## Quad-Channel, 12-Bit, Serial Input, 4 mA to 20 mA and Voltage Output DAC with Dynamic Power Control

## Data Sheet

## FEATURES

12-bit resolution and monotonicity
Dynamic power control for thermal management
Current and voltage output pins connectable to a single terminal
Current output ranges: 0 mA to $\mathbf{2 0 m A} \mathbf{4} \mathbf{~ m A}$ to $\mathbf{2 0 m A}$, and 0 mA to 24 mA
$\pm 0.1 \%$ total unadjusted error (TUE) maximum
Voltage output ranges (with $20 \%$ overrange): 0 V to 5 V , 0 V to $10 \mathrm{~V}, \pm 5 \mathrm{~V}$, and $\pm 10 \mathrm{~V}$
$\pm 0.09 \%$ total unadjusted error (TUE) maximum
User-programmable offset and gain
On-chip diagnostics
On-chip reference: $\pm 10 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ maximum
$-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ temperature range

## APPLICATIONS

Process control
Actuator control
PLCs

## GENERAL DESCRIPTION

The AD5735 is a quad-channel voltage and current output DAC that operates with a power supply range from -26.4 V to +33 V .

On-chip dynamic power control minimizes package power dissipation in current mode. This reduced power dissipation is achieved by regulating the voltage on the output driver from 7.4 V to 29.5 V using a dc-to-dc boost converter optimized for minimum on-chip power dissipation.

The AD5735 uses a versatile 3-wire serial interface that operates at clock rates of up to 30 MHz and is compatible with standard SPI, QSPI ${ }^{m}$, MICROWIRE ${ }^{*}$, DSP, and microcontroller interface standards. The serial interface also features optional CRC-8 packet error checking, as well as a watchdog timer that monitors activity on the interface.

## PRODUCT HIGHLIGHTS

1. Dynamic power control for thermal management.
2. 12-bit performance.
3. Quad channel.

## COMPANION PRODUCTS

Product Family: AD5755, AD5755-1, AD5757, AD5737
External References: ADR445, ADR02
Digital Isolators: ADuM1410, ADuM1411
Power: ADP2302, ADP2303
Additional companion products on the AD5735 product page

FUNCTIONAL BLOCK DIAGRAM


Figure 1.
Rev. A
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## Data Sheet

## DETAILED FUNCTIONAL BLOCK DIAGRAM



Figure 2.

## SPECIFICATIONS

$\mathrm{AV}_{\mathrm{DD}}=\mathrm{V}_{\text {Boost }}=15 \mathrm{~V} ; \mathrm{AV}_{\mathrm{SS}}=-15 \mathrm{~V} ; \mathrm{DV}_{\mathrm{DD}}=2.7 \mathrm{~V}$ to $5.5 \mathrm{~V} ; \mathrm{AV}_{\mathrm{CC}}=4.5 \mathrm{~V}$ to 5.5 V ; dc-to-dc converter disabled; AGND = DGND = GNDSW $_{x}=0 \mathrm{~V}$; REFIN $=5 \mathrm{~V}$; voltage outputs: $\mathrm{R}_{\mathrm{L}}=1 \mathrm{k} \Omega, \mathrm{C}_{\mathrm{L}}=220 \mathrm{pF}$; current outputs: $\mathrm{R}_{\mathrm{L}}=300 \Omega$; all specifications $\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\mathrm{MAX}}$, unless otherwise noted.

Table 1.

| Parameter ${ }^{1}$ | Min | Typ | Max | Unit | Test Conditions/Comments |
| :---: | :---: | :---: | :---: | :---: | :---: |
| VOLTAGE OUTPUT <br> Output Voltage Ranges <br> Resolution | $\begin{aligned} & 0 \\ & 0 \\ & -5 \\ & -10 \\ & 0 \\ & 0 \\ & -6 \\ & -12 \\ & 12 \end{aligned}$ |  | $\begin{aligned} & 5 \\ & 10 \\ & +5 \\ & +10 \\ & 6 \\ & 12 \\ & +6 \\ & +12 \end{aligned}$ | V <br> V <br> V <br> V <br> V <br> V <br> V <br> V <br> Bits |  |
| ACCURACY, VOLTAGE OUTPUT <br> Total Unadjusted Error (TUE) <br> TUE Long-Term Stability <br> Relative Accuracy (INL) <br> Differential Nonlinearity (DNL) <br> Zero-Scale Error <br> Zero-Scale TC ${ }^{2}$ <br> Bipolar Zero Error <br> Bipolar Zero TC² <br> Offset Error <br> Offset TC ${ }^{2}$ <br> Gain Error <br> Gain TC ${ }^{2}$ <br> Full-Scale Error <br> Full-Scale TC ${ }^{2}$ | -0.09 -0.13 -0.032 -1 -0.05 -0.08 -0.05 -0.08 -0.065 -0.09 -0.08 -0.15 -0.09 -0.13 | $\begin{aligned} & \pm 0.012 \\ & \pm 0.05 \\ & 35 \\ & \pm 0.006 \\ & \pm 0.004 \\ & \pm 0.004 \\ & \pm 2 \\ & \pm 0.003 \\ & \pm 0.03 \\ & \pm 2 \\ & \pm 0.005 \\ & \pm 0.03 \\ & \pm 2 \\ & \pm 0.004 \\ & \pm 0.004 \\ & \pm 3 \\ & \pm 0.01 \\ & \pm 0.05 \\ & \pm 2 \end{aligned}$ | $\begin{aligned} & +0.09 \\ & +0.13 \\ & +0.032 \\ & +1 \\ & +0.05 \\ & +0.08 \\ & +0.05 \\ & +0.08 \\ & +0.065 \\ & +0.09 \\ & \\ & +0.08 \\ & +0.15 \\ & +0.09 \\ & +0.13 \end{aligned}$ | \% FSR <br> \% FSR <br> ppm FSR <br> \% FSR <br> LSB <br> \% FSR <br> \% FSR <br> ppm FSR/ $/{ }^{\circ} \mathrm{C}$ <br> \% FSR <br> \% FSR <br> ppm FSR/ $/{ }^{\circ} \mathrm{C}$ <br> \% FSR <br> \% FSR <br> ppm FSR/ $/{ }^{\circ} \mathrm{C}$ <br> \% FSR <br> \% FSR <br> ppm FSR $/{ }^{\circ} \mathrm{C}$ <br> \% FSR <br> \% FSR <br> ppm FSR $/{ }^{\circ} \mathrm{C}$ | 0 V to $5 \mathrm{~V}, 0 \mathrm{~V}$ to $10 \mathrm{~V}, \pm 5 \mathrm{~V}, \pm 10 \mathrm{~V}$ ranges <br> On overranges ( 0 V to $6 \mathrm{~V}, 0 \mathrm{~V}$ to $12 \mathrm{~V}, \pm 6 \mathrm{~V}, \pm 12 \mathrm{~V}$ ) <br> Drift after 1000 hours, $\mathrm{T}_{\jmath}=150^{\circ} \mathrm{C}$ <br> Guaranteed monotonic <br> 0 V to $5 \mathrm{~V}, 0 \mathrm{~V}$ to 10 V ranges <br> On overranges ( 0 V to $6 \mathrm{~V}, 0 \mathrm{~V}$ to 12 V ) <br> $\pm 5 \mathrm{~V}, \pm 10 \mathrm{~V}$ ranges <br> On overranges ( $\pm 6 \mathrm{~V}, \pm 12 \mathrm{~V}$ ) <br> 0 V to $5 \mathrm{~V}, 0 \mathrm{~V}$ to $10 \mathrm{~V}, \pm 5 \mathrm{~V}, \pm 10 \mathrm{~V}$ ranges <br> On overranges ( 0 V to $6 \mathrm{~V}, 0 \mathrm{~V}$ to $12 \mathrm{~V}, \pm 6 \mathrm{~V}, \pm 12 \mathrm{~V}$ ) <br> 0 V to $5 \mathrm{~V}, 0 \mathrm{~V}$ to $10 \mathrm{~V}, \pm 5 \mathrm{~V}, \pm 10 \mathrm{~V}$ ranges <br> On overranges ( 0 V to $6 \mathrm{~V}, 0 \mathrm{~V}$ to $12 \mathrm{~V}, \pm 6 \mathrm{~V}, \pm 12 \mathrm{~V}$ ) <br> 0 V to $5 \mathrm{~V}, 0 \mathrm{~V}$ to $10 \mathrm{~V}, \pm 5 \mathrm{~V}, \pm 10 \mathrm{~V}$ ranges <br> On overranges ( 0 V to $6 \mathrm{~V}, 0 \mathrm{~V}$ to $12 \mathrm{~V}, \pm 6 \mathrm{~V}, \pm 12 \mathrm{~V}$ ) |
| OUTPUT CHARACTERISTICS, <br> VOLTAGE OUTPUT² <br> Headroom <br> Footroom <br> Output Voltage Drift vs. Time <br> Short-Circuit Current <br> Resistive Load <br> Capacitive Load Stability <br> DC Output Impedance <br> DC PSRR <br> DC Crosstalk | $12 / 6$ <br> 1 | $\begin{aligned} & 1 \\ & 1 \\ & 20 \\ & 16 / 8 \\ & \\ & \\ & 0.06 \\ & 50 \\ & 24 \end{aligned}$ | $\begin{aligned} & 2.2 \\ & 1.4 \\ & \\ & \\ & 10 \\ & 2 \end{aligned}$ | V <br> V <br> ppm FSR <br> mA <br> $\mathrm{k} \Omega$ <br> nF <br> $\mu \mathrm{F}$ <br> $\Omega$ <br> $\mu \mathrm{V} / \mathrm{V}$ <br> $\mu \mathrm{V}$ | With respect to $\mathrm{V}_{\text {Boost }}$ supply <br> With respect to the $A V_{\text {ss }}$ supply <br> Drift after 1000 hours, $3 / 4$ scale output, $\mathrm{T}_{j}=150^{\circ} \mathrm{C}$, $A V_{s s}=-15 \mathrm{~V}$ <br> Programmable by user; defaults to 16 mA typical For specified performance <br> External 220 pF compensation capacitor connected |
| CURRENT OUTPUT Output Current Ranges <br> Resolution | $\begin{aligned} & 0 \\ & 0 \\ & 4 \\ & 12 \end{aligned}$ |  | $\begin{aligned} & 24 \\ & 20 \\ & 20 \end{aligned}$ | mA <br> mA <br> mA <br> Bits |  |


| Parameter ${ }^{1}$ | Min | Typ | Max | Unit | Test Conditions/Comments |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ACCURACY, CURRENT OUTPUT (EXTERNAL Rset) |  |  |  |  | Assumes ideal resistor, see External Current Setting Resistor section for more information. |
| Total Unadjusted Error (TUE) | -0.1 | $\pm 0.019$ | +0.1 | \% FSR |  |
| TUE Long-Term Stability |  | 100 |  | ppm FSR | Drift after 1000 hours, $\mathrm{T}_{J}=150^{\circ} \mathrm{C}$ |
| Relative Accuracy (INL) | -0.032 | $\pm 0.006$ | +0.032 | \% FSR |  |
| Differential Nonlinearity (DNL) | -1 |  | +1 | LSB | Guaranteed monotonic |
| Offset Error | -0.1 | $\pm 0.012$ | +0.1 | \% FSR |  |
| Offset Error Drift ${ }^{2}$ |  | $\pm 4$ |  | ppm FSR $/{ }^{\circ} \mathrm{C}$ |  |
| Gain Error | -0.1 | $\pm 0.004$ | +0.1 | \%FSR |  |
| Gain TC ${ }^{2}$ |  | $\pm 3$ |  | ppm FSR $/{ }^{\circ} \mathrm{C}$ |  |
| Full-Scale Error | -0.1 | $\pm 0.014$ | +0.1 | \% FSR |  |
| Full-Scale TC ${ }^{2}$ |  | $\pm 5$ |  | ppm FSR/ ${ }^{\circ} \mathrm{C}$ |  |
| DC Crosstalk |  | 0.0005 |  | \% FSR | External $\mathrm{R}_{\text {SET }}$ |
| ACCURACY, CURRENT OUTPUT (INTERNAL Rset) |  |  |  |  |  |
| Total Unadjusted Error (TUE) ${ }^{\text {3,4 }}$ | -0.14 | $\pm 0.022$ | $+0.14$ | \% FSR |  |
| TUE Long-Term Stability |  | 180 |  | ppm FSR | Drift after 1000 hours, $\mathrm{T}_{\mathrm{J}}=150^{\circ} \mathrm{C}$ |
| Relative Accuracy (INL) | -0.032 | $\pm 0.006$ | +0.032 | \% FSR |  |
| Differential Nonlinearity (DNL) | -1 |  | +1 | LSB | Guaranteed monotonic |
| Offset Error ${ }^{3,4}$ | -0.1 | $\pm 0.017$ | +0.1 | \% FSR |  |
| Offset Error Drift ${ }^{2}$ |  | $\pm 6$ |  | ppm FSR/ ${ }^{\circ} \mathrm{C}$ |  |
| Gain Error | -0.12 | $\pm 0.004$ | +0.12 | $\% \text { FSR }$ |  |
| Gain TC² |  | $\pm 9$ |  | ppm FSR $/{ }^{\circ} \mathrm{C}$ |  |
| Full-Scale Error ${ }^{3,4}$ | -0.14 | $\pm 0.02$ | +0.14 | \% FSR |  |
| Full-Scale TC ${ }^{2}$ |  | $\pm 14$ |  | ppm FSR/ ${ }^{\circ} \mathrm{C}$ |  |
| DC Crosstalk ${ }^{4}$ |  | -0.011 |  | \% FSR | Internal $\mathrm{R}_{\text {SET }}$ |
| OUTPUT CHARACTERISTICS, CURRENT OUTPUT² |  |  |  |  |  |
| Current Loop Compliance Voltage |  | $\begin{aligned} & \text { V BOOST_x } \\ & 2.4 \end{aligned}$ | $\begin{aligned} & \text { V }_{\text {BOOST_x }}- \\ & 2.7 \end{aligned}$ | V |  |
| Output Current Drift vs. Time |  |  |  |  | Drift after 1000 hours, $3 / 4$ scale output, T , $=150^{\circ} \mathrm{C}$ |
|  |  | 90 |  | ppm FSR | External $\mathrm{R}_{\text {SET }}$ |
|  |  | 140 |  | ppm FSR | Internal R ${ }_{\text {SEt }}$ |
| Resistive Load |  |  | 1000 | $\Omega$ | The dc-to-dc converter has been characterized with a maximum load of $1 \mathrm{k} \Omega$, chosen such that compliance is not exceeded; see Figure 51 and the DC-DC MaxV bits in Table 28 |
| DC Output Impedance |  | 100 |  | $\mathrm{M} \Omega$ |  |
| DC PSRR |  | 0.02 | 1 | $\mu \mathrm{A} / \mathrm{V}$ |  |
| REFERENCE INPUT/OUTPUT |  |  |  |  |  |
| Reference Input ${ }^{2}$ |  |  |  |  |  |
| Reference Input Voltage | $4.95$ |  | 5.05 |  | For specified performance |
| DC Input Impedance | 45 | $150$ |  | $\mathrm{M} \Omega$ |  |
| Reference Output |  |  |  |  |  |
| Output Voltage | 4.995 | 5 | 5.005 | V | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |
| Reference TC² | -10 | $\pm 5$ | +10 | ppm $/{ }^{\circ} \mathrm{C}$ |  |
| Output Noise $(0.1 \mathrm{~Hz} \text { to } 10 \mathrm{~Hz})^{2}$ |  | 7 |  | $\mu \mathrm{V} \text { p-p }$ |  |
| Noise Spectral Density ${ }^{2}$ |  | 100 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ | At 10 kHz |
| Output Voltage Drift vs. Time ${ }^{2}$ |  | 180 |  | ppm | Drift after 1000 hours, $\mathrm{T}_{J}=150^{\circ} \mathrm{C}$ |
| Capacitive Load ${ }^{2}$ |  | 1000 |  | nF |  |
| Load Current |  | 9 |  | mA | See Figure 62 |
| Short-Circuit Current |  | 10 |  | mA |  |
| Line Regulation ${ }^{2}$ |  | 3 |  | $\mathrm{ppm} / \mathrm{V}$ | See Figure 63 |
| Load Regulation ${ }^{2}$ |  | 95 |  | $\mathrm{ppm} / \mathrm{mA}$ | See Figure 62 |
| Thermal Hysteresis ${ }^{2}$ |  | 160 |  | ppm | First temperature cycle |
|  |  | 5 |  | ppm | Second temperature cycle |


| Parameter ${ }^{1}$ | Min | Typ | Max | Unit | Test Conditions/Comments |
| :---: | :---: | :---: | :---: | :---: | :---: |
| DC-TO-DC CONVERTER |  |  |  |  |  |
| Switch |  |  |  |  |  |
| Switch On Resistance |  | 0.425 |  | $\Omega$ |  |
| Switch Leakage Current |  | 10 |  | nA |  |
| Peak Current Limit |  | 0.8 |  | A |  |
| Oscillator |  |  |  |  |  |
| Oscillator Frequency | 11.5 | 13 | 14.5 | MHz | This oscillator is divided down to provide the dc-to-dc converter switching frequency |
| Maximum Duty Cycle |  | 89.6 |  | \% | At 410 kHz dc-to-dc switching frequency |
| DIGITAL INPUTS² |  |  |  |  | JEDEC compliant |
| Input High Voltage, $\mathrm{V}_{\mathrm{IH}}$ | 2 |  |  | V |  |
| Input Low Voltage, $\mathrm{V}_{\text {IL }}$ |  |  | 0.8 | V |  |
| Input Current | -1 |  | +1 | $\mu \mathrm{A}$ | Per pin |
| Pin Capacitance |  | 2.6 |  | pF | Per pin |
| DIGITAL OUTPUTS ${ }^{2}$ |  |  |  |  |  |
| SDO, ALERT Pins |  |  |  |  |  |
| Output Low Voltage, $\mathrm{V}_{\text {oL }}$ |  |  | 0.4 | V | Sinking $200 \mu \mathrm{~A}$ |
| Output High Voltage, $\mathrm{V}_{\text {он }}$ | $D V_{D D}-0.5$ |  |  | V | Sourcing $200 \mu \mathrm{~A}$ |
| High Impedance Leakage Current | -1 |  | +1 | $\mu \mathrm{A}$ |  |
| High Impedance Output Capacitance |  | 2.5 |  | pF |  |
| $\overline{\text { FAULT Pin }}$ |  |  |  |  |  |
| Output Low Voltage, $\mathrm{V}_{\text {oL }}$ |  |  | 0.4 | V | $10 \mathrm{k} \Omega$ pull-up resistor to $\mathrm{DV}_{\mathrm{DD}}$ |
|  |  | 0.6 |  | V | At 2.5 mA |
| Output High Voltage, $\mathrm{V}_{\mathrm{OH}}$ | 3.6 |  |  | V | $10 \mathrm{k} \Omega$ pull-up resistor to $\mathrm{DV}_{\mathrm{DD}}$ |
| POWER REQUIREMENTS |  |  |  |  |  |
| AV ${ }_{\text {do }}$ | 9 |  | 33 | V |  |
| $A V_{S S}$ | -26.4 |  | -10.8 | V |  |
| DV ${ }_{\text {D }}$ | 2.7 |  | 5.5 | V |  |
| $A V_{c c}$ | 4.5 |  | 5.5 | V |  |
| Aldd |  | 8.6 | 10.5 | mA | Voltage output mode on all channels, outputs unloaded, over supplies |
|  |  | 7 | 7.5 | mA | Current output mode on all channels |
| $\mathrm{Alss}^{\text {s }}$ | -11 | -8.8 |  | mA | Voltage output mode on all channels, outputs unloaded, over supplies |
|  | -1.7 |  |  | mA | Current output mode on all channels |
| Dlcc |  | 9.2 | 11 | mA | $\mathrm{V}_{\mathrm{IH}}=\mathrm{DV} \mathrm{VD}_{\mathrm{DD}} \mathrm{V}_{\mathrm{IL}}=\mathrm{DGND}$, internal oscillator running, over supplies |
| Alcc |  |  | 1 | mA | Outputs unloaded, over supplies |
| $\mathrm{Iboost}^{5}$ |  |  | 2.7 | mA | Per channel, voltage output mode, outputs unloaded, over supplies |
|  |  |  | 1 | mA | Per channel, current output mode |
| Power Dissipation |  | 173 |  | mW | $A V_{D D}=15 \mathrm{~V}, A V_{s s}=-15 \mathrm{~V}$, dc-to-dc converter enabled, current output mode, outputs disabled |

[^0]
## Data Sheet

## AC PERFORMANCE CHARACTERISTICS

$\mathrm{AV}_{\mathrm{DD}}=\mathrm{V}_{\text {Boost }}=15 \mathrm{~V}$; $\mathrm{AV}_{\mathrm{SS}}=-15 \mathrm{~V} ; \mathrm{DV}_{\mathrm{DD}}=2.7 \mathrm{~V}$ to $5.5 \mathrm{~V} ; \mathrm{AV}_{\mathrm{CC}}=4.5 \mathrm{~V}$ to 5.5 V ; dc-to-dc converter disabled; AGND $=\mathrm{DGND}=$ GNDSW $=0$ V; REFIN $=5 \mathrm{~V}$; voltage outputs: $\mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega, \mathrm{C}_{\mathrm{L}}=220 \mathrm{pF}$; current outputs: $\mathrm{R}_{\mathrm{L}}=300 \Omega$; all specifications $\mathrm{T}_{\mathrm{MIN}}$ to $\mathrm{T}_{\mathrm{MAX}}$, unless otherwise noted.

Table 2.


[^1]
## TIMING CHARACTERISTICS

$\mathrm{AV}_{\mathrm{DD}}=\mathrm{V}_{\text {Boost }}=15 \mathrm{~V} ; \mathrm{AV}_{\text {SS }}=-15 \mathrm{~V} ; \mathrm{DV}_{\mathrm{DD}}=2.7 \mathrm{~V}$ to $5.5 \mathrm{~V} ; \mathrm{AV}_{\mathrm{CC}}=4.5 \mathrm{~V}$ to 5.5 V ; dc-to-dc converter disabled; AGND = DGND = GNDSW $_{x}=0 \mathrm{~V}$; REFIN $=5 \mathrm{~V}$; voltage outputs: $\mathrm{R}_{\mathrm{L}}=1 \mathrm{k} \Omega, \mathrm{C}_{\mathrm{L}}=220 \mathrm{pF}$; current outputs: $\mathrm{R}_{\mathrm{L}}=300 \Omega$; all specifications $\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\mathrm{MAX}}$, unless otherwise noted.

Table 3.

| Parameter ${ }^{1,2,3}$ | Limit at Tmin, $\mathbf{T}_{\text {max }}$ | Unit | Description |
| :---: | :---: | :---: | :---: |
| $\mathrm{t}_{1}$ | 33 | ns min | SCLK cycle time |
| $\mathrm{t}_{2}$ | 13 | ns min | SCLK high time |
| $\mathrm{t}_{3}$ | 13 | ns min | SCLK low time |
| $\mathrm{t}_{4}$ | 13 | $n \mathrm{n}$ min | $\overline{\text { SYNC }}$ falling edge to SCLK falling edge setup time |
| $\mathrm{t}_{5}$ | 13 | ns min | 24th/32nd SCLK falling edge to $\overline{\text { SYNC }}$ rising edge (see Figure 76) |
| $\mathrm{t}_{6}$ | 198 | ns min | $\overline{\text { SYNC }}$ high time |
| $\mathrm{t}_{7}$ | 5 | $n \mathrm{~ns}$ min | Data setup time |
| $\mathrm{t}_{8}$ | 5 | ns min | Data hold time |
| $\mathrm{t}_{9}$ | 20 | $\mu \mathrm{s}$ min | $\overline{\text { SYNC }}$ rising edge to $\overline{\text { LDAC }}$ falling edge (all DACs updated or any channel has digital slew rate control enabled) |
|  | 5 | $\mu \mathrm{s}$ min | $\overline{\text { SYNC }}$ rising edge to $\overline{\mathrm{LDAC}}$ falling edge (single DAC updated) |
| $\mathrm{t}_{10}$ | 10 | $n \mathrm{~ns}$ min | $\overline{\text { LDAC }}$ pulse width low |
| $\mathrm{t}_{11}$ | 500 | ns max | $\overline{\text { LDAC }}$ falling edge to DAC output response time |
| $\mathrm{t}_{12}$ | See Table 2 | $\mu \mathrm{s}$ max | DAC output settling time |
| $\mathrm{t}_{13}$ | 10 | ns min | CLEAR high time |
| $\mathrm{t}_{14}$ | 5 | $\mu \mathrm{s}$ max | CLEAR activation time |
| $\mathrm{t}_{15}$ | 40 | ns max | SCLK rising edge to SDO valid |
| $\mathrm{t}_{16}$ |  |  | $\overline{\text { SYNC }}$ rising edge to DAC output response time ( $\overline{\mathrm{LDAC}}=0$ ) |
|  | 21 | $\mu \mathrm{s}$ min | All DACs updated |
|  | 5 | $\mu s$ min | Single DAC updated |
| $\mathrm{t}_{17}$ | 500 | $n \mathrm{n}$ min | $\overline{\text { LDAC }}$ falling edge to $\overline{\text { SYNC }}$ rising edge |
| $\mathrm{t}_{18}$ | 800 | ns min | $\overline{\mathrm{RESET}}$ pulse width |
| $\mathrm{t}_{19}{ }^{4}$ |  |  | $\overline{\text { SYNC }}$ high to next $\overline{\text { SYNC }}$ low (digital slew rate control enabled) |
|  | 20 | $\mu \mathrm{s}$ min | All DACs updated |
|  | 5 | $\mu \mathrm{s}$ min | Single DAC updated |

${ }^{1}$ Guaranteed by design and characterization; not production tested.
${ }^{2}$ All input signals are specified with $\mathrm{t}_{\text {RISE }}=\mathrm{t}_{\text {FALL }}=5 \mathrm{~ns}\left(10 \%\right.$ to $90 \%$ of $\left.D V_{D D}\right)$ and timed from a voltage level of 1.2 V .
${ }^{3}$ See Figure 3, Figure 4, Figure 5, and Figure 6.
${ }^{4}$ This specification applies if $\overline{\overline{L D A C}}$ is held low during the write cycle; otherwise, see $\mathrm{t}_{9}$.

## Data Sheet

Timing Diagrams


Figure 3. Serial Interface Timing Diagram


## AD5735



Figure 5. Status Readback During Write, Timing Diagram


Figure 6. Load Circuit for SDO Timing Diagrams

## ABSOLUTE MAXIMUM RATINGS

$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted. Transient currents of up to 100 mA do not cause SCR latch-up.

Table 4.

| Parameter | Rating |
| :---: | :---: |
| $\mathrm{AV}_{\text {DD }}, \mathrm{V}_{\text {Boost_x }}$ to AGND, DGND | -0.3 V to +33V |
| $A V_{\text {ss }}$ to AGND, DGND | +0.3 V to -28 V |
| $A V_{\text {DD }}$ to $A V_{S S}$ | -0.3 V to +60 V |
| AV $\mathrm{Cc}^{\text {to }}$ AGND | -0.3 V to +7 V |
| DVDD to DGND | -0.3 V to +7 V |
| Digital Inputs to DGND | $\begin{aligned} & -0.3 \mathrm{~V} \text { to } \mathrm{DV} \mathrm{DD}+0.3 \mathrm{~V} \text { or }+7 \mathrm{~V} \\ & \text { (whichever is less) } \end{aligned}$ |
| Digital Outputs to DGND | $\begin{aligned} & -0.3 \mathrm{~V} \text { to } \mathrm{DV} \text { DD }+0.3 \mathrm{~V} \text { or }+7 \mathrm{~V} \\ & \text { (whichever is less) } \end{aligned}$ |
| REFIN, REFOUT to AGND | $\begin{aligned} & -0.3 \mathrm{~V} \text { to } \mathrm{AV} \mathrm{VD}+0.3 \mathrm{~V} \text { or }+7 \mathrm{~V} \\ & \text { (whichever is less) } \end{aligned}$ |
| Voutex to AGND | $\mathrm{AV}_{\text {ss }}$ to $\mathrm{V}_{\text {Boost_x }}$ or 33 V if using the dc-to-dc converter |
| $+\mathrm{V}_{\text {SENSE-X }}$ - $\mathrm{V}_{\text {SENSE-x }}$ to AGND | $\mathrm{AV}_{\text {ss }}$ to $\mathrm{V}_{\text {Boost_x }}$ or 33 V if using the dc-to-dc converter |
| lout_x to AGND | $\mathrm{AV}_{\text {ss }}$ to $\mathrm{V}_{\text {Boost_x }}$ or 33 V if using the dc-to-dc converter |
| SWx to AGND | -0.3 V to +33 V |
| AGND, GNDSW ${ }_{\text {x }}$ to DGND | -0.3 V to +0.3 V |
| Operating Temperature Range $\left(T_{A}\right)$ Industrial ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ |
| Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Junction Temperature (T, max) | $125^{\circ} \mathrm{C}$ |
| Power Dissipation | ( $\mathrm{T}, ~_{\text {max }}-\mathrm{T}_{\mathrm{A}}$ ) $/ \theta_{\text {J }}$ |
| Lead Temperature | JEDEC industry standard |
| Soldering | J-STD-020 |

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## THERMAL RESISTANCE

Junction-to-air thermal resistance $\left(\theta_{J A}\right)$ is specified for a JEDEC 4-layer test board.

Table 5. Thermal Resistance

| Package Type | $\boldsymbol{\theta}_{\mathrm{JA}}$ | Unit |
| :--- | :--- | :--- |
| 64-Lead LFCSP (CP-64-3) | 20 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

## ESD CAUTION

|  | ESD (electrostatic discharge) sensitive device. <br> Charged devices and circuit boards can discharge <br> without detection. Although this product features <br> patented or proprietary protection circuitry, damage <br> may occur on devices subjected to high energy ESD. <br> Therefore, proper ESD precautions should be taken to <br> avoid performance degradation or loss of functionality. |
| :--- | :--- |

## PIN CONFIGURATION AND FUNCTION DESCRIPTIONS



## NOTES

1.THE EXPOSED PADDLE SHOULD BE CONNECTED TO THE POTENTIAL OF THE AV ${ }_{\text {SS }}$ PIN, OR, ALTERNATIVELY, IT CAN BE LEFT ELECTRICALLY UNCONNECTED. IT IS RECOMMENDED THAT THE PADDLE BE THERMALLY CONNECTED TO A COPPER PLANE FOR ENHANCED THERMAL PERFORMANCE.

Figure 7. Pin Configuration

Table 6. Pin Function Descriptions

| Pin No. | Mnemonic | Description |
| :---: | :---: | :---: |
| 1 | RSEt_B | An external, precision, low drift, $15 \mathrm{k} \Omega$ current setting resistor can be connected to this pin to improve the lout_B temperature drift performance. For more information, see the External Current Setting Resistor section. |
| 2 | RsEt_A | An external, precision, low drift, $15 \mathrm{k} \Omega$ current setting resistor can be connected to this pin to improve the lout_A temperature drift performance. For more information, see the External Current Setting Resistor section. |
| 3 | REFGND | Ground Reference Point for Internal Reference. |
| 4 | REFGND | Ground Reference Point for Internal Reference. |
| 5 | ADO | Address Decode for the Device Under Test (DUT) on the Board. |
| 6 | AD1 | Address Decode for the DUT on the Board. |
| 7 | $\overline{\text { SYNC }}$ | Frame Synchronization Signal for the Serial Interface. Active low input. When $\overline{\text { SYNC }}$ is low, data is clocked into the input shift register on the falling edge of SCLK. |
| 8 | SCLK | Serial Clock Input. Data is clocked into the input shift register on the falling edge of SCLK. The serial interface operates at clock speeds of up to 30 MHz . |
| 9 | SDIN | Serial Data Input. Data must be valid on the falling edge of SCLK. |
| 10 | SDO | Serial Data Output. Used to clock data from the serial register in readback mode (see Figure 4 and Figure 5). |
| 11 | DV ${ }_{\text {D }}$ | Digital Supply Pin. The voltage range is from 2.7 V to 5.5 V . |
| 12 | DGND | Digital Ground. |
| 13 | $\overline{\text { LDAC }}$ | Load DAC. This active low input is used to update the DAC register and, consequently, the DAC outputs. When $\overline{\text { LDAC }}$ is tied permanently low, the addressed DAC data register is updated on the rising edge of $\overline{\text { SYNC. If } \overline{L D A C}}$ is held high during the write cycle, the DAC input register is updated, but the DAC output is updated only on the falling edge of $\overline{\overline{L D A C}}$ (see Figure 3). Using this mode, all analog outputs can be updated simultaneously. The $\overline{\text { LDAC }}$ pin must not be left unconnected. |
| 14 | CLEAR | Active High, Edge Sensitive Input. When this pin is asserted, the output current and voltage are set to the programmed clear code bit setting. Only channels enabled to be cleared are cleared. For more information, see the Asynchronous Clear section. When CLEAR is active, the DAC output register cannot be written to. |


| Pin No. | Mnemonic | Description |
| :---: | :---: | :---: |
| 15 | ALERT | Active High Output. This pin is asserted when there is no SPI activity on the interface pins for a preset time. For more information, see the Alert Output section. |
| 16 | $\overline{\text { FAULT }}$ | Active Low, Open-Drain Output. This pin is asserted low when any of the following conditions is detected: open circuit in current mode; short circuit in voltage mode; PEC error; or an overtemperature condition (see the Fault Output section). |
| 17 | POC | Power-On Condition. This pin determines the power-on condition and is read during power-on and after a device reset. If $P O C=0$, the device is powered up with the voltage and current channels in tristate mode. If $P O C=1$, the device is powered up with a $30 \mathrm{k} \Omega$ pull-down resistor to ground on the voltage output channel, and the current channel is in tristate mode. |
| 18 | $\overline{\text { RESET }}$ | Hardware Reset, Active Low Input. |
| 19 | AV ${ }_{\text {D }}$ | Positive Analog Supply Pin. The voltage range is from 9 V to 33 V . |
| 20 | COMPLV_A | Optional Compensation Capacitor Connection for Vout_A Output Buffer. Connecting a 220 pF capacitor between this pin and the Vout_A pin allows the voltage output to drive up to $2 \mu \mathrm{~F}$. Note that the addition of this capacitor reduces the bandwidth of the output amplifier, increasing the settling time. |
| 21 | - $\mathrm{V}_{\text {SENSE_A }}$ | Sense Connection for the Negative Voltage Output Load Connection for Vout_A. This pin must stay within $\pm 3.0 \mathrm{~V}$ of AGND for specified operation. |
| 22 | $+\mathrm{V}_{\text {SENSEA }}$ | Sense Connection for the Positive Voltage Output Load Connection for Vout_A. The difference in voltage between this pin and the Vout_A pin is added directly to the headroom requirement. |
| 23 | COMPdCDC_A | DC-to-DC Compensation Capacitor. Connect a 10 nF capacitor from this pin to ground. Used to regulate the feedback loop of the Channel A dc-to-dc converter. Alternatively, if using an external compensation resistor, place a resistor in series with a capacitor to ground from this pin. For more information, see the DC-to-DC Converter Compensation Capacitors section and the Alcc Supply Requirements-Slewing section. |
| 24 | VBoost_A | Supply for Channel A Current Output Stage (see Figure 71). This pin is also the supply for the Vout_A stage, which is regulated to 15 V by the dc-to-dc converter. To use the dc-to-dc converter, connect this pin as shown in Figure 77. |
| 25 | Vout_A | Buffered Analog Output Voltage for DAC Channel A. |
| 26 | lout_A | Current Output Pin for DAC Channel A. |
| 27 | AVss | Negative Analog Supply Pin. The voltage range is from -10.8 V to -26.4 V . |
| 28 | COMPLl_b | Optional Compensation Capacitor Connection for Vout_B Output Buffer. Connecting a 220 pF capacitor between this pin and the Vout_B pin allows the voltage output to drive up to $2 \mu \mathrm{~F}$. Note that the addition of this capacitor reduces the bandwidth of the output amplifier, increasing the settling time. |
| 29 | - $\mathrm{V}_{\text {SENSE_B }}$ | Sense Connection for the Negative Voltage Output Load Connection for Vout_r. This pin must stay within $\pm 3.0 \mathrm{~V}$ of AGND for specified operation. |
| 30 | $+\mathrm{V}_{\text {SENSE_B }}$ | Sense Connection for the Positive Voltage Output Load Connection for Vout_b. The difference in voltage between this pin and the $V_{\text {out_в }}$ pin is added directly to the headroom requirement. |
| 31 | Vout_B | Buffered Analog Output Voltage for DAC Channel B. |
| 32 | COMP ${ }_{\text {dCDC }}$ B | DC-to-DC Compensation Capacitor. Connect a 10 nF capacitor from this pin to ground. Used to regulate the feedback loop of the Channel B dc-to-dc converter. Alternatively, if using an external compensation resistor, place a resistor in series with a capacitor to ground from this pin. For more information, see the DC-to-DC Converter Compensation Capacitors section and the Alcc Supply Requirements-Slewing section. |
| 33 | lout_B | Current Output Pin for DAC Channel B. |
| 34 | $V_{\text {Boost_b }}$ | Supply for Channel B Current Output Stage (see Figure 71). This pin is also the supply for the Vout_B stage, which is regulated to 15 V by the dc-to-dc converter. To use the dc-to-dc converter, connect this pin as shown in Figure 77. |
| 35 | AGND | Ground Reference Point for Analog Circuitry. This pin must be connected to 0 V . |
| 36 | SWB | Switching Output for Channel B DC-to-DC Circuitry. To use the dc-to-dc converter, connect this pin as shown in Figure 77. |
| 37 | GNDSW $^{\text {B }}$ | Ground Connection for DC-to-DC Switching Circuit. This pin should always be connected to ground. |
| 38 | $\mathrm{GNDSW}_{\text {A }}$ | Ground Connection for DC-to-DC Switching Circuit. This pin should always be connected to ground. |
| 39 | SWA | Switching Output for Channel A DC-to-DC Circuitry. To use the dc-to-dc converter, connect this pin as shown in Figure 77. |
| 40 | $\mathrm{AV}_{\text {Ss }}$ | Negative Analog Supply Pin. The voltage range is from -10.8 V to -26.4 V . |
| 41 | SWD | Switching Output for Channel D DC-to-DC Circuitry. To use the dc-to-dc converter, connect this pin as shown in Figure 77. |
| 42 | GNDSW ${ }_{\text {D }}$ | Ground Connection for DC-to-DC Switching Circuit. This pin should always be connected to ground. |
| 43 | GNDSWC | Ground Connection for DC-to-DC Switching Circuit. This pin should always be connected to ground. |
| 44 | SWc | Switching Output for Channel C DC-to-DC Circuitry. To use the dc-to-dc converter, connect this pin as shown in Figure 77. |


| Pin No. | Mnemonic | Description |
| :---: | :---: | :---: |
| 45 | AV ${ }_{\text {cc }}$ | Supply for DC-to-DC Circuitry. The voltage range is from 4.5 V to 5.5 V . |
| 46 | V ${ }_{\text {boost_C }}$ | Supply for Channel C Current Output Stage (see Figure 71). This pin is also the supply for the Vout_c stage, which is regulated to 15 V by the dc-to-dc converter. To use the dc-to-dc converter, connect this pin as shown in Figure 77. |
| 47 | lout_c | Current Output Pin for DAC Channel C. |
| 48 | COMP ${ }_{\text {dcid_c }}$ | DC-to-DC Compensation Capacitor. Connect a 10 nF capacitor from this pin to ground. Used to regulate the feedback loop of the Channel C dc-to-dc converter. Alternatively, if using an external compensation resistor, place a resistor in series with a capacitor to ground from this pin. For more information, see the DC-to-DC Converter Compensation Capacitors section and the Alcc Supply Requirements-Slewing section. |
| 49 | Vout_c | Buffered Analog Output Voltage for DAC Channel C. |
| 50 | + $\mathrm{V}_{\text {SENSE_C }}$ | Sense Connection for the Positive Voltage Output Load Connection for Vout_c. The difference in voltage between this pin and the $\mathrm{V}_{\text {out_c }}$ pin is added directly to the headroom requirement. |
| 51 | $-\mathrm{V}_{\text {SENSE_C }}$ | Sense Connection for the Negative Voltage Output Load Connection for Vout_c. This pin must stay within $\pm 3.0 \mathrm{~V}$ of AGND for specified operation. |
| 52 | COMPLl_c | Optional Compensation Capacitor Connection for Vout_c Output Buffer. Connecting a 220 pF capacitor between this pin and the Vout_c pin allows the voltage output to drive up to $2 \mu \mathrm{~F}$. Note that the addition of this capacitor reduces the bandwidth of the output amplifier, increasing the settling time. |
| 53 | $\mathrm{AV}_{\mathrm{ss}}$ | Negative Analog Supply Pin. The voltage range is from -10.8 V to -26.4 V . |
| 54 | lout_D | Current Output Pin for DAC Channel D. |
| 55 | Vout_D | Buffered Analog Output Voltage for DAC Channel D. |
| 56 | $V_{\text {boost_D }}$ | Supply for Channel D Current Output Stage (see Figure 71). This pin is also the supply for the Vout_d stage, which is regulated to 15 V by the dc-to-dc converter. To use the dc-to-dc converter, connect this pin as shown in Figure 77. |
| 57 | COMPdcde_d | DC-to-DC Compensation Capacitor. Connect a 10 nF capacitor from this pin to ground. Used to regulate the feedback loop of the Channel D dc-to-dc converter. Alternatively, if using an external compensation resistor, place a resistor in series with a capacitor to ground from this pin. For more information, see the DC-to-DC Converter Compensation Capacitors section and the Alcc Supply Requirements-Slewing section. |
| 58 | $+\mathrm{V}_{\text {SENSE_D }}$ | Sense Connection for the Positive Voltage Output Load Connection for Vout_d. The difference in voltage between this pin and the Vout_d pin is added directly to the headroom requirement. |
| 59 | - $\mathrm{V}_{\text {SENSE_D }}$ | Sense Connection for the Negative Voltage Output Load Connection for Vout_d. This pin must stay within $\pm 3.0 \mathrm{~V}$ of AGND for specified operation. |
| 60 | COMPLv_D | Optional Compensation Capacitor Connection for Vout_d Output Buffer. Connecting a 220 pF capacitor between this pin and the Vout_D pin allows the voltage output to drive up to $2 \mu \mathrm{~F}$. Note that the addition of this capacitor reduces the bandwidth of the output amplifier, increasing the settling time. |
| 61 | REFIN | External Reference Voltage Input. |
| 62 | REFOUT | Internal Reference Voltage Output. It is recommended that a $0.1 \mu \mathrm{~F}$ capacitor be placed between REFOUT and REFGND. |
| 63 | RsEt_D | An external, precision, low drift, $15 \mathrm{k} \Omega$ current setting resistor can be connected to this pin to improve the lout_d temperature drift performance. For more information, see the External Current Setting Resistor section. |
| 64 | RSEt_C | An external, precision, low drift, $15 \mathrm{k} \Omega$ current setting resistor can be connected to this pin to improve the lout_c temperature drift performance. For more information, see the External Current Setting Resistor section. |
|  | EPAD | Exposed Pad. The exposed paddle should be connected to the potential of the AV Ss pin, or, alternatively, it can be left electrically unconnected. It is recommended that the paddle be thermally connected to a copper plane for enhanced thermal performance. |

## TYPICAL PERFORMANCE CHARACTERISTICS

## VOLTAGE OUTPUTS



Figure 8. Integral Nonlinearity Error vs. DAC Code


Figure 9. Differential Nonlinearity Error vs. DAC Code


Figure 10. Total Unadjusted Error vs. DAC Code


Figure 11. Integral Nonlinearity Error vs. Temperature


Figure 12. Differential Nonlinearity Error vs. Temperature


Figure 13. Total Unadjusted Error vs. Temperature


Figure 14. Full-Scale Error vs. Temperature


Figure 15. Offset Error vs. Temperature


Figure 16. Bipolar Zero Error vs. Temperature


Figure 17. Gain Error vs. Temperature


Figure 18. Zero-Scale Error vs. Temperature


Figure 19. Integral Nonlinearity Error vs. Supply


Figure 20. Differential Nonlinearity Error vs. Supply


Figure 21. Total Unadjusted Error vs. Supply


Figure 22. Source and Sink Capability of the Output Amplifier


Figure 23. Full-Scale Positive Step


Figure 24. Full-Scale Negative Step


Figure 25. Digital-to-Analog Glitch


Figure 26. Peak-to-Peak Noise ( 0.1 Hz to 10 Hz Bandwidth)


Figure 27. Peak-to-Peak Noise (100 kHz Bandwidth)


Figure 28. Voltage vs. Time on Power-Up


Figure 29. Voltage vs. Time on Output Enable


Figure 30. Vout_x PSRR vs. Frequency

## CURRENT OUTPUTS



Figure 31. Integral Nonlinearity Error vs. DAC Code


Figure 32. Differential Nonlinearity Error vs. DAC Code


Figure 33. Total Unadjusted Error vs. DAC Code


Figure 34. Integral Nonlinearity Error vs. Temperature, Internal R SET


Figure 35. Integral Nonlinearity Error vs. Temperature, External RSET


Figure 36. Differential Nonlinearity Error vs. Temperature


Figure 37. Total Unadjusted Error vs. Temperature


Figure 38. Full-Scale Error vs. Temperature


Figure 39. Gain Error vs. Temperature


Figure 40. Integral Nonlinearity Error vs. Supply, External RSET


Figure 41. Integral Nonlinearity Error vs. Supply, Internal RSET


Figure 42. Differential Nonlinearity Error vs. Supply


Figure 43. Total Unadjusted Error vs. Supply, External RSET


Figure 44. Total Unadjusted Error vs. Supply, Internal RSET


Figure 45. Current vs. Time on Power-Up


Figure 46. Current vs. Time on Output Enable


Figure 47. Output Current and $V_{\text {Boost_x }}$ Settling Time with DC-to-DC Converter (See Figure 77)


Figure 48. Output Current Settling Time with DC-to-DC Converter over Temperature (See Figure 77)


Figure 49. Output Current Settling Time with DC-to-DC Converter over AVcc (See Figure 77)


Figure 50. Output Current, AC-Coupled vs. Time with DC-to-DC Converter (See Figure 77)


Figure 51. DC-to-DC Converter Headroom vs. Output Current (See Figure 77)


Figure 52. Iout_x PSRR vs. Frequency

## DC-TO-DC CONVERTER



Figure 53. Efficiency at $V_{B 005 T_{-} \text {vs. Output Current (See Figure 77) }}$


Figure 54. Efficiency at $V_{\text {Boost_x }}$ vs. Temperature (See Figure 77)

Figure 55. Output Efficiency vs. Output Current (See Figure 77)



Figure 56. Output Efficiency vs. Temperature (See Figure 77)


Figure 57. Switch Resistance vs. Temperature

## REFERENCE



Figure 58. REFOUT Voltage Turn-On Transient


Figure 59. REFOUT Output Noise ( 0.1 Hz to 10 Hz Bandwidth)


Figure 60. REFOUT Output Noise (100 kHz Bandwidth)


Figure 61. REFOUT Voltage vs. Temperature (When the AD5735 is soldered onto a PCB, the reference shifts due to thermal shock on the package. The average output voltage shift is -4 mV . Measurement of these parts after seven days shows that the outputs typically shift back 2 mV toward their initial values. This second shift is due to the relaxation of stress incurred during soldering.)


Figure 62. REFOUT Voltage vs. Load Current


Figure 63. REFOUT Voltage vs. $A V_{D D}$

## GENERAL



Figure 64. DIcc vs. Logic Input Voltage


Figure 65. Supply Current ( $\left.A I_{D D} / A I_{s S}\right)$ vs. Supply Voltage ( $\left.A V_{D D} /\left|A V_{S S}\right|\right)$


Figure 67. Internal Oscillator Frequency vs. Temperature


Figure 68. Internal Oscillator Frequency vs. DV $V_{D D}$ Supply Voltage

Figure 66. Supply Current (AloD) vs. Supply Voltage (AVDD)


## TERMINOLOGY

Relative Accuracy or Integral Nonlinearity (INL)
Relative accuracy, or integral nonlinearity (INL), is a measure of the maximum deviation from the best fit line through the DAC transfer function. INL is expressed in percent of full-scale range (\% FSR). Typical INL vs. code plots are shown in Figure 8 and Figure 31.

## Differential Nonlinearity (DNL)

Differential nonlinearity (DNL) is the difference between the measured change and the ideal 1 LSB change between any two adjacent codes. A specified DNL of $\pm 1$ LSB maximum ensures monotonicity. The AD5735 is guaranteed monotonic by design. Typical DNL vs. code plots are shown in Figure 9 and Figure 32.

## Monotonicity

A DAC is monotonic if the output either increases or remains constant for increasing digital input code. The AD5735 is monotonic over its full operating temperature range.

Negative Full-Scale Error or Zero-Scale Error
Negative full-scale error is the error in the DAC output voltage when 0x0000 (straight binary coding) is loaded to the DAC register.

## Zero-Scale Temperature Coefficient (TC)

Zero-scale TC is a measure of the change in zero-scale error with a change in temperature. Zero-scale TC is expressed in ppm FSR $/{ }^{\circ} \mathrm{C}$.

## Bipolar Zero Error

Bipolar zero error is the deviation of the analog output from the ideal half-scale output of 0 V when the DAC register is loaded with $0 \times 8000$ (straight binary coding).

## Bipolar Zero Temperature Coefficient (TC)

Bipolar zero TC is a measure of the change in the bipolar zero error with a change in temperature. It is expressed in ppm FSR $/{ }^{\circ} \mathrm{C}$.

## Offset Error

In voltage output mode, offset error is the deviation of the analog output from the ideal quarter-scale output when the DAC is configured for a bipolar output range and the DAC register is loaded with $0 \times 4000$ (straight binary coding).

In current output mode, offset error is the deviation of the analog output from the ideal zero-scale output when all DAC registers are loaded with 0x0000.
Offset Error Drift or Offset TC
Offset error drift, or offset TC, is a measure of the change in offset error with changes in temperature and is expressed in ppm FSR $/{ }^{\circ} \mathrm{C}$.

## Gain Error

Gain error is a measure of the span error of the DAC. It is the deviation in slope of the DAC transfer function from the ideal, expressed in \% FSR.

## Gain Temperature Coefficient (TC)

Gain TC is a measure of the change in gain error with changes in temperature and is expressed in $\mathrm{ppm} \mathrm{FSR} /{ }^{\circ} \mathrm{C}$.

## Full-Scale Error

Full-scale error is a measure of the output error when full-scale code is loaded to the DAC register. Ideally, the output should be full-scale - 1 LSB. Full-scale error is expressed in \% FSR.

## Full-Scale Temperature Coefficient (TC)

Full-scale TC is a measure of the change in full-scale error with changes in temperature and is expressed in $\mathrm{ppm} \mathrm{FSR} /{ }^{\circ} \mathrm{C}$.
Total Unadjusted Error (TUE)
Total unadjusted error (TUE) is a measure of the output error that includes all the error measurements: INL error, offset error, gain error, temperature, and time. TUE is expressed in \% FSR.

## DC Crosstalk

DC crosstalk is the dc change in the output level of one DAC in response to a change in the output of another DAC. It is measured with a full-scale output change on one DAC while monitoring another DAC, which is at midscale.

## Current Loop Compliance Voltage

The current loop compliance voltage is the maximum voltage at the Iout_x pin for which the output current is equal to the programmed value.

## Voltage Reference Thermal Hysteresis

Voltage reference thermal hysteresis is the difference in output voltage measured at $+25^{\circ} \mathrm{C}$ compared to the output voltage measured at $+25^{\circ} \mathrm{C}$ after cycling the temperature from $+25^{\circ} \mathrm{C}$ to $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ and back to $+25^{\circ} \mathrm{C}$. The hysteresis is specified for the first and second temperature cycles and is expressed in ppm.

## Output Voltage Settling Time

Output voltage settling time is the amount of time it takes for the output to settle to a specified level for a full-scale input change. Plots of settling time are shown in Figure 23, Figure 48, and Figure 49.

## Slew Rate

The slew rate of a device is a limitation in the rate of change of the output voltage. The output slewing speed of a voltage output DAC is usually limited by the slew rate of the amplifier used at its output. Slew rate is measured from $10 \%$ to $90 \%$ of the output signal and is given in $V / \mu s$.

## Power-On Glitch Energy

Power-on glitch energy is the impulse injected into the analog output when the AD5735 is powered on. It is specified as the area of the glitch in nV-sec (see Figure 28 and Figure 45).

## Data Sheet

## Digital-to-Analog Glitch Energy

Digital-to-analog glitch energy is the impulse injected into the analog output when the input code in the DAC register changes state but the output voltage remains constant. It is normally specified as the area of the glitch in nV-sec and is measured when the digital input code is changed by 1 LSB at the major carry transition ( $\sim 0 \mathrm{x} 7 \mathrm{FFF}$ to 0x8000). See Figure 25.

## Glitch Impulse Peak Amplitude

Glitch impulse peak amplitude is the peak amplitude of the impulse injected into the analog output when the input code in the DAC register changes state. It is specified as the amplitude of the glitch in mV and is measured when the digital input code is changed by 1 LSB at the major carry transition ( $\sim 0 \mathrm{x} 7 \mathrm{FFF}$ to 0x8000). See Figure 25.

## Digital Feedthrough

Digital feedthrough is a measure of the impulse injected into the analog output of the DAC from the digital inputs of the DAC but is measured when the DAC output is not updated. It is specified in nV -sec and measured with a full-scale code change on the data bus.

## DAC-to-DAC Crosstalk

DAC-to-DAC crosstalk is the glitch impulse transferred to the output of one DAC due to a digital code change and a subsequent output change of another DAC. DAC-to-DAC crosstalk includes both digital and analog crosstalk. It is measured by loading one DAC with a full-scale code change (all 0 s to all $1 s$ and vice versa) with $\overline{\text { LDAC }}$ low while monitoring the output of another DAC. The energy of the glitch is expressed in nV -sec.

Power Supply Rejection Ratio (PSRR)
PSRR indicates how the output of the DAC is affected by changes in the power supply voltage.

## Reference Temperature Coefficient (TC)

Reference TC is a measure of the change in the reference output voltage with changes in temperature. It is expressed in $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$.

## Line Regulation

Line regulation is the change in the reference output voltage due to a specified change in supply voltage. It is expressed in $\mathrm{ppm} / \mathrm{V}$.

## Load Regulation

Load regulation is the change in the reference output voltage due to a specified change in load current. It is expressed in $\mathrm{ppm} / \mathrm{mA}$.

## DC-to-DC Converter Headroom

DC-to-DC converter headroom is the difference between the voltage required at the current output and the voltage supplied by the dc-to-dc converter (see Figure 51).

## Output Efficiency

Output efficiency is defined as the ratio of the power delivered to a channel's load and the power delivered to the channel's dc-to-dc input. The $\mathrm{V}_{\text {boost_x }}$ quiescent current is considered part of the dc-to-dc converter's losses.

$$
\frac{I_{O U T}^{2} \times R_{L O A D}}{A V_{C C} \times A I_{C C}}
$$

## Efficiency at $\mathbf{V}_{\text {boost_x }}$

The efficiency at $V_{\text {boost_x }}$ is defined as the ratio of the power delivered to a channel's Voost_x supply and the power delivered to the channel's dc-to-dc input. The Vboost_x quiescent current is considered part of the dc-to-dc converter's losses.

$$
\frac{I_{\text {OUT }} \times V_{\text {BOOST_ }} x}{A V_{C C} \times A I_{C C}}
$$

## THEORY OF OPERATION

The AD5735 is a quad, precision digital-to-current loop and voltage output converter designed to meet the requirements of industrial process control applications. It provides a high precision, fully integrated, low cost, single-chip solution for generating current loop and unipolar/bipolar voltage outputs.
The current ranges available are 0 mA to $20 \mathrm{~mA}, 4 \mathrm{~mA}$ to 20 mA , and 0 mA to 24 mA . The voltage ranges available are 0 V to 5 V , $\pm 5 \mathrm{~V}, 0 \mathrm{~V}$ to 10 V , and $\pm 10 \mathrm{~V}$. The current and voltage outputs are available on separate pins, and only one output is active at any one time. The output configuration is user-selectable via the DAC control register.
On-chip dynamic power control minimizes package power dissipation in current mode (see the Dynamic Power Control section).

## DAC ARCHITECTURE

The DAC core architecture of the AD5735 consists of two matched DAC sections. A simplified circuit diagram is shown in Figure 69. The four MSBs of the 12-bit data-word are decoded to drive 15 switches, E1 to E15. Each switch connects one of 15 matched resistors either to ground or to the reference buffer output. The remaining eight bits of the data-word drive Switch S0 to Switch S7 of an 8-bit voltage mode R-2R ladder network.


Figure 69. DAC Ladder Structure
The voltage output from the DAC core can be

- Buffered and scaled to output a software selectable unipolar or bipolar voltage range (see Figure 70)
- Converted to a current, which is then mirrored to the supply rail so that the application sees only a current source output (see Figure 71)

Both the voltage and current outputs are supplied by $\mathrm{V}_{\text {Boost_x. }}$. The current and voltage are output on separate pins and cannot be output simultaneously. The current and voltage output pins of a channel can be tied together (see the Voltage and Current Output Pins on the Same Terminal section).


Figure 70. Voltage Output


Figure 71. Voltage-to-Current Conversion Circuitry

## Voltage Output Amplifier

The voltage output amplifier is capable of generating both unipolar and bipolar output voltages. It is capable of driving a load of $1 \mathrm{k} \Omega$ in parallel with $1 \mu \mathrm{~F}$ (with an external compensation capacitor) to AGND. The source and sink capabilities of the output amplifier are shown in Figure 22. The slew rate is $1.9 \mathrm{~V} / \mu \mathrm{s}$ with a full-scale settling time of $18 \mu \mathrm{~s} \max (10 \mathrm{~V}$ step). If remote sensing of the load is not required, connect $+V_{\text {SENSE_x }}$ directly to Vout_x and connect $-V_{\text {SENSE_x }}$ directly to AGND. $-\mathrm{V}_{\text {SENSE_x }}$ must stay within $\pm 3.0 \mathrm{~V}$ of AGND for specified operation. The difference in voltage between $+V_{\text {SENSE_x }}$ and $V_{\text {out_x }}$ should be added directly to the headroom requirement.

## Driving Large Capacitive Loads

The voltage output amplifier is capable of driving capacitive loads of up to $2 \mu \mathrm{~F}$ with the addition of a 220 pF , nonpolarized compensation capacitor on each channel. The 220 pF capacitor is connected between the COMP ${ }_{\text {Lv_x }}$ pin and the Vout_x pin.
Care should be taken to choose an appropriate value of compensation capacitor. This capacitor, while allowing the AD5735 to drive higher capacitive loads and reduce overshoot, increases the settling time of the part and, therefore, affects the bandwidth of the system. Without the compensation capacitor, capacitive loads of up to 10 nF can be driven.

## Reference Buffers

The AD5735 can operate with either an external or internal reference. The reference input requires a 5 V reference for specified performance. This input voltage is then buffered before it is applied to the DAC.

## POWER-ON STATE OF THE AD5735

On initial power-up of the AD5735, the state of the power-on reset circuit is dependent on the power-on condition (POC) pin.

- If $\mathrm{POC}=0$, both the voltage output and current output channels power up in tristate mode.
- If POC $=1$, the voltage output channel powers up with a $30 \mathrm{k} \Omega$ pull-down resistor to ground, and the current output channel powers up in tristate mode.

The output ranges are not enabled, but the default output range is 0 V to 5 V , and the clear code register is loaded with all 0 s . Therefore, if the user clears the part after power-up, the output is actively driven to 0 V if the channel has been enabled for clear.
After device power on, or a device reset, it is recommended to wait $100 \mu$ s or more before writing to the device to allow time for internal calibrations to take place.

## SERIAL INTERFACE

The AD5735 is controlled by a versatile 3-wire serial interface that operates at clock rates of up to 30 MHz and is compatible with SPI, QSPI, MICROWIRE, and DSP standards. Data coding is always straight binary.

## Input Shift Register

The input shift register is 24 bits wide. Data is loaded into the device MSB first as a 24 -bit word under the control of the serial clock input, SCLK. Data is clocked in on the falling edge of SCLK.
If packet error checking (PEC) is enabled, an additional eight bits must be written to the AD5735, creating a 32-bit serial interface (see the Packet Error Checking section).
The DAC outputs can be updated in one of two ways: individual DAC updating or simultaneous updating of all DACs.

## Individual DAC Updating

To update an individual DAC, $\overline{\mathrm{LDAC}}$ is held low while data is clocked into the DAC data register. The addressed DAC output is updated on the rising edge of SYNC. See Table 3 and Figure 3 for timing information.

## Simultaneous Updating of All DACs

To update all DACs simultaneously, $\overline{\text { LDAC }}$ is held high while data is clocked into the DAC data register. After $\overline{\mathrm{LDAC}}$ is taken high, only the first write to the DAC data register of each channel is valid; subsequent writes to the DAC data register are ignored, although these subsequent writes are returned if a readback is initiated. All DAC outputs are updated by taking $\overline{\text { LDAC }}$ low after $\overline{\text { SYNC }}$ is taken high.


Figure 72. Simplified Serial Interface of the Input Loading Circuitry for One DAC Channel

## TRANSFER FUNCTION

Table 7 shows the input code to ideal output voltage relationship for the AD5735 for straight binary data coding of the $\pm 10 \mathrm{~V}$ output range.

Table 7. Input Code to Ideal Output Voltage Relationship

| Digital Input |  |  |  | Analog Output |
| :---: | :---: | :---: | :---: | :---: |
| Straight Binary Data Coding |  |  |  |  |
|  |  |  |  | Vout |
| 1111 | 1111 | 1111 | XXXX | $+2 \mathrm{~V}_{\text {ReF }} \times(2047 / 2048)$ |
| 1111 | 1111 | 1110 | XXXX | $+2 \mathrm{~V}_{\text {REF }} \times(2046 / 2048)$ |
| 1000 | 0000 | 0000 | XXXX | 0 V |
| 0000 | 0000 | 0001 | XXXX | $-2 V_{\text {ReF }} \times(2047 / 2048)$ |
| 0000 | 0000 | 0000 | XXXX | $-2 \mathrm{~V}_{\text {REF }}$ |

${ }^{1} \mathrm{X}=$ don't care.

## REGISTERS

Table 8, Table 9, and Table 10 provide an overview of the registers for the AD5735.
Table 8. Data Registers for the AD5735

| Register | Description |
| :--- | :--- |
| DAC Data Registers | The four DAC data registers (one register per DAC channel) are used to write a DAC code to each DAC <br> channel. The DAC data bits are D15 to D4. |
| Gain Registers | The four gain registers (one register per DAC channel) are used to program the gain trim on a per-channel <br> basis. The gain data bits are D15 to D4. |
| Offset Registers | The four offset registers (one register per DAC channel) are used to program the offset trim on a per-channel <br> basis. The offset data bits are D15 to D4. |
| Clear Code Registers | The four clear code registers (one register per DAC channel) are used to program the clear code on a per- <br> channel basis. The clear code data bits are D15 to D4. |

Table 9. Control Registers for the AD5735

| Register | Description |
| :--- | :--- |
| Main Control Register | The main control register is used to configure functions for the entire part. These functions include the <br> following: enabling status readback during a write; enabling the output on all four DAC channels simulta- <br> neously; power-on of the dc-to-dc converter on all four DAC channels simultaneously; and enabling and <br> configuring the watchdog timer. For more information, see the Main Control Register section. |
| DAC Control Registers | The four DAC control registers (one register per DAC channel) are used to configure the following functions <br> on a per-channel basis: output range (for example, 4 mA to 20 mA or 0 V to 10 V ); selection of the internal <br> current sense resistor or an external current sense resistor; enabling/disabling the use of a clear code; <br> enabling/disabling overrange on a voltage channel; enabling/disabling the internal circuitry (dc-to-dc <br> converter, DAC, and internal amplifiers); power-on/power-off of the dc-to-dc converter; and enabling/ <br> disabling the output channel. |
| Software Register | The software register is used to perform a reset, to toggle the user bit in the status register, and, as part of <br> the watchdog timer feature, to verify correct data communication operation. |
| DC-to-DC Control Register | The dc-to-dc control register is used to set the control parameters for the dc-to-dc converter: maximum <br> output voltage, phase, and switching frequency. This register is also used to select the internal compensa- <br> tion resistor or an external compensation resistor for the dc-to-dc converter. |
| Slew Rate Control Registers | The four slew rate control registers (one register per DAC channel) are used to program the slew rate of <br> the DAC output. |

Table 10. Readback Register for the AD5735

| Register | Description |
| :--- | :--- |
| Status Register | The status register contains any fault information, as well as a user toggle bit. |

## Data Sheet

## ENABLING THE OUTPUT

To correctly write to and set up the part from a power-on condition, use the following sequence:

1. Perform a hardware or software reset after initial power-on.
2. Configure the dc-to-dc converter supply block. Set the dc-to-dc switching frequency, the maximum output voltage allowed, and the dc-to-dc converter phase between channels.
3. Configure the DAC control register on a per-channel basis. Select the output range, and enable the dc-to-dc converter block (DC_DC bit). Other control bits can also be configured. Set the INT_ENABLE bit, but do not set the OUTEN (output enable) bit.
4. Write the required code to the DAC data register. This step implements a full internal DAC calibration. For reduced output glitch, allow at least $200 \mu$ s before performing Step 5 .
5. Write to the DAC control register again to enable the output (set the OUTEN bit).

Figure 73 provides a flowchart of this sequence.


Figure 73. Programming Sequence to Correctly Enable the Output

## REPROGRAMMING THE OUTPUT RANGE

When changing the range of an output, the same sequence described in the Enabling the Output section should be used. It is recommended that the range be set to 0 V (zero scale or midscale) before the output is disabled. Because the dc-to-dc switching frequency, maximum output voltage, and phase have already been selected, there is no need to reprogram these values. Figure 74 provides a flowchart of this sequence.


Figure 74. Programming Sequence to Change the Output Range

## DATA REGISTERS

The input shift register is 24 bits wide. When PEC is enabled, the input shift register is 32 bits wide, with the last eight bits corresponding to the PEC code (see the Packet Error Checking section for more information about PEC). When writing to a data register, the format shown in Table 11 must be used.

## DAC Data Register

When writing to a DAC data register, Bit D15 to Bit D4 are the DAC data bits. Table 13 shows the register format, and Table 12 describes the functions of Bit D23 to Bit D16.

Table 11. Input Shift Register for a Write Operation to a Data Register MSB

LSB

| D23 | D22 | D21 | D20 | D19 | D18 | D17 | D16 | D15 to D0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| R/ $\bar{W}$ | DUT_AD1 | DUT_AD0 | DREG2 | DREG1 | DREG0 | DAC_AD1 | DAC_AD0 | Data |

Table 12. Descriptions of Data Register Bits[D23:D16]

| Bit Name | Description |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| R/W | This bit indicates whether the addressed register is written to or read from. $0=$ write to the addressed register. <br> 1 = read from the addressed register. |  |  |  |
| DUT_AD1, DUT_AD0 | Used in association with the external pins AD1 and AD0, these bits determine which AD5735 device is being addressed by the system controller. |  |  |  |
|  | DUT_AD1 | DUT_ADO | Part Addressed |  |
|  | $\begin{aligned} & \hline 0 \\ & 0 \\ & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & \hline 0 \\ & 1 \\ & 0 \\ & 1 \end{aligned}$ | $\begin{aligned} & \text { Pin AD1 }=0, \operatorname{Pin} \text { AD0 }=0 \\ & \text { Pin AD1 }=0, \operatorname{Pin} \text { AD0 }=1 \\ & \text { Pin AD1 }=1, \operatorname{Pin} \text { AD0 }=0 \\ & \text { Pin AD1 }=1, \operatorname{Pin} A D 0=1 \end{aligned}$ |  |
| DREG2, DREG1, DREG0 | These bits select the register to be written to. If a control register is selected (DREG[2:0] = 111), the CREG bits in the control register select the specific control register to be written to (see Table 20). |  |  |  |
|  | DREG2 | DREG1 | DREGO | Function |
|  | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & 1 \\ & 1 \\ & 0 \\ & 0 \\ & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & \hline 0 \\ & 1 \\ & 0 \\ & 1 \\ & 0 \\ & 1 \\ & 0 \\ & 1 \end{aligned}$ | Write to DAC data register (one DAC channel) Reserved <br> Write to gain register (one DAC channel) Write to gain registers (all DAC channels) Write to offset register (one DAC channel) Write to offset registers (all DAC channels) Write to clear code register (one DAC channel) Write to a control register |
| DAC_AD1, DAC_AD0 | These bits are used to specify the DAC channel. If a write to the part does not apply to a specific DAC channel, these bits are don't care bits. |  |  |  |
|  | DAC_AD1 | DAC_ADO | DAC Channel |  |
|  | 0 0 1 1 | 0 1 0 1 | DAC A <br> DAC B <br> DAC C <br> DAC D |  |

Table 13. Programming the DAC Data Register

| D23 | D22 | D21 | D20 | D19 | D18 | D17 | D16 | D15 to D4 | D3 to D0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| R/ $\bar{W}$ | DUT_AD1 | DUT_AD0 | 0 | 0 | 0 | DAC_AD1 | DAC_AD0 | DAC data | $X^{1}$ |

${ }^{1} \mathrm{X}=$ don't care.

## Data Sheet

## Gain Register

The 12-bit gain register allows the user to adjust the gain of each channel in steps of 1 LSB. To write to the gain register of one DAC channel, set the DREG[2:0] bits to 010 (see Table 14). To write the same gain code to all four DAC channels at the same time, set the DREG[2:0] bits to 011 . The gain register coding is straight binary, as shown in Table 15. The default code in the gain register is $0 x F F F F$. The maximum recommended gain trim is approximately $50 \%$ of the programmed range to maintain accuracy (for more information, see the Digital Offset and Gain Control section).

## Offset Register

The 12-bit offset register allows the user to adjust the offset of each channel by -2048 LSB to +2047 LSB in steps of 1 LSB. To write to the offset register of one DAC channel, set the

DREG[2:0] bits to 100 (see Table 16). To write the same offset code to all four DAC channels at the same time, set the DREG[2:0] bits to 101. The offset register coding is straight binary, as shown in Table 17. The default code in the offset register is $0 \times 8000$, which results in zero offset programmed to the output (for more information, see the Digital Offset and Gain Control section).

## Clear Code Register

The 12-bit clear code register allows the user to set the clear value of each channel. To configure a channel to be cleared when the CLEAR pin is activated, set the CLR_EN bit in the DAC control register for that channel (see Table 24). To write to the clear code register, set the DREG[2:0] bits to 110 (see Table 18). The default clear code is $0 x 0000$ (for more information, see the Asynchronous Clear section).

Table 14. Programming the Gain Register

| R/产 | DUT_AD1 | DUT_AD0 | DREG2 | DREG1 | DREG0 | DAC_AD1 | DAC_AD0 | D15 to D4 | D3 to D0 |
| :--- | :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0 | Device address | 0 | 1 | 0 | DAC channel address | Gain adjustment | 1111 |  |  |

Table 15. Gain Register Bit Descriptions

| Gain Adjustment | G15 | G14 | G13 to G5 | G4 | G3 to G0 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| +4096 LSB | 1 | 1 | 111111111 | 1 | 1111 |
| +4095 LSB | 1 | 1 | 111111111 | 0 | 1111 |
| $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | 1111 |  |
| 1 LSB | 0 | 0 | 000000000 | 1 | 1111 |
| 0 LSB | 0 | 00000000 | 0 | 1111 |  |

Table 16. Programming the Offset Register

| R/ $\overline{\mathbf{W}}$ | DUT_AD1 | DUT_AD0 | DREG2 | DREG1 | DREG0 | DAC_AD1 | DAC_AD0 | D15 to D4 | D3 to D0 |
| :--- | :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0 | Device address | 1 | 0 | 0 | DAC channel address | Offset adjustment | 0000 |  |  |

Table 17. Offset Register Bit Descriptions

| Offset Adjustment | OF15 | OF14 | OF13 | OF12 to OF5 | OF4 | OF3 to OF0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| +2047 LSB | 1 | 1 | 1 | 11111111 | 1 | 0000 |
| +2046 LSB | 1 | 1 | 1 | 11111111 | 0 | 0000 |
| $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | 0000 |  |
| No Adjustment (Default) | 1 | $\ldots$ | $\ldots$ | $\ldots$ | 0000 |  |
| $\ldots$ | 0 | 0 | 0 | 0 | 0000 |  |
| -2047 LSB | 0 | 0 | 000000 | 0 | 0000 |  |
| -2048 LSB |  |  | $\ldots$ | 1 | 0000 |  |

Table 18. Programming the Clear Code Register

| R/产 | DUT_AD1 | DUT_AD0 | DREG2 | DREG1 | DREG0 | DAC_AD1 | DAC_AD0 | D15 to D4 | D3 to D0 |
| :--- | :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0 | Device address | 1 | 1 | 0 | DAC channel address | Clear code | 0000 |  |  |

## AD5735

## CONTROL REGISTERS

When writing to a control register, the format shown in Table 19 must be used. See Table 12 for information about the configuration of Bit D23 to Bit D16. The control registers are addressed by setting the DREG[2:0] bits (Bits[D20:D18] in the input shift register) to 111 and then setting the CREG[2:0] bits to select the specific control register (see Table 20).

## Main Control Register

The main control register options are shown in Table 21 and Table 22. See the Device Features section for more information about the features controlled by the main control register.

Table 19. Input Shift Register for a Write Operation to a Control Register
MSB

| D23 | D22 | D21 | D20 | D19 | D18 | D17 | D16 | D15 | D14 | D13 | D12 to D0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| R/ $\bar{W}$ | DUT_AD1 | DUT_AD0 | 1 | 1 | 1 | DAC_AD1 | DAC_AD0 | CREG2 | CREG1 | CREG0 | Data |

Table 20. Control Register Addresses (CREG[2:0] Bits)

| CREG2 (D15) | CREG1 (D14) | CREG0 (D13) | Control Register |
| :--- | :--- | :--- | :--- |
| 0 | 0 | 0 | Slew rate control register (one per channel) |
| 0 | 0 | 1 | Main control register |
| 0 | 1 | 0 | DAC control register (one per channel) |
| 0 | 1 | 1 | DC-to-DC control register |
| 1 | 0 | 0 | Software register |

Table 21. Programming the Main Control Register

| D15 | D14 | D13 | D12 | D11 | D10 | D9 | D8 | D7 | D6 | D5 | D4 | D3 to D0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0 | 0 | 1 | POC | STATREAD | EWD | WD1 | WD0 | $X^{1}$ | ShtCctLim | OUTEN_ALL | DCDC_ALL | X $^{1}$ |

${ }^{1} \mathrm{X}=$ don't care.

Table 22. Main Control Register Bit Descriptions

| Bit Name | Description |  |  |
| :---: | :---: | :---: | :---: |
| POC | The POC bit determines the state of the voltage output channels during normal operation. <br> POC $=0$ : the output goes to the value set by the POC hardware pin when the voltage output is not enabled (default). $P O C=1$ : the output goes to the opposite value of the POC hardware pin when the voltage output is not enabled. |  |  |
| STATREAD | Enable status readback during a write. See the Status Readback During a Write section. $0=$ disable status readback (default). <br> 1 = enable status readback. |  |  |
| EWD | Enable the watchdog timer. See the Watchdog Timer section. $0=$ disable the watchdog timer (default). <br> 1 = enable the watchdog timer. |  |  |
| WD1, WD0 | Timeout select bits. Used to select the timeout period for the watchdog timer. |  |  |
|  | WD1 | WDO | Time |
|  | $\begin{aligned} & 0 \\ & 0 \\ & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 0 \\ & 1 \\ & 0 \\ & 1 \end{aligned}$ | $\begin{aligned} & 5 \\ & 10 \\ & 100 \\ & 200 \end{aligned}$ |
| ShtCctLim | Programmable short-circuit limit on the $V_{\text {out_x }}$ pin in the event of a short-circuit condition.$\begin{aligned} & 0=16 \mathrm{~mA} \text { (default). } \\ & 1=8 \mathrm{~mA} . \end{aligned}$ |  |  |
| OUTEN_ALL | Setting this bit to 1 enables the output on all four DACs simultaneously. Do not use the OUTEN_ALL bit when using the OUTEN bit in the DAC control register. |  |  |
| DCDC_ALL | Setting this bit to 1 powers up the dc-to-dc converter on all four channels simultaneously. To power down the dc-to-dc converters, all channel outputs must first be disabled. Do not use the DCDC_ALL bit when using the DC_DC bit in the DAC control register. |  |  |

## Data Sheet

## DAC Control Register

The DAC control register is used to configure each DAC channel. The DAC control register options are shown in Table 23 and Table 24.

Table 23. Programming the DAC Control Register

| D15 | D14 | D13 | D12 | D11 | D10 | D9 | D8 | D7 | D6 | D5 | D4 | D3 | D2 | D1 | D0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0 | 1 | 0 | $\mathrm{X}^{1}$ | $\mathrm{X}^{1}$ | $\mathrm{X}^{1}$ | $\mathrm{X}^{1}$ | INT_ENABLE | CLR_EN | OUTEN | RSET | DC_DC | OVRNG | R2 | R1 | R0 |

${ }^{1} \mathrm{X}=$ don't care.

Table 24. DAC Control Register Bit Descriptions

| Bit Name | Description |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| INT_ENABLE | Powers up the dc-to-dc converter, DAC, and internal amplifiers for the selected channel. This bit applies to individual channels only; it does not enable the output. After setting this bit, it is recommended that a $>200 \mu$ s delay be observed before enabling the output to reduce the output enable glitch. See Figure 29 and Figure 46 for plots of this glitch. |  |  |  |
| CLR_EN | Per-channel clear enable bit. This bit specifies whether the selected channel is cleared when the CLEAR pin is activated. $0=$ channel is not cleared when the part is cleared (default). <br> 1 = channel is cleared when the part is cleared. |  |  |  |
| OUTEN | Enables or disables the selected output channel. <br> $0=$ channel disabled (default). <br> $1=$ channel enabled. |  |  |  |
| RSET | Selects the internal current sense resistor or an external current sense resistor for the selected DAC channel. $0=$ external resistor selected (default). <br> 1 = internal resistor selected. |  |  |  |
| DC_DC | Powers up or powers down the dc-to-dc converter on the selected channel. All dc-to-dc converters can be powered up simultaneously using the DCDC_ALL bit in the main control register. To power down the dc-to-dc converter, the OUTEN and INT_ENABLE bits must also be set to 0 . <br> $0=$ dc-to-dc converter is powered down (default). <br> 1 = dc-to-dc converter is powered up. |  |  |  |
| OVRNG | Enables $20 \%$ overrange on the voltage output channel only. No current output overrange is available. $0=$ overrange disabled (default). <br> 1 = overrange enabled. |  |  |  |
| R2, R1, R0 | Selects the output range to be enabled. |  |  |  |
|  | R2 | R1 | R0 | Output Range Selected |
|  | 0 | 0 | 0 | 0 V to 5 V voltage range (default) |
|  | 0 | 0 | 1 | 0 V to 10 V voltage range |
|  | 0 | 1 | 0 | $\pm 5 \mathrm{~V}$ voltage range |
|  | 0 | 1 | 1 | $\pm 10 \mathrm{~V}$ voltage range |
|  | 1 | 0 | 0 | 4 mA to 20 mA current range |
|  | 1 | 0 | 1 | 0 mA to 20 mA current range |
|  | 1 | 1 | 0 |  |

## Software Register

The software register allows the user to perform a software reset of the part. This register is also used to set the user toggle bit, D11, in the status register and as part of the watchdog timer feature when that feature is enabled.
Bit D12 in the software register can be used to ensure that communication has not been lost between the MCU and the AD5735 and that the datapath lines are working properly (that is, SDIN, SCLK, and $\overline{\text { SYNC }}$ ).

When the watchdog timer feature is enabled, the user must write 0x195 to Bits[D11:D0] of the software register within the timeout period. If this command is not received within the timeout period, the ALERT pin signals a fault condition. This command is only required when the watchdog timer feature is enabled.

## DC-to-DC Control Register

The dc-to-dc control register allows the user to configure the dc-to-dc switching frequency and phase, as well as the maximum allowable dc-to-dc output voltage. The dc-to-dc control register options are shown in Table 27 and Table 28.

Table 25. Programming the Software Register

| D15 | D14 | D13 | D12 | D11 to D0 |
| :--- | :--- | :--- | :--- | :--- |
| 1 | 0 | 0 | User program | Reset code/SPI code |

Table 26. Software Register Bit Descriptions

| Bit Name | Description |  |
| :--- | :--- | :--- |
| User Program | This bit is mapped to Bit D11 of the status register. When this bit is set to 1, Bit D11 of the status register is set to 1. <br> When this bit is set to 0, Bit D11 of the status register is also set to 0. This feature can be used to ensure that the SPI <br> pins are working correctly by writing a known bit value to this register and then reading back Bit D11 from the <br> status register. | Description |
| Reset Code/SPI Code | Option | Writing 0x555 to Bits[D11:D0] performs a software reset of the AD5735. <br> If the watchdog timer feature is enabled, 0x195 must be written to the software register <br> (Bits[D11:D0]) within the programmed timeout period (see Table 22). |
|  | Reset code <br> SPI code |  |

Table 27. Programming the DC-to-DC Control Register

| D15 | D14 | D13 | D12 to D7 | D6 | D5 to D4 | D3 to D2 | D1 to D0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0 | 1 | 1 | $X^{1}$ | DC-DC comp | DC-DC phase | DC-DC freq | DC-DC MaxV |

${ }^{1} \mathrm{X}=$ don't care.
Table 28. DC-to-DC Control Register Bit Descriptions

| Bit Name | Description |
| :---: | :---: |
| DC-DC Comp | Selects the internal compensation resistor or an external compensation resistor for the dc-to-dc converter. See the DC-to-DC Converter Compensation Capacitors section and the Alcc Supply Requirements-Slewing section. $0=$ selects the internal $150 \mathrm{k} \Omega$ compensation resistor (default). <br> 1 = bypasses the internal compensation resistor. When this bit is set to 1 , an external compensation resistor must be used; this resistor is placed at the COMP DCDC_ $^{x}$ pin in series with the 10 nF dc-to-dc compensation capacitor to ground. Typically, a resistor of $\sim 50 \mathrm{k} \Omega$ is recommended. |
| DC-DC Phase | User-programmable dc-to-dc converter phase (between channels). <br> $00=$ all dc-to-dc converters clock on the same edge (default). <br> 01 = Channel A and Channel B clock on the same edge; Channel C and Channel D clock on the opposite edge. <br> $10=$ Channel A and Channel C clock on the same edge; Channel B and Channel D clock on the opposite edge. <br> 11 = Channel A, Channel B, Channel C, and Channel D clock $90^{\circ}$ out of phase from each other. |
| DC-DC Freq | Switching frequency for the dc-to-dc converter; this frequency is divided down from the internal 13 MHz oscillator (see Figure 67 and Figure 68). $\begin{aligned} & 00=250 \mathrm{kHz} \pm 10 \% . \\ & 01=410 \mathrm{kHz} \pm 10 \% \text { (default). } \\ & 10=650 \mathrm{kHz} \pm 10 \% . \end{aligned}$ |
| DC-DC MaxV | Maximum allowed $\mathrm{V}_{\text {Boost_ } \mathrm{x}}$ voltage supplied by the dc-to-dc converter. $\begin{aligned} & 00=23 \mathrm{~V}+1 \mathrm{~V} /-1.5 \mathrm{~V} \text { (default). } \\ & 01=24.5 \mathrm{~V} \pm 1 \mathrm{~V} . \\ & 10=27 \mathrm{~V} \pm 1 \mathrm{~V} . \\ & 11=29.5 \mathrm{~V} \pm 1 \mathrm{~V} . \end{aligned}$ |

## Data Sheet

## Slew Rate Control Register

This register is used to program the slew rate control for the selected DAC channel. This feature is available on both the current and voltage outputs. The slew rate control is enabled/ disabled and programmed on a per-channel basis. See Table 29 and the Digital Slew Rate Control section for more information.

## READBACK OPERATION

Readback mode is invoked by setting the $\mathrm{R} / \overline{\mathrm{W}}$ bit = 1 in the serial input register write. See Table 30 for the bits associated with a readback operation. The DUT_AD1 and DUT_AD0 bits, in association with Bits[RD4:RD0], select the register to be read (see Table 31). The remaining data bits in the write sequence are don't care bits. During the next SPI transfer, the data that appears on the SDO output contains the data from the previously addressed register
(see Figure 4). This second SPI transfer should be either a request to read another register on a third data transfer or a no operation command. The no operation command for DUT Address 00 is $0 x 1$ CE000, for other DUT addresses, Bit D22 and Bit D21 are set accordingly.

## Readback Example

To read back the gain register of AD5735 Device 1, Channel A, implement the following sequence:

1. Write 0xA80000 to the input register to configure Device Address 1 for read mode with the gain register of Channel A selected. The data bits, D15 to D0, are don't care bits.
2. Execute another read command or a no operation command (0x3CE000). During this command, the data from the Channel A gain register is clocked out on the SDO line.

Table 29. Programming the Slew Rate Control Register

| D15 | D14 | D13 | D12 | D11 to D7 | D6 to D3 | D2 to D0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0 | 0 | 0 | SREN | $X^{1}$ | SR_CLOCK | SR_STEP |

${ }^{1} \mathrm{X}=$ don't care.
Table 30. Input Shift Register for a Read Operation MSB

| D23 | D22 | D21 | D20 | D19 | D18 | D17 | D16 | D15 to D0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| R/ $\bar{W}$ | DUT_AD1 | DUT_AD0 | RD4 | RD3 | RD2 | RD1 | RD0 | X $^{1}$ |

${ }^{1} \mathrm{X}=$ don't care.
Table 31. Read Addresses (Bits[RD4:RD0])

| RD4 | RD3 | RD2 | RD1 | RDO | Function |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | 0 | 0 | 0 | Read DAC A data register |
| 0 | 0 | 0 | 0 | 1 | Read DAC B data register |
| 0 | 0 | 0 | 1 | 0 | Read DAC C data register |
| 0 | 0 | 0 | 1 | 1 | Read DAC D data register |
| 0 | 0 | 1 | 0 | 0 | Read DAC A control register |
| 0 | 0 | 1 | 0 | 1 | Read DAC B control register |
| 0 | 0 | 1 | 1 | 0 | Read DAC C control register |
| 0 | 0 | 1 | 1 | 1 | Read DAC D control register |
| 0 | 1 | 0 | 0 | 0 | Read DAC A gain register |
| 0 | 1 | 0 | 0 | 1 | Read DAC B gain register |
| 0 | 1 | 0 | 1 | 0 | Read DAC C gain register |
| 0 | 1 | 0 | 1 | 1 | Read DAC D gain register |
| 0 | 1 | 1 | 0 | 0 | Read DAC A offset register |
| 0 | 1 | 1 | 0 | 1 | Read DAC B offset register |
| 0 | 1 | 1 | 1 | 0 | Read DAC C offset register |
| 0 | 1 | 1 | 1 | 1 | Read DAC D offset register |
| 1 | 0 | 0 | 0 | 0 | Read DAC A clear code register |
| 1 | 0 | 0 | 0 | 1 | Read DAC B clear code register |
| 1 | 0 | 0 | 1 | 0 | Read DAC C clear code register |
| 1 | 0 | 0 | 1 | 1 | Read DAC D clear code register |
| 1 | 0 | 1 | 0 | 0 | Read DAC A slew rate control register |
| 1 | 0 | 1 | 0 | 1 | Read DAC B slew rate control register |
| 1 | 0 | 1 | 1 | 0 | Read DAC C slew rate control register |
| 1 | 0 | 1 | 1 | 1 | Read DAC D slew rate control register |
| 1 | 1 | 0 | 0 | 0 | Read status register |
| 1 | 1 | 0 | 0 | 1 | Read main control register |
| 1 | 1 | 0 | 1 | 0 | Read dc-to-dc control register |

## Status Register

The status register is a read-only register. This register contains any fault information, as a well as a ramp active bit (Bit D9) and a user toggle bit (Bit D11). When the STATREAD bit in the main control register is set, the status register contents can be
read back on the SDO pin during every write sequence. Alternatively, if the STATREAD bit is not set, the status register can be read using the normal readback operation (see the Readback Operation section).

Table 32. Decoding the Status Register
MSB

| D15 | 114 | D13 | D12 | D11 | D10 | D9 | D8 | D7 | D6 | D5 | D4 | D3 | D2 | D1 | D0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| DC-DCD | DC-DCC | DC-DCB | DC-DCA | User <br> toggle | PEC <br> error | Ramp <br> active | Over <br> temp | Vout_D <br> fault | Vout_C <br> fault | Vout_B <br> fault | Vout_A <br> fault | lout_D <br> fault | lout_c <br> fault | louT_B <br> fault | lout_A <br> fault |

Table 33. Status Register Bit Descriptions

| Bit Name | Description |
| :---: | :---: |
| DC-DCD | In current output mode, this bit is set if the dc-to-dc converter on Channel D cannot maintain compliance, for example, if the dc-to-dc converter is reaching its $\mathrm{V}_{\text {max }}$ voltage; in this case, the lout_d fault bit is also set. See the DC-to-DC Converter $\mathrm{V}_{\text {max }}$ Functionality section for more information about the operation of this bit under this condition. <br> In voltage output mode, this bit is set if the dc-to-dc converter on Channel D is unable to regulate to 15 V as expected. When this bit is set, it does not result in the FAULT pin going high. |
| DC-DCC | In current output mode, this bit is set if the dc-to-dc converter on Channel C cannot maintain compliance, for example, if the dc-to-dc converter is reaching its $\mathrm{V}_{\text {max }}$ voltage; in this case, the lout_c fault bit is also set. See the DC-to-DC Converter $\mathrm{V}_{\text {max }}$ Functionality section for more information about the operation of this bit under this condition. <br> In voltage output mode, this bit is set if the dc-to-dc converter on Channel C is unable to regulate to 15 V as expected. When this bit is set, it does not result in the FAULT pin going high. |
| DC-DCB | In current output mode, this bit is set if the dc-to-dc converter on Channel B cannot maintain compliance, for example, if the dc-to-dc converter is reaching its $\mathrm{V}_{\text {MAX }}$ voltage; in this case, the lout_B fault bit is also set. See the DC-to-DC Converter $\mathrm{V}_{\text {max }}$ Functionality section for more information about the operation of this bit under this condition. <br> In voltage output mode, this bit is set if the dc-to-dc converter on Channel B is unable to regulate to 15 V as expected. When this bit is set, it does not result in the FAULT pin going high. |
| DC-DCA | In current output mode, this bit is set if the dc-to-dc converter on Channel A cannot maintain compliance, for example, if the dc-to-dc converter is reaching its $\mathrm{V}_{\text {max }}$ voltage; in this case, the lout_A fault bit is also set. See the DC-to-DC Converter $\mathrm{V}_{\text {max }}$ Functionality section for more information about the operation of this bit under this condition. <br> In voltage output mode, this bit is set if the dc-to-dc converter on Channel A is unable to regulate to 15 V as expected. When this bit is set, it does not result in the FAULT pin going high. |
| User Toggle | User toggle bit. This bit is set or cleared via the software register and can be used to verify data communications, if needed. |
| PEC Error | Denotes a PEC error on the last data-word received over the SPI interface. |
| Ramp Active | This bit is set while any output channel is slewing (digital slew rate control is enabled on at least one channel). |
| Over Temp | This bit is set if the AD5735 core temperature exceeds approximately $150^{\circ} \mathrm{C}$. |
| Vout_d Fault | This bit is set if a fault is detected on the $V_{\text {out_o }}$ pin. |
| Vout_c Fault | This bit is set if a fault is detected on the $V_{\text {out_c }}$ pin. |
| Vout_b Fault | This bit is set if a fault is detected on the V out_b $^{\text {pin }}$. |
| Vout_A Fault | This bit is set if a fault is detected on the $\mathrm{V}_{\text {Out_A }}$ pin. |
| lout_d Fault | This bit is set if a fault is detected on the lout_ pin. |
| lout_c Fault | This bit is set if a fault is detected on the lout_c pin. |
| lout_b Fault | This bit is set if a fault is detected on the lout_ pin. |
| lout_A Fault | This bit is set if a fault is detected on the lout_A pin. |

## DEVICE FEATURES

## FAULT OUTPUT

The AD5735 is equipped with a $\overline{\text { FAULT }}$ pin, an active low, open-drain output that allows several AD5735 devices to be connected together to one pull-up resistor for global fault detection. The $\overline{\text { FAULT }}$ pin is forced active by any one of the following fault conditions:

- The voltage at Iout_x attempts to rise above the compliance range due to an open-loop circuit or insufficient power supply voltage. The internal circuitry that develops the fault output avoids using a comparator with windowed limits because this requires an actual output error before the $\overline{\text { FAULT }}$ output becomes active. Instead, the signal is generated when the internal amplifier in the output stage has less than approximately 1 V of remaining drive capability. Thus, the $\overline{\text { FAULT }}$ output is activated slightly before the compliance limit is reached.
- A short circuit is detected on a voltage output pin. The short-circuit current is limited to 16 mA or 8 mA , which is programmable by the user. If the AD5735 is used in unipolar supply mode, a short-circuit fault may be generated if the output voltage is below 50 mV .
- An interface error is detected due to a PEC failure (see the Packet Error Checking section).
- The core temperature of the AD5735 exceeds approximately $150^{\circ} \mathrm{C}$.

The Vout_x fault, Iout_x fault, PEC error, and over temp bits of the status register are used in conjunction with the FAULT output to inform the user which fault condition caused the $\overline{\text { FAULT }}$ output to be activated.

## VOLTAGE OUTPUT SHORT-CIRCUIT PROTECTION

Under normal operation, the voltage output sinks/sources up to 12 mA and maintains specified operation. The maximum output current or short-circuit current is programmable by the user and can be set to 16 mA or 8 mA . If a short circuit is detected, the $\overline{\text { FAULT }}$ pin goes low, and the relevant Vout_x fault bit is set in the status register (see Table 33).

## DIGITAL OFFSET AND GAIN CONTROL

Each DAC channel has a gain (M) register and an offset (C) register, which allow trimming out of the gain and offset errors of the entire signal chain. Data from the DAC data register is operated on by a digital multiplier and adder controlled by the contents of the gain and offset registers; the calibrated DAC data is then stored in the DAC input register (see Figure 75).


Figure 75. Digital Offset and Gain Control
Although Figure 75 indicates a multiplier and adder for each channel, the device has only one multiplier and one adder, which are shared by all four channels. This design has implications for the update speed when several channels are updated at once (see Table 3).
When data is written to the gain (M) or offset (C) register, the output is not automatically updated. Instead, the next write to the DAC channel uses the new gain and offset values to perform a new calibration and automatically updates the channel.

The output data from the calibration is routed to the DAC input register. This data is then loaded to the DAC, as described in the Serial Interface section. Both the gain register and the offset register have 12 bits of resolution. The correct order to calibrate the gain and offset is to first calibrate the gain and then calibrate the offset.

The value (in decimal) that is written to the DAC input register can be calculated as follows:

$$
\begin{equation*}
\text { Code }_{\text {DACRegistr }}=D \times \frac{(M+1)}{2^{12}}+C-2^{11} \tag{1}
\end{equation*}
$$

where:
$D$ is the code loaded to the DAC data register of the DAC channel.
$M$ is the code in the gain register (default code $=2^{12}-1$ ).
$C$ is the code in the offset register (default code $=2^{11}$ ).

## STATUS READBACK DURING A WRITE

The AD5735 can be configured to read back the contents of the status register during every write sequence. This feature is enabled using the STATREAD bit in the main control register. When this feature is enabled, the user can continuously monitor the status register and act quickly in the case of a fault.
When status readback during a write is enabled, the contents of the 16 -bit status register (see Table 33) are output on the SDO pin, as shown in Figure 5.
When the AD5735 is powered up, the status readback during a write feature is disabled. When this feature is enabled, readback of registers other than the status register is not available. To read back any other register, clear the STATREAD bit before following the readback sequence (see the Readback Operation section). The STATREAD bit can be set high again after the register read.

## ASYNCHRONOUS CLEAR

CLEAR is an active high, edge sensitive input that allows the output to be cleared to a preprogrammed 12-bit code. This code is user-programmable via a per-channel 12-bit clear code register.

For a channel to be cleared, set the CLR_EN bit in the DAC control register for that channel. If the clear function on a channel is not enabled, the output remains in its current state, independent of the level of the CLEAR pin.
When the CLEAR signal returns low, the relevant outputs remain cleared until a new value is programmed to them.

## PACKET ERROR CHECKING

To verify that data has been received correctly in noisy environments, the AD5735 offers the option of packet error checking based on an 8 -bit cyclic redundancy check (CRC-8). The device controlling the AD5735 should generate an 8-bit frame check sequence using the following polynomial:

$$
C(x)=x_{8}+x_{2}+x_{1}+1
$$

This value is added to the end of the data-word, and 32 bits are sent to the AD5735 before $\overline{\text { SYNC }}$ goes high. If the AD5735 sees a 32-bit frame, it performs the error check when SYNC goes high. If the error check is valid, the data is written to the selected register. If the error check fails, the $\overline{\mathrm{FAULT}}$ pin goes low and the PEC error bit in the status register is set. After the status register is read, $\overline{\text { FAULT }}$ returns high (assuming that there are no other faults), and the PEC error bit is cleared automatically.


32-BIT DATA TRANSFER WITH ERROR CHECKING Figure 76. PEC Timing
Packet error checking can be used for transmitting and receiving data packets. If status readback during a write is enabled, the PEC values returned during the status readback operation should be
ignored. If status readback during a write is disabled, the user can still use the normal readback operation to monitor status register activity with PEC.

## WATCHDOG TIMER

When enabled, an on-chip watchdog timer generates an alert signal if $0 \times 195$ is not written to the software register within the programmed timeout period. This feature is useful to ensure that communication has not been lost between the MCU and the AD5735 and that the datapath lines are working properly (that is, SDIN, SCLK, and $\overline{\text { SYNC }}$ ). If $0 \times 195$ is not received by the software register within the timeout period, the ALERT pin signals a fault condition. The ALERT pin is active high and can be connected directly to the CLEAR pin to enable a clear in the event that communication from the MCU is lost.

To enable the watchdog timer and set the timeout period ( 5 ms , $10 \mathrm{~ms}, 100 \mathrm{~ms}$, or 200 ms ), program the main control register (see Table 21 and Table 22).

## ALERT OUTPUT

The AD5735 is equipped with an ALERT pin. This pin is an active high CMOS output. The AD5735 also has an internal watchdog timer. When enabled, the watchdog timer monitors SPI communications. If $0 \times 195$ is not received by the software register within the timeout period, the ALERT pin is activated.

## INTERNAL REFERENCE

The AD5735 contains an integrated 5 V voltage reference with initial accuracy of $\pm 5 \mathrm{mV}$ maximum and a temperature coefficient of $\pm 10 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ maximum. The reference voltage is buffered and is externally available for use elsewhere within the system.

## EXTERNAL CURRENT SETTING RESISTOR

$\mathrm{R}_{\text {SET }}$ is an internal sense resistor that is part of the voltage-tocurrent conversion circuitry (see Figure 71). The stability of the output current value over temperature is dependent on the stability of the $\mathrm{R}_{\text {SET }}$ value. To improve the stability of the output current over temperature, the internal $\mathrm{R}_{\text {SET }}$ resistor, R1, can be bypassed and an external, $15 \mathrm{k} \Omega$, low drift resistor can be connected to the $\mathrm{R}_{\text {sET_x }} \mathrm{p}$ in of the AD5735. The external resistor is selected via the DAC control register (see Table 24).
Table 1 provides the performance specifications for the AD5735 with both the internal $\mathrm{R}_{\text {SET }}$ resistor and an external, $15 \mathrm{k} \Omega$ RSET resistor. The use of an external $\mathrm{R}_{\text {SET }}$ resistor allows for improved performance over the internal RSET resistor option. The external $\mathrm{R}_{\text {SET }}$ resistor specifications assume an ideal resistor; the actual performance depends on the absolute value and temperature coefficient of the resistor used. This directly affects the gain error of the output and, thus, the total unadjusted error. To arrive at the gain/TUE error of the output with a specific external RSET resistor, add the absolute error percentage of the R RET resistor directly to the gain/TUE error of the AD5735 with the external $\mathrm{R}_{\text {SET }}$ resistor, as shown in Table 1 (expressed in \% FSR).

## DIGITAL SLEW RATE CONTROL

The digital slew rate control feature of the AD5735 allows the user to control the rate at which the output value changes. This feature is available on both the current and voltage outputs. With the slew rate control feature disabled, the output value changes at a rate limited by the output drive circuitry and the attached load. To reduce the slew rate, the user can enable the digital slew rate control feature using the SREN bit of the slew rate control register (see Table 29).
When slew rate control is enabled, the output, instead of slewing directly between two values, steps digitally at a rate defined by the SR_CLOCK and SR_STEP parameters. These parameters are accessible via the slew rate control register (see Table 29).

- SR_CLOCK defines the rate at which the digital slew is updated; for example, if the selected update rate is 8 kHz , the output is updated every $125 \mu$ s.
- SR_STEP defines by how much the output value changes at each update.

Together, these parameters define the rate of change of the output value. Table 34 and Table 35 list the range of values for the SR_CLOCK and SR_STEP parameters, respectively.

Table 34. Slew Rate Update Clock Options

| SR_CLOCK | Update Clock Frequency ${ }^{1}$ |
| :--- | :--- |
| 0000 | 64 kHz |
| 0001 | 32 kHz |
| 0010 | 16 kHz |
| 0011 | 8 kHz |
| 0100 | 4 kHz |
| 0101 | 2 kHz |
| 0110 | 1 kHz |
| 0111 | 500 Hz |
| 1000 | 250 Hz |
| 1001 | 125 Hz |
| 1010 | 64 Hz |
| 1011 | 32 Hz |
| 1100 | 16 Hz |
| 1101 | 8 Hz |
| 1110 | 4 Hz |
| 1111 | 0.5 Hz |

${ }^{1}$ These clock frequencies are divided down from the 13 MHz internal oscillator (see Table 1, Figure 67, and Figure 68).

Table 35. Slew Rate Step Size Options

| SR_STEP | Step Size (LSB) |
| :--- | :--- |
| 000 | 1 |
| 001 | 2 |
| 010 | 4 |
| 011 | 16 |
| 100 | 32 |
| 101 | 64 |
| 110 | 128 |
| 111 | 256 |

The following equation describes the slew rate as a function of the step size, the update clock frequency, and the LSB size.

$$
\begin{aligned}
& \text { Slew Rate }= \\
& \frac{\text { Output Change }}{\text { Step Size } \times \text { Update Clock Frequency } \times \text { LSB Size }}
\end{aligned}
$$

where:
Slew Rate is expressed in seconds.
Output Change is expressed in amperes for Iout_x or in volts for Vout_x.
The update clock frequency for any given value is the same for all output ranges. The step size, however, varies across output ranges for a given value of step size because the LSB size is different for each output range.
When the slew rate control feature is enabled, all output changes occur at the programmed slew rate (see the DC-to-DC Converter Settling Time section for more information). For example, if the CLEAR pin is asserted, the output slews to the clear value at the programmed slew rate (assuming that the channel is enabled to be cleared).
If more than one channel is enabled for digital slew rate control, care must be taken when asserting the CLEAR pin. If a channel under slew rate control is slewing when the CLEAR pin is asserted, other channels under slew rate control may change directly to their clear code not under slew rate control.

## DYNAMIC POWER CONTROL

When configured in current output mode, the AD5735 provides integrated dynamic power control using a dc-to-dc boost converter circuit. This circuit reduces power consumption compared with standard designs.

In standard current input module designs, the load resistor values can range from typically $50 \Omega$ to $750 \Omega$. Output module systems must source enough voltage to meet the compliance voltage requirement across the full range of load resistor values. For example, in a 4 mA to 20 mA loop when driving 20 mA , a compliance voltage of $>15 \mathrm{~V}$ is required. When driving 20 mA into a $50 \Omega$ load, a compliance voltage of only 1 V is required.

The AD5735 circuitry senses the output voltage and regulates this voltage to meet the compliance requirements plus a small headroom voltage. The AD5735 is capable of driving up to 24 mA through a $1 \mathrm{k} \Omega$ load.

## DC-TO-DC CONVERTERS

The AD5735 contains four independent dc-to-dc converters. These are used to provide dynamic control of the $V_{\text {Boost_x }}$ supply voltage for each channel (see Figure 71). Figure 77 shows the discrete components needed for the dc-to-dc circuitry, and the following sections describe component selection and operation of this circuitry.


Figure 77. DC-to-DC Circuit
Table 36. Recommended Components for a DC-to-DC Converter

| Symbol | Component | Value | Manufacturer |
| :--- | :--- | :--- | :--- |
| LDCDC | XAL4040-103 | $10 \mu \mathrm{H}$ | Coilcraft $^{\oplus}$ |
| CDCDC | GRM32ER71H475KA88L | $4.7 \mu \mathrm{~F}$ | Murata |
| D DCDC | PMEG3010BEA | $0.285 \mathrm{~V}_{\mathrm{F}}$ | NXP |

It is recommended that a $10 \Omega, 100 \mathrm{nF}$ low-pass RC filter be placed after $\mathrm{C}_{\mathrm{DCDC}}$. This filter consumes a small amount of power but reduces the amount of ripple on the $\mathrm{V}_{\text {Boost_x }}$ supply.

## DC-to-DC Converter Operation

The on-board dc-to-dc converters use a constant frequency, peak current mode control scheme to step up an $\mathrm{AV}_{\mathrm{CC}}$ input of 4.5 V to 5.5 V to drive the AD5735 output channel. These converters are designed to operate in discontinuous conduction mode with a duty cycle of $<90 \%$ typical. Discontinuous conduction mode refers to a mode of operation where the inductor current goes to zero for an appreciable percentage of the switching cycle. The dc-to-dc converters are nonsynchronous; that is, they require an external Schottky diode.

## DC-to-DC Converter Output Voltage

When a channel current output is enabled, the converter regulates the $\mathrm{V}_{\text {Boost_x }}$ supply to $7.4 \mathrm{~V}( \pm 5 \%)$ or ( $\mathrm{Iout} \times \mathrm{R}_{\text {LOAD }}+$ Headroom) , whichever is greater (see Figure 51 for a plot of headroom supplied vs. output current). In voltage output mode with the output disabled, the converter regulates the $V_{\text {boost_x }}$ supply to $15 \mathrm{~V}( \pm 5 \%)$. In current output mode with the output disabled, the converter regulates the $\mathrm{V}_{\text {Boost_x }}$ supply to $7.4 \mathrm{~V}( \pm 5 \%)$.
Within a channel, the Vout_x and Iout_x stages share a common V $_{\text {boost_x }}$ supply; therefore, the outputs of the Iout_x and Vout_x stages can be tied together (see the Voltage and Current Output Pins on the Same Terminal section).

## DC-to-DC Converter Settling Time

In current output mode, the settling time for a step greater than $\sim 1 \mathrm{~V}\left(\right.$ Iout $\left.\times \mathrm{R}_{\text {LOAD }}\right)$ is dominated by the settling time of the dc-todc converter. The exception to this is when the required voltage at the Iout_x pin plus the compliance voltage is below $7.4 \mathrm{~V}( \pm 5 \%)$. Figure 47 shows a typical plot of the output settling time. This plot is for a $1 \mathrm{k} \Omega$ load. The settling time for smaller loads is faster. The settling time for current steps less than 24 mA is also faster.

## DC-to-DC Converter $V_{\text {MAX }}$ Functionality

The maximum $V_{\text {Boost_x }}$ voltage is set in the dc-to-dc control register ( $23 \mathrm{~V}, 24.5 \mathrm{~V}, 27 \mathrm{~V}$, or 29.5 V ; see Table 28). When the maximum voltage is reached, the dc-to-dc converter is disabled, and the $V_{\text {boost_x }}$ voltage is allowed to decay by $\sim 0.4 \mathrm{~V}$. After the $\mathrm{V}_{\text {boost_x }}$ voltage decays by $\sim 0.4 \mathrm{~V}$, the dc-to-dc converter is reenabled, and the voltage ramps up again to $\mathrm{V}_{\mathrm{max}}$, if still required. This operation is shown in Figure 78.


Figure 78. Operation on Reaching $V_{\text {MAX }}$
As shown in Figure 78, the DC-DCx bit in the status register is asserted when the AD5735 ramps up to the $\mathrm{V}_{\text {max }}$ value but is deasserted when the voltage decays to $\mathrm{V}_{\mathrm{max}}-\sim 0.4 \mathrm{~V}$.

## DC-to-DC Converter On-Board Switch

The AD5735 contains a $0.425 \Omega$ internal switch. The switch current is monitored on a pulse-by-pulse basis and is limited to 0.8 A peak current.

## DC-to-DC Converter Switching Frequency and Phase

The AD5735 dc-to-dc converter switching frequency can be selected from the dc-to-dc control register (see Table 28). The phasing of the channels can also be adjusted so that the dc-to-dc converters can clock on different edges. For typical applications, a 410 kHz frequency is recommended. At light loads (low output current and small load resistor), the dc-to-dc converter enters a pulse-skipping mode to minimize switching power dissipation.

## DC-to-DC Converter Inductor Selection

For typical 4 mA to 20 mA applications, a $10 \mu \mathrm{H}$ inductor (such as the XAL4040-103 from Coilcraft), combined with a switching frequency of 410 kHz , allows up to 24 mA to be driven into a load resistance of up to $1 \mathrm{k} \Omega$ with an AV CC supply of 4.5 V to 5.5 V. It is important to ensure that the inductor can handle the peak current without saturating, especially at the maximum ambient temperature. If the inductor enters saturation mode, efficiency decreases. The inductance value also drops during saturation and may result in the dc-to-dc converter circuit not being able to supply the required output power.

## DC-to-DC Converter External Schottky Diode Selection

The AD5735 requires an external Schottky diode for correct operation. Ensure that the Schottky diode is rated to handle the maximum reverse breakdown voltage expected in operation and that the maximum junction temperature of the diode is not exceeded. The average current of the diode is approximately equal to the $\mathrm{I}_{\text {LOAD }}$ current. Diodes with larger forward voltage drops result in a decrease in efficiency.

## DC-to-DC Converter Compensation Capacitors

Because the dc-to-dc converter operates in discontinuous conduction mode, the uncompensated transfer function is essentially a single-pole transfer function. The pole frequency of the transfer function is determined by the output capacitance, input and output voltage, and output load of the dc-to-dc converter. The AD5735 uses an external capacitor in conjunction with an internal $150 \mathrm{k} \Omega$ resistor to compensate the regulator loop.
Alternatively, an external compensation resistor can be used in series with the compensation capacitor by setting the DC-DC comp bit in the dc-to-dc control register (see Table 28). In this case, a resistor of $\sim 50 \mathrm{k} \Omega$ is recommended. The advantages of this configuration are described in the AIcc Supply RequirementsSlewing section. For typical applications, a 10 nF dc-to-dc compensation capacitor is recommended.

## DC-to-DC Converter Input and Output Capacitor Selection

The output capacitor affects the ripple voltage of the dc-to-dc converter and indirectly limits the maximum slew rate at which the channel output current can rise. The ripple voltage is caused by a combination of the capacitance and the equivalent series resistance (ESR) of the capacitor. For typical applications, a ceramic capacitor of $4.7 \mu \mathrm{~F}$ is recommended. Larger capacitors or parallel capacitors improve the ripple at the expense of reduced slew rate. Larger capacitors also affect the current requirements of the $\mathrm{AV}_{\mathrm{CC}}$ supply while slewing (see the $\mathrm{AI}_{\mathrm{CC}}$ Supply Requirements-Slewing section). The capacitance at the output of the dc-to-dc converter should be $>3 \mu \mathrm{~F}$ under all operating conditions.
The input capacitor provides much of the dynamic current required for the dc-to-dc converter and should be a low ESR component. For the AD5735, a low ESR tantalum or ceramic capacitor of $10 \mu \mathrm{~F}$ is recommended for typical applications. Ceramic capacitors must be chosen carefully because they can exhibit a large sensitivity to dc bias voltages and temperature. X5R or X7R dielectrics are preferred because these capacitors remain stable over wider operating voltage and temperature ranges. Care must be taken if selecting a tantalum capacitor to ensure a low ESR value.

## Alcc SUPPLY REQUIREMENTS—STATIC

The dc-to-dc converter is designed to supply a $V_{\text {Boost_x }}$ voltage of

$$
\begin{equation*}
V_{B O O S T_{-} x}=I_{\text {out }} \times R_{\text {LOAD }}+\text { Headroom } \tag{2}
\end{equation*}
$$

See Figure 51 for a plot of headroom supplied vs. output current. Therefore, for a fixed load and output voltage, the output current of the dc-to-dc converter can be calculated by the following formula:

$$
\begin{equation*}
A I_{C C}=\frac{\text { Power Out }}{\text { Efficiency } \times A V_{C C}}=\frac{I_{\text {OUT }} \times V_{\text {BOOST }}}{\eta_{V_{\text {Boost }}} \times A V_{C C}} \tag{3}
\end{equation*}
$$

where:
$I_{\text {OUT }}$ is the output current from Iout_x in amperes.
$\eta_{V_{\text {BOOST }}}$ is the efficiency at $V_{\text {Boost_x }}$ as a fraction (see Figure 53 and Figure 54).

## Alcc ${ }_{\text {CC }}$ SUPPLY REQUIREMENTS—SLEWING

The AIcc current requirement while slewing is greater than in static operation because the output power increases to charge the output capacitance of the dc-to-dc converter. This transient current can be quite large (see Figure 79), although the methods described in the Reducing $\mathrm{AI}_{\mathrm{CC}}$ Current Requirements section can reduce the requirements on the $\mathrm{AV}_{\mathrm{CC}}$ supply.
If not enough $\mathrm{AI}_{\mathrm{CC}}$ current can be provided, the $\mathrm{AV}_{\mathrm{CC}}$ voltage drops. Due to this $\mathrm{AV}_{\mathrm{CC}}$ drop, the $\mathrm{AI}_{\mathrm{CC}}$ current required for slewing increases further, causing the voltage at $A V_{C C}$ to drop further (see Equation 3). In this case, the $V_{\text {boost }}$ x voltage and, therefore, the output voltage, may never reach their intended values. Because the $A V_{C C}$ voltage is common to all channels, this voltage drop may also affect other channels.


Figure 79. Alcc Current vs. Time for 24 mA Step Through $1 \mathrm{k} \Omega$ Load with Internal Compensation Resistor

## Reducing Alcc Current Requirements

Two main methods can be used to reduce the $\mathrm{AI}_{\mathrm{CC}}$ current requirements. One method is to add an external compensation resistor, and the other is to use slew rate control. These methods can be used together.

## Adding an External Compensation Resistor

A compensation resistor can be placed at the COMP ${ }_{\text {DCDC_x }}$ pin in series with the 10 nF compensation capacitor. A $51 \mathrm{k} \Omega$ external compensation resistor is recommended. This compensation increases the slew time of the current output but reduces the $\mathrm{AI}_{\mathrm{CC}}$ transient current requirements. Figure 80 shows a plot of $\mathrm{AI}_{\mathrm{CC}}$ current for a 24 mA step through a $1 \mathrm{k} \Omega$ load when using a $51 \mathrm{k} \Omega$ compensation resistor. The compensation resistor reduces the current requirements through smaller loads even further, as shown in Figure 81.


Figure 80. Alcc Current vs. Time for 24 mA Step Through $1 \mathrm{k} \Omega$ Load with External $51 \mathrm{k} \Omega$ Compensation Resistor


Figure 81. Alcc Current vs. Time for 24 mA Step Through $500 \Omega$ Load with External $51 \mathrm{k} \Omega$ Compensation Resistor

## Using Slew Rate Control

Using slew rate control can greatly reduce the current requirements of the $\mathrm{AV}_{\mathrm{CC}}$ supply, as shown in Figure 82.


Figure 82. Alcc Current vs. Time for $24 m A$ Step Through $1 \mathrm{k} \Omega$ Load with Slew Rate Control

When using slew rate control, it is important to remember that the output cannot slew faster than the dc-to-dc converter. The dc-to-dc converter slews slowest at higher currents through large loads (for example, $1 \mathrm{k} \Omega$ ). The slew rate is also dependent on the configuration of the dc-to-dc converter. Two examples of the dc-to-dc converter output slew are shown in Figure 80 and Figure 81. ( $\mathrm{V}_{\text {boost }}$ corresponds to the output voltage of the dc-to-dc converter.)

## APPLICATIONS INFORMATION

## VOLTAGE AND CURRENT OUTPUT PINS ON THE SAME TERMINAL

When using a channel of the AD5735, the current and voltage output pins can be connected to two separate terminals or tied together and connected to a single terminal. The two output pins can be tied together because only the voltage output or the current output can be enabled at any one time. When the current output is enabled, the voltage output is in tristate mode, and when the voltage output is enabled, the current output is in tristate mode. When the two output pins are tied together, the POC pin must be tied low and the POC bit in the main control register set to 0 , or, if the POC pin is tied high, the POC bit in the main control register must be set to 1 before the current output is enabled.

As shown in the Absolute Maximum Ratings section, the output tolerances are the same for both the voltage and current output pins. The $+V_{\text {Sense_x }}$ and $-V_{\text {sense_x }}$ connections are buffered so that current leakage into these pins is negligible when the part is operated in current output mode.

## CURRENT OUTPUT MODE WITH INTERNAL Rset

When using the internal Rset resistor in current output mode, the output is significantly affected by how many other channels using the internal $\mathrm{R}_{\text {SET }}$ are enabled and by the dc crosstalk from these channels. The internal Rset specifications in Table 1 are for all four channels enabled with the internal $R_{\text {SET }}$ selected and outputting the same code.
For every channel enabled with the internal $\mathrm{R}_{\text {SET }}$, the offset error decreases. For example, with one current output enabled using the internal $\mathrm{R}_{\text {sEt }}$, the offset error is $0.075 \%$ FSR. This value decreases proportionally as more current channels are enabled; the offset error is $0.056 \%$ FSR on each of two channels, $0.029 \%$ FSR on each of three channels, and $0.01 \%$ FSR on each of four channels. Similarly, the dc crosstalk when using the internal $\mathrm{R}_{\text {SET }}$ is proportional to the number of current output channels enabled with the internal $\mathrm{R}_{\text {set. }}$. For example, with the measured channel at 0x8000 and another channel going from zero to full scale, the dc crosstalk is $-0.011 \%$ FSR. With two other channels going from zero to full scale, the dc crosstalk is $-0.019 \%$ FSR, and with all three other channels going from zero to full scale, it is $-0.025 \%$ FSR.

For the full-scale error measurement in Table 1, all channels are at $0 \times$ FFFFF. This means that as any channel goes to zero scale, the full-scale error increases due to the dc crosstalk. For example,
with the measured channel at 0xFFFF and three channels at zero scale, the full-scale error is $0.025 \%$ FSR. Similarly, if only one channel is enabled in current output mode with the internal $\mathrm{R}_{\mathrm{SET}}$, the full-scale error is $0.025 \%$ FSR $+0.075 \%$ FSR $=0.1 \%$ FSR.

## PRECISION VOLTAGE REFERENCE SELECTION

To achieve the optimum performance from the AD5735 over its full operating temperature range, a precision voltage reference must be used. Care should be taken with the selection of the precision voltage reference. The voltage applied to the reference inputs is used to provide a buffered reference for the DAC cores. Therefore, any error in the voltage reference is reflected in the outputs of the AD5735.
Four possible sources of error must be considered when choosing a voltage reference for high accuracy applications: initial accuracy, long-term drift, temperature coefficient of the output voltage, and output voltage noise.

Initial accuracy error on the output voltage of an external reference can lead to a full-scale error in the DAC. Therefore, to minimize these errors, a reference with a low initial accuracy error specification is preferred. Choosing a reference with an output trim adjustment, such as the ADR435, allows a system designer to trim out system errors by setting the reference voltage to a voltage other than the nominal. The trim adjustment can be used at any temperature to trim out any error.

Long-term drift is a measure of how much the reference output voltage drifts over time. A reference with a tight long-term drift specification ensures that the overall solution remains relatively stable over its entire lifetime.
The temperature coefficient of the reference output voltage affects INL, DNL, and TUE. A reference with a tight temperature coefficient specification should be chosen to reduce the dependence of the DAC output voltage on ambient temperature.

In high accuracy applications, which have a relatively low noise budget, reference output voltage noise must be considered. Choosing a reference with as low an output noise voltage as practical for the system resolution required is important. Precision voltage references such as the ADR 435 (XFET ${ }^{\ominus}$ design) produce low output noise in the 0.1 Hz to 10 Hz bandwidth. However, as the circuit bandwidth increases, filtering the output of the reference may be required to minimize the output noise.

Table 37. Recommended Precision Voltage References

| Part No. | Initial Accuracy <br> (mV Maximum) | Long-Term Drift <br> (ppm Typical) | Temperature Coefficient <br> (ppm/ ${ }^{\circ}$ C Maximum) | $\mathbf{0 . 1} \mathbf{~ H z ~ t o ~ 1 0 ~ H z ~ N o i s e ~}$ <br> $(\boldsymbol{\mu V}$ p-p Typical) |
| :--- | :--- | :--- | :--- | :--- |
| ADR445 | $\pm 2$ | 50 | 3 | 2.25 |
| ADR02 | $\pm 3$ | 50 | 3 | 10 |
| ADR435 | $\pm 2$ | 40 | 3 | 8 |
| ADR395 | $\pm 5$ | 50 | 9 | 8 |
| AD586 | $\pm 2.5$ | 15 | 10 | 4 |

## DRIVING INDUCTIVE LOADS

When driving inductive or poorly defined loads, a capacitor may be required between the Iout_x pin and the AGND pin to ensure stability. A $0.01 \mu \mathrm{~F}$ capacitor between Iout_x and AGND ensures stability of a load of 50 mH . The capacitive component of the load may cause slower settling, although this may be masked by the settling time of the AD5735. There is no maximum capacitance limit for the current output of the AD5735.

## TRANSIENT VOLTAGE PROTECTION

The AD5735 contains ESD protection diodes that prevent damage from normal handling. The industrial control environment can, however, subject I/O circuits to much higher transients. To protect the AD5735 from excessively high voltage transients, external power diodes and a surge current limiting resistor $\left(R_{P}\right)$ are required, as shown in Figure 83. A typical value for $\mathrm{R}_{\mathrm{p}}$ is $10 \Omega$. The two protection diodes and the resistor $\left(\mathrm{R}_{\mathrm{P}}\right)$ must have appropriate power ratings.


Figure 83. Output Transient Voltage Protection
Further protection can be provided using transient voltage suppressors (TVSs), also referred to as transorbs. These components are available as unidirectional suppressors, which protect against positive high voltage transients, and as bidirectional suppressors, which protect against both positive and negative high voltage transients. Transient voltage suppressors are available in a wide range of standoff and breakdown voltage ratings. The TVS should be sized with the lowest breakdown voltage possible while not conducting in the functional range of the current output.
It is recommended that all field connected nodes be protected. The voltage output node can be protected with a similar circuit, where D 2 and the transorb are connected to $\mathrm{AV}_{\text {ss }}$. For the voltage output node, the $+V_{\text {SENSE_x }}$ pin should also be protected with a large value series resistance to the transorb, such as $5 \mathrm{k} \Omega$. In this way, the Iout_x and Vout_x pins can also be tied together and share the same protection circuitry.

## MICROPROCESSOR INTERFACING

Microprocessor interfacing to the AD5735 is via a serial bus that uses a protocol compatible with microcontrollers and DSP processors. The communication channel is a 3 -wire minimum interface consisting of a clock signal, a data signal, and a latch signal. The AD5735 requires a 24 -bit data-word with data valid on the falling edge of SCLK.
The DAC output update is initiated either on the rising edge of $\overline{\text { LDAC }}$ or, if $\overline{\text { LDAC }}$ is held low, on the rising edge of $\overline{\text { SYNC. The }}$ contents of the registers can be read using the readback function.

## AD5735-to-ADSP-BF527 Interface

The AD5735 can be connected directly to the SPORT interface of the ADSP-BF527, an Analog Devices, Inc., Blackfin ${ }^{\circledR}$ DSP. Figure 84 shows how the SPORT interface can be connected to control the AD5735.


Figure 84. AD5735-to-ADSP-BF527 SPORT Interface

## LAYOUT GUIDELINES

## Grounding

In any circuit where accuracy is important, careful consideration of the power supply and ground return layout helps to ensure the rated performance. The printed circuit board on which the AD5735 is mounted should be designed so that the analog and digital sections are separated and confined to certain areas of the board. If the AD5735 is in a system where multiple devices require an AGND-to-DGND connection, the connection should be made at one point only. The star ground point should be established as close as possible to the device.
The GNDSW $x$ pin and the ground connection for the $\mathrm{AV}_{\mathrm{CC}}$ supply are referred to as PGND. PGND should be confined to certain areas of the board, and the PGND-to-AGND connection should be made at one point only.

## Supply Decoupling

The AD5735 should have ample supply bypassing of $10 \mu \mathrm{~F}$ in parallel with $0.1 \mu \mathrm{~F}$ on each supply, located as close to the package as possible, ideally right up against the device. The $10 \mu \mathrm{~F}$ capacitors are the tantalum bead type. The $0.1 \mu \mathrm{~F}$ capacitors should have low effective series resistance (ESR) and low effective series inductance (ESL), such as the common ceramic types, which provide a low impedance path to ground at high frequencies to handle transient currents due to internal logic switching.

## Traces

The power supply lines of the AD5735 should use as large a trace as possible to provide low impedance paths and reduce the effects of glitches on the power supply line. Fast switching signals such as clocks should be shielded with digital ground to prevent radiating noise to other parts of the board and should never be run near the reference inputs. A ground line routed between the SDIN and SCLK traces helps reduce crosstalk between them (not required on a multilayer board that has a separate ground plane, but separating the lines helps). It is essential to minimize noise on the REFIN line because it couples through to the DAC output.
Avoid crossover of digital and analog signals. Traces on opposite sides of the board should run at right angles to each other to reduce the effects of feedthrough on the board. A microstrip technique is by far the best method, but it is not always possible with a double-sided board. In this technique, the component side of the board is dedicated to ground plane, and signal traces are placed on the solder side.

## DC-to-DC Converters

To achieve high efficiency, good regulation, and stability, a well-designed printed circuit board layout is required.
Follow these guidelines when designing printed circuit boards (see Figure 77):

- Keep the low ESR input capacitor, $\mathrm{C}_{\mathrm{IN}}$, close to $\mathrm{AV}_{\mathrm{CC}}$ and PGND.
- Keep the high current path from $\mathrm{C}_{\text {IN }}$ through the inductor ( $\mathrm{L}_{\mathrm{DCDC}}$ ) to $\mathrm{SW}_{\mathrm{x}}$ and PGND as short as possible.
- Keep the high current path from $\mathrm{C}_{\text {IN }}$ through the inductor ( $\mathrm{L}_{\mathrm{DCDC}}$ ), the diode ( $\mathrm{D}_{\mathrm{DCDC}}$ ), and the output capacitor $\left(\mathrm{C}_{\mathrm{DCDC}}\right)$ as short as possible.
- Keep high current traces as short and as wide as possible. The path from $\mathrm{C}_{\mathrm{IN}}$ through the inductor ( $\mathrm{L}_{\mathrm{DCDC}}$ ) to $\mathrm{SW}_{\mathrm{x}}$ and PGND should be able to handle a minimum of 1 A .
- Place the compensation components as close as possible to the $\mathrm{COMP}_{\mathrm{DCDC}_{-} \mathrm{x}}$ pin.
- Avoid routing high impedance traces near any node connected to $\mathrm{SW}_{\mathrm{x}}$ or near the inductor to prevent radiated noise injection.


## GALVANICALLY ISOLATED INTERFACE

In many process control applications, it is necessary to provide an isolation barrier between the controller and the unit being controlled to protect and isolate the controlling circuitry from any hazardous common-mode voltages that may occur. The Analog Devices iCoupler ${ }^{\oplus}$ products can provide voltage isolation in excess of 2.5 kV . The serial loading structure of the AD5735 makes it ideal for isolated interfaces because the number of interface lines is kept to a minimum. Figure 85 shows a 4 -channel isolated interface to the AD5735 using an ADuM1411. For more information, visit www.analog.com.


Figure 85. 4-Channel Isolated Interface to the AD5735

## OUTLINE DIMENSIONS



## ORDERING GUIDE

| Model $^{1}$ | Resolution (Bits) | Temperature Range | Package Description | Package Option |
| :--- | :--- | :--- | :--- | :--- |
| AD5735ACPZ | 12 | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | 64 -Lead LFCSP_VQ | CP-64-3 |
| AD5735ACPZ-REEL7 | 12 | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | 64-Lead LFCSP_VQ | CP-64-3 |

${ }^{1} Z=$ RoHS Compliant Part.


[^0]:    ${ }^{1}$ Temperature range: $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$; typical at $+25^{\circ} \mathrm{C}$.
    ${ }^{2}$ Guaranteed by design and characterization; not production tested.
    ${ }^{3}$ For current outputs with internal Rset $^{2}$, the offset, full-scale, and TUE measurements exclude dc crosstalk. The measurements are made with all four channels enabled and loaded with the same code.
    ${ }^{4}$ See the Current Output Mode with Internal $\mathrm{R}_{\text {SET }}$ section for more information about dc crosstalk.
    ${ }^{5}$ Efficiency plots in Figure 53 through Figure 56 include the I Iооот quiescent current.

[^1]:    ${ }^{1}$ Guaranteed by design and characterization; not production tested.

