## DATA SHEET

## TDA8580J <br> Multi-purpose power amplifier

Preliminary specification
File under Integrated Circuits, IC01

## Multi-purpose power amplifier

## FEATURES

## General

- Supply voltage range from 8 to 24 V
- Low distortion
- Few external components, fixed gain
- High output power
- Can be used as a stereo amplifier in Bridge-Tied Load (BTL) or quad Single-Ended (SE) amplifiers
- Single-ended mode without loudspeaker capacitor
- Mute and standby mode with one- or two-pin operation
- Diagnostic information for Dynamic Distortion Detector (DDD), high temperature ( $145{ }^{\circ} \mathrm{C}$ ) and short-circuit
- No switch on/off plops when switching between standby and mute or mute and on; an external RC-network is prescribed to ensure plop-free operation
- Low offset variation at outputs between mute and on
- Fast mute on supply voltage drops.


## Protection

- Short-circuit proof to ground, positive supply voltage and across load; the supply voltage ranges where the different short circuit conditions are guaranteed are given in Chapter "Limiting values"
- ESD protected on all pins
- Thermal protection against temperatures exceeding $150^{\circ} \mathrm{C}$.


## GENERAL DESCRIPTION

The TDA8580J is a stereo Bridge-Tied Load (BTL) or a quad Single-Ended (SE) amplifier that operates over a wide supply voltage range from 8 to 24 V . This makes it suitable for applications such as television, home-sound systems and active speakers.

Because of an internal voltage buffer, this device can be used without a capacitor connected in series with the load (SE application). A combined BTL and $2 \times$ SE application can also be configured (one chip stereo and subwoofer application).

## ORDERING INFORMATION

| TYPE <br> NUMBER | PACKAGE |  |  |
| :---: | :---: | :---: | :---: |
|  | NAME | DESCRIPTION | VERSION |
| TDA8580J | DBS17P | plastic DIL-bent-SIL power package; 17 leads (lead length 12 mm) | SOT243-1 |

## QUICK REFERENCE DATA

| SYMBOL | PARAMETER | CONDITIONS | MIN. | TYP. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{P}$ | operating supply voltage |  | 8.0 | 14.4 | 24 | V |
| $\mathrm{I}_{\mathrm{q}(\text { tot) }}$ | total quiescent current | $\mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V}$ | - | 140 | 170 | mA |
| $1{ }_{\text {stb }}$ | standby supply current | $\mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V}$ | - | 1 | 50 | $\mu \mathrm{A}$ |
| Bridge-tied load application |  |  |  |  |  |  |
| $\mathrm{G}_{\mathrm{v}}$ | voltage gain |  | 31 | 32 | 33 | dB |
| $\mathrm{P}_{0}$ | output power | THD $=0.5 \%$; $\mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V} ; \mathrm{R}_{\mathrm{L}}=4 \Omega$ | 14 | 15 | - | W |
|  |  | THD $=0.5 \%$; $\mathrm{V}_{\mathrm{P}}=24 \mathrm{~V} ; \mathrm{R}_{\mathrm{L}}=8 \Omega$ | 21 | 23 | - | W |
| THD | total harmonic distortion | $\begin{aligned} & \mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz} ; \mathrm{P}_{\mathrm{o}}=1 \mathrm{~W} ; \mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V} ; \\ & \mathrm{R}_{\mathrm{L}}=4 \Omega \end{aligned}$ | - | 0.05 | 0.1 | \% |
|  |  | $\begin{aligned} & \mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz} ; \mathrm{P}_{\mathrm{o}}=10 \mathrm{~W} ; \mathrm{V}_{\mathrm{P}}=24 \mathrm{~V} ; \\ & \mathrm{R}_{\mathrm{L}}=8 \Omega \end{aligned}$ | - | 0.02 | 0.05 | \% |
| $\mathrm{V}_{\text {offset(DC) }}$ | DC output offset voltage | $\mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V}$; mute condition; $\mathrm{R}_{\mathrm{L}}=4 \Omega$ | - | 10 | 20 | mV |
|  |  | $\mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V}$; on condition | - | 0 | 140 | mV |
| $\mathrm{V}_{\mathrm{no}}$ | noise output voltage | $\mathrm{R}_{\mathrm{s}}=1 \mathrm{k} \Omega ; \mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V}$ | - | 100 | 150 | $\mu \mathrm{V}$ |
| SVRR | supply voltage ripple rejection | $\mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz}$; $\mathrm{V}_{\text {ripple(p-p) }}=2 \mathrm{~V}$; on or mute condition; $\mathrm{R}_{\mathrm{S}}=0 \Omega$ | 50 | 60 | - | dB |
| Single-ended application |  |  |  |  |  |  |
| $\mathrm{G}_{v}$ | voltage gain |  | 25 | 26 | 27 | dB |
| $\mathrm{P}_{0}$ | output power | THD $=0.5 \%$; $\mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V} ; \mathrm{R}_{\mathrm{L}}=4 \Omega$ | 3.8 | 4.0 | - | W |
|  |  | THD $=0.5 \%$; $\mathrm{V}_{\mathrm{P}}=24 \mathrm{~V} ; \mathrm{R}_{\mathrm{L}}=4 \Omega$ | 10.5 | 11.5 | - | W |
| $\mathrm{V}_{\text {offset(DC) }}$ | DC output offset voltage | $\mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V}$; mute condition; $\mathrm{R}_{\mathrm{L}}=4 \Omega$ | - | 10 | 20 | mV |
|  |  | $\mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V}$; on condition | - | 0 | 100 | mV |
| $\mathrm{V}_{\text {no }}$ | noise output voltage | $\mathrm{R}_{\mathrm{S}}=1 \mathrm{k} \Omega ; \mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V}$ | - | 80 | 120 | $\mu \mathrm{V}$ |
| SVRR | supply voltage ripple rejection | $\mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz} ; \mathrm{V}_{\text {ripple(p-p) }}=2 \mathrm{~V}$; on or mute condition; $\mathrm{R}_{\mathrm{s}}=0 \Omega$ | 40 | 45 | - | dB |

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## BLOCK DIAGRAM



Fig. 1 Block diagram.

PINNING

| SYMBOL | PIN | DESCRIPTION |
| :--- | :---: | :--- |
| OUT1+ | 1 | non-inverting output 1 |
| PGND1 | 2 | power ground 1 |
| VP1 $_{\text {P1 }}$ | 3 | supply voltage 1 |
| OUT2- | 4 | inverting output 2 |
| STANDBY | 5 | standby/mute/on selection input |
| DIAG | 6 | diagnostic output |
| IN1 | 7 | input 1 |
| IN2 | 8 | input 2 |
| BUFFER | 9 | single-ended buffer output |
| IN3 | 10 | input 3 |
| IN4 | 11 | input 4 |
| IN5 | 12 | input 5; signal ground capacitor <br> connection |
| MUTE | 13 | mute/on selection input |
| OUT3- | 14 | inverting output 3 |
| V P2 $^{15}$ | 15 | supply voltage 2 |
| PGND2 | 16 | power ground 2 |
| OUT4+ | 17 | non-inverting output 4 |



Fig. 2 Pin configuration.

## FUNCTIONAL DESCRIPTION

The TDA8580J is a multi-purpose power amplifier with four amplifiers which can be connected in the following configurations with high output power and low distortion (at minimum quiescent current):

- Dual bridge-tied load amplifiers
- Quad single-ended amplifiers
- Dual single-ended amplifiers and one bridge-tied load amplifier.

The amplifier can be switched in on, mute and off (standby) by the MUTE and STANDBY pins (for interfacing directly with a microcontroller). One-pin operation is also possible by applying a voltage greater than 8 V to the STANDBY pin to switch the amplifier in on mode.
Special attention is given to the dynamic behaviour as follows:

- Slow offset change between mute and on (controlled by MUTE and STANDBY pins)
- Low noise levels, which are independent of the supply voltage.

Protections are included to avoid the IC being damaged at:

- Over temperature: $\mathrm{T}_{\mathrm{j}}>150^{\circ} \mathrm{C}$
- Short-circuit of the output pin(s) to ground or supply rail; when short-circuited, the power dissipation is limited
- ESD protection (Human Body Model 3000 V, Machine Model 300 V)
- Energy handling. A DC voltage of 6 V can be connected to the output of any amplifier while the supply pins are short-circuited to ground.

Diagnostics are available for the following conditions (see Figs 3, 4 and 5):

- Chip temperature above $145{ }^{\circ} \mathrm{C}$
- Distortion over $2 \%$ due to clipping
- Short-circuit protection active.


## LIMITING VALUES

In accordance with the Absolute Maximum Rating System (IEC 60134).

| SYMBOL | PARAMETER | CONDITIONS | MIN. | MAX. | UNIT |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathrm{V}_{\mathrm{P}}$ | supply voltage | operating | - | 24 | V |
|  |  | no signal condition | - | 28 | V |
| $\mathrm{~V}_{\text {DIAG }}$ | voltage on pin DIAG |  | - | 18 | V |
| $\mathrm{I}_{\text {OSM }}$ | non-repetitive peak output current |  | - | 6 | A |
| $\mathrm{I}_{\text {ORM }}$ | repetitive peak output current |  | - | 4.5 | A |
| $\mathrm{~V}_{\mathrm{P}(\text { scol) }}$ | supply voltage with short-circuit across load |  | - | 28 | V |
| $\mathrm{~V}_{\mathrm{P}(\text { scg })}$ | supply voltage with short-circuit from output <br> to ground |  | - | 26 | V |
| $\mathrm{~V}_{\mathrm{P}(\text { scs })}$ | supply voltage with short-circuit from output <br> to supply |  | - | 16 | V |
| $\mathrm{~V}_{\mathrm{P}(\mathrm{rp})}$ | reverse polarity |  | - | 6 | V |
| $\mathrm{P}_{\text {tot }}$ | total power dissipation |  | - | 75 | W |
| $\mathrm{~T}_{\mathrm{j}}$ | junction temperature |  | - | 150 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\text {stg }}$ | storage temperature |  | -55 | +150 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\text {amb }}$ | ambient temperature |  | -40 | +85 | ${ }^{\circ} \mathrm{C}$ |

THERMAL CHARACTERISTICS

| SYMBOL | PARAMETER | CONDITIONS | VALUE | UNIT |
| :--- | :--- | :--- | :---: | :---: |
| $\mathrm{R}_{\mathrm{th}(\mathrm{ja})}$ | thermal resistance from junction to ambient | in free air | 40 | K/W |
| $\mathrm{R}_{\mathrm{th}(\mathrm{j} \text { - })}$ | thermal resistance from junction to case |  | 1.5 | $\mathrm{~K} / \mathrm{W}$ |

## CHARACTERISTICS

$V_{P}=14.4 \mathrm{~V} ; \mathrm{T}_{\mathrm{amb}}=25^{\circ} \mathrm{C} ; \mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz} ; \mathrm{R}_{\mathrm{L}}=\infty$; measured in test circuit of Fig. 28 ; unless otherwise specified.

| SYMBOL | PARAMETER | CONDITIONS | MIN. | TYP. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Supplies |  |  |  |  |  |  |
| $\mathrm{V}_{\mathrm{P}}$ | operating supply voltage |  | 8.0 | 14.4 | 24 | V |
| $\mathrm{I}_{\mathrm{q}(\text { tot) }}$ | total quiescent current |  | - | 140 | 170 | mA |
| $\mathrm{I}_{\text {stb }}$ | standby current |  | - | 1 | 50 | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\mathrm{O}}$ | DC output voltage |  | - | 7.0 | - | V |
| $\mathrm{V}_{\mathrm{P} \text { (mute) }}$ | low supply voltage mute |  | 6.0 | 7.0 | 8.0 | V |
| $\mathrm{V}_{1}$ | DC input voltage |  | - | 4.0 | - | V |
| Control pins |  |  |  |  |  |  |
| Standby Pin (see Table 1) |  |  |  |  |  |  |
| $\mathrm{V}_{5 \text { (stb) }}$ | voltage at STANDBY pin for standby condition |  | 0 | - | 0.8 | V |
| $\mathrm{V}_{\text {hys(5)(stb) }}$ | hysteresis voltage at STANDBY pin for standby condition | note 1 | - | 0.2 | - | V |
| $\mathrm{V}_{5 \text { (mute) }}$ | voltage at STANDBY pin for mute condition | $\mathrm{V}_{13}<0.8 \mathrm{~V}$ | 2.0 | - | 5.3 | V |
| $V_{5 \text { (on) }}$ | voltage at STANDBY pin for on condition | V ${ }^{\text {> }} 9 \mathrm{~V}$; note 2 | 8.0 | - | 18 | V |
| MUTE PIN (see Table 1) |  |  |  |  |  |  |
| $\mathrm{V}_{13 \text { (mute) }}$ | voltage at MUTE pin for mute condition | $\mathrm{V}_{5}=5 \mathrm{~V}$ | 0 | - | 0.8 | V |
| $\mathrm{V}_{13 \text { (on) }}$ | voltage at MUTE pin for on condition | $\mathrm{V}_{5}=5 \mathrm{~V}$ | 2.5 | - | 5.3 | V |

Diagnostic; output buffer (open-collector); see Figs 3, 4 and 5

| $\mathrm{V}_{\mathrm{OL}}$ | LOW-level output voltage | $\mathrm{I}_{\text {Sink }}=1 \mathrm{~mA}$ | - | 0.2 | 0.8 | V |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathrm{I}_{\mathrm{LI}}$ | leakage current | $\mathrm{V}_{\text {DIAG }}=14.4 \mathrm{~V}$ | - | - | 1 | $\mu \mathrm{~A}$ |
| CD | clip detector | $\mathrm{V}_{\text {DIAG }}<0.8 \mathrm{~V}$ | 1 | 2 | 4 | $\%$ |
| $\mathrm{~T}_{\mathrm{j} \text { (diag) }}$ | junction temperature for high <br> temperature warning | $\mathrm{V}_{\text {DIAG }}<0.8 \mathrm{~V}$ | - | 145 | - | ${ }^{\circ} \mathrm{C}$ |

Stereo BTL application; see Figs 6, 7, 10, 11, 14, 15, 18, 19, 21, 22, 23, 24, 26 and 28

| THD | total harmonic distortion | $\begin{aligned} & \mathrm{f}_{\mathrm{i}}=10 \mathrm{kHz} ; \mathrm{P}_{\mathrm{o}}=1 \mathrm{~W} ; \mathrm{R}_{\mathrm{L}}=4 \Omega \text {; } \\ & \text { filter: } 22 \mathrm{~Hz}<\mathrm{f}<30 \mathrm{kHz} \end{aligned}$ | - | 0.2 | 0.3 | \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz} ; \mathrm{P}_{\mathrm{o}}=1 \mathrm{~W} ; \mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V} ; \\ & \mathrm{R}_{\mathrm{L}}=4 \Omega \end{aligned}$ | - | 0.05 | 0.1 | \% |
|  |  | $\begin{aligned} & \mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz} ; \mathrm{P}_{\mathrm{o}}=10 \mathrm{~W} ; \mathrm{V}_{\mathrm{P}}=24 \mathrm{~V} ; \\ & \mathrm{R}_{\mathrm{L}}=8 \Omega \end{aligned}$ | - | 0.02 | 0.05 | \% |
| Po | output power | THD $=0.5 \%$; $\mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V} ; \mathrm{R}_{\mathrm{L}}=4 \Omega$ | 14 | 15 | - | W |
|  |  | THD $=0.5 \% ; \mathrm{V}_{\mathrm{P}}=24 \mathrm{~V} ; \mathrm{R}_{\mathrm{L}}=8 \Omega$ | 21 | 23 | - | W |
|  |  | THD $=10 \% ; \mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V} ; \mathrm{R}_{\mathrm{L}}=4 \Omega$ | 18 | 20 | - | W |
|  |  | THD $=10 \% ; \mathrm{V}_{\mathrm{P}}=24 \mathrm{~V} ; \mathrm{R}_{\mathrm{L}}=8 \Omega$ | 28 | 30 | - | W |
| $\mathrm{G}_{v}$ | voltage gain | $\mathrm{V}_{\mathrm{o} \text { (rms) }}=3 \mathrm{~V}$ | 31 | 32 | 33 | dB |


| SYMBOL | PARAMETER | CONDITIONS | MIN. | TYP. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\alpha_{\text {cs }}$ | channel separation | $\mathrm{P}_{\mathrm{o}}=2 \mathrm{~W} ; \mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz} ; \mathrm{R}_{\mathrm{L}}=4 \Omega$ | 60 | 65 | - | dB |
| $\left\|\Delta \mathrm{G}_{\mathrm{v}}\right\|$ | channel unbalance |  | - | - | 1 | dB |
| $\mathrm{V}_{\text {offset(DC) }}$ | DC output offset voltage | on condition | - | 0 | 140 | mV |
|  |  | mute condition; $\mathrm{R}_{\mathrm{L}}=4 \Omega$ | - | 10 | 20 | mV |
| $\mathrm{V}_{\text {no }}$ | noise output voltage | $\mathrm{R}_{\mathrm{S}}=1 \mathrm{k} \Omega$; $\mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V}$; note 3 | - | 100 | 150 | $\mu \mathrm{V}$ |
| $\mathrm{V}_{\text {no(mute) }}$ | noise output voltage mute | note 3 | - | 0 | 20 | $\mu \mathrm{V}$ |
| $\mathrm{V}_{\text {O(mute) }}$ | output voltage mute | $\mathrm{V}_{\mathrm{i}(\mathrm{rms})}=1 \mathrm{~V}$ | - | 3 | 500 | $\mu \mathrm{V}$ |
| SVRR | supply voltage ripple rejection | $\mathrm{R}_{\mathrm{S}}=0 \Omega ; \mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz}$; $\mathrm{V}_{\text {ripple(p-p) }}=2 \mathrm{~V}$; on or mute condition | 50 | 60 | - | dB |
| $\mathrm{Z}_{\mathrm{i}}$ | input impedance |  | 23 | 30 | 37 | $\mathrm{k} \Omega$ |
| CMRR | common mode rejection ratio | $\mathrm{R}_{\mathrm{S}}=0 \Omega ; \mathrm{V}_{\mathrm{i}(\mathrm{rms})}=0.5 \mathrm{~V} ; \mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz}$ | - | 60 | - | dB |

Quad SE application; see Figs 8, 9, 12, 13, 16, 17, 20, 25, 27 and 29

| THD | total harmonic distortion | $\mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz} ; \mathrm{P}_{0}=1 \mathrm{~W} ; \mathrm{R}_{\mathrm{L}}=4 \Omega$ | - | 0.05 | 0.1 | \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & f_{i}=10 \mathrm{kHz} ; \mathrm{P}_{\mathrm{o}}=1 \mathrm{~W} ; \mathrm{R}_{\mathrm{L}}=4 \Omega \text {; } \\ & \text { filter: } 22 \mathrm{~Hz}<\mathrm{f}<30 \mathrm{kHz} \end{aligned}$ | - | 0.2 | 0.3 | \% |
|  |  | $\begin{aligned} & \hline \mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz} ; \mathrm{P}_{\mathrm{o}}=1 \mathrm{~W} ; \mathrm{V}_{\mathrm{P}}=24 \mathrm{~V}, \\ & \mathrm{R}_{\mathrm{L}}=4 \Omega ; \text { filter: } 22 \mathrm{~Hz}<\mathrm{f}<30 \mathrm{kHz} \end{aligned}$ | - | 0.05 | 0.1 | \% |
| Po | output power | THD $=0.5 \% ; \mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V} ; \mathrm{R}_{\mathrm{L}}=4 \Omega$ | 3.8 | 4.0 | - | W |
|  |  | THD $=0.5 \% ; \mathrm{V}_{\mathrm{P}}=24 \mathrm{~V} ; \mathrm{R}_{\mathrm{L}}=4 \Omega$ | 10.5 | 11.5 | - | W |
|  |  | THD $=10 \% ; \mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V} ; \mathrm{R}_{\mathrm{L}}=4 \Omega$ | 4.9 | 5.2 | - | W |
|  |  | THD $=10 \% ; \mathrm{V}_{\mathrm{P}}=24 \mathrm{~V} ; \mathrm{R}_{\mathrm{L}}=4 \Omega$ | 14 | 15 | - | W |
| $\mathrm{G}_{\mathrm{v}}$ | voltage gain | $\mathrm{V}_{\mathrm{o} \text { (rms) }}=3 \mathrm{~V}$ | 25 | 26 | 27 | dB |
| $\alpha_{c s}$ | channel separation | $\mathrm{P}_{\mathrm{o}}=2 \mathrm{~W} ; \mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz} ; \mathrm{R}_{\mathrm{L}}=4 \Omega$ | 40 | 46 | - | dB |
| $\left\|\Delta G_{v}\right\|$ | channel unbalance |  | - | - | 1 | dB |
| $\mathrm{V}_{\text {offset(DC) }}$ | DC output offset voltage | $\mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V}$; on condition | - | 0 | 100 | mV |
|  |  | $\mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V}$; mute condition; $\mathrm{R}_{\mathrm{L}}=4 \Omega$ | - | 10 | 20 | mV |
| $\mathrm{V}_{\text {no }}$ | noise output voltage | $\mathrm{R}_{\mathrm{S}}=1 \mathrm{k} \Omega$; $\mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V}$; note 3 | - | 80 | 120 | $\mu \mathrm{V}$ |
| $\mathrm{V}_{\text {no(mute) }}$ | noise output voltage mute | note 3 | - | 0 | 20 | $\mu \mathrm{V}$ |
| $\mathrm{V}_{\text {O(mute) }}$ | output voltage mute | $\mathrm{V}_{\mathrm{i}(\mathrm{rms})}=1 \mathrm{~V}$ | - | 3 | 500 | $\mu \mathrm{V}$ |
| SVRR | supply voltage ripple rejection | $\begin{aligned} & \mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz} ; \mathrm{V}_{\text {ripple }(p-p)}=2 \mathrm{~V} \text {, on or } \\ & \text { mute condition; } \mathrm{R}_{\mathrm{s}}=0 \Omega \end{aligned}$ | 40 | 45 | - | dB |
| $\mathrm{Z}_{i}$ | input impedance |  | 46 | 60 | 74 | $\mathrm{k} \Omega$ |
| CMRR | common mode rejection ratio | $\mathrm{V}_{\mathrm{i}(\mathrm{rms})}=0.5 \mathrm{~V} ; \mathrm{f}_{\mathrm{i}}=1 \mathrm{kHzz} ; \mathrm{R}_{\mathrm{s}}=0 \Omega$ | - | 60 | - | dB |

## Notes

1. Hysteresis between the rise and fall voltage when pin STANDBY is controlled with low ohmic voltage source.
2. At lower $V_{P}$ the voltage at the STANDBY pin for on condition will be adjusted automatically to maintain an on condition at low battery voltage (down to 8 V ) when using one-pin operation.
3. The noise output is measured in a bandwidth of 20 Hz to 20 kHz .

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Table 1 Selection of standby, mute and on

| VOLTAGE AT PIN STANDBY | VOLTAGE AT PIN MUTE | FUNCTION |
| :--- | :--- | :--- |
| $<0.8 \mathrm{~V}$ | don't care | standby (off) |
| 2 to 5.3 V | $<0.8 \mathrm{~V}$ | mute (DC settled) |
| 2 to 5.3 V | 2.5 to 5.3 V | on (AC operating) |
| $\geq 8.0 \mathrm{~V}$ | don't care | on (AC operating) |



Fig. 3 Diagnostic waveform: temperature overload.


Fig. 4 Diagnostic waveform: DDD function.


Fig. 5 Diagnostic waveform: short-circuit to GND or $V_{P}$.


Fig. 7 Total harmonic distortion as a function of frequency; BTL mode.


Fig. 6 Total harmonic distortion as a function of frequency; BTL mode.


Fig. 8 Total harmonic distortion as a function of frequency; SE mode.

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$R_{L}=4 \Omega ; V_{P}=24 \mathrm{~V} ; 4$ channel driven.
(1) $\mathrm{P}_{0}=5 \mathrm{~W}$.
(2) $\mathrm{P}_{\mathrm{o}}=1 \mathrm{~W}$.

Fig. 9 Total harmonic distortion as a function of frequency; SE mode.

$\mathrm{R}_{\mathrm{L}}=4 \Omega ; \mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V} ; 2$ channel driven.
(1) $f_{i}=10 \mathrm{kHz}$.
(2) $f_{i}=1 \mathrm{kHz}$.
(3) $f_{i}=100 \mathrm{~Hz}$.

Fig. 10 Total harmonic distortion as a function of output power; BTL mode.

$\mathrm{R}_{\mathrm{L}}=4 \Omega ; \mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V} ; 4$ channel driven
(1) $f_{i}=10 \mathrm{kHz}$.
(2) $f_{i}=1 \mathrm{kHz}$.
(3) $f_{i}=100 \mathrm{~Hz}$.

Fig. 12 Total harmonic distortion as a function of output power; SE mode.

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Fig. 13 Total harmonic distortion as a function of output power; SE mode.

$\mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz} ; \mathrm{R}_{\mathrm{L}}=8 \Omega ; \mathrm{V}_{\mathrm{P}}=24 \mathrm{~V} ; 2$ channel driven.
Fig. 15 Power dissipation as a function of output power; BTL mode.

$f_{i}=1 \mathrm{kHz} ; \mathrm{R}_{\mathrm{L}}=4 \Omega ; \mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V} ; 2$ channel driven.

Fig. 14 Power dissipation as a function of output power; BTL mode.

$f_{i}=1 \mathrm{kHz} ; \mathrm{R}_{\mathrm{L}}=4 \Omega ; \mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V} ; 4$ channel driven.
Fig. 16 Power dissipation as a function of output power; SE mode.

$\mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz} ; \mathrm{R}_{\mathrm{L}}=4 \Omega ; \mathrm{V}_{\mathrm{P}}=24 \mathrm{~V} ; 4$ channel driven.
Fig. 17 Power dissipation as a function of output power; SE mode.

$f_{i}=1 \mathrm{kHz} ; \mathrm{R}_{\mathrm{L}}=8 \Omega ; 2$ channel driven.
(1) $\mathrm{THD}=10 \%$.
(2) $\mathrm{THD}=0.5 \%$

Fig. 19 Output power as a function of supply voltage; BTL mode.

$\mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz} ; \mathrm{R}_{\mathrm{L}}=4 \Omega ; 2$ channel driven.
(1) $\mathrm{THD}=10 \%$.
(2) $\mathrm{THD}=0.5 \%$.

Fig. 18 Output power as a function of supply voltage; BTL mode.

$\mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz} ; \mathrm{R}_{\mathrm{L}}=4 \Omega ; 2$ channel driven.
(1) $\mathrm{THD}=0.5 \%$.
(2) $\mathrm{THD}=10 \%$

Fig. 20 Output power as a function of supply voltage; SE mode.

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$\mathrm{C}_{\mathrm{i}}=470 \mathrm{nF}$.

Fig. 21 Gain as a function of input frequency; BTL mode.

$T H D=0.5 \% ; R_{L}=8 \Omega ; V_{P}=24 \mathrm{~V}$.
Fig. 23 Power bandwidth as a function of frequency; BTL mode.


THD $=0.5 \% ; R_{L}=4 \Omega ; V_{P}=14.4 \mathrm{~V}$.
Fig. 22 Power bandwidth as a function of frequency; BTL mode.

$\mathrm{P}_{\mathrm{o}}=2 \mathrm{~W} ; \mathrm{R}_{\mathrm{L}}=4 \Omega ; \mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V}$.
(1) Channels 3 and 4 to channels 1 and 2.
(2) Channels 1 and 2 to channels 3 and 4.

Fig. 24 Channel separation as a function of frequency; BTL mode.

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$\mathrm{P}_{\mathrm{o}}=2 \mathrm{~W} ; \mathrm{R}_{\mathrm{S}}=0 \Omega ; \mathrm{R}_{\mathrm{L}}=4 \Omega ; \mathrm{V}_{\mathrm{P}}=14.4 \mathrm{~V}$.
(1) Channel 1 to channel 2.
(2) Channel 1 to channel 3.
(3) Channel 1 to channel 4.

Fig. 25 Channel separation as a function of frequency; SE mode.

$\mathrm{R}_{\mathrm{s}}=0 \Omega$; $\mathrm{V}_{\text {ripple }(p-\mathrm{p})}=2 \mathrm{~V}$.
(1) $\mathrm{V}_{\mathrm{p}}=14.4 \mathrm{~V}$.
(2) $\mathrm{V}_{\mathrm{p}}=24 \mathrm{~V}$.

Fig. 26 SVRR as a function of frequency; BTL mode.
$\mathrm{R}_{\mathrm{s}}=0 \Omega ; \mathrm{V}_{\text {ripple(p-p) }}=2 \mathrm{~V}$.
(1) $V_{p}=14.4 \mathrm{~V}$.
(2) $\mathrm{V}_{\mathrm{p}}=24 \mathrm{~V}$.

Fig. 27 SVRR as a function of frequency; SE mode.

## APPLICATION INFORMATION

The application circuit depends on the supply voltage used. For supply voltages below 18 V the application circuits are shown in Figs 28, 29 and 30.

The typical application circuits for the different supply voltage ranges are shown in Figs 31, 32 and 33.

## Additional information for the applications shown in

 Figs 28, 29 and 30The RC-network connected to pin 5 determines the amplifier switch on/off behaviour as follows;

- Switched from STANDBY to MUTE when $\mathrm{V}_{\text {switching }}$ (typically 9 V ) is enabled and the switch SW1 is closed. During MUTE there is no output noise and no offset.
- Switched from MUTE to ON when the switch SW1 is opened. During switching ON the offset and noise are gradually built up. The time constant is fixed by $\mathrm{R} 1 \times \mathrm{C} 1$.

The inputs can be tied together and connected to one input capacitor. Because the input resistance is decreased by a factor of 2, the low frequency roll-off is shifted to a higher frequency when $C_{i}$ is kept the same value.

The low frequency cut-off is determined by;
$\mathrm{f}_{-3 \mathrm{~dB}}=1 /\left(2 \pi \times \mathrm{R}_{\mathrm{i}} \times \mathrm{C}_{\mathrm{i}}\right)$

$$
=\frac{1}{2 \pi \times 60 \times 10^{3} \times 220 \times 10^{-9}}=12 \mathrm{~Hz}
$$

The Boucherot network connected to the buffer (pin 9) is necessary to guarantee a low output resistance at high frequencies when the buffer is loaded (only in SE applications).

## Additional information for the applications shown in

 Figs 31, 32 and 33Short circuit behaviour at high supply voltages $\left(\mathrm{V}_{\mathrm{p}}>18 \mathrm{~V}\right)$ :

- When $\mathrm{V}_{\mathrm{p}}>18 \mathrm{~V}$ it is advisable to use the applications given in Figs 32 and 33. In these applications the diagnostics output is tied to pin 5 (one pin operation) or pin 13 (two pin operation). During a fault condition the amplifier is soft-muted and the amplitude of the output signal is reduced at:
- over temperature (still large dynamic range)
- short to ground and over load (output current reduced)
- The $4.7 \mu \mathrm{~F}$ capacitor and the $10 \mathrm{k} \Omega$ resistor connected to pin 5 or to pin 13 are used to:
- provide a stable loop
- control the switch on/off behaviour
- minimize the effect due to clip detection.


## Use of common buffer

In SE applications the buffer output is used in place of a SE capacitor. To minimize the crosstalk (high channel separation) and distortion it is advised to connect the speaker wires as closely as possible to pin 9 without using a shared wire. Internally in the IC all the efforts have been taken to minimize the crosstalk by locating the feedback loops as close as possible to pin 9.

If a common wire is shared by all the speakers, the series resistance of this shared wire will introduce added signal voltages resulting from the currents flowing through this wire when a connected amplifier is driven by a signal.

## Optimize the THD performance

The TDA8580J application can be optimized to gain the lowest THD possible by applying the following guidelines:

- SE application: minimize the shared wires to pin 9 (see section "Use of common buffer").
- Because the inputs are quasi differential, ground loops can be avoided by connecting the negative terminal of the $100 \mu \mathrm{~F}$ signal ground capacitor (connected to pin 12) to the ground pin of the signal processor.
Note: do not leave the inputs in the open condition to prevent HF oscillation.
- Increase the value of electrolytic supply capacitor (typical value $1000 \mu \mathrm{~F}$ ) to the maximum possible to minimize cross talk and distortion at low signal frequencies, due to the PSRR (power supply rejection ratio). For suppressing high frequency transients on the supply line a capacitor (typical value 100 nF ) with a low ESR is required to be connected in parallel with the electrolytic capacitor. The capacitor combination must be placed as close as possible to the IC (using short interconnection tracks).


## Headroom

A typical CD requires at least 12 dB dynamic headroom (a factor of 15.85), compared with the average power output, for passing the loudest parts without distortion.

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For BTL application at $\mathrm{V}_{\mathrm{p}}=24 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=8 \Omega$ and $\mathrm{P}_{\mathrm{o}}$ at THD $=0.5 \%$ (see Fig.15), the Average Listening Level (ALL) for music power without distortion yields:
$P_{o(A L L)}=\frac{23}{15.85}=1.45 \mathrm{~W}$.
Table $2 P_{d}$ as a function of headroom (music signals) for $\mathrm{P}_{\mathrm{o}}=2 \times 23 \mathrm{~W}(\mathrm{THD}=0.5 \%)$.

| HEADROOM | $\mathbf{P}_{\mathbf{d}}$ |
| :--- | :--- |
| 0 dB | 32 W |
| 12 dB | 16 W |

So for the average music listening level a total power dissipation of 16 W can be used for calculating the optimum heat sink thermal resistance.

## Heatsink calculation

The measured thermal resistance of this package $R_{\text {th( }(-\mathrm{c})}$ is a maximum of $1.5 \mathrm{~K} / \mathrm{W}$. For a maximum ambient temperature of $60^{\circ} \mathrm{C}$ the required heatsink thermal resistance can be calculated as shown in the following example.

EXAMPLE
Measured or given values:

$$
\begin{aligned}
& \mathrm{V}_{\mathrm{p}}=24 \mathrm{~V} \\
& \mathrm{R}_{\mathrm{L}}=8 \Omega(2 \times \mathrm{BTL})
\end{aligned}
$$

$$
\text { Measured worst case } P_{d}(\text { sine wave })=32 \mathrm{~W}
$$

$$
\mathrm{T}_{\mathrm{j}(\max )}=150^{\circ} \mathrm{C}
$$

$$
\mathrm{T}_{\mathrm{amb}(\max )}=60^{\circ} \mathrm{C}
$$

$$
\mathrm{R}_{\mathrm{th}(j-\mathrm{c})}=1.5 \mathrm{~K} / \mathrm{W}
$$

$$
R_{t h(h s)}=\frac{T_{j(\max )}-T_{a m b(\max )}}{P_{d}}-R_{t h(j-c)}
$$

$$
=\frac{150-60}{32}-1.5=1.3 \mathrm{~K} / \mathrm{W}
$$

Table 3 Heatsink thermal resistance as a function of headroom for $\mathrm{P}_{\mathrm{o}}=2 \times 23 \mathrm{~W}$ (THD $=0.5 \%$ ).

| HEAD ROOM | $\mathbf{P}_{\mathbf{d}}$ | $\mathbf{R}_{\text {th(hs }}$ |
| :--- | :--- | :--- |
| 0 dB | 32 W | $1.3 \mathrm{~K} / \mathrm{W}$ |
| 12 dB | 16 W | $4.12 \mathrm{~K} / \mathrm{W}$ |



Fig. 28 Stereo bridge-tied load application; $\mathrm{V}_{\mathrm{P}} \leq 18 \mathrm{~V}$.


Fig. 29 Quad single-ended application; $\mathrm{V}_{\mathrm{P}} \leq 18 \mathrm{~V}$.

(1) $R 1$ and $R 2$ values depend on $V_{\text {switching }}$ applied; the value of $R 1$ and $R 2$ connected in parallel should be minimum $10 \mathrm{k} \Omega$.

Fig. 30 Dual single-ended and one bridge-tied load application; $\mathrm{V}_{\mathrm{P}} \leq 18 \mathrm{~V}$.

(1) Load conditions: quad SE ( $4 \times 4 \Omega$ ), or dual $\operatorname{BTL}(2 \times 8 \Omega)$, or dual SE $(2 \times 4 \Omega)$ and one $\operatorname{BTL}(1 \times 8 \Omega)$.
(2) RC combination not required in BTL mode.
(3) R1 and R2 values depend on $\mathrm{V}_{\text {switching }}$ applied; the value of R1 and R2 connected in parallel should be minimum $10 \mathrm{k} \Omega$.

Fig. 31 Application 1 ; supply voltage range $8 \mathrm{~V}<\mathrm{V}_{\mathrm{P}} \leq 18 \mathrm{~V}$; 1-pin and 2-pin operation.

(1) Load conditions: quad SE ( $4 \times 4 \Omega$ ), or dual BTL ( $2 \times 8 \Omega$ ), or dual SE $(2 \times 4 \Omega)$ and one $\operatorname{BTL}(1 \times 8 \Omega)$,
(2) RC combination not required in BTL mode.
(3) R1 and R2 values depend on $V_{\text {switching }}$ applied; the value of $R 1$ and $R 2$ connected in parallel should be minimum $10 \mathrm{k} \Omega$.

Fig. 32 Application 2; supply voltage range $18 \mathrm{~V}<\mathrm{V}_{\mathrm{P}} \leq 24 \mathrm{~V}$; 1-pin operation.

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(1) Load conditions: quad SE ( $4 \times 4 \Omega$ ), or dual BTL ( $2 \times 8 \Omega$ ), or dual SE $(2 \times 4 \Omega)$ and one $\operatorname{BTL}(1 \times 8 \Omega)$
(2) $R C$ combination not required in BTL mode.

Fig. 33 Application 3; supply voltage range $18 \mathrm{~V}<\mathrm{V}_{\mathrm{P}} \leq 24 \mathrm{~V}$; 2-pin operation.

## INTERNAL PIN CONFIGURATION

| PIN | NAME | EQUIVALENT CIRCUIT |
| :---: | :---: | :---: |
| $7,8,10,11$ <br> and 12 | Inputs |  |
| $1,4,9,14$ |  |  |
| and 17 |  |  |$\quad$ Outputs

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| PIN | NAME | EQUIVALENT CIRCUIT |
| :---: | :---: | :---: |
| 5 | STANDBY |  |
| 13 | MUTE |  |
| 6 | DIAG |  |

## PACKAGE OUTLINE

DBS17P: plastic DIL-bent-SIL power package; 17 leads (lead length 12 mm)
SOT243-1

view $\mathbf{B}$ : mounting base side


DIMENSIONS (mm are the original dimensions)

| UNIT | $\mathbf{A}$ | $\mathbf{A}_{\mathbf{2}}$ | $\mathbf{b}_{\mathbf{p}}$ | $\mathbf{c}$ | $\mathbf{D}^{(\mathbf{1})}$ | $\mathbf{d}$ | $\mathbf{D}_{\mathbf{h}}$ | $\mathbf{E}^{(\mathbf{1})}$ | $\mathbf{e}$ | $\mathbf{e}_{\mathbf{1}}$ | $\mathbf{e}_{\mathbf{2}}$ | $\mathbf{E}_{\mathbf{h}}$ | $\mathbf{j}$ | $\mathbf{L}$ | $\mathbf{L}_{\mathbf{3}}$ | $\mathbf{m}$ | $\mathbf{Q}$ | $\mathbf{v}$ | $\mathbf{w}$ | $\mathbf{x}$ | $\mathbf{Z}^{(\mathbf{1})}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mm | 17.0 | 4.6 | 0.75 | 0.48 | 24.0 | 20.0 | 10 | 12.2 | 2.54 | 1.27 | 5.08 | 6 | 3.4 | 12.4 | 2.4 |  | 4.3 | 2.1 | 0.8 | 0.4 | 0.03 |
|  | 15.5 | 4.4 | 0.60 | 0.38 | 23.6 | 19.6 |  | 11.8 | 2.54 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1.45 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Note

1. Plastic or metal protrusions of 0.25 mm maximum per side are not included.

| OUTLINE <br> VERSION | REFERENCES |  |  |  | EUROPEAN <br> PROJECTION | ISSUE DATE |
| :--- | :--- | :--- | :--- | :--- | :--- | :---: |
|  | IEC | JEDEC | EIAJ |  |  |  |
| SOT243-1 |  |  |  |  | $-97-12-16$ |  |

## Multi-purpose power amplifier

## SOLDERING

## Introduction to soldering through-hole mount packages

This text gives a brief insight to wave, dip and manual soldering. A more in-depth account of soldering ICs can be found in our "Data Handbook IC26; Integrated Circuit Packages" (document order number 9398652 90011).

Wave soldering is the preferred method for mounting of through-hole mount IC packages on a printed-circuit board.

## Soldering by dipping or by solder wave

The maximum permissible temperature of the solder is $260^{\circ} \mathrm{C}$; solder at this temperature must not be in contact with the joints for more than 5 seconds.

The total contact time of successive solder waves must not exceed 5 seconds.

The device may be mounted up to the seating plane, but the temperature of the plastic body must not exceed the specified maximum storage temperature ( $\mathrm{T}_{\text {stg }}$ (max) $)$. If the printed-circuit board has been pre-heated, forced cooling may be necessary immediately after soldering to keep the temperature within the permissible limit.

## Manual soldering

Apply the soldering iron ( 24 V or less) to the lead(s) of the package, either below the seating plane or not more than 2 mm above it. If the temperature of the soldering iron bit is less than $300^{\circ} \mathrm{C}$ it may remain in contact for up to 10 seconds. If the bit temperature is between 300 and $400^{\circ} \mathrm{C}$, contact may be up to 5 seconds.

Suitability of through-hole mount IC packages for dipping and wave soldering methods

| PACKAGE | SOLDERING METHOD |  |
| :---: | :--- | :--- |
|  | DIPPING |  |
| DBS, DIP, HDIP, SDIP, SIL | suitable | WAVE |

## Note

1. For SDIP packages, the longitudinal axis must be parallel to the transport direction of the printed-circuit board.

## DATA SHEET STATUS

| DATA SHEET STATUS | PRODUCT <br> STATUS | DEFINITIONS ${ }^{(1)}$ |
| :--- | :--- | :--- |
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## Note

1. Please consult the most recently issued data sheet before initiating or completing a design.

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