

500MHz, $3nV/\sqrt{Hz}$, $A_V \ge 10$ Operational Amplifier

FEATURES

■ Gain-Bandwidth: 500MHz

■ Gain of 10 Stable Uncompensated

■ Slew Rate: 200V/µs

■ Input Noise Voltage: 3nV/√Hz

■ C-Load[™] Op Amp Drives Capacitive Loads

■ External Compensation Pin

■ Maximum Input Offset Voltage: 300µV

Maximum Input Bias Current: 300nA

Maximum Input Offset Current: 300nA

■ Minimum Output Swing Into 500Ω: ±12V

■ Minimum DC Gain: 100V/mV, $R_I = 500\Omega$

■ Settling Time to 0.1%: 75ns, 10V Step

Settling Time to 0.01%: 120ns, 10V Step

■ Differential Gain: 0.4%, $A_V = 2$, $R_I = 150\Omega$

■ Differential Phase: 0.1° , $A_V = 2$, $R_L = 150\Omega$

APPLICATIONS

- Wideband Amplifiers
- Buffers
- Active Filters
- Video and RF Amplification
- Cable Drivers
- 8-, 10-, 12-Bit Data Acquisition Systems

DESCRIPTION

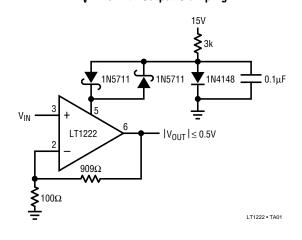
The LT1222 is a low noise, very high speed operational amplifier with superior DC performance. The LT1222 is stable in a noise gain of 10 or greater without compensation, or the part can be externally compensated for lower closed-loop gain at the expense of lower bandwidth and slew rate. It features reduced input offset voltage, lower input bias currents, lower noise and higher DC gain than devices with comparable bandwidth and slew rate. The circuit is a single gain stage that includes proprietary DC gain enhancement circuitry to obtain precision with high speed. The high gain and fast settling time make the circuit an ideal choice for data acquisition systems. The circuit is also capable of driving capacitive loads which makes it useful in buffer or cable driver applications. The compensation node can also be used to clamp the output swing.

The LT1222 is a member of a family of fast, high performance amplifiers that employ Linear Technology Corporation's advanced complementary bipolar processing. For unity-gain stable applications the LT1220 can be used, and for gains of 4 or greater the LT1221 can be used.

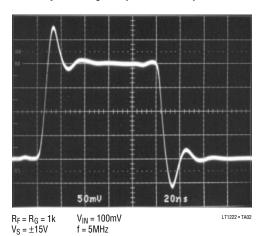
and LTC are registered trademarks and LT is a trademark of Linear Technology Corporation. C-Load is a trademark of Linear Technology Cortporation.

TYPICAL APPLICATION

 $A_V = 10$ with Output Clamping



 $A_V = -1$, $C_C = 30$ pF Pulse Response

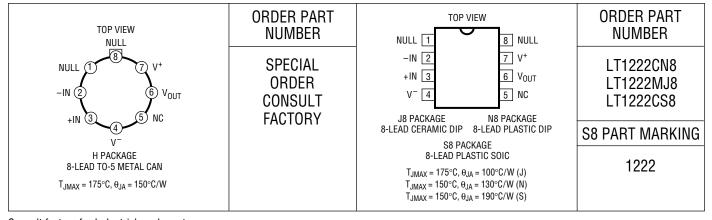


ABSOLUTE MAXIMUM RATINGS

Total Supply Voltage (V + to V -)
Differential Input Voltage ±6V
Input Voltage ±V _S
Output Short-Circuit Duration (Note 1) Indefinite
Specified Temperature Range
LT1222C (Note 2) 0°C to 70°C
LT1222M –55°C to 125°C

Operating Temperature Range	
LT1222C40°C TO 85	oC
LT1222M55°C to 125	O°
Maximum Junction Temperature (See Below)	
Plastic Package 150	O°
Ceramic Package 175	oC
Storage Temperature Range65°C to 150°	oC
Lead Temperature (Soldering, 10 sec) 300	oC

PACKAGE/ORDER INFORMATION



Consult factory for Industrial grade parts.

ELECTRICAL CHARACTERISTICS $V_S = \pm 15V$, $T_A = 25^{\circ}C$, $V_{CM} = 0V$, unless otherwise specified.

SYMBOL	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
V_{0S}	Input Offset Voltage	(Note 3)		100	300	μV
I _{OS}	Input Offset Current			100	300	nA
I _B	Input Bias Current			100	300	nA
e _n	Input Noise Voltage	f = 10kHz		3		nV/√Hz
i _n	Input Noise Current	f = 10kHz		2		pA/√Hz
R _{IN}	Input Resistance	V _{CM} = ±12V Differential	20	45 12		MΩ kΩ
C _{IN}	Inut Capacitance			2		pF
	Input Voltage Range (Positive) Input Voltage Range (Negative)		12	14 -13	-12	V
CMRR	Common-Mode Rejection Ratio	V _{CM} = ±12V	100	120		dB
PSRR	Power Supply Rejection Ratio	$V_S = \pm 5V \text{ to } \pm 15V$	98	110		dB
A _{VOL}	Large-Signal Voltage Gain	$V_{OUT} = \pm 10V$, $R_L = 500\Omega$	100	200		V/mV
V _{OUT}	Output Swing	$R_L = 500\Omega$	12	13		±V
I _{OUT}	Output Current	V _{OUT} = ±12V	24	26		mA
SR	Slew Rate	(Note 4)	150	200		V/µs
	Full Power Bandwidth	10V Peak (Note 5)		3.2		MHz
GBW	Gain-Bandwidth	f = 1MHz		500		MHz

ELECTRICAL CHARACTERISTICS $v_s = \pm 15 V$, $T_A = 25 ^{\circ}C$, $v_{CM} = 0 V$, unless otherwise specified.

SYMBOL	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
t _r , t _f	Rise Time, Fall Time	A _V = 10, 10% to 90%, 0.1V		2.4		ns
	Overshoot	A _V = 10, 0.1V		45		%
	Propagation Delay	A _V = 10, 50% V _{IN} to 50% V _{OUT} , 0.1V		5.2		ns
t _s	Settling Time	10V Step, 0.1% 10V Step, 0.01%		75 120		ns ns
	Differential Gain	$A_V = 2$, $C_C = 50$ pF, $f = 3.58$ MHz, $R_L = 150\Omega$ (Note 6) $A_V = 10$, $C_C = 0$ pF, $f = 3.58$ MHz, $R_L = 1$ k (Note 6)		0.40 0.15		% %
	Differential Phase	$A_V = 2$, $C_C = 50$ pF, $f = 3.58$ MHz, $R_L = 150\Omega$ (Note 6) $A_V = 10$, $C_C = 0$ pF, $f = 3.58$ MHz, $R_L = 1$ k (Note 6)		0.10 0.01		DEG DEG
$\overline{R_0}$	Output Resistance	A _V = 10, f = 1MHz		0.1		Ω
Is	Supply Current			8	10.5	mA

$V_S = \pm 15 V$, $0^{\circ}C \le T_A \le 70^{\circ}C$, $V_{CM} = 0 V$, unless otherwise specified.

SYMBOL	PARAMETER	CONDITIONS		MIN	TYP	MAX	UNITS
V_{0S}	Input Offset Voltage	(Note 3)	•		100	600	μV
	Input V _{OS} Drift				5		μV/°C
I _{OS}	Input Offset Current		•		100	400	nA
IB	Input Bias Current		•		100	400	nA
CMRR	Common-Mode Rejection Ratio	$V_{CM} = \pm 12V$	•	100	120		dB
PSRR	Power Supply Rejection Ratio	$V_S = \pm 5V$ to $\pm 15V$	•	98	110		dB
A _{VOL}	Large-Signal Voltage Gain	$V_{OUT} = \pm 10V, R_L = 500\Omega$	•	100	200		V/mV
V _{OUT}	Output Swing	$R_L = 500\Omega$	•	12	13		±V
I _{OUT}	Output Current	$V_{OUT} = \pm 12V$	•	24	26		mA
SR	Slew Rate	(Note 4)	•	150	200		V/µs
Is	Supply Current		•		8	11	mA

$V_S=\pm 15V,\, -55^{\circ}C \leq T_A \leq 125^{\circ}C,\, V_{CM}=0V,$ unless otherwise specified.

SYMBOL	PARAMETER	CONDITIONS		MIN	TYP	MAX	UNITS
$\overline{V_{0S}}$	Input Offset Voltage	(Note 3)	•		100	600	μV
	Input V _{OS} Drift				5		μV/°C
I _{OS}	Input Offset Current		•		100	800	nA
I _B	Input Bias Current		•		100	1000	nA
CMRR	Common-Mode Rejection Ratio	$V_{CM} = \pm 12V$	•	98	120		dB
PSRR	Power Supply Rejection Ratio	$V_S = \pm 5V$ to $\pm 15V$	•	98	110		dB
A _{VOL}	Large-Signal Voltage Gain	$V_{OUT} = \pm 10V$, $R_L = 500\Omega$	•	50	200		V/mV
V _{OUT}	Output Swing	$R_L = 500\Omega$ $R_L = 1k$	•	10 12	13 13		±V ±V
I _{OUT}	Output Current	$V_{OUT} = \pm 10V$ $V_{OUT} = \pm 12V$	•	20 12	26 13		mA mA
SR	Slew Rate	(Note 4)	•	110	200		V/µs
I _S	Supply Current		•		8	11	mA

The ● denotes specifications which apply over the full temperature range.

 $\textbf{Note 1:} \ A \ heat \ sink \ may \ be \ required \ when \ the \ output \ is \ shorted \ indefinitely.$

Note 2: Commercial parts are designed to operate over -40° C to 85° C, but are not tested nor guaranteed beyond 0° C to 70° C. Industrial grade parts specified and tested over -40° C to 85° C are available on special request. Consult factory.

Note 3: Input offset voltage is pulse tested and is exclusive of warm-up drift.

Note 4: Slew rate is measured between $\pm 10 V$ on an output swing of $\pm 12 V.$

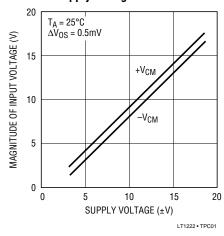
Note 5: FPBW = $SR/2\pi V_P$.

Note 6: Differential Gain and Phase are tested with five amps in series. Attenuators of 1/Gain are used as loads.

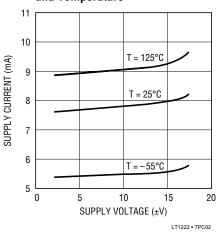


TYPICAL PERFORMANCE CHARACTERISTICS

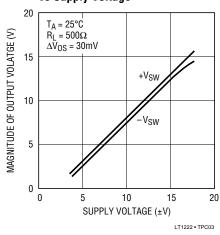
Input Common-Mode Range vs Supply Voltage



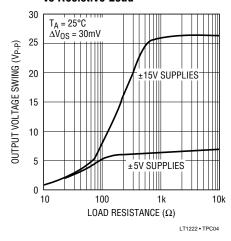
Supply Current vs Supply Voltage and Temperature



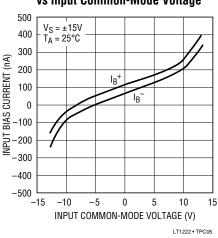
Output Voltage Swing vs Supply Voltage



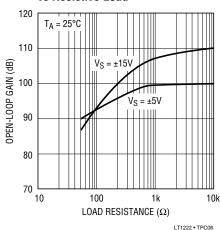
Output Voltage Swing vs Resistive Load



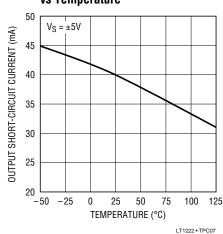
Input Bias Current vs Input Common-Mode Voltage



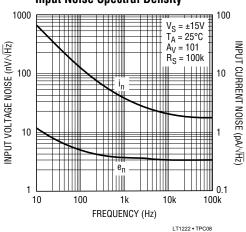
Open-Loop Gain vs Resistive Load



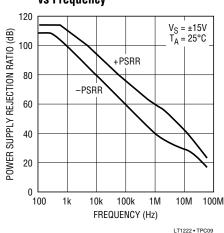
Output Short-Circuit Current vs Temperature



Input Noise Spectral Density

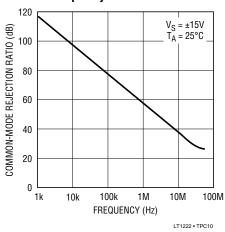


Power Supply Rejection Ratio vs Frequency

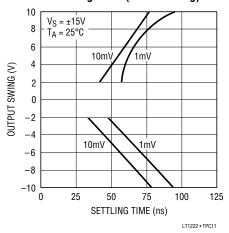


TYPICAL PERFORMANCE CHARACTERISTICS

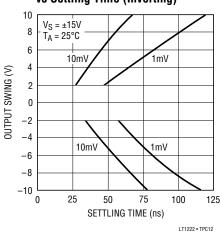
Common-Mode Rejection Ratio vs Frequency



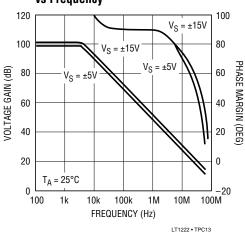
Output Swing and Error vs Settling Time (Noninverting)



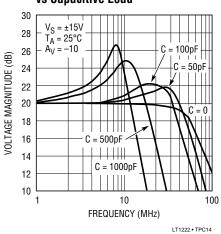
Output Swing and Error vs Settling Time (Inverting)



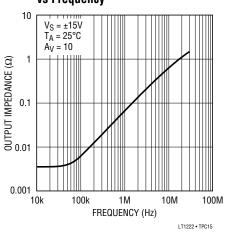
Voltage Gain and Phase vs Frequency



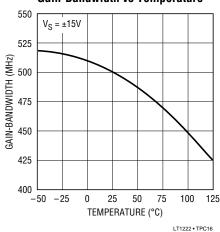
Frequency Response vs Capacitive Load



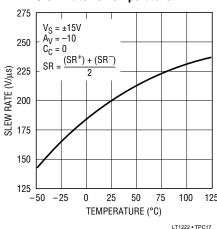
Closed-Loop Output Impedance vs Frequency



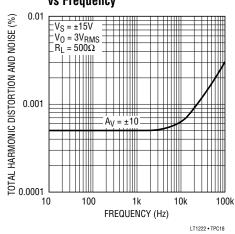
Gain-Bandwidth vs Temperature



Slew Rate vs Temperature

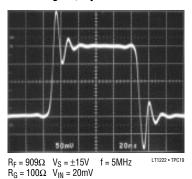


Total Harmonic Distortion vs Frequency

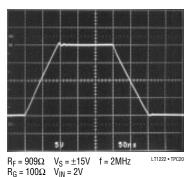


TYPICAL PERFORMANCE CHARACTERISTICS

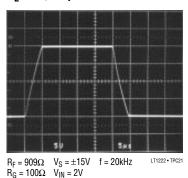
Small Signal, A_V = 10



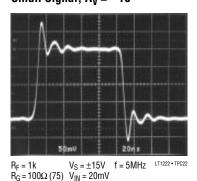
Large Signal, $A_V = 10$



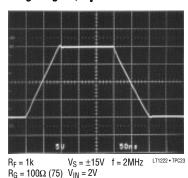
Large Signal, $A_V = 10$, $C_1 = 10,000$ pF



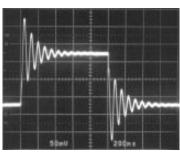
Small Signal, $A_V = -10$



Large Signal, $A_V = -10$



Small Signal, $A_V = -10$, $C_L = 1,000pF$

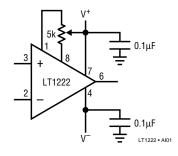


 $R_F=1k$ $V_S=\pm15V$ f=500kHz LT1222 • TPC24 $R_G=100\Omega$ (75) $V_{IN}=15mV$

APPLICATIONS INFORMATION

The LT1222 is stable in noise gains of 10 or greater and may be inserted directly into HA2520/2/5, HA2541/2/4, AD817, AD847, EL2020, EL2044 and LM6361 applications, provided that the nulling circuitry is removed and the amplifier configuration has a high enough noise gain. The suggested nulling circuit for the LT1222 is shown in the following figure.

Offset Nulling



Layout and Passive Components

The LT1222 amplifier is easy to apply and tolerant of less than ideal layouts. For maximum performance (for example, fast settling time) use a ground plane, short lead lengths and RF-quality bypass capacitors $(0.01\mu\text{F to }0.1\mu\text{F})$. For high drive current applications use low ESR bypass capacitors (1µF to 10µF tantalum). Sockets should be avoided when maximum frequency performance is required. For more details see Design Note 50. Feedback resistors greater than 5k are not recommended because a pole is formed with the input capacitance which can cause peaking or oscillations. Stray capacitance on pin 5 should be minimized. Bias current cancellation circuitry is employed on the inputs of the LT1222 so the input bias current and input offset current have identical specifications. For this reason, matching the impedance on the inputs to reduce bias current errors is not necessary.



APPLICATIONS INFORMATION

Output Clamping

Access to the internal compensation node at pin 5 allows the output swing of the LT1222 to be clamped. An example is shown on the first page of this data sheet. The compensation node is approximately one diode drop above the output and can source or sink 1.2mA. Back-to-back Schottky diodes clamp pin 5 to a diode drop above ground so the output is clamped to $\pm 0.5 \text{V}$ (the drop of the Schottkys at 1.2mA). The diode reference is bypassed for good AC response. This circuit is useful for amplifying the voltage at false sum nodes used in settling time measurements.

Capacitive Loading

The LT1222 is stable with capacitive loads. This is accomplished by sensing the load induced output pole and adding compensation at the amplifier gain node. As the capacitive load increases, both the bandwidth and phase margin decrease. There will be peaking in the frequency domain as shown in the curve of Frequency Response vs Capacitive Load. The small-signal transient response will have more overshoot as shown in the photo of the small-signal response with 1000pF load. The large-signal response with a 10,000pF load shows the output slew rate being limited to 4V/µs by the short-circuit current. The LT1222 can drive coaxial cable directly, but for best pulse fidelity a resistor of value equal to the characteristic impedance of the cable (i.e., 75Ω) should be placed in series with the output. The other end of the cable should be terminated with the same value resistor to ground.

Compensation

The LT1222 has a typical gain-bandwidth product of 500MHz which allows it to have wide bandwidth in high gain configurations (i.e., in a gain of 100, it will have a bandwidth of about 5MHz). For added flexibility the amplifier frequency response may be adjusted by adding capacitance from pin 5 to ground. The compensation capacitor

may be used to reduce overshoot, to allow the amplifier to be used in lower noise gains, or simply to reduce bandwidth. Table 1 shows gain and compensation capacitor vresus – 3dB bandwidth, maximum frequency peaking and small-signal overshoot.

Table 1

A _V	C _C (pF)	f _{-3dB} (MHz)	Max Peaking (dB)	Overshoot (%)
-1	30	99	4.2	36
-1 -1	50	70	0.9	13
-1	82	32	0	0
-1	150	13	0	0
5	10	140	3.8	35
5	20	100	0	5
5	30	34	0	1
5	50	15	0	0
10	0	150	9.5	45
10	5	111	0.2	10
10	10	40	0	2
10	20	17	0	0
20	0	82	0.1	10
20	5	24	0	0
20	10	14	0	0

For frequencies < 10MHz the frequency response of the amplifier is approximately:

$$f = 1/[2\pi \times 53\Omega \times (C_C + 6pF) \times (Noise Gain)]$$

The slew rate is affected as follows:

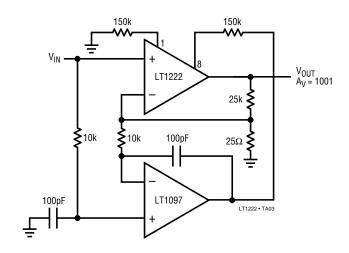
$$SR = 1.2mA/(C_C + 6pF)$$

An example would be a gain of -10 (noise gain of 11) and $C_C = 20 pF$ which has 10.5 MHz bandwidth and $46 V/\mu s$ slew rate. It should be noted that the LT1222 is not stable in $A_V = 1$ unless $C_C = 50 pF$ and a 1k resistor is used as the feedback resistor. The 1k and input capacitance increase the noise gain at frequency to aid stability.

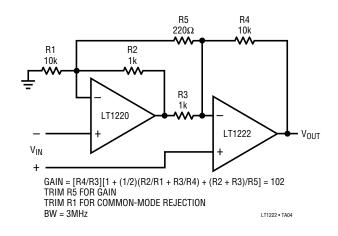


TYPICAL APPLICATIONS

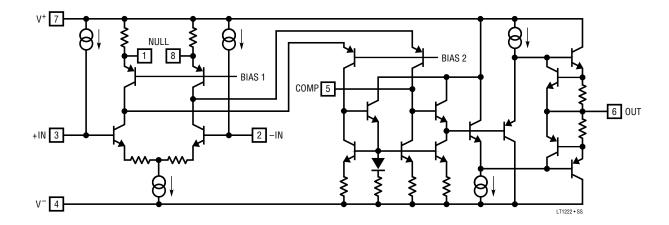
Vos Null Loop



Two Op Amp Instrumentation Amplifier

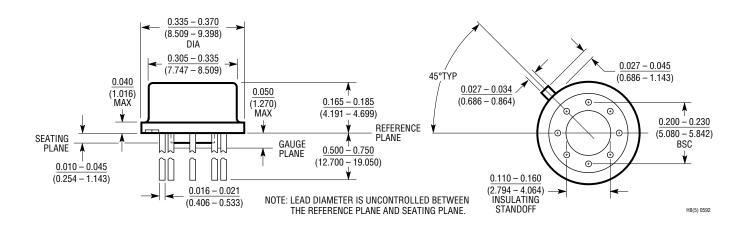


SIMPLIFIED SCHEMATIC

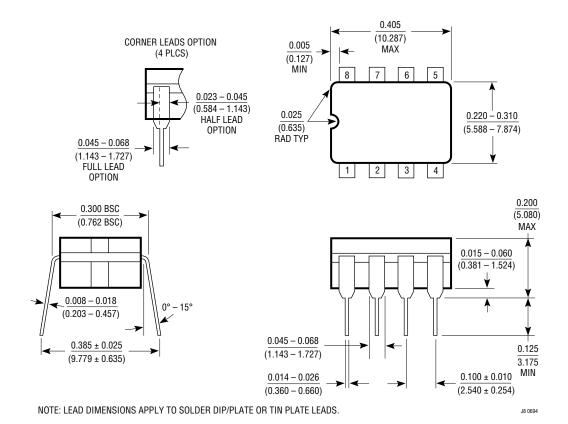


PACKAGE DESCRIPTION Dimensions in inches (millimeters) unless otherwise noted.

H8 Package 8-Lead TO-5 Metal Can

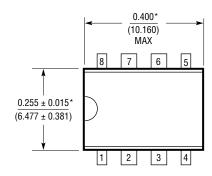


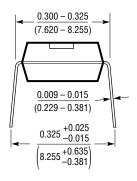
J8 Package 8-Lead Ceramic Dip

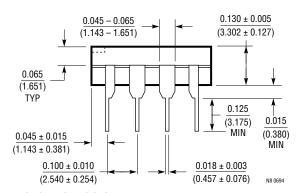


PACKAGE DESCRIPTION Dimensions in inches (millimeters) unless otherwise noted.

N8 Package 8-Lead Plastic Dip



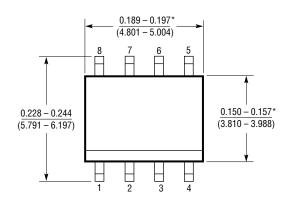


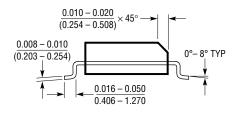


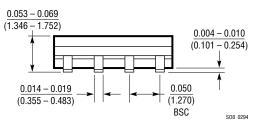
*THESE DIMENSIONS DO NOT INCLUDE MOLD FLASH OR PROTRUSIONS. MOLD FLASH OR PROTURSIONS SHALL NOT EXCEED 0.010 INCH (0.254mm).

PACKAGE DESCRIPTION Dimensions in inches (millimeters) unless otherwise noted.

S8 Package 8-Lead Plastic SOIC







*THESE DIMENSIONS DO NOT INCLUDE MOLD FLASH OR PROTRUSIONS. MOLD FLASH OR PROTRUSIONS SHALL NOT EXCEED 0.006 INCH (0.15mm).

NORTHEAST REGION Linear Technology Corporation

3220 Tillman Drive, Suite 120 Bensalem, PA 19020 Phone: (215) 638-9667 FAX: (215) 638-9764

Linear Technology Corporation

266 Lowell St., Suite B-8 Wilmington, MA 01887 Phone: (508) 658-3881 FAX: (508) 658-2701

FRANCE

Linear Technology S.A.R.L.

Immeuble "Le Quartz" 58 Chemin de la Justice 92290 Chatenay Malabry France

Phone: 33-1-41079555 FAX: 33-1-46314613

GERMANY

Linear Techonolgy GmbH

Untere Hauptstr. 9 D-85386 Eching Germany

Phone: 49-89-3197410 FAX: 49-89-3194821

JAPAN

Linear Technology KK

5F YZ Bldg.

4-4-12 lidabashi, Chiyoda-Ku Tokyo, 102 Japan

Phone: 81-3-3237-7891 FAX: 81-3-3237-8010

U.S. Area Sales Offices

SOUTHEAST REGION

Linear Technology Corporation

17060 Dallas Parkway

Suite 208 Dallas, TX 75248 Phone: (214) 733-3071 FAX: (214) 380-5138

CENTRAL REGION

FAX: (708) 620-6977

Linear Technology Corporation

Chesapeake Square 229 Mitchell Court, Suite A-25 Addison, IL 60101 Phone: (708) 620-6910

International Sales Offices

KOREA

Linear Technology Korea Branch

Namsong Building, #505 Itaewon-Dong 260-199 Yongsan-Ku, Seoul Korea

Phone: 82-2-792-1617 FAX: 82-2-792-1619

SINGAPORE

Linear Technology Pte. Ltd.

507 Yishun Industrial Park A Singapore 2776 Phone: 65-753-2692 FAX: 65-754-4113

SOUTHWEST REGION

Linear Technology Corporation

22141 Ventura Blvd. Suite 206 Woodland Hills, CA 91364 Phone: (818) 703-0835 FAX: (818) 703-0517

NORTHWEST REGION Linear Technology Corporation

782 Sycamore Dr. Milpitas, CA 95035 Phone: (408) 428-2050 FAX: (408) 432-6331

TAIWAN

Linear Technology Corporation

Rm. 801, No. 46, Sec. 2 Chung Shan N. Rd. Taipei, Taiwan, R.O.C. Phone: 886-2-521-7575 FAX: 886-2-562-2285

UNITED KINGDOM

Linear Technology (UK) Ltd.

The Coliseum, Riverside Way Camberley, Surrey GU15 3YL

United Kingdom Phone: 44-276-677676 FAX: 44-276-64851

World Headquarters

Linear Technology Corporation

1630 McCarthy Blvd. Milpitas, CA 95035-7487 Phone: (408) 432-1900 FAX: (408) 434-0507

0794