\mathbf{L}_{\text {PRI -LEAK }}$ <br> $(\mathbf{n H})$ | $\mathbf{N}$ | $\mathbf{R}_{\text {PRI }}$ <br> $(\mathbf{m} \Omega)$ | $\mathbf{R}_{\text {SEC }}(\Omega)$ | Manufacturer |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
| $\mathrm{T}-15-089$ | $6.4 \times 7.7 \times 4$ | 12 | 400 | $10: 2$ | 211 | 27 | Tokyo Coil Eng. <br> www.tokyo-coil.co.jp |
| $\mathrm{T}-15-083$ | $8 \times 8.9 \times 2$ | 20 | 500 | $10: 2$ | 675 | 35 | w |


| SBL-5.6-1 | $5.6 \times 8.5 \times 4$ | 10 | 200 | $10: 2$ | 103 | 26 | Kijima Musen <br> Kijimahk@netvigator.com |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| PAO367 | $9.1 \times 9.1 \times 5.1$ | 24 |  | $12: 1$ |  |  | Pulse <br> www.pulseeng.com |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |

## ZXSC440

## Output power calculation

This is approximately the power stored in the coil times the frequency of operation times the efficiency. Assuming a current of 1.2 amps in a $30 \mu \mathrm{H}$ primary, the stored energy will be $21.6 \mu$ ]. The frequency is set by the time it takes the primary to reach 1.2 amps plus the $1.7 \mu \mathrm{~s}$ time allowed to discharge the energy into the reservoir capacitor. Using 3 volts, the ramp time is $12 \mu \mathrm{~s}$, so the frequency will be 73 kHz , giving an input power of about 1.6 watts. With an efficiency of $75 \%$ the output power will be 1.2 watts. An $80 \mu \mathrm{~F}$ capacitor charged to 300 volts stores 3.6 J , so 1.2 watts will take 3 seconds to charge it. Higher input voltages reduce the ramp time, the frequency therefore goes up and the output power is increased, resulting in shorter charging times.

## Output voltage adjustment

The ZXSC440 are adjustable output converters allowing the end user the maximum flexibility. For adjustable operation a potential divider network is connected as follows:

The output voltage is determined by the equation:

$$
V_{\text {OUT }}=\mathrm{V}_{\mathrm{FB}}(1+\mathrm{RA} / \mathrm{RB}),
$$

$$
\text { where } \mathrm{V}_{\mathrm{FB}}=300 \mathrm{mV}
$$

In a circuit giving 300 volts, the " 1 " in the above equation becomes negligible compared to the ratio which is around 1000. It will not be exactly 1000because of the negative input current in the feedback pin. The resistor values, RA and RB, should be maximized to improve efficiency and decrease battery drain. Optimization can be achieved by providing a minimum current of $\mathrm{I}_{\mathrm{FB}(\mathrm{MAX})}=200 \mathrm{nA}$ to the $\mathrm{V}_{\text {FB }}$ pin. Output is adjustable from $\mathrm{V}_{F B}$ to the (BR) $\mathrm{V}_{\text {CEO }}$ of the switching transistor, Q1.
In practice, there will be some stray capacitance across RA and this will cause a lead in the feedback which can affect hysteresis (it makes the device shut down too early) and it is best to swamp this with a capacitor CA and then use a capacitor CB across RB where CB/CA $=$ RA/RB. This is similar to the method used for compensating oscilloscope probes.


## ZXSC440

## Layout issues

Layout is critical for the circuit to function in the most efficient manner in terms of electrical efficiency, thermal considerations and noise.
For 'step-up converters' there are four main current loops, the input loop, power-switch loop, rectifier loop and output loop. The supply charging the input capacitor forms the input loop. The power-switch loop is defined when Q1 is 'on', current flows from the input through the transformer primary, Q1, Rsense and to ground. When Q1 is 'off', the energy stored in the transformer is transferred from the secondary to the output capacitor and load via D1, forming the rectifier loop. The output loop is formed by the output capacitor supplying the load when Q1 is switched back off.

To optimize for best performance each of these loops kept separate from each other and interconnected with short, thick traces thus minimizing parasitic inductance, capacitance and resistance. Also the RSENSE resistor should be connected, with minimum trace length, between emitter lead of Q1 and ground, again minimizing stray parasitics.

## ZXSC440

## REFERENCE DESIGNS

General camera photoflash charger Circuit diagram

## Specification

| $\mathrm{V}_{\text {IN }}=$ | 5 V |
| :--- | :--- |
| $\mathrm{~V}_{\text {out }}=$ | 275 V |
| Efficiency $=$ | $71 \%$ |
| Charging time $=$ | 4 seconds |



| Bill of materials |
| :--- |
| Ref Value Package Part number Manufacturer Notes <br> U1  MSOP8 ZXSC440 Zetex  <br> Q1  SOT23 ZXMN6A07F Zetex 60 V N-channel M OSFET <br> D1 ${ }^{(2)}$ 200 V SOT23 BAS21 Philips x2 200V fast rectifier diodes <br> connected in series <br> Tx1    Pulse See note ${ }^{(1)}$ <br> R1 $22 \mathrm{~m} \Omega$ 0805 RL1210 Cyntec  <br> R2 $10 \mathrm{M} \Omega / 400 \mathrm{~V}$ Axial Generic Generic Output voltage across resistor <br> R3 $10 \mathrm{k} \Omega$ 0805 Generic Generic  <br> R4 $100 \mathrm{k} \Omega$ 0805 Generic Generic  <br> C1 $100 \mathrm{uF} / 10 \mathrm{~V}$ 0805 Generic Murata  <br> C2 $10 \mathrm{pF} / 500 \mathrm{~V}$ 1206 Generic Generic Output voltage seen across capacitor <br> C3 $10 \mathrm{nF} / 6 \mathrm{~V} 3$ 1206 Generic Generic  <br> C4 $120 \mathrm{uF} / 330 \mathrm{~V}$ Radial FW Series Rubycon Photoflash capacitor |

## NOTES:

(1) Transformer specification: Primary inductance: 24uH, Core: Pulse PAO367, Turns ratio: 1:12
(2) Two BAS21 200V rectifier diodes are connected in series and used in place of a 400 V rectifier diode to provide faster switching speeds and higher efficiency

ISSUE 1-J ANUARY 2005

## High power digital camera photoflash charger

Specification

| VIN $=$ | 3 V |
| :--- | :--- |
| Vout $=$ | 275 V |
| Efficiency $=$ | $69 \%$ |
| Charging time $=$ | 5 seconds |

## Circuit diagram



Bill of materials

| Ref | Value | Package | Part number | Manufacturer | Notes |
| :--- | :--- | :--- | :--- | :--- | :--- |
| U1 |  | MSOP8 | ZXSC440 | Zetex |  |
| U2 |  | SOT23-6 | ZXTD6717 | Zetex | NPN/PNP dual |
| Q1 |  | SOT23 | FMMT619 | Zetex | 50V NPN low sat |
| D1 | 200 V | SOT23 | BAS21 | Philips | 200V fast rectifier |
| D2 | 200 V | SOT23 | BAS21 | Philips | 200V fast rectifier |
| D3 | 2 A | SOT23-6 | ZLLS2000 | Zetex | 2A Schottky diode |
| Tx1 |  |  | PAO367 | Pulse | See note ${ }^{(1)}$ |
| R1 | $22 \mathrm{~m} \Omega$ | 0805 | RL1210 | Cyntec |  |
| R2 | $130 \Omega$ | 0805 | Generic | Generic |  |
| R3 | $2 \mathrm{k} 2 \Omega$ | 0805 | Generic | Generic |  |
| R4 | $10 \mathrm{M} \Omega / 400 \mathrm{~V}$ | Axial | Generic | Generic | Output voltage across resistor |
| R5 | $10 \mathrm{k} \Omega$ | 0805 | Generic | Generic |  |
| C1 | $100 \mathrm{uF/10V}$ | 0805 | Generic | Murata |  |
| C2 | 220 nF | 0805 | GRM Series | Murata |  |
| C3 | $10 \mathrm{pF} / 500 \mathrm{~V}$ | 1206 | Generic | Generic | Output voltage seen across capacitor |
| C4 | $10 \mathrm{nF} / 6 \mathrm{~V} 3$ | 1206 | Generic | Generic |  |
| C5 | $120 \mathrm{uF} / 330 \mathrm{~V}$ | Radial | FW Series | Rubycon | Photoflash capacitor |

notes:
(1) Transformer specification: Primary inductance: 24 uH , Core: Pulse PAO367, Turns ratio: 1:12

## ZXSC440

## Low power digital camera photoflash charger

## Specification

| VIN $=$ | 3 V |
| :--- | :--- |
| $\mathrm{~V}_{\text {OUT }}=$ | 275 V |
| Efficiency $=$ | $58 \%$ |
| Charging time $=$ | 6.8 seconds |

VOUT $=\quad 275 \mathrm{~V}$
Charging time $=6.8$ seconds

Circuit diagram


Bill of materials

| Ref | Value | Package | Part number | Manufacturer | Notes |
| :--- | :--- | :--- | :--- | :--- | :--- |
| U1 |  | MSOP8 | ZXSC440 | Zetex |  |
| U2 |  | SOT23-6 | ZXTD6717 | Zetex | NPN/PNP dual |
| Q1 |  | SOT23 | FMMT619 | Zetex | 50V NPN low sat |
| D1 | 200 V | SOT23 | BAS21 | Philips | 200V fast rectifier |
| D2 | 200 V | SOT23 | BAS21 | Philips | 200V fast rectifier |
| D3 | 2 A | SOT23-6 | ZLLS2000 | Zetex | 2A Schottky diode |
| Tx1 |  |  |  | Sumida | See note ${ }^{(1)}$ |
| R1 | $33 \mathrm{~m} \Omega$ | 0805 | RL1210 | Cyntec |  |
| R2 | $200 \Omega$ | 0805 | Generic | Generic |  |
| R3 | $2 \mathrm{k} 2 \Omega$ | 0805 | Generic | Generic |  |
| R4 | $10 \mathrm{M} \Omega / 400 \mathrm{~V}$ | Axial | Generic | Generic | Output voltage across resistor |
| R5 | $10 \mathrm{k} \Omega$ | 0805 | Generic | Generic |  |
| C1 | $100 \mathrm{uF} / 10 \mathrm{~V}$ | 0805 | Generic | Murata |  |
| C2 | 220 nF | 0805 | GRM Series | Murata |  |
| C3 | $10 \mathrm{pF} / 500 \mathrm{~V}$ | 1206 | Generic | Generic | Output voltage seen across capacitor |
| C4 | $10 \mathrm{nF} / 6 \mathrm{~V} 3$ | 1206 | Generic | Generic |  |
| C5 | $80 \mathrm{uF} / 330 \mathrm{~V}$ | Radial | FW Series | Rubycon | Photoflash capacitor |

NOTES:
(1) Transformer specification: Primary inductance: 32uH, Core: Sumida CEEH64, Turns ratio: 1:10

ISSUE 1-J ANUARY 2005

## ZXSC440

NOTES:

Downloaded from Elcodis.com electronic components distributor

## ZXSC440

NOTES:

ISSUE 1 - J ANUARY 2005

## ZXSC440

NOTES:

Downloaded from Elcodis.com electronic components distributor

## ZXSC440

PACKAGE OUTLINE


Controlling dimensions are in millimeters. Approximate conversions are given in inches
PACKAGE DIMENSIONS

| DIM | Millimeters |  | Inches |  | DIM | Millimeters |  | Inches |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Min | Max | Min | Max |  | Min | Max | Min | Max |
| A | - | 1.10 | - | 0.0433 | E | 4.90 BSC |  | 0.025 BSC |  |
| A1 | 0.05 | 0.15 | 0.002 | 0.006 | E1 | 2.90 | 3.10 | 0.114 | 0.122 |
| A2 | 0.75 | 0.95 | 0.0295 | 0.0374 | e | 0.65 BSC |  | 0.193 BSC |  |
| b | 0.25 | 0.40 | 0.010 | 0.0157 | L | 0.40 | 0.70 | 0.0157 | 0.0192 |
| c | 0.13 | 0.23 | 0.005 | 0.009 | R | 0.07 | - | 0.0027 | - |
| D | 2.90 | 3.10 | 0.114 | 0.122 | R1 | 0.07 | - | 0.0027 | - |

© Zetex Semiconductors plc 2005

| Europe | Americas | Asia Pacific | Corporate Headquaters |
| :--- | :--- | :--- | :--- |
|  |  |  |  |
| Zetex GmbH | Zetex Inc | Zetex (Asia) Ltd | Zetex Semiconductors plc |
| Streitfeldstraße 19 | 700 Veterans Memorial Hwy | 3701-04 Metroplaza Tower 1 | Zetex Technology Park |
| D-81673 München | Hauppauge, NY 11788 | Hing Fong Road, Kwai Fong | Chadderton, Oldham, OL9 9LL |
| Germany | USA | Hong Kong | United Kingdom |
|  |  | Telephone: (852) 26100 611 | Telephone (44) 161 622 4444 |
| Telefon: (49) 89 45 49 49 0 | Telephone: (1) 631 360 2222 | Fax: (852) 24250494 | Fax: (44) 161622 4446 |
| Fax: (49) 89 45 49 49 49 | Fax: (1) 631 360 8222 | asia.sales@zetex.com | hq@zetex.com |
| europe.sales@zetex.com | usa.sales@zetex.com |  |  |

europe.sales@zetex.com usa.sales@zetex.com asia.sales@zetex.com
These offices are supported by agents and distributors in major countries world-wide.
This publication is issued to provide outline information only which (unless agreed by the Company in writing) may not be used, applied or reproduced for any purpose or form part of any order or contract or be regarded as a representation relating to the products or services concerned. The Company reserves the right to alter without notice the specification, design, price or conditions of supply of any product or service.
For the latest product information, log on to wWW.zetex.com

