# 5V/12V/15V or Adjustable, High-Efficiency, Low IQ, Step-Up DC-DC Controllers 


#### Abstract

General Description The MAX770-MAX773 step-up switching controllers provide $90 \%$ efficiency over a 10 mA to 1 A load. A unique current-limited pulse-frequency-modulation (PFM) control scheme gives these devices the benefits of pulse-width-modulation (PWM) converters (high efficiency at heavy loads), while using less than $110 \mu \mathrm{~A}$ of supply current (vs. 2 mA to 10 mA for PWM converters). These ICs use tiny external components. Their high switching frequencies (up to 300 kHz ) allow surfacemount magnetics of 5 mm height and 9 mm diameter. The MAX770/MAX771/MAX772 accept input voltages from 2 V to 16.5 V . Output voltages are preset at 5 V , (MAX770), 12V (MAX771), and 15V (MAX772); they can also be adjusted using two resistors. The MAX773 accepts inputs from 3 V to 16.5 V . For a wider input range, it features an internal shunt regulator that allows unlimited higher input voltages. The MAX773's output can be set to $5 \mathrm{~V}, 12 \mathrm{~V}$, or 15 V , or it can be adjusted with two resistors. The MAX770-MAX773 drive external N-channel MOSFET switches, allowing them to power loads up to 15 W . If less power is required, use the MAX756/MAX757 or MAX761/MAX762 step-up switching regulators with onboard MOSFETs.


## Applications

Palmtops/Handy-Terminals
High-Efficiency DC-DC Converters
Battery-Powered Applications
Positive LCD-Bias Generators
Portable Communicators
Flash Memory Programmers

Typical Operating Circuit


Features

- $90 \%$ Efficiency for 10 mA to 1A Load Currents
- Up to 15W Output Power
- 110 $\mu \mathrm{A}$ Max Supply Current
- $5 \mu \mathrm{~A}$ Max Shutdown Current
- 2V to 16.5V Input Range
(MAX770/MAX771/MAX772)
- Internal Shunt Regulator for High Input Voltages (MAX773)
- Preset or Adjustable Output Voltages

MAX770: 5V or Adjustable
MAX771: 12V or Adjustable
MAX772: 15V or Adjustable
MAX773: 5V, 12V, 15V, or Adjustable

- Current-Limited PFM Control Scheme
- 300kHz Switching Frequency

Ordering Information

| PART | TEMP. RANGE | PIN-PACKAGE |
| :--- | :--- | :--- |
| MAX770CPA | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | Plastic DIP |
| MAX 770 CSA | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | 8 SO |
| MAX $770 \mathrm{C} / \mathrm{D}$ | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | Dice ${ }^{*}$ |
| MAX 770 EPA | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 Plastic DIP |
| MAX 770 ESA | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 SO |
| MAX 770 MJA | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8 CERDIP ${ }^{\star \star}$ |

Ordering Information continued at end of data sheet.
*Contact factory for dice specifications.
**Contact factory for availability and processing to MIL-STD-883B.
Pin Configurations


Pin Configurations continued at end of data sheet.

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# 5V/12V/15V or Adjustable, High-Efficiency, Low IQ, Step-Up DC-DC Controllers 

ABSOLUTE MAXIMUM RATINGS
Supply Voltages



Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## ELECTRICAL CHARACTERISTICS

$\left(\mathrm{V}+=5 \mathrm{~V}, \mathrm{I}_{\text {LOAD }}=0 \mathrm{~mA}, \mathrm{~T}_{\mathrm{A}}=\mathrm{T}_{\text {MIN }}\right.$ to $\mathrm{T}_{\mathrm{MAX}}$, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$. $)$

| PARAMETER | SYMBOL | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Input Voltage Range |  | MAX770-772 (internal feedback resistors) |  | 2.0 |  | 16.5 |  |
|  |  | MAX770-772C/E (external resistors) |  | 3.0 |  | 16.5 |  |
|  |  | MAX770-772MJA (external resistors) |  | 3.1 |  | 16.5 | V |
|  |  | MAX773C/E |  | 3.0 |  | 16.5 |  |
|  |  | MAX773MJD |  | 3.1 |  | 16.5 |  |
| Minimum Start-Up Voltage |  | MAX770/MAX771/MAX772 |  |  | 1.8 | 2.0 | V |
| Supply Current |  | $\mathrm{V}_{+}=16.5 \mathrm{~V}, \mathrm{SHDN}=0 \mathrm{~V}$ (normal operation) |  |  | 85 | 110 | $\mu \mathrm{A}$ |
| Standby Current |  | $\mathrm{V}_{+}=10.0 \mathrm{~V}, \mathrm{SHDN} \geq 1.6 \mathrm{~V}$ (shutdown) |  |  | 2 | 5 |  |
|  |  | $\mathrm{V}_{+}=16.5 \mathrm{~V}, \mathrm{SHDN} \geq 1.6 \mathrm{~V}$ (shutdown) |  |  | 4 |  |  |
| Output Voltage (Note 1) |  | $\mathrm{V}+=2.0 \mathrm{~V}$ to 5.0 V , over full load range |  | 4.80 | 5.0 | 5.20 |  |
|  |  | $\mathrm{V}+=2.0 \mathrm{~V}$ to 12.0 V , over full load range |  | 11.52 | 12.0 | 12.48 | V |
|  |  | $\mathrm{V}+=2.0 \mathrm{~V}$ to 15.0 V , over full load range |  | 14.40 | 15.0 | 15.60 |  |
| Output Voltage Line Regulation (Note 2) |  | Figure $2 \mathrm{a}, \mathrm{V}+=2.7 \mathrm{~V}$ to 4.5 V , ILOAD $=700 \mathrm{~mA}$, VOUT $=5 \mathrm{~V}$ |  |  | 5 |  | mV/V |
| Output Voltage Load Regulation (Note 2) |  | Figure $2 \mathrm{a}, \mathrm{V}+=3 \mathrm{~V}, \mathrm{I}_{\text {LOAD }}=30 \mathrm{~mA}$ to 1 A , Vout $=5 \mathrm{~V}$ |  |  | 20 |  | mV/A |
| Maximum Switch On-Time | ton(max) |  |  | 12 | 16 | 20 | $\mu \mathrm{s}$ |
| Minimum Switch Off-Time | toff(min) |  |  | 1.8 | 2.3 | 2.8 | $\mu \mathrm{s}$ |
| Efficiency |  | $\mathrm{V}+=4 \mathrm{~V}, \mathrm{LLOAD}=500 \mathrm{~mA}, \mathrm{~V}$ OUT $=5 \mathrm{~V}$ |  |  | 87 |  | \% |
| Reference Voltage | Vref | $I_{\text {REF }}=0 \mu \mathrm{~A}$ | MAX77_C | 1.4700 | 1.5 | 1.5300 | V |
|  |  |  | MAX77_E | 1.4625 | 1.5 | 1.5375 |  |
|  |  |  | MAX77_M | 1.4550 | 1.5 | 1.5450 |  |

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## ELECTRICAL CHARACTERISTICS (continued)

$\left(\mathrm{V}+=5 \mathrm{~V}, \mathrm{ILOAD}^{2}=0 \mathrm{~mA}, \mathrm{~T}_{\mathrm{A}}=\mathrm{T}_{\mathrm{MIN}}\right.$ to $\mathrm{T}_{\mathrm{MAX}}$, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.)

| PARAMETERS | SYMBOL | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| REF Load Regulation |  | $0 \mu \mathrm{~A} \leq \mathrm{IREF} \leq 100 \mu \mathrm{~A}$ | MAX77_C/E |  | 4 | 10 | mV |
|  |  |  | MAX77_M |  | 4 | 15 |  |
| REF Line Regulation |  | $3 \mathrm{~V} \leq \mathrm{V}+\leq 16.5 \mathrm{~V}$ |  |  | 40 | 100 | $\mu \mathrm{V} / \mathrm{V}$ |
| FB Trip-Point Voltage | $V_{\text {FB }}$ | MAX77_C |  | 1.4700 | 1.50 | 1.5300 | V |
|  |  | MAX77_E |  | 1.4625 | 1.50 | 1.5375 |  |
|  |  | MAX77_M |  | 1.4550 | 1.50 | 1.5450 |  |
| FB Input Current | IFB | MAX77_C |  |  |  | $\pm 20$ | nA |
|  |  | MAX77_E |  |  |  | $\pm 40$ |  |
|  |  | MAX77_M |  |  |  | $\pm 60$ |  |
| SHDN Input High Voltage | $\mathrm{V}_{\mathrm{IH}}$ | $\mathrm{V}_{+}=2.0 \mathrm{~V}$ to 16.5 V |  | 1.6 |  |  | V |
| SHDN Input Low Voltage | VIL | MAX77_C/E, V+ = 2.0V to 16.5V |  |  |  | 0.4 | V |
|  |  | MAX77_M, V+ = 2.0V to 16.5 V |  |  |  | 0.2 |  |
| SHDN Input Current |  | $\mathrm{V}_{+}=16.5 \mathrm{~V}, \mathrm{SHDN}=0 \mathrm{~V}$ or $\mathrm{V}_{+}$ |  |  |  | $\pm 1$ | $\mu \mathrm{A}$ |
| LBI Input Current |  | MAX773, $\mathrm{V}_{+}=16.5 \mathrm{~V}, \mathrm{LBI}=1.5 \mathrm{~V}$ |  |  |  | $\pm 20$ | nA |
| LBI Hysteresis |  | MAX773 |  |  | 20 |  | mV |
| LBI Delay |  | 5 mV overdrive |  |  | 2.5 |  | $\mu \mathrm{s}$ |
| LBI Threshold Voltage |  | MAX773, LBI falling | MAX77_C | 1.4700 | 1.50 | 1.5300 | V |
|  |  |  | MAX77_E | 1.4625 | 1.50 | 1.5375 |  |
|  |  |  | MAX77_M | 1.4550 | 1.50 | 1.5450 |  |
| LBO Leakage Current |  | MAX773, $\mathrm{V}_{+}=16.5 \mathrm{~V}, \mathrm{~V}_{\text {LBO }}=16.5 \mathrm{~V}$ |  |  | 0.01 | 1.00 | $\mu \mathrm{A}$ |
| LBO Output Voltage Low | VoL | MAX773, $\mathrm{V}_{+}=5 \mathrm{~V}$, LBO sinking 1mA |  |  | 0.1 | 0.4 | V |
| Current-Limit Trip Level | VCS | $\mathrm{V}+=5 \mathrm{~V}$ to 16.5 V |  | 170 | 200 | 230 | mV |
| CS Input Current |  |  |  |  | 0.01 | $\pm 1$ | $\mu \mathrm{A}$ |
| EXT Rise Time |  | $\mathrm{V}+=5 \mathrm{~V}, 1 \mathrm{nF}$ from EXT to ground (Note 3) |  |  | 55 |  | ns |
| EXT Fall Time |  | $\mathrm{V}_{+}=5 \mathrm{~V}, 1 \mathrm{nF}$ from EXT to ground (Note 3) |  |  | 55 |  | ns |
| Supply Voltage in Shunt Mode | $\mathrm{V}_{\text {SHUNT }}$ | $\begin{aligned} & \text { MAX773, ISHUNT }=1 \mathrm{~mA} \text { to } 20 \mathrm{~mA}, \\ & \text { SGND }=0 \mathrm{~V}, \mathrm{CSHUNT}=0.1 \mu \mathrm{~F} \end{aligned}$ |  | 5.5 |  | 6.3 | V |

Note 1: Output voltage guaranteed using preset voltages. See Figures 7a-7d for output current capability versus input voltage.
Note 2: Output voltage line and load regulation depend on external circuit components.
Note 3: For the MAX773, EXT is EXTH and EXTL shorted together.

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$\left(\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}\right.$, unless otherwise noted.)

M AX770 EFFICIENCY vs. OUTPUT CURRENT (BOOTSTRAPPED)


MAX771
EFFICIENCY vs. OUTPUT CURRENT
(NON-BOOTSTRAPPED)




M AX770
LOAD CURRENT vs.
MINIMUM START-UP INPUT VOLTAGE



MAX772
EFFICIENCY vs. OUTPUT CURRENT (BOOTSTRAPPED)


M AX771
LOAD CURRENT vs.
MINIMUM START-UP INPUT VOLTAGE


EXT RISE/FALL TIME vs. SUPPLY VOLTAGE


# 5V/12V/15V or Adjustable, High-Efficiency, Low IQ, Step-Up DC-DC Controllers 

Typical Operating Characteristics (continued)
( $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted.)







## 5V/12V/15V or Adjustable, High-Efficienc y, Low IQ, Step-Up DC-DC Controllers

Typical Operating Characteristics (continued)
(Circuit of Figure $2 \mathrm{a}, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted.)

MAX770
HEAVY-LOAD SWITCHNG WAVEFORMS


20us/div
$\mathrm{V}_{\text {IN }}=2.9 \mathrm{~V}$, IOUT $=0.9 \mathrm{~A}$
A: EXT VOLTAGE, 5V/div
B: INDUCTORCURRENT 1A/div
C: Vout RIPPLE $100 \mathrm{mV} / \mathrm{div}$, AC-COUPLED

MAX770
LINE-TRANSIENT RESPONSE


IOUT $=0.7 \mathrm{~A}$
A: $\mathrm{V}_{\mathrm{IN}}, 2.7 \mathrm{~V}$ TO $4.5 \mathrm{~V}, 2 \mathrm{~V} / \mathrm{div}$
B: VOUT RIPPLE, $100 \mathrm{mV} / \mathrm{div}$, AC-COUPLED

MAX770
LIGHT-LOAD SWITCHING WAVEFORMS

$20 \mu \mathrm{~s} / \mathrm{div}$
$\mathrm{V}+=3 \mathrm{~V}$, $\mathrm{IOUT}=165 \mathrm{~mA}$
A: EXT VOLTAGE, 5V/div
B: INDUCTOR CURRENT, 1A/div
C: Vout RIPPLE $100 \mathrm{mV} / \mathrm{div}$, AC-COUPLED

MAX770
LOAD-TRANSIENT RESPONSE

$V_{I N}=3 V$
A: LOAD CURRENT 0.5A/div (0A to 1A)
B: VOUT RIPPLE, $100 \mathrm{mV} / \mathrm{div}$, AC-COUPLED

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Typical Operating Characteristics（continued）
（Circuit of Figure $2 \mathrm{a}, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ ，unless otherwise noted．）
MAX770
EXITING SHUTDOWN


200 $\mu \mathrm{s} / \mathrm{div}$
$\mathrm{V}_{\mathrm{IN}}=3 \mathrm{~V}$ ，IOUT $=0.5 \mathrm{~A}$
A：SHDN，2V／div
B：Vout，2V／div
Pin Description

| PIN |  | NAME | FUNCTION |
| :---: | :---: | :---: | :---: |
| MAX770 MAX771 MAX772 | MAX773 |  |  |
| 1 | － | EXT | Gate drive for external N－channel power transistor |
| 2 | 3 | V＋ | Power－supply input．Also acts as a voltage－sense point when in bootstrapped mode for the MAX770／MAX771／MAX772，or as a shunt regulator when SGND is connected to ground for the MAX773．Bypass to SGND with $0.1 \mu \mathrm{~F}$ when using the shunt regulator． |
| 3 | 6 | FB | Feedback input for adjustable－output operation．Connect to ground for fixed－output operation．Use a resistor divider network to adjust the output voltage．See Setting the Output Voltage section． |
| 4 | 7 | SHDN | Active－high TTL／CMOS logic－level shutdown input．In shutdown mode，Vout is a diode drop below $\mathrm{V}_{+}$（due to the DC path from $\mathrm{V}_{+}$to the output）and the supply current drops to $5 \mu \mathrm{~A}$ maximum．Connect to ground for normal operation． |
| 5 | 8 | REF | 1.5 V reference output that can source $100 \mu \mathrm{~A}$ for external loads．Bypass to GND with $0.1 \mu \mathrm{~F}$ ． The reference is disabled in shutdown． |
| 6 | － | AGND | Analog ground |
| 7 | 9 | GND | High－current ground return for the output driver |
| 8 | 11 | CS | Positive input to the current－sense amplifier．Connect the current－sense resistor between CS and GND． |
| － | 1 | V12 | Input sense point for 12V－output operation．Connect VOUT to V12 for 12V－output operation． Leave unconnected for adjustable－output operation． |
| － | 2 | V5 | Input sense point for 5V－output operation．Connect VOUT to V5 for 5V－output operation．Leave unconnected for adjustable－output operation． |
| － | 4 | LBO | Low－battery output is an open－drain output that goes low when LBI is less than 1．5V．Connect to $\mathrm{V}_{+}$ through a pull－up resistor．Leave floating if not used．LBO is high impedance in shutdown mode． |
| － | 5 | LBI | Input to the internal low－battery comparator．Tie to GND or V＋if not used． |
| － | 10 | SGND | Shunt regulator ground．Leave unconnected if the shunt regulator is not used． |

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# Pin Description (continued) 

| PIN |  | NAME |  |
| :---: | :---: | :---: | :--- |
| MAX770 <br> MAX771 <br> MAX772 | MAX773 |  |  |
| - | 12 | EXTL | Low-level gate/base drive for external power transistor. Connect to the gate of an external <br> N-channel MOSFET or to the base of an external NPN transistor. |
| - | 13 | EXTH | High-level gate/base drive for external power transistor. Connect to EXTL when using an external <br> N-channel MOSFET. When using an external NPN transistor, connect a resistor RBASE from <br> EXTH to the base of the NPN to set the maximum base-drive current. |
| - | 14 | V15 | Input sense point for 15V-output operation. Connect VOUT to V15 for 15V-output operation. <br> Leave unconnected for adjustable-output operation |

## Detailed Description

The MAX770-MAX773 are BiCMOS, step-up, switchmode power-supply controllers that provide preset 5 V , 12 V , and 15 V output voltages, in addition to adjustableoutput operation. Their unique control scheme combines the advantages of pulse-frequency modulation (low supply current) and pulse-width modulation (high efficiency with heavy loads), providing high efficiency over a wide output current range, as well as increased output current capability over previous PFM devices. In addition, the external sense resistor and power transistor allow the user to tailor the output current capability for each application. Figure 1 shows the MAX770-MAX773 block diagram.
The MAX770-MAX773 offer three main improvements over prior pulse-skipping control solutions: 1) the converters operate with tiny ( 5 mm height and less than 9 mm diameter) surface-mount inductors due to their 300 kHz switching frequency; 2) the current-limited PFM control scheme allows 87\% efficiencies over a wide range of load currents; and 3) the maximum supply current is only $110 \mu \mathrm{~A}$.
The MAX773 can be configured to operate from an internal 6V shunt regulator, allowing very high input/output voltages. Its output can be configured for an adjustable voltage or for one of three fixed voltages $(5 \mathrm{~V}, 12 \mathrm{~V}$, or 15 V ), and it has a power-fail comparator for low-battery detection.
All devices have shutdown capability, reducing the supply current to $5 \mu \mathrm{~A}$ max.

## Bootstrapped/Non-Bootstrapped Modes

Figures 2 and 3 show standard application circuits for bootstrapped and non-bootstrapped modes. In bootstrapped mode, the IC is powered from the output (VOUT, which is connected to $\mathrm{V}_{+}$) and the input voltage
range is 2 V to VOUT. The voltage applied to the gate of the external power transistor is switched from VOUT to ground, providing more switch gate drive and thus reducing the transistor's on resistance.
In non-bootstrapped mode, the IC is powered from the input voltage ( $\mathrm{V}_{+}$) and operates with minimum supply current. In this mode, FB is the output voltage sense point. Since the voltage swing applied to the gate of the external power transistor is reduced (the gate swings from V+ to ground), the power transistor's on resistance increases at low input voltages. However, the supply current is also reduced because $\mathrm{V}_{+}$is at a lower voltage, and because less energy is consumed while charging and discharging the external MOSFET's gate capacitance. The minimum input voltage for the MAX770-MAX773 is 3 V when using external feedback resistors. With supply voltages below 5 V , bootstrapped mode is recommended.
Note: When using the MAX770/MAX771/MAX772 in non-bootstrapped mode, there is no preset output operation because $\mathrm{V}_{+}$is also the output voltage sense point for fixed-output operation. External resistors must be used to set the output voltage. Use $1 \%$ external feedback resistors when operating in adjustable-output mode (Figures 2c, 2d, 3b, 3d, 3e) to achieve an overall output voltage accuracy of $\pm 5 \%$. The MAX773 can be operated in non-bootstrapped mode without using external feedback resistors because $V_{+}$does not act as the output voltage sense point with preset-output operation. To achieve highest efficiency, operate in bootstrapped mode whenever possible.

MAX773 Shunt-Regulator Operation
The MAX773 has an internal 6V shunt regulator that allows the device to step up from very high input voltages (Figure 4).

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Figure 1. Block Diagram

Floating the shunt-regulator ground (SGND) disables the shunt regulator. To enable it, connect SGND to GND. The shunt regulator requires 1 mA minimum current for proper operation; the maximum current must not exceed 20mA. The MAX773 operates in non-bootstrapped mode when the shunt regulator is used, and EXT swings between the 6 V shunt-regulator voltage and GND.

When using the shunt regulator, use an N-channel power FET instead of an NPN power transistor as the power switch. Otherwise, excessive base drive will collapse the shunt regulator.

## External Power-Transistor Control Circ uitry

PFM Control Scheme The MAX770-MAX773 use a proprietary current-limited PFM control scheme to provide high efficiency over a wide range of load currents. This control scheme combines the ultra-low supply current of PFM converters (or pulse skippers) with the high full-load efficiency of PWM converters.
Unlike traditional PFM converters, the MAX770MAX773 use a sense resistor to control the peak inductor current. They also operate with high switching

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Figure 2a. 5V Preset Output, Bootstrapped


Figure 2c. 12V Output, Non-Bootstrapped
frequencies (up to 300 kHz ), allowing the use of tiny external components.
As with traditional PFM converters, the power transistor is not turned on until the voltage comparator senses that the output is out of regulation. However, unlike traditional PFM converters, the MAX770-MAX773 switch using the combination of a peak current limit and a pair of one-shots that set the maximum on-time $(16 \mu \mathrm{~s})$ and


Figure 2b. 12V Preset Output, Bootstrapped


Figure 2d. 9V Output, Bootstrapped
minimum off-time $(2.3 \mu \mathrm{~s})$; there is no oscillator. Once off, the minimum off-time one-shot holds the switch off for $2.3 \mu \mathrm{~s}$. After this minimum time, the switch either 1) stays off if the output is in regulation, or 2 ) turns on again if the output is out of regulation.
The control circuitry allows the ICs to operate in contin-uous-conduction mode (CCM) while maintaining high efficiency with heavy loads. When the power switch is

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Figure 3a. 12V Preset Output, Bootstrapped, N-Channel Power MOSFET


Figure 3c. 15V Preset Output, Non-Bootstrapped N-Channel Power MOSFET

$\varepsilon \angle L X \forall W-0 \angle L X \forall W$

Figure 3b. 24V Output, Non-Bootstrapped, NPN Power Transistor


Figure 3d. 16V Output, Bootstrapped, N-Channel Power MOSFET

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Figure 3e. 100V Output, Shunt Regulator, N-Channel Power MOSFET
turned on, it stays on until either 1) the maximum ontime one-shot turns it off (typically $16 \mu \mathrm{~s}$ later), or 2 ) the switch current reaches the peak current limit set by the current-sense resistor.
To increase light-load efficiency, the current limit for the first two pulses is set to one-half the peak current limit. If those pulses bring the output voltage into regulation, the error comparator holds the MOSFET off and the current limit remains at one-half the peak current limit. If the output voltage is still out of regulation after two pulses, the current limit for the next pulse is raised to the peak current limit set by the external sense resistor (see inductor current waveforms in the Typical Operating Characteristics).
The MAX770-MAX773 switching frequency is variable (depending on load current and input voltage), causing variable switching noise. However, the subharmonic noise generated does not exceed the peak current limit times the filter capacitor equivalent series resistance (ESR). For example, when generating a 12 V output at 500 mA from a 5 V input, only 180 mV of output ripple occurs using the circuit of Figure 2 b .


Figure 4. MAX773 Shunt Regulator

## Low-Voltage Start-Up Oscillator

The MAX770/MAX771/MAX772 feature a low input voltage start-up oscillator that guarantees start-up with no load down to 2 V when operating in bootstrapped mode and using internal feedback resistors. At these low voltages, the supply voltage is not large enough for proper error-comparator operation and internal biasing. The start-up oscillator has a fixed $50 \%$ duty cycle and the MAX770/MAX771/MAX772 disregard the error-comparator output when the supply voltage is less than 2.5 V . Above 2.5 V , the error-comparator and normal oneshot timing circuitry are used. The low voltage start-up circuitry is disabled if non-bootstrapped mode is selected (FB is not tied to ground).
The MAX773 does not provide the low-voltage $50 \%$ duty-cycle oscillator. Its minimum start-up voltage is 3 V for all modes.

## External Transistor

An N-FET power switch is recommended for the MAX770/MAX771/MAX772.
The MAX773 can drive either an N -channel MOSFET ( $\mathrm{N}-\mathrm{FET}$ ) or an NPN because it provides two separate

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drive outputs (EXTH and EXTL) that operate $180^{\circ}$ out of phase (Figures 3a and 3b). In Figure 3b, the resistor in series with EXTH limits the base current, and EXTL (which is connected directly to the base) turns the transistor off.

Shutdown Mode
When SHDN is high, the MAX770-MAX773 enter shutdown mode. In this mode, the internal biasing circuitry is turned off (including the reference) and VOUT falls to a diode drop below VIN (due to the DC path from the input to the output). In shutdown mode, the supply current drops to less than $5 \mu \mathrm{~A}$. SHDN is a TTL/CMOS logic-level input. Connect SHDN to GND for normal operation.
The MAX773's shunt regulator is not disabled in shutdown mode.

Low-Battery Detector The MAX773 provides a low-battery comparator that compares the voltage on LBI to the reference voltage. When the LBI voltage is below Vref, LBO (an opendrain output) goes low. The low-battery comparator's 20 mV of hysteresis adds noise immunity, preventing repeated triggering of LBO. Use a resistor-divider network between $\mathrm{V}_{+}$, LBI, and GND to set the desired trip voltage VTRIP. LBO is high impedance in shutdown mode.

## Design Procedure

## Setting the Output Voltage

To set the output voltage, first determine the mode of operation, either bootstrapped or non-bootstrapped. Bootstrapped mode provides more output current capability, while non-bootstrapped mode reduces the supply current (see Typical Operating Characteristics). If a decaying voltage source (such as a battery) is used, see the additional notes in the Low Input Voltage Operation section.
Use the MAX770/MAX771/MAX772 unless one or more of the following conditions applies. If one or more of the following is true, use the MAX773:

1) An NPN power transistor will be used as the power switch
2) The LBI/LBO function is required
3) The shunt regulator must accommodate a high input voltage
4) Preset-output non-bootstrapped operation is desired-for example, to reduce the no-load supply current in a 5 V to 12 V application.


Figure 5. Adjustable Output Circuit
See Table 1 for a summary of operating characteristics and requirements for the ICs in bootstrapped and nonbootstrapped modes.
The MAX770-MAX773's output voltage can be adjusted from very high voltages down to 3 V , using external resistors R1 and R2 configured as shown in Figure 5. For adjustable-output operation, select feedback resistor R1 in the range of $10 \mathrm{k} \Omega$ to $500 \mathrm{k} \Omega$. R2 is given by:

$$
\mathrm{R} 2=(\mathrm{R} 1)\left(\frac{\mathrm{V}_{\text {OUT }}}{\mathrm{V}_{\mathrm{REF}}}-1\right)
$$

where $V_{\text {REF }}$ equals 1.5 V .
For preset-output operation, tie FB to GND (this forces bootstrapped-mode operation for the MAX770/MAX771/MAX772).
Configure the MAX773 for a preset voltage of 5 V , 12 V , or 15 V by connecting the output to the corresponding sense input pin (i.e., V5, V12, or V15). FB must be tied to ground for preset-output operation. Leave all unused sense input pins unconnected. Failure to do so will cause an incorrect output voltage. The MAX773 can provide a preset output voltage in both bootstrapped and nonbootstrapped modes.
Figures 2 and 3 show various circuit configurations for bootstrapped/non-bootstrapped, preset/adjustable operation.

## Shunt-Regulator Operation

When using the shunt regulator, connect SGND to ground and place a $0.1 \mu \mathrm{~F}$ capacitor between $\mathrm{V}_{+}$and SGND, as close to the IC as possible. Increase C2 to $1.0 \mu \mathrm{~F}$ to improve shunt regulators performance with heavy loads. Select RSHUNT such that $1 \mathrm{~mA} \leq \mathrm{ISHUNT} \leq 20 \mathrm{~mA}$.

# 5V/12V/15V or Adjustable, High-Efficiency, Low IQ, Step-Up DC-DC Controllers 

Table 1. Bootstrapped vs. Non-Bootstrapped Operation

| PARAMETER | BOOTSTRAPPED* | NON-BOOTSTRAPPED |
| :---: | :---: | :---: |
| Gate Drive | GND to VOUT | GND to V+ |
| FET On Resistance | Lower | Higher |
| Gate-Drive Capacitive Losses | Higher | Lower |
| No-Load Supply Current | Higher | Lower |
| Possible Input Voltage Range | 2V to 16.5V (MAX770/MAX771/MAX772), (internal feedback resistors) 3V to 16.5V (MAX770/MAX771/MAX772), (external feedback resistors) 3V to 16.5V (MAX773) | 3 V to 16.5 V <br> (MAX770/MAX771/MAX772), <br> 3 V and up (MAX773) |
| Normally Recommended Input Voltage Range | 2V to 5V (MAX770/MAX771/MAX772), <br> 3V to 5V (MAX773) | ```5V to 16.5V (MAX770/MAX771/MAX772), 5V and up (MAX773)``` |
| Fixed Output Available | MAX770-MAX773(N) | MAX773(N)/MAX773(S) |
| Adjustable Output Available | MAX770-MAX773(N) | MAX770/MAX771/MAX772/ MAX773(N)/MAX773(S) |

*MAX773(S) indicates shunt mode; MAX773(N) indicates NOT in shunt mode.

Use an N-channel FET as the power switch when using the shunt regulator (see MAX773 Shunt-Regulator Operation in the Detailed Description). The shunt-regulator current powers the MAX773 and also provides the FET gate-drive current, which depends largely on the FET's total gate charge at VGS $=5 \mathrm{~V}$. To determine the shunt-resistor value, first determine the maximum shunt current required.
ISHUNT = ISUPP + IGATE

See N-Channel MOSFETs in the Power-Transistor Selection section to determine IGATE.
Determine the shunt-resistor value using the following equation:

$$
\text { RSHUNT(max })=\frac{\operatorname{VIN}_{\operatorname{IN}}(\min )-\mathrm{V}_{\text {SHUNT }}(\max )}{\mathrm{I}_{\text {SHUNT }}}
$$

where $\mathrm{V}_{\text {SHUNT }}$ (max) is 6.3 V .
The shunt regulator is not disabled in shutdown mode, and continues to draw the calculated shunt current.
If the calculated shunt regulator current exceeds 20 mA , or if the shunt current exceeds 5 mA and less shunt regulator current is desired, use the circuit of Figure 6 to provide increased drive and reduced shunt current when driving N-FETs with large gate capacitances. Select ISHUNT $=3 \mathrm{~mA}$. This provides adequate biasing current for this circuit, although higher shunt currents can be used.


Figure 6. Increased N-FET Gate Drive when Using the Shunt Regulator

To prevent the shunt regulator from drawing current in shutdown mode, place a switch in series with the shunt resistor.

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Figure 7a. Maximum Output Current vs. Input Voltage ( VOUT $=5 \mathrm{~V}$ )


Figure 7c. Maximum Output Current vs. Input Voltage (VOUT = 15V)

## Determining Rsense

The Typical Operating Characteristics graphs show the output current capability for various modes, sense resistors, and input/output voltages. Use these graphs, along with the theoretical output current curves shown in Figures 7a-7d, to select RSENSE. These theoretical curves assume that an external N -FET power switch is used. They were derived using the minimum (worstcase) current-limit comparator threshold value, and the inductance value. No tolerance was included for RSENSE. The voltage drop across the diode was assumed to be 0.5 V , and the drop across the power switch rDS(ON) and coil resistance was assumed to be 0.3 V . To use the graphs, locate the graph with the appropriate output voltage or the graph having the nearest output voltage higher than the desired output voltage. On this graph, find the curve for the largest


Figure 7b. Maximum Output Current vs. Input Voltage ( VOUT $=12 \mathrm{~V}$ )


Figure 7d. Maximum Output Current vs. Input Voltage (VOUT = 24V)
sense-resistor value with an output current that is adequate at the lowest input voltage.

## Determining the Inductor (L)

 Practical inductor values range from $10 \mu \mathrm{H}$ to $300 \mu \mathrm{H}$. $20 \mu \mathrm{H}$ is a good choice for most applications. In applications with large input/output differentials, the IC's output current capability will be much less when the inductance value is too low, because the IC will always operate in discontinuous mode. If the inductor value is too low, the current will ramp up to a high level before the current-limit comparator can turn off the switch. The minimum on-time for the switch (ton(min)) is approximately $2 \mu \mathrm{~s}$; select an inductor that allows the current to ramp up to ILIM/2 in no less than $2 \mu \mathrm{~s}$. Choosing a value of ILIM/2 allows the half-size current pulses to occur, increasing light-load efficiency and minimizing output ripple.
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Figure 8a. Use an N-Channel MOSFET with the MAX770/MAX771/MAX772


Figure 8b. Using an N-Channel MOSFET with the MAX773
The standard operating circuits use a $22 \mu \mathrm{H}$ inductor. If a different inductance value is desired, select $L$ such that:

$$
\mathrm{L} \geq \frac{\mathrm{V} \operatorname{IN}(\max ) \times \operatorname{toN}(\min )}{\mathrm{ILIM}^{2} / 2}
$$

Larger inductance values tend to increase the start-up time slightly, while smaller inductance values allow the coil current to ramp up to higher levels before the switch turns off, increasing the ripple at light loads.
Inductors with a ferrite core or equivalent are recommended; powder iron cores are not recommended for use with high switching frequencies. Make sure the inductor's saturation current rating (the current at which the core begins to saturate and the inductance starts to fall) exceeds the peak current rating set by RSENSE. However, it is generally acceptable to bias the inductor into saturation by approximately $20 \%$ (the point where the inductance is $20 \%$ below the nominal value). For highest efficiency, use a coil with low DC resistance,


Figure 8c. Using an NPN Transistor with the MAX773
preferably under $20 \mathrm{~m} \Omega$. To minimize radiated noise, use a toroid, a pot core, or a shielded coil.
Table 2 lists inductor suppliers and specific recommended inductors.

Power Transistor Selection
Use an N-channel MOSFET power transistor with the MAX770/MAX771/MAX772 (Figure 8a).
Use an N-FET whenever possible with the MAX773. An NPN transistor can be used, but be extremely careful when determining the base current (see NPN Transistors section). An NPN transistor is not recommended when using the shunt regulator.

N-Channel MOSFETs
To ensure the external N -channel MOSFET ( N -FET) is turned on hard, use logic-level or low-threshold N -FETs when the input drive voltage is less than 8 V . This applies even in bootstrapped mode, to ensure start-up.
N -FETs provide the highest efficiency because they do not draw any DC gate-drive current, but they are typically more expensive than NPN transistors. When using an N-FET with the MAX773, connect EXTH and EXTL to the N -FET's gate (Figure 8b).
When selecting an N-FET, three important parameters are the total gate charge $\left(\mathrm{Q}_{\mathrm{g}}\right)$, on resistance (rDS(ON)), and reverse transfer capacitance (CRSS).
$\mathrm{Q}_{\mathrm{g}}$ takes into account all capacitances associated with charging the gate. Use the typical $\mathrm{Q}_{\mathrm{g}}$ value for best results; the maximum value is usually grossly overspecified since it is a guaranteed limit and not the measured value. The typical total gate charge should be 50 nC or less. With larger numbers, the EXT pins may not be able to adequately drive the gate. The EXT rise/fall time with various capacitive loads as shown in the Typical Operating Characteristics.

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The two most significant losses contributing to the N -FET's power dissipation are I2R losses and switching losses. Select a transistor with low rDS(ON) and low CRSS to minimize these losses.
Determine the maximum required gate-drive current from the $Q_{g}$ specification in the N-FET data sheet.
The MAX773's maximum allowed switching frequency during normal operation is 300 kHz ; but at start-up the maximum frequency can be 500 kHz , so the maximum current required to charge the N-FET's gate is $f(\max ) \times \mathrm{Q}_{\mathrm{g}}$ (typ). Use the typical $\mathrm{Q}_{\mathrm{g}}$ number from the transistor data sheet. For example, the Si9410DY has a $\mathrm{Qg}_{\mathrm{g}}$ (typ) of 17 nC (at $\mathrm{VGS}=5 \mathrm{~V}$ ), therefore the current required to charge the gate is:

$$
\operatorname{IGATE}(\max )=(500 \mathrm{kHz})(17 \mathrm{nC})=8.5 \mathrm{~mA} .
$$

The bypass capacitor on $\mathrm{V}_{+}$(C2) must instantaneously furnish the gate charge without excessive droop (e.g., less than 200 mV ):

$$
\Delta \mathrm{V}_{+}=\frac{\mathrm{Qg}_{\mathrm{g}}}{\mathrm{C} 2}
$$

Continuing with the example, $\Delta \mathrm{V}+=17 \mathrm{nC} / 0.1 \mu \mathrm{~F}=170 \mathrm{mV}$. Use IGATE when calculating the appropriate shunt resistor. See the Shunt Regulator Operation section.
Figure 2a's application circuit uses an MTD3055EL logic-level N-FET with a guaranteed threshold voltage ( $\mathrm{V}_{\mathrm{TH}}$ ) of 2V. Figure 2b's application circuit uses an 8 -pin Si9410DY surface-mount N-FET that has $50 \mathrm{~m} \Omega$ on resistance with $4.5 \mathrm{~V} \mathrm{~V}_{\mathrm{GS}}$, and a guaranteed $\mathrm{V}_{\mathrm{TH}}$ of less than 3V.

## NPN Transistors

The MAX773 can drive NPN transistors, but be extremely careful when determining the base-current requirements. Too little base current can cause excessive power dissipation in the transistor; too much base current can cause the base to oversaturate, so the transistor remains on continually. Both conditions can damage the transistor.
When using the MAX773 with an NPN transistor, connect EXTL to the transistor's base, and connect RBASE between EXTH and the base (Figure 8c).
To determine the required peak inductor current, IC(PEAK), observe the Typical Operating Characteristics efficiency graphs and the theoretical output current capability vs. input voltage graphs to determine a sense resistor that will allow the desired output current. Divide the 170 mV worst-case (smallest) voltage across the current-sense amplifier $\mathrm{V}_{\mathrm{CS}}(\max )$ by the senseresistor value. To determine $\mathrm{I}_{\mathrm{B}}$, set the peak inductor current (lLIM) equal to the peak transistor collector cur-
rent $\operatorname{IC}($ PEAK ). Calculate IB as follows:

$$
\mathrm{IB}=\mathrm{ILIM} / \mathrm{B}
$$

Use the worst-case (lowest) value for $ß$ given in the transistor's electrical specification, where the collector current used for the test is approximately equal to ILIM. It may be necessary to use even higher base currents (e.g., IB = ILIM/10), although excessive IB may impair operation by extending the transistor's turn-off time.
RBASE is determined by:

$$
\mathrm{R}_{\mathrm{BASE}}=\frac{\left(\mathrm{V}_{\mathrm{EXTH}}-\mathrm{V}_{\mathrm{BE}}-\mathrm{V}_{\mathrm{CS}}(\min )\right)}{\mathrm{I}_{\mathrm{B}}}
$$

Where $\mathrm{V}_{\text {EXTH }}$ is the voltage at $\mathrm{V}_{+}$(in bootstrapped mode $\mathrm{V}_{\text {EXTH }}$ is the output voltage), $\mathrm{V}_{B E}$ is the 0.7 V transistor base-emitter voltage, $\mathrm{VCS}(\mathrm{min})$ is the voltage drop across the current-sense resistor, and $\mathrm{I}_{\mathrm{B}}$ is the minimum base current that forces the transistor into saturation. This equation reduces to ( $\mathrm{V}_{+}-700 \mathrm{mV}$ 170 mV ) / Ib.
For maximum efficiency, make RBASE as large as possible, but small enough to ensure the transistor is always driven near saturation. Highest efficiency is obtained with a fast-switching NPN transistor ( $\mathrm{fT} \geq 150 \mathrm{MHz}$ ) with a low collector-emitter saturation voltage and a high current gain. A good transistor to use is the Zetex ZTX694B.

## Diode Selection

The MAX770-MAX773's high switching frequency demands a high-speed rectifier. Schottky diodes such as the 1N5817-1N5822 are recommended. Make sure that the Schottky diode's average current rating exceeds the peak current limit set by RSENSE, and that its breakdown voltage exceeds Vout. For high-temperature applications, Schottky diodes may be inadequate due to their high leakage currents; high-speed silicon diodes may be used instead. At heavy loads and high temperatures, the benefits of a Schottky diode's low forward voltage may outweigh the disadvantages of its high leakage current.

## Capacitor Selection <br> Output Filter Capacitor

The primary criterion for selecting the output filter capacitor (C2) is low effective series resistance (ESR). The product of the peak inductor current and the output filter capacitor's ESR determines the amplitude of the ripple seen on the output voltage. An OS-CON $300 \mu \mathrm{~F}$, 6.3 V output filter capacitor has approximately $50 \mathrm{~m} \Omega$ of ESR and typically provides 180 mV ripple when stepping up from 3 V to 5 V at 1 A (Figure 2a).

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Smaller capacitors are acceptable for light loads or in applications that can tolerate higher output ripple.
Since the output filter capacitor's ESR affects efficiency, use low-ESR capacitors for best performance. The smallest low-ESR surface-mount tantalum capacitors currently available are the Sprague 595D series. Sanyo OS-CON organic semiconductor through-hole capacitors and the Nichicon PL series also exhibit low ESR. See Table 2.

## Input Bypass Capacitors

The input bypass capacitor (C1) reduces peak currents drawn from the voltage source and also reduces noise at the voltage source caused by the switching action of the MAX770-MAX773. The input voltage source impedance determines the size of the capacitor required at the $\mathrm{V}_{+}$input. As with the output filter capacitor, a lowESR capacitor is recommended. For output currents up to $1 \mathrm{~A}, 150 \mu \mathrm{~F}$ (C1) is adequate, although smaller bypass capacitors may also be acceptable.
Bypass the IC with a $0.1 \mu \mathrm{~F}$ ceramic capacitor (C2) placed close to the $\mathrm{V}+$ and GND pins.

Reference Capacitor Bypass REF with a $0.1 \mu \mathrm{~F}$ capacitor (C3). REF can source up to $100 \mu \mathrm{~A}$ of current.

## Setting the Low-Battery-Detector Voltage

 To set the low-battery detector's falling trip voltage (VTRIP(falling)), select R3 between $10 \mathrm{k} \Omega$ and $500 \mathrm{k} \Omega$ (Figure 9), and calculate R4 as follows:$$
R 4=(R 3)\left(\frac{V_{T R I P}-V_{R E F}}{V_{\text {REF }}}\right)
$$

where VREF $=1.5 \mathrm{~V}$.
The rising trip voltage is higher because of the comparator's approximately 20 mV of hysteresis, and is determined by:

$$
\mathrm{V}_{\mathrm{TRIP}}(\text { rising })=\left(\mathrm{V}_{\mathrm{REF}}+20 \mathrm{mV}\right)\left(1+\frac{\mathrm{R} 4}{\mathrm{R} 3}\right)
$$

Connect a high value resistor (larger than R3 + R4) between LBI and LBO if additional hysteresis is required. Connect a pull-up resistor (e.g., $100 \mathrm{k} \Omega$ ) between LBO and $\mathrm{V}_{+}$. Tie LBI to GND and leave LBO floating if the low-battery detector is not used.


Figure 9. Input Voltage Monitor Circuit

## Applications Information <br> MAX773 Operation with High Input/Output Voltages

The MAX773's shunt regulator input allows high voltages to be converted to very high voltages. Since the MAX773 runs off the 6 V shunt (bootstrapped operation is not allowed), the IC will not see the high input voltage. Use an external logic-level N-FET as the power switch, since only 6 V of $\mathrm{V}_{\mathrm{GS}}$ are available. Also, make sure all external components are rated for very high output voltage. Figure 3e shows a circuit that converts 28 V to 100 V .

## Low Input Voltage Operation

When using a power supply that decays with time (such as a battery), the N-FET transistor will operate in its linear region when the voltage at EXT approaches the threshold voltage of the FET, dissipating excessive power. Prolonged operation in this mode may damage the FET. This effect is much more significant in nonbootstrapped mode than in bootstrapped mode, since bootstrapped mode typically provides much higher VGS voltages. To avoid this condition, make sure $V_{E X T}$ is above the $V_{T H}$ of the FET, or use a voltage detector (such as the MAX8211) to put the IC in shutdown mode once the input supply voltage falls below a predetermined minimum value. Excessive loads with low input voltages can also cause this condition.

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## Starting Up under Load

The Typical Operating Characteristics show the StartUp Voltage vs. Load Current graph for bootstrappedmode operation. This graph depends on the type of power switch used. The MAX770-MAX773 are not designed to start up under full load in bootstrapped mode with low input voltages.

## Layout Considerations

Due to high current levels and fast switching waveforms, which radiate noise, proper PC board layout is essential. Protect sensitive analog grounds by using a star ground configuration. Minimize ground noise by connecting GND, the input bypass capacitor ground
lead, and the output filter capacitor ground lead to a single point (star ground configuration). Also, minimize lead lengths to reduce stray capacitance, trace resistance, and radiated noise. Place input bypass capacitor C 2 as close as possible to $\mathrm{V}_{+}$and GND.
Excessive noise at the $V_{+}$input may falsely trigger the timing circuitry, resulting in short pulses at EXT. If this occurs it will have a negligible effect on circuit efficiency. If desired, place a $4.7 \mu \mathrm{~F}$ directly across the $\mathrm{V}+$ and GND pins (in parallel with the $0.1 \mu \mathrm{~F}$ C2 bypass capacitor) to reduce the noise at $\mathrm{V}_{+}$.

Table 2. Component Suppliers

| PRODUCTION | INDUCTORS | CAPACITORS | TRANSISTORS | DIODES |
| :---: | :---: | :---: | :---: | :---: |
| Surface Mount | Sumida <br> CD54 series <br> CDR125 series <br> Coiltronics <br> CTX20 series | Matsuo 267 series Sprague 595D series | N-FET <br> Siliconix <br> Si9410DY <br> Si9420DY (high voltage) <br> Motorola <br> MTP3055EL <br> MTD20N03HDL | Nihon EC10 series |
| Through Hole | Sumida <br> RCH855 series RCH110 series Renco RL1284-18 | Sanyo OS-CON series Nichicon PL series United Chemi-Con LXF series | NPN <br> Zetex <br> ZTX694B | Motorola <br> 1N5817-1N5822 <br> MUR115 (high voltage) |


| SUPPLIER | PHONE | FAX |
| :--- | :--- | :--- |
| Coiltronics | USA: $(561)$ 241-7876 | $(561) 241-9339$ |
| Matsuo | USA: (714) 969-2491 | $(714) 960-6492$ |
|  | Japan: 81-6-337-6450 | $81-6-337-6456$ |
| Nichicon | USA: (847) 843-7500 | $(847) 843-2798$ |
| Nihon | USA: (805) 867-2555 | $(805) 867-2698$ |
| Renco | USA: (516) 586-5566 | $(516) 586-5562$ |
| Sanyo | USA: (619) 661-6835 | $(619) 661-1055$ |
|  | Japan: 81-7-2070-6306 | $81-7-2070-1174$ |
| Sumida | USA: (847) 956-0666 |  |
|  | Japan: 81-3-3607-5111 | $81-3-3607-5144$ |
| United Chemi-Con | USA: (714) 255-9500 | $(714) 255-9400$ |
| Zetex | USA: (516) 543-7100 | $(516) 864-7630$ |
|  | UK: 44-61-627-4963 | $44-61-627-5467$ |

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__Ordering Information (continued)

| PART | TEMP. RANGE | PIN-PACKAGE |
| :--- | :--- | :--- |
| MAX771CPA | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | 8 Plastic DIP |
| MAX771CSA | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | 8 SO |
| MAX771C/D | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | Dice ${ }^{*}$ |
| MAX771EPA | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 Plastic DIP |
| MAX771ESA | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 SO |
| MAX771MJA | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8 CERDIP |
| MAX772CPA | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | 8 Plastic DIP |
| MAX772CSA | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | 8 SO |
| MAX772C/D | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | Dice |
| MAX772EPA | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 Plastic DIP |
| MAX772ESA | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 SO |
| MAX772MJA | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8 CERDIP |
| MAX773CPD | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | 14 Plastic DIP |
| MAX773CSD | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | 14 SO |
| MAX773C/D | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | Dice ${ }^{\star}$ |
| MAX773EPD | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 14 Plastic DIP |
| MAX773ESD | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 14 Narrow SO |
| MAX773MJD | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14 CERDIP |

*Contact factory for dice specifications.
Pin Configurations (continued)

$\qquad$ Chip Topographies

MAX770/MAX771/MAX772


TRANSISTOR COUNT: 501; SUBSTRATE CONNECTED TO V+.

MAX773


TRANSISTOR COUNT: 501;
SUBSTRATE CONNECTED TO V+.

