## EVALUATION KIT AVAILABLE

 Current Sources with Synchronous RectifierGeneral Description
The MAX1640/MAX1641 CMOS, adjustable-output, switch-mode current sources operate from a +5.5 V to +26 V input, and are ideal for microprocessor-controlled battery chargers. Charging current, maximum output voltage, and pulse-trickle charge are programmed with external resistors. Programming the off-time modifies the switching frequency, suppressing undesirable harmonics in noise-sensitive circuits. The MAX1640's highside current sensing allows the load to connect directly to ground, eliminating ground-potential errors. The MAX1641 incorporates a low-side current sense.
The MAX1640/MAX1641 step-down pulse-width-modulation (PWM) controllers use an external P-channel MOSFET switch and an optional, external N-channel MOSFET synchronous rectifier for increased efficiency. An internal low-dropout linear regulator provides power for the internal reference and circuitry as well as the gate drive for the N -channel synchronous rectifier.
The MAX1640/MAX1641 are available in space-saving, 16-pin narrow QSOP packages.

## Applications

Battery-Powered Equipment
Laptop, Notebook, and Palmtop Computers Handy Terminals
Portable Consumer Products
Cordless Phones
Cellular Phones
PCS Phones
Backup Battery Charger
Pin Configuration

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For pricing, delivery, and ordering information, please contact Maxim/Dallas Direct! at 1-888-629-4642, or visit Maxim's website at www.maxim-ic.com.

# Adjustable-Output, Switch-Mode Current Source with Synchronous Rectifier 

## ABSOLUTE MAXIMUM RATINGS



PGND to GND. $\pm 0.3 \mathrm{~V}$
LDOH to IN +0.3 V to -6 V LDOL to GND .........................................................-0.3V to +6 V PDRV to GND .............................. (VLDOH - 0.3V) to (VIN +0.3 V ) NDRV to GND ........................................-0.3V to (VLDOL + 0.3V) TOFF, REF, SET, TERM, CC to GND ......-0.3V to (VLDOL + 0.3V) CS+, CS- to GND
-0.3 V to +28 V
Continuous Power Dissipation $\left(\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}\right)$ QSOP (derate $8.30 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $+70^{\circ} \mathrm{C}$ )................... 667 mW Operating Temperature Range MAX164_EEE. $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range ............................. $65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
Lead Temperature (soldering, 10 sec ) ............................ $+300^{\circ} \mathrm{C}$

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## ELECTRICAL CHARACTERISTICS

$\left(\mathrm{V}_{\text {IN }}=+12 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=6 \mathrm{~V}\right.$, Circuit of Figure $2, \mathrm{~T}_{\mathrm{A}}=\mathbf{0}^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.)

| PARAMETER | SYMBOL | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Input Voltage Range | V IN |  |  | 5.5 |  | 26 | V |
| Linear-Regulator Output Voltage, VIN Referenced | VLDOH | V IN $=5.5 \mathrm{~V}$ to 26 V , $\operatorname{l}$ LOAD $=0$ to 20 mA |  | $\begin{gathered} \text { VIN - } \\ 5.5 \end{gathered}$ | $\begin{gathered} \mathrm{V}_{\mathrm{IN}}- \\ 5.0 \end{gathered}$ | $\begin{gathered} \mathrm{V}_{\mathrm{IN}}- \\ 4.5 \end{gathered}$ | V |
| Linear-Regulator Output Voltage, Ground Referenced | VLDOL | $\mathrm{V}_{\mathrm{IN}}=5.5 \mathrm{~V}$ to 26 V , $\mathrm{I}_{\text {LOAD }}=0$ to 20 mA |  | 4.5 | 5.0 | 5.5 | V |
| Full-Scale Current-Sense Threshold |  | MAX1640 |  | 142 | 150 | 158 | mV |
|  |  | MAX1641 |  | 147 | 150 | 153 |  |
| Quarter-Scale Current-Sense Threshold |  | MAX1640 |  | 36 | 42 | 48 | mV |
|  |  | MAX1641 |  | 34 | 37.5 | 41 |  |
| Current-Sense Line Regulation |  | $\mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {OUT }}+0.5 \mathrm{~V}$ to 26 V |  |  | 0.03 |  | \%/V |
| Output Current Compliance |  | VOUT $=2 \mathrm{~V}$ to 24 V | MAX1640 |  | 0.1 | 0.4 | \%/V |
|  |  |  | MAX1641 |  | 0.1 |  |  |
| Quiescent VIN Supply Current |  | D0 or D1 = high |  |  | 2 | 4 | mA |
|  |  | D0 = D1 = low (off mode) |  |  | 500 |  | $\mu \mathrm{A}$ |
| Output Current in Off Mode |  | D0 = D1 = low |  |  |  | 1 | $\mu \mathrm{A}$ |
| VLDOL Undervoltage Lockout |  |  |  | 4.05 | 4.20 | 4.35 | V |
| Reference Voltage | VREF |  |  | 1.96 | 2.00 | 2.04 | V |
| Reference Load Regulation |  | IREF $=0$ to $50 \mu \mathrm{~A}$ |  |  | 4 | 10 | mV |
| $V_{\text {SET }}$ Input Current |  |  |  |  |  | 1 | $\mu \mathrm{A}$ |
| FET Drive Output Resistance |  | PFET and NFET drive |  |  |  | 12 | $\Omega$ |
| Off-Time Range |  |  |  | 1 |  | 10 | $\mu \mathrm{s}$ |
| Off-Time Accuracy |  | RTOFF $=62 \mathrm{k} \Omega$ |  | 1.7 | 2.2 | 2.7 | $\mu \mathrm{s}$ |
| Pulse-Trickle Mode Duty-Cycle Period |  | D0 $=$ low, $\mathrm{D} 1=$ high, $\mathrm{RTOFF}=100 \mathrm{k} \Omega$ |  | 27 | 33 | 40 | ms |
| Pulse-Trickle Mode Duty Cycle (Note 1) |  | D0 $=$ low, $\mathrm{D} 1=$ high, RTOFF $=100 \mathrm{k} \Omega$ |  |  | 12.5 |  | \% |

Note 1: This ratio is generated by a 1:8 clock divider and is not an error source for current calculations.

# Adjustable-Output, Switch-Mode Current Source with Synchronous Rectifier 

## ELECTRICAL CHARACTERISTICS (continued)

$\left(\mathrm{V}_{\text {IN }}=+12 \mathrm{~V}\right.$, $\mathrm{V}_{\text {OUT }}=6 \mathrm{~V}$, Circuit of Figure 2, $\mathrm{T}_{\mathbf{A}}=\mathbf{0}^{\circ} \mathbf{C}$ to $+85^{\circ} \mathrm{C}$, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PWM Maximum Duty Cycle |  |  | 100 |  | \% |
| Input Low Voltage | VIL | D0, D1 |  | 0.8 | V |
| Input High Voltage | $\mathrm{V}_{\mathrm{IH}}$ | D0, D1 | 2.4 |  | V |
| Input Leakage Current | IIN | D0, D1 |  | $\pm 1$ | $\mu \mathrm{A}$ |

## ELECTRICAL CHARACTERISTICS

( $\mathrm{V}_{\mathrm{IN}}=+12 \mathrm{~V}$, VOUT $=6 \mathrm{~V}$, Circuit of Figure $2, \mathrm{~T}_{\mathrm{A}}=-\mathbf{4 0 ^ { \circ }} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$, unless otherwise noted.)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Input Voltage Range | VIN |  | 5.5 | 26 | V |
| Linear-Regulator Output Voltage, VIN Referenced | VLDOH | $\mathrm{V}_{\mathrm{IN}}=5.5 \mathrm{~V}$ to 26 V , ILOAD $=0$ to 20 mA | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}- \\ & 55 \end{aligned}$ | $\begin{gathered} \mathrm{V}_{\mathrm{IN}}- \\ 4.5 \end{gathered}$ | V |
| Linear-Regulator Output Voltage, Ground Referenced | VLDOL | $\mathrm{V}_{\mathrm{IN}}=5.5 \mathrm{~V}$ to 26 V , ILOAD $=0$ to 20 mA | 4.5 | 5.5 | V |
| Full-Scale Current-Sense Threshold |  | MAX1640 | 141 | 159 | mV |
|  |  | MAX1641 | 146 | 154 |  |
| Quarter-Scale Current-Sense Threshold |  | MAX1640 | 34 | 48 | mV |
|  |  | MAX1641 | 33 | 42 |  |
| Output Current Compliance |  | VOUT = 2V to 24V (MAX1640) |  | 0.4 | \%/V |
| Quiescent VIN Supply Current |  | D0 or D1 = high |  | 4 | mA |
| Output Current in Off Mode |  | D0 = D1 = low |  | 1 | $\mu \mathrm{A}$ |
| VLDOL Undervoltage Lockout |  |  | 4.0 | 4.4 | V |
| Reference Voltage | $V_{\text {REF }}$ |  | 1.94 | 2.06 | V |
| Reference Load Regulation |  | IREF $=0$ to $50 \mu \mathrm{~A}$ |  | 10 | mV |
| $\mathrm{V}_{\text {SET }}$ Input Current |  |  |  | 1 | $\mu \mathrm{A}$ |
| FET Drive Output Resistance |  |  |  | 12 | $\Omega$ |
| Off-Time Range |  |  | 1.5 | 8 | $\mu \mathrm{s}$ |
| Off-Time Accuracy |  | RTOFF $=62 \mathrm{k} \Omega$ | 1.5 | 2.5 | $\mu \mathrm{s}$ |
| Pulse-Trickle Mode Duty-Cycle Period |  | $\mathrm{D} 0=$ low, $\mathrm{D} 1=$ high, $\mathrm{RTOFF}=50 \mathrm{k} \Omega$ | 25 | 42 | ms |
| PWM Maximum Duty Cycle |  |  | 100 |  | \% |
| Input Low Voltage | $\mathrm{V}_{\text {IL }}$ | D0, D1 |  | 0.8 | V |
| Input High Voltage | $\mathrm{V}_{\mathrm{IH}}$ | D0, D1 | 2.4 |  | V |
| Input Leakage Current | IIN | D0, D1 |  | $\pm 1$ | $\mu \mathrm{A}$ |

## Adjustable-Output, Switch-Mode Current Source with Synchronous Rectifier



MAX1641
OUTPUT CURRENT vs. INPUT VOLTAGE


MAX1640
OUTPUT CURRENT vs. INPUT VOLTAGE


MAX1641
OUTPUT CURRENT vs. OUTPUT VOLTAGE


OFF-MODE SUPPLY CURRENT


Typical Operating Characteristics
(Circuit of Figure $2, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted.)

# Adjustable-Output, Switch-Mode Current Source with Synchronous Rectifier 

Typical Operating Characteristics (continued)
(Circuit of Figure 2, $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted.)

CURRENT-M ODE CHANGE RESPONSE TIME

$V_{I N}=12 V, V_{S E T}=1 V$, RLOAD $=4 \Omega$, NO OUTPUT CAPACITOR
A: OUTPUT CURRENT, DO = D1 = $0 \quad 1 \mathrm{~A} / \mathrm{div}$
B: LOAD VOLTAGE, AC coupled, $500 \mathrm{mV} / \mathrm{div}$

$\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}$, RLOAD $=4 \Omega$
$A: D 0=D 1=1 \quad 2 \mathrm{~V} / \mathrm{div}$
B: OUTPUT CURRENT, $0.5 \mathrm{~A} / \mathrm{div}$

Pin Description

| PIN | NAME | FUNCTION |
| :---: | :---: | :---: |
| 1 | LDOL | Internal, Ground-Referenced Low-Dropout Linear Regulator Output. Bypass with a $0.1 \mu \mathrm{~F}$ capacitor in parallel with a $4.7 \mu \mathrm{~F}$ capacitor to GND. |
| 2 | TOFF | Off-Time Select Input. A resistor (RTOFF) connected from this pin to GND programs the off-time for the hysteretic PWM step-down converter. This resistor also sets the period in duty-cycle mode. See Duty-Cycle Mode and Programming the Off-Time. |
| 3, 4 | D1, D0 | Digital Inputs. Select mode of operation (Table 1). |
| 5 | CC | Constant-Current Loop Compensation Input. Bypass with a $0.01 \mu \mathrm{~F}$ capacitor to GND. |
| 6 | REF | Reference Voltage Output ( $\mathrm{V}_{\text {REF }}=2 \mathrm{~V}$ ). Bypass with a $0.1 \mu \mathrm{~F}$ capacitor to GND. |
| 7 | SET | Current Select Input. Program the desired current level by applying a voltage at SET between OV and VREF, ( $I=V_{\text {SET }} / 13.3 R$ SENSE $)$. See Figure 3. |
| 8 | TERM | Maximum Output Voltage Termination Input. When $\mathrm{V}_{\text {TERM }}$ exceeds the reference voltage, the comparator resets the internal PWM latch, shutting off the external P-channel FET. |
| 9 | GND | Ground |
| 10 | CS- | Negative Current-Sense Comparator Input |
| 11 | CS+ | Positive Current-Sense Comparator Input |
| 12 | PGND | High-Current Ground Return for the Output Drivers |
| 13 | NDRV | Gate Drive for an Optional N-Channel FET Synchronous Rectifier |
| 14 | PDRV | Gate Drive for the P-Channel FET |
| 15 | LDOH | Internal, Input-Referenced Low-Dropout Linear Regulator Output. Bypass with a $0.33 \mu \mathrm{~F}$ capacitor to IN . |
| 16 | IN | Power-Supply Input. Input of the internal, low-dropout linear regulators. |

## Adjustable-Output, Switch-Mode Current Source with Synchronous Rectifier



Figure 1. MAX1640/MAX1641 Functional Diagram
$\qquad$

# Adjustable-Output, Switch-Mode Current Source with Synchronous Rectifier 



Figure 2a. Standard Application Circuit

## Detailed Description

The MAX1640/MAX1641 switch-mode current sources utilize a hysteretic, current-mode, step-down pulse-width-modulation (PWM) topology with constant offtime. Internal comparators control the switching mechanism. These comparators monitor the current through a sense resistor (RSENSE) and the voltage at TERM. When inductor current reaches the current limit [(VCS+ - $\left.\mathrm{V}_{\mathrm{CS}}-\right) /$ RSENSE], the P-channel FET turns off and the N -channel FET synchronous rectifier turns on. Inductor energy is delivered to the load as the current ramps down. This ramp rate depends on Rtoff and inductor values. When off-time expires, the P-channel FET turns back on and the N -channel FET turns off.
Two digital inputs, D0 and D1, select between four possible current levels (Table 1). In pulse-trickle mode, the


Figure 2b. Standard Application Circuit
part operates for $12.5 \%$ of the period set by RTOFF, resulting in a lower current for pulse-trickle charging. Figure 1 is the MAX1640/MAX1641 functional diagram. Figure 2 shows the standard application circuits.

## Charge Mode: Programming the Output Currents

The sense resistor, RSENSE, sets two charging current levels. Choose between these two levels by holding D0 high, and toggling D1 either high or low (Table 1). The fast-charge current level equals VCS / RSENSE where $\mathrm{V}_{\mathrm{CS}}$ is the full-scale current-sense voltage of 150 mV . Alternatively, calculate this current by VREF / (13.3RSENSE). The top-off current equals VSET / (13.3RSENSE). A resistor-divider from REF to GND programs the voltage at SET (Figure 3).

## Adjustable-Output, Switch-Mode Current Source with Synchronous Rectifier

The voltage at SET is given by:
R1 = R2 (VREF / VSET -1 ); 10k $\Omega<$ R2 $<300 \mathrm{k} \Omega$
where $\mathrm{V}_{\text {REF }}=2 \mathrm{~V}$ and $\mathrm{V}_{\text {SET }}$ is proportional to the desired output current level.

Table 1. Selecting Output Current Levels

| D1 | DO | MODE | OUTPUT CURRENT (A) |
| :---: | :---: | :---: | :---: |
| 0 | 0 | OFF | 0 |
| 0 | 1 | Top-Off | $V_{\text {SET }} /$ (13.3RSENSE) |
| 1 | 0 | Pulse-Trickle | $\mathrm{V}_{\text {SET }} /$ (13.3R RENSE ) 12.5\% duty cycle |
| 1 | 1 | Fast Charge | VREF / (13.3RSENSE) |



Figure 3. Adjusting the Output Current Level


Figure 4a. Setting the Maximum Output Voltage Level


Figure 4b. Setting the Maximum Output Voltage Level
The MAX1640/MAX1641 are specified for VSET
 increases linearly (with reduced accuracy) until it clamps at $\mathrm{V}_{\text {SET }} \approx 4 \mathrm{~V}$.

## Pulse-Trickle Mode: Selecting the Pulse-Trickle Current

Pulling D0 low and D1 high selects pulse-trickle mode. This current equals VSET / (13.3RSENSE) and remains on for $12.5 \%$ of the period set by RTOFF. Pulse-trickle current maintains full charge across the battery and can slowly charge a cold battery before fast charging commences.

$$
\text { PERIOD }=3.2 \times 10^{-7} \times \mathrm{R}_{\text {TOFF }}(\mathrm{sec})
$$

Off Mode: Turning Off the Output Current Pulling D0 and D1 low turns off the P-channel FET and hence the output current flow. This mode also controls end of charge and protects the battery against excessive temperatures.

## Setting the Maximum Output Voltage Level

 The maximum output voltage should be programmed to a level higher than the output/battery voltage (ILOAD x RLOAD). An external resistor-divider between the output and ground (Figure 4) sets the voltage at TERM. Once the voltage at TERM exceeds the reference, the internal comparator turns off the P-channel FET, terminating current flow. Select R4 in the $10 \mathrm{k} \Omega$ to $500 \mathrm{k} \Omega$ range. R3 is given by:$$
\text { R3 }=\text { R4 (VOUT / VTERM) }-1
$$

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where V TERM $=2 \mathrm{~V}$ and VOUT is the desired output voltage.

Programming the Off-Time
When programming the off-time, consider such factors as maximum inductor current ripple, maximum output voltage, inductor value, and inductor current rating. The output current ripple is less than the inductor current ripple and depends heavily on the output capacitor's size.
Perform the following steps to program the off-time:

1) Select the maximum output current ripple. $\operatorname{IR}(A)$
2) Select the maximum output voltage. VOUT(MAX)(V)
3) Calculate the inductor value range as follows:
$L_{\text {MIN }}=($ VOUTMAX $\times 1 \mu \mathrm{~s}) / I_{R}$
LMAX $=($ VOUTMAX $\times 10 \mu s) / I_{R}$
4) Select an inductor value in this range.
5) Calculate toff as follows:

$$
t_{\text {OFF }}=\frac{L \times \mathrm{l}_{\mathrm{R}}}{\mathrm{~V}_{\text {OUTMAX }}}
$$

6) Program toff by selecting Rtoff from:

$$
\text { RTOFF }=\left(29.3 \times 10^{9}\right) \times \text { tOFF }
$$

7) Calculate the switching frequency by:

$$
\mathrm{fs}=1 /(\mathrm{tON}+\mathrm{tOFF})
$$

where ton $=\left(I_{R} \times L\right) /\left(\mathrm{V}_{\mathrm{IN}}-\mathrm{V}_{\text {OUT }}\right)$ and $\mathrm{I}_{\mathrm{R}}=($ VOUT x tOFF) / L . L is the inductor value, VIN is the input voltage, VOUT is the output voltage, and $I_{R}$ is the output peak-to-peak current ripple.
Note that RTOFF sets both the off-time and the pulsetrickle charge period.

## Reference

The on-chip reference is laser trimmed for a precise 2V at REF. REF can source no more than $50 \mu \mathrm{~A}$. Bypass REF with a $0.1 \mu \mathrm{~F}$ capacitor to ground.

## Constant-Current Loop: AC Loop

 CompensationThe constant-current loop's output is brought out at CC. To reduce noise due to variations in switching currents, bypass CC with a 1 nF to 100 nF capacitor to ground. A large capacitor value maintains a constant average output current but slows the loop response to changes in switching current. A small capacitor value speeds up the loop response to changes in switching current,
generating increased ripple at the output. Select Ccc to optimize the ripple vs. loop response.

Synchronous Rectification
Synchronous rectification reduces conduction losses in the rectifier by shunting the Schottky diode with a lowresistance MOSFET switch. In turn, efficiency increases by about $3 \%$ to $5 \%$ at heavy loads. To prevent crossconduction or "shoot-through," the synchronous rectifier turns on shortly after the P-channel power MOSFET

## Table 2. Component Manufacturers

| COMPONENT | MANUFACTURER |  |
| :--- | :--- | :--- |
| Inductor | Sumida | CDRH125 series |
|  | Coilcraft | D03316P series |
|  | Coiltronics | UP2 series |
| MOSFETs | International Rectifier | IRF7309 |
|  | Siliconix | S14539DY |
| Sense Resistor | Dale | WSL-2010 series |
|  | IRC | LR2010-01 series |
| Capacitors | AVX | TPS series |
|  | Sprague | 595D series |
| Rectifier | Motorola | MBAR5340t3 |
|  |  | IN5817-IN5822 |
|  | Nihon | NSQ03A04 |

turns off. The synchronous rectifier remains off for 90\% of the off-time. In low-cost designs, the synchronous rectifier FET may be replaced by a Schottky diode.

## Component Selection

External Switching Transistors
The MAX1640/MAX1641 drive an enhancement-mode P-channel MOSFET and a synchronous-rectifier Nchannel MOSFET (Table 2).
When selecting a P-channel FET, some important parameters to consider are on-resistance (rDS(ON)), maximum drain-to-source voltage (VDS max), maximum gate-to-source voltage (VGS max), and minimum threshold voltage ( $\mathrm{V}_{\mathrm{TH}} \mathrm{min}$ ).

In high-current applications, MOSFET package power dissipation often becomes a dominant design factor. I2R power losses are the greatest heat contributor for both high-side and low-side MOSFETs. Switching losses affect the upper MOSFET only (P-channel), since the Schottky rectifier or the N-FET body diode clamps the switching node before the synchronous rectifier turns on.

## Rectifier Diode

If an N-channel MOSFET synchronous rectifier is not used, a Schottky rectifier is needed. The MAX1640/

# Adjustable-Output, Switch-Mode Current Source with Synchronous Rectifier 



Figure 5. Microcontroller Battery Charger

MAX1641's high switching frequency demands a highspeed rectifier (Table 2). Schottky diodes such as the 1N5817-1N5822 are recommended. Make sure the Schottky diode's average current rating exceeds the peak current limit and that its breakdown voltage exceeds the output voltage (VOUT). For high-temperature applications, Schottky diodes may be inadequate due to their high leakage current; high-speed silicon diodes such as the MUR105 or EC11FS1 can be used instead. At heavy loads and high temperatures, the benefits of a Schottky diode's low forward voltage may outweigh the disadvantage of high leakage current. If the application uses an N -channel MOSFET synchronous rectifier, a parallel Schottky diode is usually unnecessary except with very high charge current (> 3 amps). Best efficiency is achieved with both an N -channel MOSFET and a Schottky diode.

Inductor Value Refer to the section Programming the Off-Time to select the proper inductor value. There is a trade-off between
inductor value, off-time, output current ripple, and switching frequency.

Applications Information
All-Purpose Mic rocontroller Battery Charger: NiCd, NiMH In applications where a microcontroller is available, the MAX1640/MAX1641 can be used as a low-cost battery charger (Figure 5). The controller takes over fast charge, pulse-trickle charge, charge termination, and other smart functions. By monitoring the output voltage at VOUT, the controller initiates fast charge (set D0 and D1 high), terminates fast charge and initiates top-off (set D0 high and D1 low), enters trickle charge (set D0 low and D1 high), or shuts off and terminates current flow (set D0 and D1 low).

Layout and Grounding Due to high current levels and fast switching waveforms, proper PC board layout is essential. High-current ground paths should be connected in a star

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configuration to PGND. These traces should be wide to reduce resistance and as short as possible to reduce stray inductance. All low-current ground paths should be connected to GND. Place the input bypass capacitor as close as possible to the IN pin. See MAX1640 EV kit for layout example.

TRANSISTOR COUNT: 1233

Package Information
(The package drawing(s) in this data sheet may not reflect the most current specifications. For the latest package outline information, go to www.maxim-ic.com/packages.)


|  | INCHES |  | MILLIMETERS |  |
| :---: | :---: | :---: | :---: | :---: |
| DIM | MIN | MAX | MIN | MAX |
| A | . 061 | 068 | 1.55 | 1.73 |
| A1 | . 004 | . 0098 | 0.127 | 0.25 |
| A2 | . 055 | 061 | 1.40 | 1.55 |
| B | . 008 | 012 | 0.20 | 0.31 |
| C | . 0075 | . 0098 | 0.19 | 0.25 |
| D | SEE VARIATIDNS |  |  |  |
| E | . 150 | 157 | 3.81 | 3.99 |
| e | 025 BSC |  | 0.635 BSC |  |
| H | . 230 | 244 | 5.84 | 6.20 |
| h | . 010 | 016 | 0.25 | 0.41 |
| L | . 016 | 035 | 0.41 | 0.89 |
| N | SEE VARIATIDNS |  |  |  |
| S | SEE VARIATIDNS |  |  |  |
| ? | $0^{\circ}$ | $8^{\circ}$ | $0^{\circ}$ | $8^{\circ}$ |



| $D$ | .337 | .344 | 8.56 | 8.74 | 24 | AC |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | .0250 | .0300 | 0.64 | 0.76 |  |  |
|  |  |  |  |  |  |  |


| $D$ | .386 | .393 | 9.80 | 9.98 | 28 | AD |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :---: |
|  | S | .0250 | .0300 | 0.64 | 0.76 |  |  |
|  |  |  |  |  |  |  |  |


NUTES:

1. D \& E DU NDT INCLUDE MILD FLASH aR PRETRUSIINS
2. MULD FLASH GR PRDTRUSIUNS NDT TI EXCEED .006"
3. CDNTRDLLING DIMENSIDNS: INCHES


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