LOW-COST ${ }^{2} \mathrm{C}$ CONTROLLED DEFLECTION PROCESSOR FOR MULTISYNC MONITOR

## FEATURES

## General

- ${ }^{2} \mathrm{C}$-BUS-CONTROLLED DEFLECTION PROCESSOR DEDICATED FOR LOW-END CRT MONITORS
- SINGLE SUPPLY VOLTAGE 12V
- VERY LOW JITTER
- DC/DC CONVERTER CONTROLLER
- ADVANCED EW DRIVE
- AUTOMATIC MULTISTANDARD SYNCHRONIZATION
- DYNAMIC CORRECTION WAVEFORM OUTPUT
- X-RAY PROTECTION AND SOFT-START \& STOP ON HORIZONTAL AND DC/DC DRIVE OUTPUTS


## Horizontal section

- 150 kHz maximum frequency
- Corrections of geometric asymmetry: Pin cushion asymmetry, Parallelogram
- Tracking of asymmetry corrections with vertical size and position
- Horizontal moiré cancellation output


## Vertical section

- 200 Hz maximum frequency
- Vertical ramp for DC-coupled output stage with adjustments of: C-correction, S-correction for super-flat CRT, Vertical size, Vertical position
- Vertical moiré cancellation through vertical ramp waveform
- Compensation of vertical breathing with EHT variation


## EW section

- Symmetrical geometry corrections: Pin cushion, Keystone
- Horizontal size adjustment
- Tracking of EW waveform with Vertical size and position and adaptation to frequency
- Compensation of horizontal breathing through EW waveform


## Dynamic correction section

- Vertical dynamic correction waveform output for dynamic corrections like focus, brightness uniformity, ...
- Fixed on screen by means of tracking system


## DC/DC controller section

- Step-up and step-down conversion modes
- External sawtooth configuration
- Synchronization on hor. frequency with phase selection
- Selectable polarity of drive signal


## DESCRIPTION

The TDA9115 is a monolithic integrated circuit assembled in a 32-pin shrink dual-in-line plastic package. This IC controls all the functions related to horizontal and vertical deflection in multimode or multi-frequency computer display monitors.
The device only requires very few external components.
Combined with other ST components dedicated for CRT monitors (microcontroller, video preamplifier, video amplifier, OSD controller) the TDA9115 allows fully $1^{2} C$ bus-controlled computer display monitors to be built with a reduced number of external components.


SHRINK 32 (Plastic Package) ORDER CODE: TDA9115

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## 1 - PIN CONFIGURATION




## 3 - PIN FUNCTION REFERENCE

| Pin | Name | Function |
| :---: | :---: | :---: |
| 1 | H/HVSyn | TTL compatible Horizontal / Horizontal and Vertical Sync. input |
| 2 | VSyn | TTL compatible Vertical Sync. input |
| 3 | HLckVBk | Horizontal PLL1 Lock detection and Vertical early Blanking composite output |
| 4 | HOscF | High Horizontal Oscillator sawtooth threshold level Filter input |
| 5 | HPLL2C | Horizontal PLL2 loop Capacitive filter input |
| 6 | CO | Horizontal Oscillator Capacitor input |
| 7 | HGND | Horizontal section GrouND |
| 8 | RO | Horizontal Oscillator Resistor input |
| 9 | HPLL1F | Horizontal PLL1 loop Filter input |
| 10 | HPosF | Horizontal Position Filter and soft-start time constant capacitor input |
| 11 | HMoiré | Horizontal Moiré cancellation output |
| 12 | HFly | Horizontal Flyback input |
| 13 | RefOut | Reference voltage Output |
| 14 | BComp | B+ DC/DC error amplifier (Comparator) output |
| 15 | BRegln | Regulation feedback Input of the B+ DC/DC converter controller |
| 16 | BISense | B+ DC/DC converter current (I) Sense input |
| 17 | HEHTIn | Input for compensation of Horizontal amplitude versus EHT variation |
| 18 | VEHTIn | Input for compensation of Vertical amplitude versus EHT variation |
| 19 | VOscF | Vertical Oscillator sawtooth low threshold Filter (capacitor to be connected to VGND) |
| 20 | VAGCCap | Input for storage Capacitor for Automatic Gain Control loop in Vertical oscillator |
| 21 | VGND | Vertical section GrouND |
| 22 | VCap | Vertical sawtooth generator Capacitor |
| 23 | VOut | Vertical deflection drive Output for a DC-coupled output stage |
| 24 | EWOut | E/W Output |
| 25 | XRay | X-Ray protection input |
| 26 | HOut | Horizontal drive Output |
| 27 | GND | Main GrouND |
| 28 | BOut | B+ DC/DC converter controller Output |
| 29 | Vcc | Supply voltage |
| 30 | SCL | $I^{2} \mathrm{C}$ bus Serial CLock Input |
| 31 | SDA | $1^{2} \mathrm{C}$ bus Serial DAta input/output |
| 32 | VDyCor | Vertical Dynamic Correction output |

## 4 - QUICK REFERENCE DATA

| Characteristic | Value | Unit |
| :---: | :---: | :---: |
|  |  |  |
| Package | SDIP 32 |  |
| Supply voltage | 12 | V |
| Supply current | 55 | mA |
| Application category | Low-end |  |
| Means of control/Maximum clock frequency | $1^{2} \mathrm{C}$ Bus/400 | kHz |
| EW drive | Yes |  |
| DC/DC convertor controller | Yes |  |
| Morizontal section |  |  |
| Frequency range | 15 to 150 | kHz |
| Autosync frequency ratio (can be enlarged in application) | 4.28 |  |
| Positive/Negative polarity of horizontal sync signal/Automatic adaptation | Yes/Yes/Yes |  |
| Duty cycle of the drive signal | 48 | \% |
| Position adjustment range with respect to H period | $\pm 11$ | \% |
| Soft start/Soft stop feature | Yes/Yes |  |
| Hardware/Software PLL lock indication | Yes/No |  |
| Parallelogram | Yes |  |
| Pin cushion asymmetry correction (also called Side pin balance) | Yes |  |
| Top/Bottom/Common corner asymmetry correction | No/No/No |  |
| Tracking of asymmetry corrections with vertical size \& position | Yes |  |
| Horizontal moiré cancellation (ext.) for Combined/Separated architecture | Yes/Yes |  |
| Vertical section/.......... |  |  |
| Frequency range | 35 to 200 | Hz |
| Autosync frequency range (150nF at VCap and 470nF at VAGCCap) | 50 to 180 | Hz |
| Positive/Negative polarity of vertical sync signal/Automatic adaptation | Yes/Yes/Yes |  |
| S-correction/C-correction/Super-flat tube characteristic | Yes/Yes/Yes |  |
| Vertical size/Vertical position adjustment | Yes/Yes |  |
| Vertical moiré cancellation (internal) | Yes |  |
| Vertical breathing compensation | Yes |  |
| EW/ sectionת».\% |  |  |
| Pin cushion correction | Yes |  |
| Keystone correction | Yes |  |
| Top/Bottom/Common corner correction | No/No/No |  |
| Horizontal size adjustment | Yes |  |
| Tracking of EW waveform with Frequency/Vertical size \& position | Yes/Yes |  |
| Breathing compensation on EW waveform | Yes |  |
| Dynamic correction section (dyn. focus, dyn. brightness...) |  |  |
| Vertical dynamic correction output VDyCor | Yes |  |
| Horizontal dynamic correction output | No |  |
| Composite HV dynamic correction output | No |  |
| Tracking of horizontal waveform with Horizontal size/EHT | No/No |  |
| Tracking of vertical waveform with V. size \& position | Yes |  |
| DCFDe controller section..... |  |  |
| Step-up/Step-down conversion mode | Yes/Yes |  |
| Internal/External sawtooth configuration | No/Yes |  |
| Bus-controlled output voltage | No |  |
| Soft start/Soft stop feature | Yes/Yes |  |
| Positive(N-MOS)/Negative(P-MOS) polarity of BOut signal | Yes/Yes |  |

## 5 - ABSOLUTE MAXIMUM RATINGS

All voltages are given with respect to ground.
Currents flowing from the device (sourced) are signed negative. Currents flowing to the device are signed positive.

| Symbol | Parameter | Value |  | Unit |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Min | Max |  |
| $\mathrm{V}_{\mathrm{CC}}$ | Supply voltage (pin Vcc) | -0.4 | 13.5 | V |
| $V_{\text {(pin) }}$ | Pins HEHTIn, VEHTIn, XRay, HOut, BOut <br> Pins H/HVSyn, VSyn, SCL, SDA <br> Pins HLckVBk, CO, RO, HPLL1F, HPosF, HMoiré, BRegln, BI- <br> Sense, VAGCCap, VCap, VDyCor, HOscF, VOscF <br> Pin HPLL2C <br> Pin HFly | $\begin{aligned} & \hline-0.4 \\ & -0.4 \\ & -0.4 \\ & -0.4 \\ & -0.4 \end{aligned}$ | $\begin{gathered} \hline V_{\mathrm{CC}} \\ 5.5 \\ \mathrm{~V}_{\text {RefO }} \\ V_{\text {Refo }} / 2 \\ V_{\text {Refo }} \end{gathered}$ | $\begin{aligned} & \hline \mathrm{V} \\ & \mathrm{~V} \\ & \mathrm{~V} \\ & \mathrm{~V} \\ & \mathrm{~V} \end{aligned}$ |
| $\mathrm{V}_{\text {ESD }}$ | ESD susceptibility (human body model: discharge of 100 pF through $1.5 \mathrm{k} \Omega$ ) | -2000 | 2000 | V |
| $\mathrm{T}_{\text {stg }}$ | Storage temperature | -40 | 150 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\mathrm{j}}$ | Junction temperature |  | 150 | ${ }^{\circ} \mathrm{C}$ |

## 6 - ELECTRICAL PARAMETERS AND OPERATING CONDITIONS

Medium (middle) value of an $I^{2} C$ Bus control or adjustment register composed of bits $\mathrm{D} 0, \mathrm{D} 1, \ldots, \mathrm{Dn}$ is the one having Dn at " 1 " and all other bits at " 0 ". Minimum value is the one with all bits at 0 , maximum value is the one with all at "1".

Currents flowing from the device (sourced) are signed negative. Currents flowing to the device are signed positive.
$\mathrm{T}_{\mathrm{H}}$ is period of horizontal deflection.

### 6.1 THERMAL DATA

| Symbol | Parameter | Value |  |  | Unit |
| :---: | :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| $\mathrm{T}_{\text {amb }}$ | Operating ambient temperature | 0 |  | 70 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{R}_{\text {th }(j-a)}$ | Junction-ambience thermal resistance |  | 65 |  | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

### 6.2 SUPPLY AND REFERENCE VOLTAGES

$\mathrm{T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$

| Symbol | Parameter | Test Conditions | Value |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. |  |
| $\mathrm{V}_{\mathrm{CC}}$ | Supply voltage at Vcc pin |  | 10.8 | 12 | 13.2 | V |
| $\mathrm{I}_{\mathrm{CC}}$ | Supply current to Vcc pin | $\mathrm{V}_{C C}=12 \mathrm{~V}$ |  | 55 |  | mA |
| $\mathrm{V}_{\text {Refo }}$ | Reference output voltage at RefOut pin | $\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{I}_{\text {RefO }}=-2 \mathrm{~mA}$ | 7.4 | 8 | 8.6 | V |
| $\mathrm{I}_{\text {RefO }}$ | Current sourced by RefOut output |  | -5 |  | 0 | mA |

### 6.3 SYNCHRONIZATION INPUTS

$\mathrm{Vcc}=12 \mathrm{~V}, \mathrm{~T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$

| Symbol | Parameter | Test Conditions | Value |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. |  |
| $\mathrm{V}_{\text {Loh/HVSyn }}$ | LOW level voltage on H/HVSyn |  | 0 |  | 0.8 | V |
| $\mathrm{V}_{\text {HiH/HVSyn }}$ | HIGH level voltage on H/HVSyn |  | 2.2 |  | 5 | V |
| $\mathrm{V}_{\text {LoVSyn }}$ | LOW level voltage on VSyn |  | 0 |  | 0.8 | V |
| $\mathrm{V}_{\text {HivSyn }}$ | HIGH level voltage on VSyn |  | 2.2 |  | 5 | V |
| $\mathrm{R}_{\text {PdSyn }}$ | Internal pull-down on H/HVSyn, VSyn |  | 100 | 175 | 250 | $\mathrm{k} \Omega$ |
| $t_{\text {PulseHSyn }}$ | H sync. pulse duration on H/HVSyn pin |  | 0.5 |  |  | $\mu \mathrm{s}$ |
| $\mathrm{t}_{\text {Pulse }}$ HSyn $/ \mathrm{T}_{\mathrm{H}}$ | Proportion of H sync pulse to H period | Pin H/HVSyn |  |  | 0.2 |  |
| $\mathrm{t}_{\text {PulseVSyn }}$ | V sync. pulse duration | Pins H/HVSyn, VSyn | 0.5 |  | 750 | $\mu \mathrm{s}$ |
| $\mathrm{t}_{\text {PulseVSyn }} / \mathrm{T}_{\mathrm{V}}$ | Proportion of V sync pulse to V period | Pins H/HVSyn, VSyn |  |  | 0.15 |  |
| $t_{\text {extr }} / \mathrm{T}_{\mathrm{H}}$ | Proportion of sync pulse length to H period for extraction as V sync pulse | Pin H/HVSyn, <br> cap. on pin CO $=820 \mathrm{pF}$ | 0.21 | 0.3 |  |  |
| $\mathrm{t}_{\text {HPolDet }}$ | Polarity detection time (after change) | Pin H/HVSyn | 0.75 |  |  | ms |

### 6.4 HORIZONTAL SECTION

$\mathrm{Vcc}=12 \mathrm{~V}, \mathrm{~T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$

| Symbol | Parameter | Test Conditions | Value |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. |  |
| PLL1 |  |  |  |  |  |  |
| $\mathrm{I}_{\mathrm{RO}}$ | Current load on RO pin |  |  |  | 1.5 | mA |
| $\mathrm{C}_{\mathrm{CO}}$ | Capacitance on CO pin |  | 390 |  |  | pF |
| ${ }_{\mathrm{f} \mathrm{HO}}$ | Frequency of hor. oscillator |  |  |  | 150 | kHz |
| ${ }^{\mathrm{H} \mathrm{O}}$ (0) | Free-running frequency of hor. oscill. ${ }^{(1)}$ | $\mathrm{R}_{\mathrm{RO}}=5.23 \mathrm{k} \Omega, \mathrm{C}_{\mathrm{CO}}=820 \mathrm{pF}$ | 27 | 28.5 | 29.9 | kHz |
| ${ }_{\text {f HoCapt }}$ | Hor. PLL1 capture frequency ${ }^{(4)}$ | $\mathrm{f}_{\mathrm{HO}(0)}=28.5 \mathrm{kHz}$ | 29 |  | 122 | kHz |
| $\frac{\Delta f^{\text {HO(0) }}}{}{ }^{\text {f }}$ | Temperature drift of free-running freq. ${ }^{(3)}$ |  |  | -150 |  | ppm $/{ }^{\circ} \mathrm{C}$ |
| $\Delta \mathrm{f}_{\mathrm{HO}} / \Delta \mathrm{V}_{\mathrm{HO}}$ | Average horizontal oscillator sensitivity | $\mathrm{f}_{\mathrm{HO}(0)}=28.5 \mathrm{kHz}$ |  | 19.6 |  | kHz/V |
| $\mathrm{V}_{\mathrm{HO}}$ | H. oscill. control voltage on pin HPLL1F | $\mathrm{V}_{\text {Refo }}=8 \mathrm{~V}$ | 1.4 |  | 6.0 | V |
| $\mathrm{V}_{\text {HOThrfr }}$ | Threshold on H. oscill. control voltage on HPLL1F pin for tracking of EW with freq. | $\mathrm{V}_{\text {Refo }}=8 \mathrm{~V}$ |  | 5.0 |  | V |
| $V_{\text {HPosF }}$ | Control voltage on HPosF pin | $\begin{array}{\|l} \hline \text { HPOS (Sad01): } \\ 11111111 \mathrm{~b} \\ 10000000 \mathrm{~b} \\ 00000000 \mathrm{~b} \end{array}$ | $\begin{aligned} & 2.60 \\ & 3.30 \\ & 3.85 \end{aligned}$ | $\begin{aligned} & 2.8 \\ & 3.4 \\ & 4.0 \end{aligned}$ | $\begin{aligned} & 3.05 \\ & 3.55 \\ & 4.15 \end{aligned}$ | $\begin{aligned} & V \\ & V \\ & V \end{aligned}$ |
| $\mathrm{V}_{\text {HOThrLo }}$ | Bottom of hor. oscillator sawtooth ${ }^{(6)}$ |  |  | 1.6 |  | V |
| $\mathrm{V}_{\text {HOThrHi }}$ | Top of hor. oscillator sawtooth ${ }^{(6)}$ |  |  | 6.4 |  | V |
| PLL2 |  |  |  |  |  |  |
| $\mathrm{R}_{\ln (\mathrm{HFIy})}$ | Input impedance on HFly input (2) | $\mathrm{V}_{(\text {HFly })}>\mathrm{V}_{\text {ThrHFly }}$ | 300 | 500 | 700 | $\Omega$ |
| $\mathrm{I}_{\text {InHFly }}$ | Current into HFly input | At top of H flyback pulse |  |  | 5 | mA |
| $\mathrm{V}_{\text {ThrHFly }}$ | Voltage threshold on HFly input |  | 0.6 | 0.7 |  | V |
| $\mathrm{V}_{\text {S(0) }}$ | H flyback lock middle point ${ }^{(6)}$ | No PLL2 phase modulation |  | 4.0 |  | V |
| $\mathrm{V}_{\text {BothPLL2C }}$ | Low clamping voltage on HPLL2C pin ${ }^{(5)}$ |  |  | 1.6 |  | V |
| $\mathrm{V}_{\text {TopHPLL2C }}$ | High clamping voltage on HPLL2C pin ${ }^{(5)}$ |  | 3.75 | 4.0 | 4.25 | V |
| $\mathrm{t}_{\mathrm{ph}}(\mathrm{min}) / \mathrm{T}_{\mathrm{H}}$ | Min. advance of H -drive OFF before middle of H flyback ${ }^{(7)}$ | Null asym. correction |  | 0 |  | \% |
| $\mathrm{t}_{\mathrm{ph}}(\mathrm{max}) / \mathrm{T}_{\mathrm{H}}$ | Max. advance of H -drive OFF before middle of H flyback ${ }^{(8)}$ | Null asym. correction |  | 44 |  | \% |
| H-drive output on pin HOul |  |  |  |  |  |  |
| $\mathrm{I}_{\text {HOut }}$ | Current into HOut output | Output driven LOW |  |  | 30 | mA |
| $\mathrm{t}_{\mathrm{Hoff}} / \mathrm{T}_{\mathrm{H}}$ | Duty cycle of H-drive signal | Soft-start/Soft-stop value |  | $\begin{aligned} & 48 \\ & 85 \end{aligned}$ |  | $\begin{aligned} & \% \\ & \% \end{aligned}$ |

## Picture geometry corrections through PLL1 \& PLL2

| $\mathrm{t}_{\mathrm{Hph}} / \mathrm{T}_{\mathrm{H}}$ | H-flyback (center) static phase vs. sync signal (via PLL1), see Figure 7 | $\begin{aligned} & \text { HPOS (Sad01): } \\ & \text { 11111111b } \\ & \text { 00000000b } \end{aligned}$ | $\begin{aligned} & +11 \\ & -11 \end{aligned}$ | \% |
| :---: | :---: | :---: | :---: | :---: |


| Symbol | Parameter | Test Conditions | Value |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. |  |
| $\mathrm{tpCaC} / \mathrm{T}_{\mathrm{H}}$ | Contribution of pin cushion asymmetry correction to phase of H -drive vs. static phase (via PLL2), measured in corners | PCAC (Sad11h) full span VPOS at medium VSIZE at minimum VSIZE at medium VSIZE at maximum |  | $\begin{aligned} & \pm 1.0 \\ & \pm 1.8 \\ & \pm 2.8 \end{aligned}$ |  | $\begin{aligned} & \% \\ & \% \\ & \% \end{aligned}$ |
| $\mathrm{t}_{\text {paralc }} / \mathrm{T}_{\mathrm{H}}$ | Contribution of parallelogram correction to phase of H -drive vs. static phase (via PLL2), measured in corners ${ }^{(9)}$ | PARAL (Sad12h) full span VPOS at medium <br> VSIZE at minimum <br> VSIZE at medium <br> VSIZE at maximum <br> VPOS at max. or min. <br> VSIZE at minimum |  | $\begin{gathered} \pm 1.75 \\ \pm 2.2 \\ \pm 2.8 \\ \pm 1.75 \end{gathered}$ |  | $\begin{aligned} & \% \\ & \% \\ & \% \\ & \% \\ & \% \end{aligned}$ |

Note 1: Frequency at no sync signal condition. For correct operation, the frequency of the sync signal applied must always be higher than the free-running frequency. The application must consider the spread of values of real electrical components in $\mathrm{R}_{\mathrm{RO}}$ and $\mathrm{C}_{\mathrm{CO}}$ positions so as to always meet this condition. The formula to calculate the free-running frequency is $f_{H O(0)}=0.12125 /\left(R_{R O} C_{C O}\right)$
Note 2: Base of NPN transistor with emitter to ground is internally connected on pin HFly through a series resistance of about $500 \Omega$ and a resistance to ground of about $20 \mathrm{k} \Omega$.
Note 3: Evaluated and figured out during the device qualification phase. Informative. Not tested on every single unit.
Note 4: This capture range can be enlarged by external circuitry.
Note 5: The voltage on HPLL2C pin corresponds to immediate phase of leading edge of H -drive signal on HOut pin with respect to internal horizontal oscillator sawtooth. It must be between the two clamping levels given. Voltage equal to one of the clamping values indicates a marginal operation of PLL2 or non-locked state.
Note 6: Internal threshold. See Figure 7.
Note 7: The $t_{\mathrm{ph}}(\mathrm{min}) / T_{\mathrm{H}}$ parameter is fixed by the application. For correct operation of asymmetry corrections through dynamic phase modulation, this minimum must be increased by maximum of the total dynamic phase required in the direction leading to bending of corners to the left. Marginal situation is indicated by reach of $\mathrm{V}_{\text {TopHPLL2C }}$ high clamping level by waveform on pin HPLL2C. Also refer to Note 5 and Figure 7.
Note 8: The $\mathrm{t}_{\mathrm{ph}}(\max ) / T_{\mathrm{H}}$ parameter is fixed by the application. For correct operation of asymmetry corrections through dynamic phase modulation, this maximum must be reduced by maximum of the total dynamic phase required in the direction leading to bending of corners to the right. Marginal situation is indicated by reach of $\mathrm{V}_{\text {BotHPLL2C }}$ low clamping level by waveform on pin HPLL2C. Also refer to Note 5 and Figure 7.
Note 9: All other dynamic phase corrections of picture asymmetry set to their neutral (medium) positions.

### 6.5 VERTICAL SECTION

$\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$

| Symbol | Parameter | Test Conditions | Value |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. |  |


| $\mathrm{R}_{\mathrm{L} \text { (VAGCCap) }}$ | Ext. load resistance on VAGCCap pin ${ }^{(10)}$ | $\Delta \mathrm{V}_{\text {amp }} / \mathrm{V}_{\text {amp }}(\mathrm{R}=\infty) \leq 1 \%$ | 65 |  |  | $\mathrm{M} \Omega$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {VOB }}$ | Sawtooth bottom voltage on VCap pin ${ }^{(11)}$ | No load on VOscF pin ${ }^{(11)}$ | 1.8 | 1.9 | 2.0 | V |
| $\mathrm{V}_{\text {VOT }}$ | Sawtooth top voltage on VCap pin | AGC loop stabilized <br> V sync present No V sync |  | $\begin{gathered} 5 \\ 4.9 \end{gathered}$ |  | $\begin{aligned} & \text { V } \\ & \text { V } \end{aligned}$ |
| tvodis | Sawtooth Discharge time | $\mathrm{C}_{\mathrm{VCap}}=150 \mathrm{nF}$ |  | 80 |  | us |
| $\mathrm{f}_{\mathrm{VO}(0)}$ | Free-running frequency | $\mathrm{C}_{\mathrm{VCap}}=150 \mathrm{nF}$ |  | 100 |  | Hz |
| $\mathrm{f}_{\text {VoCapt }}$ | AGC loop capture frequency | $\mathrm{C}_{\mathrm{VCap}}=150 \mathrm{nF}$ | 50 |  | 185 | Hz |
| $\frac{\Delta \mathrm{V}_{\text {Vodev }}}{\mathrm{V}_{\text {VOamp }}{ }^{(16)}}$ | Sawtooth non-linearity ${ }^{(12)}$ | AGC loop stabilized, ${ }^{(12)}$ |  | 0.5 |  | \% |
| $\frac{\Delta \mathrm{V}_{\text {VOS }} \text { cor }}{}$ | S-correction range | $\begin{aligned} & \hline \text { AGC loop stabilized, }{ }^{(13)} \\ & \mathrm{t}_{\mathrm{VR}}=1 / 4 \mathrm{~T}_{\mathrm{VR}}(15) \\ & \mathrm{t}_{\mathrm{VR}}=3 / 4 \mathrm{~T}_{\mathrm{VR}} \\ & \hline \end{aligned}$ |  | $\begin{aligned} & -5 \\ & +5 \end{aligned}$ |  | $\begin{aligned} & \% \\ & \% \end{aligned}$ |
| $\frac{\Delta \mathrm{V}_{\text {Voc-cor }}}{\mathrm{V}_{\text {Voamp }}}$ | C-correction range | $\begin{aligned} & \text { AGC loop stabilized, }{ }^{(14)} \\ & \mathrm{t}_{\mathrm{VR}}=1 / 2 \mathrm{~T}_{\mathrm{VR}}{ }^{(15)} \\ & \text { CCOR } \mathrm{SadOA}) \text { : } \\ & \times 0000000 \mathrm{~b} \\ & \times 1000000 \mathrm{~b} \\ & \text { x1111111b } \end{aligned}$ |  | -3 0 +3 |  | \% |
| $\frac{\Delta \mathrm{V}_{\text {VOamp }}}{\mathrm{V}_{\text {VOamp }} \cdot \Delta \mathrm{f}_{\text {Vo }}}$ | Frequency drift of sawtooth amplitude ${ }^{(17)(18)}$ | AGC loop stabilized $f_{\text {VOCapt }}{ }^{\text {min }}{ }^{\leq} \mathrm{f}_{\text {VO }} \leq \mathrm{f}_{\text {VOCapt }}($ max $)$ |  | 200 |  | ppm/Hz |

Vertical output drive signal (on pin VOut) $\mathrm{V}_{\text {Retio }}=8 \mathrm{~V}$

| $\mathrm{V}_{\text {mid (VOut) }}$ | Middle point on VOut sawtooth | $\begin{aligned} & \text { VPOS (Sad08): } \\ & \text { x0000000b } \\ & \times 1000000 \mathrm{~b} \\ & \text { x1111111b } \end{aligned}$ | 3.65 | $\begin{aligned} & 3.2 \\ & 3.5 \\ & 3.8 \end{aligned}$ | 3.3 | V V V |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $V_{\text {amp }}$ | Amplitude of VOut sawtooth (peak-to-peak voltage) | $\begin{aligned} & \hline \text { VSIZE (Sad07): } \\ & \text { x0000000b } \\ & \text { x1000000b } \\ & \text { x1111111b } \end{aligned}$ | 3.5 | $\begin{gathered} 2.25 \\ 3.0 \\ 3.75 \end{gathered}$ | 2.5 | $\begin{aligned} & V \\ & V \\ & V \end{aligned}$ |
| $\mathrm{V}_{\text {offVOut }}$ | Level on VOut pin at V-drive "off" | $\mathrm{I}^{2} \mathrm{Cbit}$ VOutEn at 0 |  | 3.8 |  | V |
| ${ }^{\text {V }}$ Out | Current delivered by VOut output |  | -5 |  | 5 | mA |
| $\mathrm{V}_{\text {VEHT }}$ | Control input voltage range on VEHTIn pin |  | 1 |  | $V_{\text {Refo }}$ | V |
| $\frac{\Delta \mathrm{V}_{\mathrm{amp}}}{\mathrm{~V}_{\mathrm{amp}} \cdot \Delta \mathrm{~V}_{\mathrm{VEHT}}}$ | Breathing compensation | $V_{\text {VEHT }}>V_{\text {Refo }}$ <br> $\mathrm{V}_{\text {VEHT }}(\min ) \leq \mathrm{V}_{\text {VEHT }} \leq \mathrm{V}_{\text {Refo }}$ |  | $\begin{gathered} 0 \\ 2.5 \end{gathered}$ |  | $\begin{aligned} & \% / V \\ & \% / V \end{aligned}$ |

Note 10: Value of acceptable cumulated parasitic load resistance due to humidity, AGC storage capacitor leakage, etc., for less than $1 \%$ of $\mathrm{V}_{\mathrm{amp}}$ change.

Note 11: The threshold for $\mathrm{V}_{\mathrm{VOB}}$ is generated internally and routed to VOscF pin. Any DC current on this pin will influence the value of $\mathrm{V}_{\text {VOB }}$.
Note 12: Maximum of deviation from an ideally linear sawtooth ramp at null SCOR (Sad09 at x0000000b) and null CCOR (Sad0A at x1000000b). The same rate applies to V-drive signal on VOut pin.
Note 13: Maximum SCOR (Sad09 at x1111111b), null CCOR (Sad0A at x1000000b).
Note 14: Null SCOR (Sad09 at x0000000b).
Note 15: "t $t_{V R}$ " is time from the beginning of vertical ramp of $V$-drive signal on VOut pin. " $T_{V R}$ " is duration of this ramp, see chapter TYPICAL OUTPUT WAVEFORMS and Figure 19.
Note 16: $\mathrm{V}_{\text {VOamp }}=\mathrm{V}_{\text {VOT }}-\mathrm{V}_{\text {VOB }}$
Note 17: The same rate applies to V-drive signal on VOut pin.
Note 18: Informative, not tested on each unit.

### 6.6 EW DRIVE SECTION

| Symbol | Parameter | Test Conditions | Value |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. |  |
| $\mathrm{V}_{\text {EW }}$ | Output voltage on EWOut pin |  | 1.8 |  | 6.5 | V |
| IEwOut | Current sourced by EWOut output |  | -1.5 |  | 0 | mA |
| $\mathrm{V}_{\text {HEHT }}$ | Control voltage range on HEHTIn pin |  | 1 |  | $\mathrm{V}_{\text {RefO }}$ | V |
| $\mathrm{V}_{\text {EW-DC }}$ | DC component of the EW-drive signal on EWOut pin | (19)(20)(21)(28) $\mathrm{t}_{\mathrm{VR}}=1 / 2 \mathrm{~T}_{\mathrm{VR}}^{(15)}$ HSIZE (Sad10h): 00000000 b 10000000 b 1111111 b |  | $\begin{gathered} 2 \\ 3.25 \\ 4.5 \end{gathered}$ |  | $\begin{aligned} & \text { V } \\ & \text { V } \\ & \text { V } \end{aligned}$ |
| $\frac{\Delta \mathrm{V}_{\mathrm{EW}-\mathrm{DC}}}{\Delta \mathrm{~V}_{\mathrm{HEHT}}}$ | Breathing compensation on $V_{E W-D C}$ | $\begin{aligned} & 199)(20) \\ & \mathrm{t}_{\mathrm{VR}}=1 / 2 \mathrm{TVR}_{\mathrm{V}}(15) \\ & \mathrm{V}_{\mathrm{HEHT}}>\mathrm{V}_{\text {Refo }} \\ & \mathrm{V}_{\mathrm{HEHT}}(\min ) \leq \mathrm{V}_{\mathrm{HEHT}} \leq \mathrm{V}_{\text {Refo }} \\ & \hline \end{aligned}$ |  | $\begin{gathered} 0 \\ -0.125 \end{gathered}$ |  | $\begin{aligned} & \text { V/V } \\ & \text { V/V } \end{aligned}$ |
| $\frac{\Delta V_{E W-D C}}{\mathrm{~V}_{E W-D C} \cdot \Delta T}$ | Temperature drift of DC component of the EW-drive signal on EWOut pin | $\begin{aligned} & (18)(19)(21)(28) \\ & t_{V R}=1 / 2 T_{V R}{ }^{(15)} \end{aligned}$ |  | 100 |  | ppm $/{ }^{\circ} \mathrm{C}$ |
| $\mathrm{V}_{\text {EW-PCC }}$ | Pin cushion correction component of the EW-drive signal on EWOut pin | (19)(21)(22)(23)(24)(28) VSIZE at maximum PCC (Sad0C): $\times 0000000 \mathrm{~b}$ $\times 100000 \mathrm{~b}$ $\times 111111 \mathrm{~b}$ Tracking with VSIZE : PCC at $\times 1000000 \mathrm{~b}$ VSIZE (Sad07): $\times 0000000 \mathrm{~b}$ $\times 1000000 \mathrm{~b}$ |  | $\begin{gathered} 0 \\ 0.7 \\ 1.5 \\ \\ \\ 0.25 \\ 0.5 \end{gathered}$ |  | $\begin{aligned} & \text { V } \\ & \text { V } \\ & \text { V } \\ & \text { V } \\ & \text { V } \end{aligned}$ |
| $\begin{array}{\|l} \mathrm{V}_{\mathrm{EW}-\mathrm{PCC}}\left[\mathrm{t}_{\mathrm{Vr}}=0\right] \\ \left.\mathrm{EW}-\mathrm{PCCC}^{\left[\mathrm{t}_{\mathrm{Vr}}\right.}=\mathrm{T}_{\mathrm{VR}}\right] \end{array}$ | Tracking of PCC component of the EW-drive signal with vertical position adjustment | (19)(22)(25)(27)(28) PCC at $\times 111111 \mathrm{~b}$ VPOS (Sad08): x0000000b x111111b |  | $\begin{aligned} & 0.52 \\ & 1.92 \end{aligned}$ |  |  |


| Symbol | Parameter | Test Conditions | Value |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. |  |
|  |  | (20)(21)(22)(25)(26)(28) |  |  |  |  |
| $V_{\text {EW-Key }}$ | Keystone correction component of the EW-drive signal on EWOut pin | $\begin{aligned} & \text { KEYST (SadOD): } \\ & \text { x0000000b } \\ & \text { x1111111b } \end{aligned}$ |  | $\begin{gathered} 0.4 \\ -0.4 \end{gathered}$ |  | $\begin{aligned} & \text { V } \\ & \text { V } \end{aligned}$ |
| $\frac{\Delta V_{E W}}{\left.V_{E W}{ }^{[f} \max \right] \cdot \Delta V_{H O}}$ | Tracking of EW-drive signal with horizontal frequency ${ }^{(30)}$ | $\mathrm{V}_{\mathrm{HO}}>\mathrm{V}_{\mathrm{HOThrfr}}$ <br> $\mathrm{V}_{\mathrm{HO}}(\mathrm{min}) \leq \mathrm{V}_{\mathrm{HO}} \leq \mathrm{V}_{\mathrm{HOThrfr}}$ |  | $\begin{gathered} 0 \\ 20 \end{gathered}$ |  | $\begin{aligned} & \% / V \\ & \% / V \end{aligned}$ |
| $\frac{\Delta V_{E W-A C}}{V_{E W-A C} \cdot \Delta V_{H E H T}}$ | Breathing compensation on $\mathrm{V}_{\mathrm{EW}-\mathrm{AC}}(29)$ | $\begin{aligned} & \mid(23)(24) \\ & V_{\text {HEHT }}>\mathrm{V}_{\text {RefO }} \\ & \mathrm{V}_{\text {HEHT }}(\min ) \leq \mathrm{V}_{\text {HEHT }} \leq \mathrm{V}_{\text {Refo }} \end{aligned}$ |  | $\begin{gathered} 0 \\ 1.75 \end{gathered}$ |  | $\begin{aligned} & \% / V \\ & \% / V \end{aligned}$ |

Note 19: KEYST at medium (neutral) value.
Note 20: $P C C$ at minimum value.
Note 21: VPOS at medium (neutral) value.
Note 22: HSIZE at minimum value.
Note 23: Defined as difference of (voltage at $t_{V R}=0$ ) minus (voltage at $t_{V R}=1 / 2 T_{V R}$ ).
Note 24: Defined as difference of (voltage at $t_{V R}=T_{V R}$ ) minus (voltage at $t_{V R}=1 / 2 T_{V R}$ ).
Note 25: VSIZE at maximum value.
Note 26: Difference: (voltage at $\mathrm{t}_{\mathrm{VR}}=0$ ) minus (voltage at $\mathrm{t}_{\mathrm{VR}}=\mathrm{T}_{\mathrm{VR}}$ ).
Note 27: Ratio " $\mathrm{A} / \mathrm{B}$ "of parabola component voltage at $\mathrm{t}_{\mathrm{VR}}=0$ versus parabola component voltage at $\mathrm{t}_{\mathrm{VR}}=\mathrm{T}_{\mathrm{VR}}$. See Figure 2.
Note 28: $\mathrm{V}_{\text {HEHT }}>\mathrm{V}_{\text {RefO }}, \mathrm{V}_{\text {VEHT }}>\mathrm{V}_{\text {RefO }}$
Note 29: $\mathrm{V}_{\mathrm{EW}-\mathrm{AC}}$ is the sum of all components other than $\mathrm{V}_{\mathrm{EW}-\mathrm{DC}}$ (contribution of PCC and keystone correction).
Note 30: More precisely tracking with voltage on HPLL1F pin which itself depends on frequency at a rate given by external components on PLL1 pins. $\mathrm{V}_{\mathrm{EW}}[f \mathrm{fmax}]$ is the value at condition $\mathrm{V}_{\mathrm{HO}}>\mathrm{V}_{\text {HOThrfr }}$.

### 6.7 DYNAMIC CORRECTION OUTPUTS SECTION

$\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$

| Symbol | Parameter | Test Conditions | Value |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. |  |
| Vertical Dynamic Correction output VDyCor |  |  |  |  |  |  |
| IVDyCor | Current sunk from VDyCor output |  | -1.5 |  | -0.1 | mA |
| $\mathrm{V}_{\text {VD-dC }}$ | DC component of the drive signal on VDyCor output | $\mathrm{R}_{\mathrm{L} \text { (VDyCor) }}=10 \mathrm{k} \Omega$ |  | 4 |  | V |
| $\left\|V_{V D-V}\right\|$ | Amplitude of V -parabola on VDyCor output ${ }^{(21)}$ | VSIZE at medium VDC-AMP (Sad15h): <br> xxxxxx00 <br> xxxxxx01 <br> xxxxxx10 <br> xxxxxx11 <br> VDC-AMP at maximum VSIZE (Sad07): <br> x0000000b <br> x1111111b |  | $\begin{aligned} & 0.25 \\ & 0.50 \\ & 0.75 \\ & 1.00 \\ & \\ & 0.6 \\ & 1.6 \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \text { V } \\ & \text { V } \\ & \text { V } \\ & \text { V } \\ & \text { V } \\ & \text { V } \end{aligned}$ |
| $\frac{\mathrm{V}_{\mathrm{VD}-\mathrm{V}}\left[\mathrm{t}_{\mathrm{vr}}=0\right]}{\mathrm{V}_{\mathrm{VD}-\mathrm{V}}\left[\mathrm{t}_{\mathrm{vr}}=\mathrm{T}_{\mathrm{VR}}\right]}$ | Tracking of V-parabola on VDyCor output with vertical position ${ }^{(31)}$ | ```VDC-AMP at maximum VPOS (Sad08): x0000000b x1111111b``` |  | $\begin{aligned} & 0.52 \\ & 1.92 \end{aligned}$ |  |  |

Note 31: Ratio "A/B"of vertical parabola component voltage at $\mathrm{t}_{\mathrm{VR}}=0$ versus vertical parabola component voltage at $\mathrm{t}_{\mathrm{VR}}=\mathrm{T}_{\mathrm{VR}}$.

### 6.8 DC/DC CONTROLLER SECTION

$\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$

| Symbol | Parameter | Test Conditions | Value |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. |  |
| $\mathrm{R}_{\mathrm{B}+\mathrm{FB}}$ | Ext. resistance applied between BComp output and BRegIn input |  | 5 |  |  | k $\Omega$ |
| AOLG | Open loop gain of error amplifier on BRegIn input | Low frequency ${ }^{(18)}$ |  | 100 |  | dB |
| ${ }_{\text {f ugbw }}$ | Unity gain bandwidth of error amplifier on BRegIn input | (18) |  | 6 |  | MHz |
| $I_{\text {RI }}$ | Bias current delivered by regulation input BRegln |  |  | -0.2 |  | $\mu \mathrm{A}$ |
| $\mathrm{I}_{\text {BComp }}$ | Output current capability of BComp output. | $\begin{aligned} & \text { HBOutEn = "Enable" } \\ & \text { HBOutEn ="Disable" (32) } \end{aligned}$ | -0.5 | 0.5 | 2.0 | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \end{aligned}$ |
| $\mathrm{A}_{\text {BISense }}$ | Voltage gain on BISense input |  |  | 3 |  |  |
| $\mathrm{V}_{\text {ThrBIsCurr }}$ | Threshold voltage on BISense input corresponding to current limitation |  | 1.98 | 2.1 | 2.22 | V |
| ${ }_{\text {BISense }}$ | Input current sourced by BISense input |  |  | -1 |  | $\mu \mathrm{A}$ |
| ${ }^{\text {BOut }}$ | Output current capability of BOut output |  | 0 |  | 10 | mA |
| $\mathrm{V}_{\text {BOSat }}$ | Saturation voltage of the internal output transistor on BOut | $\mathrm{I}_{\text {BOut }}=10 \mathrm{~mA}$ |  | 0.25 | 0.35 | V |
| $V_{\text {BReg }}$ | Regulation reference for BRegIn voltage ${ }^{(33)}$ | $\mathrm{V}_{\text {Refo }}=8 \mathrm{~V}$ | 4.7 | 4.8 | 5.0 | V |
| $t_{\text {BTrigDel }} / \mathrm{T}_{\mathrm{H}}$ | Delay of BOut "Off-to-On" edge after middle of flyback pulse, as part of $\mathrm{T}_{\mathrm{H}}$ (34) | BOutPh = "0" |  | 16 |  | \% |

Note 32: A current sink is provided by the BComp output while BOut is disabled:
Note 33: Internal reference related to $\mathrm{V}_{\text {RefO }}$. The same values to be found on pin BRegln, while regulation loop is stabilized.

Note 34: Only applies to configuration specified in "Test conditions" column, i.e. synchronization of BOut "Off-to-On" edge with horizontal flyback signal. Refer to chapter "DC/DC controller" for more details.

### 6.9 MISCELLANEOUS

| $\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Symbol | Parameter | Test Conditions | Value |  |  | Units |
|  |  |  | Min. | Typ. | Max. |  |
| Vertical blanking and horizontal lock indication composite output H $H$ ckVBk |  |  |  |  |  |  |
| $\mathrm{I}_{\text {SinkLckBk }}$ | Sink current to HLckVBk pin | (35) |  | 100 |  | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\text {OLckBk }}$ | Output voltage on HLckVBk output |  |  | $\begin{gathered} 0.1 \\ 1.1 \\ 5 \\ 6 \end{gathered}$ |  | $\begin{aligned} & \text { V } \\ & \text { V } \\ & \text { V } \\ & \text { V } \end{aligned}$ |
| Horizontal moire canceller |  |  |  |  |  |  |
| $\mathrm{V}_{\text {AC-HMoiré }}$ | H-moiré pulse amplitude on HMoiré pin | Rext=10k $\Omega$ HMOIRE (Sad02): x0000000b x1111111b |  | $\begin{aligned} & 0.1 \\ & 2.1 \end{aligned}$ |  | $\begin{aligned} & \text { V } \\ & \text { V } \end{aligned}$ |
| $\mathrm{V}_{\text {DC-HMoiré }}$ | DC level on HMoiré pin | Rext=10k $\Omega$ |  | 0.1 |  | V |
| Vertical moiré canceller |  |  |  |  |  |  |
| $\mathrm{V}_{\mathrm{V} \text {-moiré }}$ | Amplitude of modulation of V-drive signal on VOut pin by vertical moiré. | $\begin{aligned} & \text { VMOIRE (SadOBh): } \\ & \text { x0000000b } \\ & \text { x1111111b } \end{aligned}$ |  | $\begin{aligned} & 0 \\ & 3 \end{aligned}$ |  | $\begin{aligned} & \mathrm{mV} \\ & \mathrm{mV} \end{aligned}$ |
| Protection functions |  |  |  |  |  |  |
| $\mathrm{V}_{\text {Thr }}$ Ray | Input threshold on XRay input ${ }^{(36)}$ |  | 7.65 | 7.9 | 8.2 | V |
| ${ }^{\text {XRRay Delay }}$ | Delay time between XRay detection event and protection action |  |  | $2 \mathrm{~T}_{\mathrm{H}}$ |  |  |
| $V_{\text {cCEn }}$ | $\mathrm{V}_{\mathrm{CC}}$ value for start of operation at $\mathrm{V}_{\mathrm{CC}}$ ramp-up ${ }^{(37)}$ |  |  | 8.5 |  | V |
| $\mathrm{V}_{\text {CCDis }}$ | $\mathrm{V}_{\mathrm{CC}}$ value for stop of operation at $\mathrm{V}_{\mathrm{CC}}$ ramp-down ${ }^{(37)}$ |  |  | 6.5 |  | V |
| Control voltages on HPosF pin for Soft start/stop operation ${ }^{181}$ |  |  |  |  |  |  |
| $\mathrm{V}_{\mathrm{HOn}}$ | Threshold for start/stop of H-drive signal |  |  | 1 |  | V |
| $\mathrm{V}_{\mathrm{BO}}$ | Threshold for start/stop of B-drive signal |  |  | 1.7 |  | V |
| $\mathrm{V}_{\text {HBNorm }} \mathrm{f}$ | Threshold for full operational duty cycle of H -drive and B -drive signals |  |  | 2.4 |  |  |
| $\mathrm{V}_{\text {HPos }}$ | Voltage on HPosF pin as function of adjustment of HPOS register | $\begin{aligned} & \text { Normal operation } \\ & \text { HPOS (Sad01) } \\ & 00000000 \mathrm{~b} \\ & 1111111 \mathrm{~b} \end{aligned}$ | $\begin{aligned} & 3.85 \\ & 2.60 \end{aligned}$ | $\begin{aligned} & 4.0 \\ & 2.8 \\ & \hline \end{aligned}$ | $\begin{array}{r} 4.15 \\ 3.05 \\ \hline \end{array}$ | $\begin{aligned} & \text { V } \\ & \text { V } \end{aligned}$ |

Note 35: Current sunk by the pin if the external voltage is higher than one the circuit tries to force.
Note 36: The threshold is equal to actual $\mathrm{V}_{\text {Refo }}$.
Note 37: In the regions of $\mathrm{V}_{\mathrm{CC}}$ where the device's operation is disabled, the H -drive, V -drive and $\mathrm{B}+$-drive signals on HOut, VOut and BOut pins, resp., are inhibited, the $I^{2} \mathrm{C}$ Bus does not accept any data.

## 7 - TYPICAL OUTPUT WAVEFORMS Note ( ${ }^{38}$ )

| Function | Sad | Pin | Byte | Waveform | Effect on Screen |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Vertical Size | 07 | VOut | $\times 0000000$ |  |  |
|  |  |  | $\times 1111111$ |  | $\square$ |
| Vertical Position | 08 | VOut | $\times 0000000$ | $\mathrm{V}_{\text {mid(Vut) }}^{--1.5 \mathrm{~V}}$ |  |
|  |  |  | $\times 1000000$ | $1$ |  |
|  |  |  | $\times 1111111$ | $\mathrm{V}_{\text {mid(Vout }}-1-3.5 \mathrm{~V}$ |  |
| S-correction | 09 | Vout | $\times 0000000:$ Null |  |  |
|  |  |  | x1111111: <br> Max. |  |  |
| C-correction | OA | Vout | $\times 0000000$ |  |  |
|  |  |  | $\begin{gathered} \text { x1000000: } \\ \text { Null } \end{gathered}$ |  |  |
|  |  |  | $\times 1111111$ |  |  |


| Function | Sad | Pin | Byte | Waveform | Effect on Screen |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Vertical moiré amplitude | OB | VOut | $\begin{gathered} \text { x0000000: } \\ \text { Null } \end{gathered}$ |  |  |
|  |  |  | $\begin{gathered} \text { x1111111: } \\ \quad \text { Max. } \end{gathered}$ |  |  |
| Horizontal size | 10h | EWOut | 00000000 |  | H- |
|  |  |  | 11111111 |  | \|r|rers |
| Keystone correction | OD | EWOut | x0000000 |  | $\square$ |
|  |  |  | x1111111 |  | $\square$ |
| Pin cushion correction | OC | EWOut | x0000000 |  | $\square$ |
|  |  |  | x1111111 |  | $\square$ |
| Parallelogram correction | 12h |  | x0000000 |  | $\square$ |
|  |  |  | x1111111 |  |  |
| Pin cushion asymmetry correction | 11h |  | x0000000 |  | $\square$ |
|  |  |  | x1111111 |  | $\square$ |


| Function | Sad | Pin | Byte | Waveform | Effect on Screen |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Vertical dynamic correction amplitude | 15h | VDyCor | xxxxxx11 |  | Application dependent |
|  |  |  | xxxxxx00 |  |  |

Note 38: For any H and V correction component of the waveforms on EWOut and VOut pins and for internal waveform for corrections of H asymmetry, displayed in the table, weight of the other relevant components is nullified (minimum for parabola, S-correction, medium for keystone, all corner corrections, C-correction, parallelogram, parabola asymmetry correction, written in corresponding registers).

## $8-I^{2} \mathrm{C}$ BUS CONTROL REGISTER MAP

The device slave address is 8 C in write mode and 8 D in read mode.
Bold weight denotes default value at Power-On-Reset.
$I^{2} \mathrm{C}$ Bus data in the adjustment register is buffered and internally applied with discharge of the vertical oscillator.
In order to ensure compatibility with future devices, all "Reserved" bits should be set to 0 .

| Sad | D7 | D6 | D5 | D4 | D3 | D2 | D1 | D0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WRITE MODE (SLAVE ADDRESS = 8C) |  |  |  |  |  |  |  |  |
| 00 | Reserved |  |  |  |  |  |  |  |
| 01 |  |  |  | H | arizo | (ort) |  | Reserved |
|  | 1 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| 02 | HMoiré <br> 1: Separated <br> 0: Combined | HMOIRE (Horizontal moire amplitude) |  |  |  |  |  |  |
|  |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 03 | Reserved |  |  |  |  |  |  |  |
| 04 | Reserved |  |  |  |  |  |  |  |
| 05 | Reserved |  |  |  |  |  |  |  |
| 06 | BOutPol 0: Type N | Reserved |  |  |  |  |  |  |
| 07 | $$ | VSIZE (Vertical size) |  |  |  |  |  |  |
|  |  | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08 | EWTrHFr 0: No tracking | VPOS (Verfical position) |  |  |  |  |  |  |
|  |  | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 09 | Reserved | SCOR (Scorrection) |  |  |  |  |  |  |
|  |  | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| OA | Reserved | CCOR (C-correction) |  |  |  |  |  |  |
|  |  | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0B | Reserved | VMOIRE (Vertical moire amplitude) |  |  |  |  |  |  |
|  |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0C | Reserved | PCC (Pin cushion correction) |  |  |  |  |  |  |
|  |  | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0D | Reserved | \% | \% | KEYST (Keystone correction) |  |  |  |  |
|  |  | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0E | Reserved |  |  |  |  |  |  |  |
| 0F | Reserved |  |  |  |  |  |  |  |
| 10 |  |  |  |  | orizo |  |  | Reserved |
|  | 1 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| 11 | Reserved | PCAC. (Pin cushion asymmety correction) |  |  |  |  |  |  |
|  |  | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12 | Reserved | PARAL (Parallelogram correction) |  |  |  |  |  |  |
|  |  | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 13 | Reserved |  |  |  |  |  |  |  |
| 14 | Reserved |  |  |  |  |  |  |  |
| 15 | Reserved |  |  |  |  |  | VDC-AMP |  |
|  |  |  |  |  |  |  | 0 | 0 |


| Sad | D7 | D6 | D5 | D4 | D3 | D2 | D1 | D0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 16 | XRayReset <br> 0 : No effect <br> 1: Reset | VSyncAuto 1: On | VSyncSel <br> 0:Comp <br> 1:Sep | 0 | 0 | PLL1Pump <br> 1: Fast <br> 0: Slow | $\begin{gathered} \hline \text { PLL1InhEn } \\ \text { 1: On } \end{gathered}$ | $\begin{aligned} & \text { HLockEn } \\ & \text { 1: On } \end{aligned}$ |
| 17 | $\begin{gathered} \mathrm{TV} \\ \mathbf{0}: \mathrm{Off}^{(39)} \end{gathered}$ | $\begin{gathered} \text { TH } \\ \mathbf{0}: \mathrm{Off}^{(39)} \end{gathered}$ | $\begin{gathered} \text { TVM } \\ \mathbf{0}: \text { Off } 39) \end{gathered}$ | $\begin{gathered} \text { THM } \\ \mathbf{0}: \text { Off }^{(39)} \end{gathered}$ | BOHEdge <br> 0 : Falling | HBOutEn <br> 0 : Disable | VOutEn <br> 0 : Disable | BlankMode <br> 1: Perm. |

Note 39: The TV, TH, TVM and THM bits are for testing purposes and must be kept at 0 by application.

## Description of $I^{2} C$ Bus switches

## Write-to bits

## Sad02/D7 - HMoiré

Horizontal Moiré characteristics
0 : Adapted to an architecture with EHT generated in deflection section
1: Adapted to an architecture with separated deflection and EHT sections

## Sad06/D7 - BOutPol

Polarity of $B+$ drive signal on BOut pin
0: adapted to N type of power MOS - high level to make it conductive
1: adapted to $P$ type of power MOS - low level to make it conductive

## Sad07/D7 - BOutPh

Phase of start of B+ drive signal on BOut pin
0: Just after horizontal flyback pulse
1: With one of edges of line drive signal on HOut pin, selected by BOHEdge bit

## Sad08/D7 - EWTrHFr

Tracking of all corrections contained in wave-
form on pin EWOut with Horizontal Frequency
0: Not active
1: Active

## Sad16/D0 - HLockEn

Enable of output of Horizontal PLL1 Lock/unlock
status signal on pin HLckVBk
0: Disabled, vertical blanking only on the pin HLckVBk
1: Enabled
Sad16/D1 - PLL1InhEn
Enable of Inhibition of horizontal PLL1 during
extracted vertical synchronization pulse
0: Disabled, PLL1 is never inhibited
1: Enabled

## Sad16/D2 - PLL1Pump

Horizontal PLL1 charge Pump current
0: Slow PLL1, low current
1: Fast PLL1, high current

## Sad16/D5 - VSyncSel

Vertical Synchronization input Selection between the one extracted from composite HV signal on pin H/HVSyn and the one on pin VSyn. No effect if VSyncAuto bit is at 1.

0 : V . sync extracted from composite signal on H/HVSyn pin selected
1: V. sync applied on VSyn pin selected

## Sad16/D6 - VSyncAuto

Vertical Synchronization input selection Automatic mode. If enabled, the device automatically selects between the vertical sync extracted from composite HV signal on pin H/HVSyn and the one on pin VSyn, based on detection mechanism. If both are present, the one coming first is kept.

0: Disabled, selection done according to bit VSyncSel
1: Enabled, the bit VSyncSel has no effect

## Sad16/D7 - XRayReset

Reset to 0 of XRay effected with ACK bit of $I^{2} C$ Bus data transfer into register containing the XRayReset bit.

0: No effect
1: Reset with automatic return of the bit to 0 This bit is not latched, it will return to 0 by itself.

## Sad17/D0 - BlankMode <br> Blanking operation Mode

0 : Blanking pulse starting with detection of vertical synchronization pulse and ending with end of vertical oscillator discharge
(start of vertical sawtooth ramp on the VOut pin)
1: Permanent blanking - high blanking level in composite signal on pin HLckVBk is permanent

## Sad17/D1 - VOutEn

Vertical Output Enable
0 : Disabled, $V_{\text {offVout }}$ on VOut pin (see 6.5 Vertical section)
1: Enabled, vertical ramp with vertical position offset on VOut pin

## Sad17/D2 - HBOutEn

Horizontal and B+ Output Enable
0 : Disabled, levels corresponding to "power transistor off" on HOut and BOut pins (high for HOut, high or low for BOut, depending on BOutPol bit).
1: Enabled, horizontal deflection drive signal on HOut pin providing that it is not inhibited by another internal event (activated XRay protection). B+ drive signal on BOut pin.
Programming the bit to 1 after prior value of 0 , will initiate soft start mechanism of horizontal drive and of $\mathrm{B}+\mathrm{DC} / \mathrm{DC}$ convertor

## Sad17/D3 - BOHEdge

Selection of Edge of Horizontal drive signal to phase B+ drive Output signal on BOut pin. Only applies if the bit BOutPh is set to 1 , otherwise BOHEdge has no effect.

0 : Falling edge
1: Rising edge

## Sad17/D4,D5,D6,D7 - THM, TVM, TH, TV

Test bits. They must be kept at 0 level by application S/W.

## 9 - OPERATING DESCRIPTION

### 9.1 SUPPLY AND CONTROL

### 9.1.1 Power supply and voltage references

The device is designed for a typical value of power supply voltage of 12 V .
In order to avoid erratic operation of the circuit at power supply ramp-up or ramp-down, the value of $V_{C C}$ is monitored. See Figure 1 and electrical specifications. At switch-on, the device enters a "normal operation" as the supply voltage exceeds $\mathrm{V}_{\text {CCEn }}$ and stays there until it decreases below $V_{\text {CCDis. }}$. The two thresholds provide, by their difference, a hysteresis to bridge potential noise. Outside the "normal operation", the signals on HOut, BOut and VOut outputs are inhibited and the $1^{2} \mathrm{C}$ bus interface is inactive (high impedance on SDA, SCL pins, no ACK), all $\mathrm{I}^{2} \mathrm{C}$ bus control registers being reset to their default values (see chapter I ${ }^{2} \mathrm{C}$ BUS CONTROL REGISTER MAP on page 20).
Figure 1. Supply voltage monitoring


Internal thresholds in all parts of the circuit are derived from a common internal reference supply $\mathrm{V}_{\text {Refo }}$ that is lead out to RefOut pin for external filtering against ground as well as for external use with load currents limited to $I_{\text {RefO }}$. The filtering is necessary to minimize interference in output signals, causing adverse effects like e.g. jitter.

### 9.1.2 $\mathrm{I}^{2} \mathrm{C}$ Bus Control

The $\mathrm{I}^{2} \mathrm{C}$ bus is a 2 line bi-directional serial communication bus introduced by Philips. For its general
description, refer to corresponding Philips $\mathrm{I}^{2} \mathrm{C}$ bus specification.
This device is an $I^{2} \mathrm{C}$ bus slave, compatible with fast ( 400 kHz ) $\mathrm{I}^{2} \mathrm{C}$ bus protocol, with write mode slave address of 8C. Integrators are employed at the SCL (Serial Clock) input and at the input buffer of the SDA (Serial Data) input/output to filter off the spikes of up to 50 ns.
The device supports multiple data byte messages (with automatic incrementation of the $\mathrm{I}^{2} \mathrm{C}$ bus subaddress) as well as repeated Start Condition for $I^{2} C$ bus subaddress change inside the $I^{2} C$ bus messages. All ${ }^{2} \mathrm{C}$ bus registers with specified $\mathrm{I}^{2} \mathrm{C}$ bus subaddress are of WRITE ONLY type.
For the $\mathrm{I}^{2} \mathrm{C}$ bus control register map, refer to chapter $\mathrm{I}^{2} \mathrm{C}$ BUS CONTROL REGISTER MAP on page 20.

### 9.2 SYNC. PROCESSOR

### 9.2.1 Synchronization signals

The device has two inputs for TTL-level synchronization signals, both with hysteresis to avoid erratic detection and with a pull-down resistor. On H/ HVSyn input, pure horizontal or composite horizontal/vertical signal is accepted. On VSyn input, only pure vertical sync. signal is accepted. Both positive and negative polarities may be applied on either input, see Figure 2. Polarity detector and programmable inverter are provided on each of the two inputs. The signal applied on H/HVSyn pin, after polarity treatment, is directly lead to horizontal part and to an extractor of vertical sync. pulses, working on principle of integration, see Figure 3. The vertical sync. signal applied to the vertical deflection processor is selected between the signal extracted from the composite signal on H/HVSyn input and the one applied on VSyn input. The selector is controlled by VSyncSel ${ }^{2} \mathrm{C}$ bus bit.
Besides the polarity detection, the device is capable of detecting the presence of sync. signals on each of the inputs and at the output of vertical sync. extractor. The device is equipped with an automatic mode (switched on or off by VSyncAuto $I^{2} \mathrm{C}$ bus bit) that uses the detection information.

Figure 2. Horizontal sync signal


Figure 3. Extraction of V-sync signal from H/V-sync signal


### 9.2.2 Automatic sync. selection mode

$I^{2} \mathrm{C}$ bus bit VSyncAuto is set to 1 . In this mode, the device itself controls the $I^{2} \mathrm{C}$ bus bits switching the polarity inverters and the vertical sync. signal selector (VSyncSel), using the information provided by detection circuitry. If both extracted and pure vertical sync. signals are present, the one already selected is maintained. No intervention of the MCU is necessary.

### 9.3 HORIZONTAL SECTION

### 9.3.1 General

The horizontal section consists of two PLLs with various adjustments and corrections, working on horizontal deflection frequency, then phase shifting and output driving circuitry providing H -drive signal on HOut pin. Input signal to the horizontal section is output of the polarity inverter on $\mathrm{H} /$ HVSyn input. The device ensures automatically that this polarity be always positive.

### 9.3.2 PLL1

The PLL1 block diagram is in Figure 5. It consists of a voltage controlled oscillator (VCO), a shaper with adjustable threshold, a charge pump with inhibition circuit, a frequency and phase comparator and timing circuitry. The goal of the PLL1 is to make the VCO ramp signal match in frequency the sync. signal and to lock this ramp in phase to the sync. signal, with a possibility to adjust a perma-
nent phase offset. On the screen, this offset results in the change of horizontal position of the picture. The loop, by tuning the VCO accordingly, gets and maintains in coincidence the rising edge of input sync. signal with signal REF1, which is derived from the VCO ramp by a comparator with threshold adjustable through $H P O S 1^{2} \mathrm{C}$ bus control. The coincidence is identified and flagged by lock detection circuit on pin HLckVBk.
The charge pump provides positive and negative currents charging the external loop filter on HPosF pin. The loop is independent of the trailing edge of sync. signal and only locks to its leading edge. By design, the PLL1 does not suffer from any dead band even while locked. The speed of the PLL1 depends on the current value provided by the charge pump. While not locked, the current is very low, to slow down the changes of VCO frequency and thus protect the external power components at sync. signal change. In locked state, the currents are much higher, two different values being selectable via PLL1Pump $1^{2} \mathrm{C}$ bus bit to provide a mean to control the PLL1 speed by S/W. Lower values make the PLL1 slower, but more stable. Higher values make it faster and less stable. In general, the PLL1 speed should be higher for high deflection frequencies. The response speed and stability (jitter level) depends on the choice of external components making up the loop filter. A "CRC" filter is generally used (see Figure 4 on page 25).

Figure 4. H-PLL1 filter configuration


The PLL1 is internally inhibited during extracted vertical sync. pulse (if any) to avoid taking into account missing or wrong pulses on the phase comparator. Inhibition is obtained by forcing the charge
pump output to high impedance state. The inhibition mechanism can be disabled through PLL1Pump $I^{2} \mathrm{C}$ bus bit.
The Figure 7, in its upper part, shows the position of the VCO ramp signal in relation to input sync. pulse for three different positions of adjustment of horizontal position control HPOS.

Figure 5. Horizontal PLL1 block diagram


Figure 6. Horizontal oscillator (VCO) schematic diagram


### 9.3.3 Voltage controlled oscillator

The VCO makes part of both PLL1 and PLL2 loops, being an "output" to PLL1 and "input" to PLL2. It delivers a linear sawtooth. Figure 6 explains its principle of operation. The linears are obtained by charging and discharging an external capacitor on pin CO, with currents proportional to the current forced through an external resistor on pin RO, which itself depends on the input tuning voltage $\mathrm{V}_{\mathrm{HO}}$ (filtered charge pump output). The rising and falling linears are limited by $\mathrm{V}_{\text {HOThrLo }}$ and $\mathrm{V}_{\text {HOThrHi }}$ thresholds filtered through HOscF pin.
At no signal condition, the $\mathrm{V}_{\mathrm{HO}}$ tuning voltage is clamped to its minimum (see chapter ELECTRICAL PARAMETERS AND OPERATING CONDITIONS, part horizontal section), which corresponds to the free-running VCO frequency $\mathrm{f}_{\mathrm{HO}(0)}$. Refer to Note1 for the formula to calculate this frequency using external components values. The ratio between the frequency corresponding to maximum $\mathrm{V}_{\mathrm{HO}}$ and the one corresponding to minimum $\mathrm{V}_{\mathrm{HO}}$ (free-running frequency) is about 4.5. This range can easily be increased in the application. The PLL1 can only lock to input frequencies falling inside these two limits.

### 9.3.4 PLL2

The goal of the PLL2 is, by means of phasing the signal driving the power deflection transistor, to lock the middle of the horizontal flyback to a certain threshold of the VCO sawtooth. This internal threshold is affected by geometry phase corrections, like e.g., parallelogram. The PLL2 is much faster than PLL1 to be able to follow the dynamism of this phase modulation. The PLL2 control current (see Figure 7) is significantly increased during discharge of vertical oscillator (during vertical retrace period) to be able to make up for the difference of dynamic phase at the bottom and at the top of the picture. The PLL2 control current is integrated on the external filter on pin HPLL2C to obtain smoothed voltage, used, in comparison with VCO ramp, as a threshold for H -drive rising edge generation.

As both leading and trailing edges of the H-drive signal in the Figure 7 must fall inside the rising part of the VCO ramp, an optimum middle position of the threshold has been found to provide enough margin for horizontal output transistor storage time as well as for the trailing edge of H -drive signal with maximum duty cycle. Yet, the constraints thereof must be taken into account while considering the application frequency range and H -flyback duration. The Figure 7 also shows regions for rising and falling edges of the H -drive signal on HOut pin. As it is forced high during the H -flyback pulse and low during the VCO discharge period, no edge during these two events takes effect.
The flyback input configuration is in Figure 8.

### 9.3.5 Dynamic PLL2 phase control

The dynamic phase control of PLL2 is used to compensate for picture asymmetry versus vertical axis across the middle of the picture. It is done by modulating the phase of the horizontal deflection with respect to the incoming video (synchronization). Inside the device, the threshold $\mathrm{V}_{\mathrm{S}(0)}$ is compared with the VCO ramp, the PLL2 locking the middle of H -flyback to the moment of their match. The dynamic phase is obtained by modulation of the threshold by correction waveforms. Refer to Figure 12 and to chapter TYPICAL OUTPUT WAVEFORMS. The correction waveforms have no effect in vertical middle of the screen (for middle vertical position). As they are summed, their effect on the phase tends to reach maximum span at top and bottom of the picture. As all the components of the resulting correction waveform (linear for parallelogram correction and parabola of 2nd order for Pin cushion asymmetry correction) are generated from the output vertical deflection drive waveform, they both track with real vertical amplitude and position (including breathing compensation), thus being fixed on the screen. Refer to $\mathrm{I}^{2} \mathrm{C}$ BUS CONTROL REGISTER MAP on page 20 for details on $\mathrm{I}^{2} \mathrm{C}$ bus controls.

Figure 7. Horizontal timing diagram

$\mathrm{t}_{\mathrm{s}}$ : HOT storage time
Figure 8. HFly input configuration


### 9.3.6 Output section

The H-drive signal is inhibited (high level) during flyback pulse, and also when $V_{C C}$ is too low, when $I^{2} \mathrm{C}$ bus bit HBOutEn is set to 0 (default position).

The PLL2 is followed by a rapid phase shifting which accepts the signal from H-moiré canceller (see sub chapter Horizontal moiré cancellation on page 27)
The output stage consists of a NPN bipolar transistor, the collector of which is routed to HOut pin (see Figure 9).
Figure 9. HOut configuration


Non-conductive state of HOT (Horizontal Output Transistor) must correspond to non-conductive state of the device output transistor.

### 9.3.7 Soft-start and soft-stop on H-drive

The soft-start and soft-stop procedure is carried out at each switch-on or switch-off of the H-drive signal via HBOutEn $I^{2} \mathrm{C}$ bus bit to protect external power components. By its second function, the external capacitor on pin HPosF is used to time out this procedure, during which the duty cycle of $\mathrm{H}-$ drive signal starts at its maximum ("t $\mathrm{H}_{\mathrm{Hoff}} / \mathrm{T}_{\mathrm{H}}$ for soft start/stop" in electrical specifications) and slowly decreases. This is controlled by voltage on pin HPosF. See Figure 10 and sub chapter Safety functions on page 33.

### 9.3.8 Horizontal moiré cancellation

The horizontal moiré canceller is intended to blur a potential beat between the horizontal video pixel period and the CRT pixel width, which causes visible moiré patterns in the picture.
On pin HMoiré, it generates a square line-synchronized waveform with amplitude adjustable through HMOIRE I ${ }^{2}$ C bus control.
The behaviour of horizontal moiré is to be optimised for different deflection design configurations using HMoiré $\mathrm{R}^{2} \mathrm{C}$ bus bit. This bit is to be kept at 0 for common architecture ( $\mathrm{B}+$ and EHT common regulation) and at 1 for separated architecture ( $\mathrm{B}+$ and EHT each regulated separately).

Figure 10. Control of HOut and BOut at start/stop at nominal $\mathrm{V}_{\mathrm{cc}}$


### 9.4 VERTICAL SECTION

### 9.4.1 General

The goal of the vertical section is to drive vertical deflection output stage. It delivers a sawtooth waveform with an amplitude independent of deflection frequency, on which vertical geometry corrections of C- and S-type are superimposed (see chapter TYPICAL OUTPUT WAVEFORMS).
Block diagram is in Figure 11. The sawtooth is obtained by charging an external capacitor on pin VCap with controlled current and by discharging it via transistor Q1. This is controlled by the CONTROLLER. The charging starts when the voltage across the capacitor drops below $\mathrm{V}_{\text {VOB }}$ threshold. The discharging starts either when it exceeds $\mathrm{V}_{\text {Vot }}$ threshold or a short time after arrival of synchronization pulse. This time is necessary for the AGC loop to sample the voltage at the top of the sawtooth. The $\mathrm{V}_{\text {VOB }}$ reference is routed out onto VOscF pin in order to allow for further filtration.
The charging current influences amplitude and shape of the sawtooth. Just before the discharge, the voltage across the capacitor on pin VCap is sampled and stored on a storage capacitor connected on pin VAGCCap. During the following vertical period, this voltage is compared to internal reference REF ( $\mathrm{V}_{\mathrm{VOT}}$ ), the result thereof controlling the gain of the transconductance amplifier providing the charging current. Speed of this AGC loop depends on the storage capacitance on pin

VAGCCap. On the screen, this corresponds to stabilized vertical size of picture. After a change of frequency on the sync. input, the stabilization time depends on the frequency difference and on the capacitor value. The lower its value, the shorter the stabilization time, but on the other hand, the lower the loop stability. A practical compromise is a capacitance of 470 nF . The leakage current of this capacitor results in difference in amplitude between low and high frequencies. The higher its parallel resistance $R_{\text {L(VAGCCap) }}$, the lower this difference.
When the synchronization pulse is not present, the charging current is fixed. As a consequence, the free-running frequency $\mathrm{f}_{\mathrm{VO}(0)}$ only depends on the value of the capacitor on pin VCap. It can be roughly calculated using the following formula

$$
\mathrm{f}_{\mathrm{VO}(0)}=\frac{150 \mathrm{nF}}{\mathrm{C}_{(\mathrm{VCap})}} \cdot 100 \mathrm{~Hz}
$$

The frequency range in which the AGC loop can regulate the amplitude also depends on this capacitor.
The C- and S-corrections of shape serve to compensate for the vertical deflection system non-linearity. They are controlled via CCOR and SCOR $I^{2} C$ bus controls.
Shape-corrected sawtooth with regulated amplitude is lead to amplitude control stage. The dis-
charge exponential is replaced by $\mathrm{V}_{\mathrm{VOB}}$ level, which, under control of the CONTROLLER, creates a rapid falling edge and a flat part before beginning of new ramp. Mean value of the waveform output on pin VOut is adjusted by means of VPOS $\mathrm{I}^{2} \mathrm{C}$ bus control, its amplitude through VSIZE $\mathrm{I}^{2} \mathrm{C}$ bus control. Vertical moiré is superimposed.
The biasing voltage for external DC-coupled vertical power amplifier is to be derived from $\mathrm{V}_{\text {RefO }}$ voltage provided on pin RefOut, using a resistor divider, this to ensure the same temperature drift of mean (DC) levels on both differential inputs and to
compensate for spread of $\mathrm{V}_{\text {Refo }}$ value (and so mean output value) between particular devices.

### 9.4.2 Vertical moiré

To blur the interaction of deflection lines with CRT mask grid pitch that can generate moiré pattern, the picture position is to be alternated at frame frequency. For this purpose, a square waveform at half-frame frequency is superimposed on the output waveform's DC value. Its amplitude is adjustable through VMOIRE I ${ }^{2} \mathrm{C}$ bus control,.

Figure 11. Vertical section block diagram


### 9.5 EW DRIVE SECTION

The goal of the EW drive section is to provide, on pin EWOut, a waveform which, used by an external DC-coupled power stage, serves to compensate for those geometry errors of the picture that are symmetric versus vertical axis across the middle of the picture.
The waveform consists of an adjustable DC value, corresponding to horizontal size, a parabola of 2nd order for "pin cushion" correction and a linear for "keystone" correction. All of them are adjustable via $I^{2} \mathrm{C}$ bus, see $\mathrm{I}^{2} \mathrm{C}$ BUS CONTROL REGISTER MAP on page 20.

Refer to Figure 12, Figure 13 and to chapter TYPICAL OUTPUT WAVEFORMS. The correction waveforms have no effect in the vertical middle of the screen (if the VPOS control is adjusted to its medium value). As they are summed, the resulting waveform tends to reach its maximum span at top and bottom of the picture. The voltage at the EWOut is top and bottom limited (see parameter $\mathrm{V}_{\mathrm{EW}}$ ). According to Figure 13, especially the bottom limitation seems to be critical for maximum horizontal size (minimum DC). Actually it is not critical since the parabola component must always be applied. As all the components of the resulting correction waveform are generated from the out-
put vertical deflection drive waveform, they all track with real vertical amplitude and position (including breathing compensation), thus being fixed vertically on the screen. They are also affected by C - and S-corrections. The sum of components other than DC is affected by value in $H S I Z E I^{2} \mathrm{C}$ bus control in reversed sense. Refer to electrical specifications for value. The DC value, adjusted via HSIZE control, is also affected by voltage on HEHTIn input, thus providing a horizontal breathing compensation (see electrical specifications for value). The resulting waveform is conditionally multiplied with voltage on HPLL1F, which depends on
frequency. Refer to electrical specifications for value and more precision. This tracking with frequency provides a rough compensation of variation of picture geometry with frequency and allows to fix the adjustment ranges of $I^{2} \mathrm{C}$ bus controls throughout the operating range of horizontal frequencies. It can be switched off by EWTrHFr ${ }^{2} \mathrm{C}$ bus bit (off by default).
The EW waveform signal is buffered by an NPN emitter follower, the emitter of which is directly routed to EWOut output, with no internal resistor to ground. It is to be biased externally.

Figure 12. Geometric corrections' schematic diagram


Figure 13. EWOut output waveforms


### 9.6 DYNAMIC CORRECTION OUTPUT SECTION

### 9.6.1 Vertical Dynamic Correction output VDyCor

A parabola at vertical deflection frequency is available on pin VDyCor. Its amplitude is adjustable via VDC-AMP $I^{2} \mathrm{C}$ bus control. It tracks with real vertical amplitude and position (including breathing compensation). It is also affected by C - and S -corrections.
The use of this correction waveform is up to the application (e.g. dynamic focus).

### 9.7 DC/DC CONTROLLER SECTION

The section is designed to control a switch-mode DC/DC converter. A switch-mode DC/DC convertor generates a DC voltage from a DC voltage of different value (higher or lower) with little power losses. The DC/DC controller is synchronized to
horizontal deflection frequency to minimize potential interference into the picture.
Its operation is similar to that of standard UC3842.
The schematic diagram of the DC/DC controller is in Figure 14. The BOut output controls an external switching circuit (a MOS transistor) delivering pulses synchronized on horizontal deflection frequency, the phase of which depends on $I^{2} \mathrm{C}$ bus configuration, see the table at the end of this chapter. Their duration depends on feedback provided to the circuit, generally a copy of DC/DC converter output voltage and a copy of current passing through the DC/DC converter circuitry (e.g. current through external power component). The polarity of the output can be controlled by BOutPol $1^{2} \mathrm{C}$ bus bit. A NPN transistor open-collector is routed out to the BOut pin.
During the operation, a sawtooth is to be found on pin BISense, generated externally by the application. According to BOutPh ${ }^{2} \mathrm{C}$ bus bit, the R-S flipflop is set either at H -drive signal edge (rising or falling, depending on BOHEdge $I^{2} \mathrm{C}$ bus bit), or a
certain delay ( $\mathrm{t}_{\mathrm{B} \text { TrigDel }} / \mathrm{T}_{\mathrm{H}}$ ) after middle of H -flyback. The output is set On at the end of a short pulse generated by the monostable trigger.
Timing of reset of the R-S flip-flop affects duty cycle of the output square signal and so the energy transferred from DC/DC converter input to its output. A reset edge is provided by comparator C2 if the voltage on pin BISense exceeds the internal threshold $\mathrm{V}_{\text {ThrBIsCurr }}$. This represents current limitation if a voltage proportional to the current through the power component or deflection stage is available on pin BISense. This threshold is affected by the voltage on pin HPosF, which rises at soft start and descends at soft stop. This ensures self-contained soft control of duty cycle of the output signal on pin BOut. Refer to Figure 10. Another condition for the reset of the R-S flip-flop, OR-ed with the one described before, is that the voltage on pin BISense exceeds the voltage $\mathrm{V}_{\mathrm{C} 1}$, which depends on the voltage applied on input BISense of the error amplifier O1. The two voltages are
compared, and the reset signal generated by the comparator C1. The error amplifier amplifies (with a factor defined by external components) the difference between the input voltage proportional to DC/DC convertor output voltage and internal reference $V_{\text {BReg. }}$.
Both step-up (DC/DC converter output voltage higher than its input voltage) and step-down (output voltage lower than input) are possible.
DC/DC controller Off-to-On edge timing

| BOutPh <br> (Sad07/ <br> D7) | BOHEdge <br> (Sad17/ <br> D3) | Timing of Off-to-On transition <br> on BOut output |
| :---: | :---: | :---: |
| 0 | don't care | Middle of H-flyback plus t tTrigDel |
| 1 | 0 | Falling edge of H-drive signal |
| 1 | 1 | Rising edge of H-drive signal |

Figure 14. DC/DC converter controller block diagram


### 9.8 MISCELLANEOUS

### 9.8.1 Safety functions

The safety functions comprise supply voltage monitoring with appropriate actions, soft start and soft stop features on H-drive and B-drive signals on HOut and BOut outputs and X-ray protection.
For supply voltage supervision, refer to paragraph Power supply and voltage references on page 23 and Figure 1. A schematic diagram putting together all safety functions and composite PLL1 lock and V-blanking indication is in Figure 15.

### 9.8.2 Soft start and soft stop functions

For soft start and soft stop features for H -drive and B-drive signal, refer to paragraph Soft-start and soft-stop on H-drive on page 27 and sub chapterDC/DC CONTROLLER SECTION on page 31, respectively. See also the Figure 10. Regardless why the H -drive or B -drive signal are switched on or off $\left(I^{2} \mathrm{C}\right.$ bus command, power up or down, X-ray protection), the signals always phase-in and
phase-out in the way drawn in the figure, the first to phase-in and last to phase-out being the H-drive signal, which is to better protect the power stages at abrupt changes like switch-on and off. The timing of phase-in and phase-out only depends on the capacitance connected to HPosF pin which is virtually unlimited for this function. Yet it has a dual function (see paragraph PLL1 on page 24), so a compromise thereof is to be found.

### 9.8.3 X-ray protection

The X -ray protection is activated if the voltage level on XRay input exceeds $\mathrm{V}_{\text {ThrXRay }}$ threshold. As a consequence, the H -drive and B -drive signals on HOut and BOut outputs are inhibited (switched off) after a 2-horizontal deflection line delay provided to avoid erratic excessive X-ray condition detection at short parasitic spikes.
This protection is latched; it may be reset either by $V_{C C}$ drop or by ${ }^{2} \mathrm{C}$ bus bit XRayReset (see chapter $I^{2} \mathrm{C}$ BUS CONTROL REGISTER MAP on page 20).

Figure 15. Safety functions - block diagram


### 9.8.4 Composite output HLckVBk

The composite output HLckVBk provides, at the same time, information about lock state of PLL1 and early vertical blanking pulse. As both signals have two logical levels, a four level signal is used to define the combination of the two. Schematic diagram putting together all safety functions and composite PLL1 lock and V-blanking indication is in Figure 15, the combinations, their respective levels and the HLckVBk configuration in Figure 16. The early vertical blanking pulse is obtained by a logic combination of vertical synchronization pulse and pulse corresponding to vertical oscillator discharge. The combination corresponds to the drawing in Figure 16. The blanking pulse is started with
the leading edge of any of the two signals, whichever comes first. The blanking pulse is ended with the trailing edge of vertical oscillator discharge pulse. The device has no information about the vertical retrace time. Therefore, it does not cover, by the blanking pulse, the whole vertical retrace period. By means of BlankMode $I^{2} \mathrm{C}$ bus bit, when at 1 (default), the blanking level (one of two according to PLL1 status) is made available on the HLckVBk permanently. The permanent blanking, irrespective of the BlankMode $I^{2} \mathrm{C}$ bus bit, is also provided if the supply voltage is low (under $\mathrm{V}_{\text {CCEn }}$ or $\mathrm{V}_{\text {CCDis }}$ thresholds), if the X -ray protection is active or if the V-drive signal is disabled by VOutEn $I^{2} \mathrm{C}$ bus bit.

Figure 16. Levels on HLckVBk composite output


Figure 17. Ground layout recommendations


## 10-INTERNAL SCHEMATICS

Figure 18.


Figure 19.


Figure 20.


Figure 21.


Figure 22.


Figure 23.


Figure 24.


Figure 25.


Figure 26.


Figure 27.


Figure 28.


Figure 29.


Figure 30.


Figure 31.


Figure 32.


Figure 33.


Figure 34.


Figure 35.


Figure 36.


Figure 39.


Figure 37.


Figure 38.


## 11 - PACKAGE MECHANICAL DATA

32 PINS - PLASTIC SHRINK


| Dimensions | Millimeters |  |  | Inches |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Min. | Typ. | Max. | Min. | Typ. | Max. |
| A | 3.556 | 3.759 | 5.080 | 0.140 | 0.148 | 0.200 |
| A1 | 0.508 |  |  | 0.020 |  |  |
| A2 | 3.048 | 3.556 | 4.572 | 0.120 | 0.140 | 0.180 |
| B | 0.356 | 0.457 | 0.584 | 0.014 | 0.018 | 0.023 |
| B1 | 0.762 | 1.016 | 1.397 | 0.030 | 0.040 | 0.055 |
| C | .203 | 0.254 | 0.356 | 0.008 | 0.010 | 0.014 |
| D | 27.43 | 27.94 | 28.45 | 1.080 | 1.100 | 1.120 |
| E | 9.906 | 10.41 | 11.05 | 0.390 | 0.410 | 0.435 |
| E1 | 7.620 | 8.890 | 9.398 | 0.300 | 0.350 | 0.370 |
| e |  | 1.778 |  |  | 0.070 |  |
| eA |  | 10.16 |  |  | 0.400 |  |
| eB |  |  | 12.70 |  |  | 0.500 |
| L | 2.540 | 3.048 | 3.810 | 0.100 | 0.120 | 0.150 |

## 12 - GLOSSARY

| AC | Alternate Current |
| :--- | :--- |
| ACK | ACKnowledge bit of I2C-bus transfer |
| AGC | Automatic Gain Control |
| COMP | COMParator |
| CRT | Cathode Ray Tube |
| DC | Direct Current |
| EHT | Extra High Voltage |
| EW | East-West |
| H/W | HardWare |
| HOT | Horizontal Output Transistor |
| I'C | Inter-Integrated Circuit |
| IIC | Inter-Integrated Circuit |
| MCU | Micro-Controller Unit |
| NAND | Negated AND (logic operation) |
| NPN | Negative-Positive-Negative |
| OSC | OSCillator |
| PLL | Phase-Locked Loop |
| PNP | Positive-Negative-Positive |
| REF | REFerence |
| RS, R-S | Reset-Set |
| S/W | SoftWare |
| TTL | Transistor Transistor Logic |
| VCO | Voltage-Controlled Oscillator |
|  |  |

## Revision follow-up

## PRODUCT PREVIEW

## June 2000 <br> version 2.0

Document created (issued from TDA9112)
Work on figures and text; version finalized and displayed on Intranet.

July 2000
version 2.1
Sentence modified in first page : The internal sync processor.;." replaced by :"the device only requires..;"
Bloc diagram : addition of Hsize under E/W correction
Quick Reference Data: Addition of parrallelogram
Register Map: subaddress 08: 0:No tracking
Few corrections in text.

## PRELIMINARY DATA

September 2000
version 3:0
Uniformity in the writing of cross references for notes.
In internal schematics, correction of figure for pin 11.
In bloc diagram: the line between PLL2 and HMoiré controller has been deleted
In Horizontal Moiré Cancellation: 1 sentence changed
VDC AMP replaced by VDC-AMP
In electrical parameters:
$\Delta \mathrm{V}_{\text {HMoiré }}$ becomes $\Delta \mathrm{V}_{\text {AC-HMoiré }}$
Addition of $\mathrm{V}_{\mathrm{DC}}$-HMoiré, .

January 11, 2001
version 3.1
page 6: value for autosync frequency ratio replaced : 4.28 instead of 4.5 previously.

April 19, 2001
version 3.2
page 16
Section 6.9 .Vtrh-XRay: new values 7.65 min, 7.9 typ., 8.2 max.

## DATASHEET

July 18, 2001
version 4.0
Section 9.4.1 right column"The higher its value,..." ---> "The lower its value"
Section 9.5 ."...at the vertical middle..." ---> "...in the vertical middle..."
Section 6.6 : addition of [fmax] to parameter " $\Delta \mathrm{VEW} / \mathrm{VEW}[f m a x] . \Delta \mathrm{VHO}$ " .and changed its value to 20
Note 28: added: "VEW[fmax] is the value at condition VHO>VHOThrfr".
Section 6.4 : addition of min and max values for $\mathrm{V}_{\text {HPosF }}$ and $\mathrm{V}_{\text {TopHPLL2C }}$
Section 6.5 addition of min and max values for $\mathrm{V}_{\mathrm{VOB}}+$ correction of typ. value

## $\longdiv { \pi }$

Section 6.8 addition of min and max values for $\mathrm{V}_{\text {ThrBlsCurr }}$ and $\mathrm{V}_{\text {BReg }}$, max value added for $\mathrm{V}_{\mathrm{BOS}}$ at
Section 6.9 addition of min and max values for $\mathrm{V}_{\text {HPos }}$
Section 9.4 "stabilizing time" changed to "stabilization time" (twice)
Section 6.9 : max values for vertical moiré cancellers moved to typ. values

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