## DEFLECTION PROCESSOR FOR MULTISYNC MONITOR

## HORIZONTAL

- DUAL PLL CONCEPT
- 150kHz MAXIMUM FREQUENCY
- SELF-ADAPTIVE (EX : 30 TO 85kHz)
- X-RAY PROTECTION INPUT
- DC ADJUSTABLE DUTY-CYCLE
- INTERNAL 1st PLL LOCK/UNLOCK IDENTIFICATION
- 4 OUTPUTS FOR S-CORRECTION
- WIDE RANGE DC CONTROLLED H-POSITION
- ON/OFF SWITCH (FOR PWR MANAGEMENT)
- TWO H-DRIVE POLARITIES


## VERTICAL

- VERTICAL RAMP GENERATOR
- 50 TO 150 Hz AGC LOOP
- DC CONTROLLED V-AMP, V-POS, S-AMP AND SCENTERING
- ON/OFF SWITCH


## B+ REGULATOR

- INTERNAL PWM GENERATOR FOR B+ CURRENT MODE STEP-UP CONVERTER
- DC ADJUSTABLE B+ VOLTAGE
- OUTPUT PULSES SYNCHRONISED ON HORIZONTAL FREQUENCY
- INTERNAL MAXIMUM CURRENT LIMITATION


## EWPCC

- VERTICAL PARABOLA GENERATOR WITH DC CONTROLLED KEYSTONE AND AMPLITUDE


## GENERAL

- ACCEPT POS. OR NEG. H AND V SYNC POLARITIES
- SEPARATED H AND V TTL INPUT
- SAFETY BLANKING OUTPUT


## DESCRIPTION

The TDA9103 is a monolithic integrated circuit assembled in a 42 pins shrunk dual in line plastic package.
This IC controls all the functions related to the horizontal and vertical deflection in multimodes or multisync monitors. As can be seen in the block diagram, the TDA9103 includes the following functions :

- Positive or Negative sync polarities,
- Auto-sync horizontal processing,
- H-PLL lock/unlock identification,
- Auto-sync Vertical processing,
- East/West signal processing block,
- B+ controller,
- Safety blanking output.

This IC, combined with TDA9205 (RGB preamp), STV9420/21 or 22 (O.S.D. processor), ST7271 (micro controller) and TDA8172 (vertical booster), allows to realize very simple and high quality multimodes or multisync monitors.


## PIN CONNECTIONS



## PIN-OUT DESCRIPTION

| Pin ${ }^{\circ}$ | Name | Function |
| :---: | :---: | :---: |
| 1 | PLL2C | Second PLL Loop Filter |
| 2 | H-DUTY | DC Control of Horizontal Drive Output Pulse Duty-cycle. <br> If this pin is grounded, the horizontal and vertical outputs are inhibited. By connecting a capacitor on this pin a soft-start function may be realized on h-drive output. |
| 3 | H-FLY | Horizontal Flyback Input (positive Polarity) |
| 4 | H-GND | Horizontal Section Ground. Must be connected only to components related to H blocks. |
| 5 | H-REF | Horizontal Section Reference Voltage. Must be filtered by capacitor to Pin 4 |
| 6 | S4 | Hor S-CAP Switching |
| 7 | S3 | Hor S-CAP Switching |
| 8 | S2 | Hor S-CAP Switching |
| 9 | S1 | Hor S-CAP Switching |
| 10 | C0 | Horizontal Oscillator Capacitor. To be connected to Pin 4. |
| 11 | R0 | Horizontal Oscillator Resistor. To be connected to Pin 4. |
| 12 | PLL1F | First PLL Loop Filter. To be connected to Pin 4. |
| 13 | HLOCK-CAP | First PLL Lock/Unlock Time Constant Capacitor. Capacitor filtering the frequency change detected on Pin13. When frequency is changing, a blanking pulse is generated on Pin 23, the duration of this pulse is proportionnal to the capacitor on Pin 13. To be connected to Pin 4. |
| 14 | FH-MIN | DC Control for Free Running Frequency Setting. Comming from DAC output or DC voltage generated by a resistor bridge connected between Pin 5 and 4. |
| 15 | H-POS | DC Control for Horizontal Centering |
| 16 | XRAY-IN | X-RAY Protection Input (with internal latch function) |
| 17 | H-SYNC | TTL Horizontal Sync Input |
| 18 | $\mathrm{V}_{C C}$ | Supply Voltage (12V Typical) |
| 19 | GND | Ground |
| 20 | H-OUTEM | Horizontal Drive Output (emiter of internal transistor). See description on pages 15-16. |
| 21 | H-OUTCOL | Horizontal Drive Output (open collector of internal transistor). See description on pages 15-16. |
| 22 | B+ OUT | B+ PWM Regulator Output |
| 23 | SBLK OUT | Safety Blanking Output. Activated during frequency changes, when X-RAY input is triggered or when VS is too low. |
| 24 | VGND | Vertical Section Signal Ground |
| 25 | VAGCCAP | Memory Capacitor for Automatic Gain Control Loop in Vertical Ramp Generator |
| 26 | $V_{\text {REF }}$ | Vertical Section Reference Voltage |
| 27 | VCAP | Vertical Sawtooth Generator Capacitor |
| 28 | VS-AMP | DC Control of Vertical S Shape Amplitude |
| 29 | VS-CENT | DC Control of Vertical S Centering |
| 30 | VOUT | Vertical Ramp Output (with frequency independant amplitude and S-correction) |
| 31 | V-AMP | DC Control of Vertical Amplitude Adjustment |
| 32 | $V_{\text {DCOUT }}$ | Vertical Position Reference Voltage Output Temperature Matched with V-AMP Output |
| 33 | V-POS | DC Control of Vertical Position Adjustment |
| 34 | VSYNC | Vertical TTL Sync Input |
| 35 | PLL1INHIB | TTL Input for PLL1 Output Current Inhibition (To be used in case of comp sync input signal) |
| 36 | E/WOUT | East/West Pincushion Correction Parabola Output |
| 37 | E/W-AMP | DC Control of East/West Pincushion Correction Amplitude |
| 38 | KEYST | DC Control of Keystone Correction |
| 39 | B+ ADJ | DC Control of B+ Adjustment |
| 40 | REGIN | Regulation Input of B+Control Loop |
| 41 | COMP | B+ Error Amplifier Output for Frequency Compensation and Gain Setting |
| 42 | Isense | Sensing of External B+ Switching Transistor Emiter Current |

BLOCK DIAGRAM


QUICK REFERENCE DATA

| Parameter | Value | Unit |
| :--- | :---: | :---: |
| Horizontal Frequency Range | 15 to 150 | kHz |
| Autosynch Frequency Range (for Given R0, C0) | 1 to 3.7 | FH |
| $\pm$ Hor Sync Polarity Input | YES |  |
| Compatibility with Composite Sync on H-SYNC Input | YES (1) |  |
| Lock/Unlock Identification on 1st PLL | YES |  |
| DC Control for H-Position | YES |  |
| X-RAY Protection | YES |  |
| Hor DUTY Adjust | YES |  |
| Stand-by Function | YES |  |
| Hor S-CAP Switching Control | YES |  |
| Two Polarities H-Drive Outputs | YES |  |
| Supply Voltage Monitoring | YES |  |
| PLL1 Inhibition Possibility | YES |  |
| Safety Blanking Output | YES |  |
| Vertical Frequency Range | 35 to 200 | Hz |
| Vertical Autosync Range (for a Given Capacitor Value) | 50 to 150 | Hz |
| Vertical -S- Correction | YES |  |
| Vertical -C- Correction | YES |  |
| Vertical Amplitude Adjustment | YES |  |
| Vertical Position Adjustment | YES |  |
| Automatic B+ Adjustment Control Loop | YES |  |
| B+ Adjustment | YES |  |
| East/West Parabola Output | YES |  |
| PCC (Pin Cushion Correction) Amplitude Adjustment | YES |  |
| Keystone Adjustment | YES |  |
| Reference Voltage | YES (2) |  |
| Mode Detection | NO |  |
| Dynamic Focus | NO |  |
| Blanking Output | NO |  |
|  |  | I |

Notes: 1. See application diagram.
2. One for Horizontal section and one for Vertical section.

ABSOLUTE MAX RATING

| Symbol |  | Parameter | Value | Unit |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {cc }}$ | Supply Voltage (Pin 18) |  | 13.5 | V |
| $\mathrm{V}_{\text {IN }}$ | Max Voltage on | Pins 2, 14, 15, 28, 29, 31, 33, 37, 38, 39 <br> Pin 3 <br> Pins 17, 34 <br> Pin 40 <br> Pin 42 <br> Pin 16 | $\begin{gathered} 8 \\ 1.8 \\ 6 \\ 8 \\ 8 \\ 5.5 \end{gathered}$ | V |
| VESD | ESD Succeptibility Human Body Model, 100pF Discharge through $1.5 \mathrm{k} \Omega$ EIAJ Norm, 200pF Discharge through $0 \Omega$ |  | $\begin{gathered} 2 \\ 300 \end{gathered}$ | $\stackrel{\mathrm{kV}}{\mathrm{~V}}$ |
| $\mathrm{T}_{\text {stg }}$ | Storage Temperature |  | $-40,+150$ | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\mathrm{j}}$ | Max Operating Junction Temperature |  | 150 | ${ }^{\circ} \mathrm{C}$ |
| Toper | Operating Temperature |  | $0,+70$ | ${ }^{\circ} \mathrm{C}$ |

## THERMAL DATA

| Symbol | Parameter | Value | Unit |
| :---: | :---: | :---: | :---: |
| $\mathrm{R}_{\mathrm{th}(\mathrm{j}-\mathrm{a})}$ | Junction-Ambient Thermal Resistance | Max. | 65 |
| ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |  |  |  |

HORIZONTAL SECTION
Operating conditions

| Symbol | Parameter | Test conditions | Min. | Typ. | Max. | Unit |
| :---: | :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| VCO |  |  |  |  |  |  |
| R0min Oscillator Resistor Min Value Pin 11 6   $\mathrm{k} \Omega$ <br> COmin Oscillator Capacitor Min Value Pin 10 390   pF <br> Fmax Maximum Oscillator Frequency    150 kHz <br> HsVR Horizontal Sync Input Voltage Range Pin 17 0  5.5 V |  |  |  |  |  |  |$.$

infut SECTION

| MinD | Minimum Input Pulses Duration | Pin 17 | 0.7 |  |  | $\mu \mathrm{~S}$ |
| :---: | :--- | :--- | :--- | :--- | :--- | :---: |
| Mduty | Maximum Input Signal Duty Cycle | Pin 17 |  |  | 25 | $\%$ |

OUTPUT SECTION

| I3m | Maximum Input Peak Current on Pin 3 |  |  | 2 | mA |
| :---: | :--- | :--- | :--- | :---: | :---: |
| IS1 to IS4 | Maximum Current on S1 to S4 Outputs | Pins 6 to 9 |  |  | 0.5 |
| VS1 to VS4 | Maximum Voltage on S1 to S4 Outputs | Pins 6 to 9 | mA |  |  |
| HOI1 | Horizontal Drive Output Max Current | Pin 20, sourced current |  |  | 20 |
| HOI2 | Horizontal Drive Output Max Current | Pin 21, sunk current |  |  | 20 |

DC CONTROL VOLTAGES


Electrical Characteristics (VCC $=12 \mathrm{~V}, \mathrm{~T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$ )

| Symbol | Parameter | Test conditions | Min. | Typ. | Max. | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SUPPLY AND REFERENCE VOLTAGES |  |  |  |  |  |  |
| $\mathrm{V}_{\mathrm{Cc}}$ | Supply Voltage | Pin 18 | 10.8 | 12 | 13.2 | V |
| Icc | Supply Current | Pin 18, See Figure 1 |  | 40 | 60 | mA |
| $\mathrm{V}_{\text {REF-H }}$ | Reference Voltage for Horizontal Section | Pin 5, I = 2mA | 7.4 | 8 | 8.6 | V |
| IREF-H | Max Sourced Current on V ${ }_{\text {REF-H }}$ | Pin 5 |  |  | 5 | mA |
| VREF-V | Reference Voltage for Vertical Section | Pin 26, I = 2mA | 7.4 | 8 | 8.6 | V |
| IREF-V | Max Sourced Current on V REF-V | Pin 26 |  |  | 5 | mA |

INPUT SECTION/PLL1

| VInth | Hor Input Threshold Voltage Pin 17 | Low level voltage High level voltage | 2 |  | 0.8 | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vvco | VCO Control Voltage Range | $\mathrm{V}_{\text {REF-H }}=8 \mathrm{~V}$, Pin 12 | 1.6 |  | 6.2 | V |
| VCOG | VCO Gain, dF/dV Pin 12 | $\mathrm{R} 0=6.49 \mathrm{k} \Omega, \mathrm{C} 0=680 \mathrm{pF}$ |  | 15 |  | kHz/V |
| Hph | Horizontal Phase Adj Range (Pin 15) | \% of Hor period |  | $\pm 12.5$ |  | \% |
| FFadj | Free Running Frequency Adj Range (Pin 14) | Without H-sync Signal |  | $\pm 20$ |  | \% |
| S1th | VCO Input Voltage for S1 Switching | Pin 12 voltage, $\mathrm{V}_{\text {REF-H }}=8 \mathrm{~V}$ | 1.85 | 2 | 2.25 | V |
| S2th | VCO Input Voltage for S2 Switching | Pin 12 voltage, $\mathrm{V}_{\text {REF-H }}=8 \mathrm{~V}$ | 2.25 | 2.4 | 2.65 | V |
| S3th | VCO Input Voltage for S3 Switching | Pin 12 voltage, $\mathrm{V}_{\text {REF-H }}=8 \mathrm{~V}$ | 2.9 | 3 | 3.3 | V |
| S4th | VCO Input Voltage for S4 Switching | Pin 12 voltage, $\mathrm{V}_{\text {REF-H }}=8 \mathrm{~V}$ | 3.5 | 3.7 | 3.9 | V |
| F0 | Free Running Frequency | $\begin{aligned} & V_{14}=V_{\text {REF }} / 2 \\ & R 0=6.49 \mathrm{k} \Omega \\ & C 0=680 \mathrm{pF} \\ & \hline \end{aligned}$ | 23.5 | 25 | 27.5 | kHz |
| $\begin{gathered} \hline \text { VS1D to } \\ \text { VS4D } \end{gathered}$ | Low Level Output Voltage on S1 to S4 Outputs | Pins 6 to $9, \mathrm{I}=0.5 \mathrm{~mA}$ |  | 0.2 | 0.4 | V |
| CR | PLL1 Capture Range (F0 = 27kHz) <br> Fh Min <br> Fh Max | See conditions on Figure 1 | 94 |  | 28 | kHz |
| PLLinh | $\begin{aligned} & \hline \text { PLL } 1 \text { Inhibition (Pin 35) } \\ & \text { PLL ON } \\ & \text { PLL OFF } \\ & \hline \end{aligned}$ | $\begin{aligned} & V_{35} \\ & V_{35} \end{aligned}$ | 2 |  | 0.8 | V |

SECOND PLL AND HORIZONTAL OUTPUT SECTION

| FBth | Flyback Input Threshold Voltage | Pin 3 | 0.65 | 0.75 |  | V |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hjit | Horizontal Jitter |  |  | 100 |  | ppm |
| HDmin HDmin | Minimum Hor Drive Output Duty-cycle Maximum Hor Drive Output Duty-cycle | $\begin{array}{\|l} \hline \text { Pin } 20 \text { or } 21, \mathrm{~V}_{2}=2 \mathrm{~V} \\ \text { Pin } 20 \text { or } 21, \mathrm{~V}_{2}=6 \mathrm{~V} \\ \hline \end{array}$ | 45 | $\begin{aligned} & 30 \\ & 50 \end{aligned}$ | 35 | $\begin{aligned} & \% \\ & \% \end{aligned}$ |
| HDvd | Horizontal Drive Low Level Output Voltage | $\begin{aligned} & \mathrm{V}_{21}-\mathrm{V}_{20}, \text { lout }=20 \mathrm{~mA}, \\ & \text { Pin } 20 \text { to } \mathrm{GND} \end{aligned}$ |  | 1.1 | 1.7 | V |
| HDem | Horizontal Drive High Level Output Voltage (output on Pin 20) | Pin 21 to $\mathrm{V}_{\text {cc }}$, lout $=20 \mathrm{~mA}$ | 9.5 | 10 |  | V |
| XRAYth | X-RAY Protection Input Threshold Voltage | Pin 16 |  | 1.6 | 1.8 | V |
| ISblkO | Maximum Output Current on Safety Blanking Output | $\mathrm{I}_{23}$ |  |  | 10 | mA |
| VSblkO | Low-Level Voltage on Safety Blanking Output | $\mathrm{V}_{23}$ with $\mathrm{I}_{23}=10 \mathrm{~mA}$ |  | 0.25 | 0.5 | V |
| Vphi2 | Internal Clamping Voltage on 2nd PLL Loop Filter Output (Pin 1) | Vmin Vmax |  | $\begin{aligned} & 1.6 \\ & 3.2 \end{aligned}$ |  | V |
| $\mathrm{V}_{\text {OFF }}$ | Pin 2 Threshold Voltage to Stop H-out, V-out B+out and to Activate S-BLK.OFF Mode when $\mathrm{V}_{2}<\mathrm{V}_{\text {OfF }}$ | $\mathrm{V}_{2}$ |  | 1 |  | V |

B+ SECTION
Operating Conditions

| Symbol | Parameter | Test conditions | Min. | Typ. | Max. | Unit |
| :---: | :--- | :--- | :---: | :---: | :---: | :---: |
| EAOI | Maximum Error Amplifier Output Current | $\begin{array}{l}\text { Sourced by Pin 41 } \\ \text { Sunk by Pin 41 }\end{array}$ |  |  | 0.5 |  |
| 2 |  |  |  |  |  |  | \(\left.\begin{array}{c}\mathrm{mA} <br>


\mathrm{mA}\end{array}\right]\)| FeedRes | Minimum Feedback Resistor | Resistor between Pins 40 <br> and 41 | 5 |
| :---: | :---: | :---: | :---: |

Electrical Characteristics ( $\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$ )

| Symbol | Parameter | Test conditions | Min. | Typ. | Max. | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OLG | Error Amplifier Open Loop Gain | At low frequency (see Note 1) |  | 85 |  | dB |
| UGBW | Unity Gain Bandwidth | (see Note 1) |  | 6 |  | MHz |
| IRI | Regulation Input Bias Current | Current sourced by Pin 40 (PNP base) |  | 0.2 |  | $\mu \mathrm{A}$ |
| EAOI | Maximum Guaranted Error Amplifier Output Current | Current sourced by Pin 41 Current sunk by Pin 41 | $\begin{gathered} 0.5 \\ 2 \\ \hline \end{gathered}$ |  |  | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \end{aligned}$ |
| CSG | Current Sense Input Voltage Gain | Pin 42 |  | 3 |  |  |
| MCEth | Max Curent Sense Input Threshold Voltage | Pin 42 |  | 1.2 |  | V |
| ISI | Current Sense Input Bias Current | Current sunk by Pin 42 (NPN base) |  | 1 |  | $\mu \mathrm{A}$ |
| Tonmax | Maximum External Power Transistor on Time | \% of H-period <br> @ f0 = 27kHz |  | 75 |  | \% |
| B+OSV | B+ Output Low Level Saturation Voltage | $\mathrm{V}_{22}$ with $\mathrm{I}_{22}=10 \mathrm{~mA}$ |  | 0.25 |  | V |
| IV VEF | Internal Reference Voltage | On error amp (+) input for $\mathrm{V}_{39}=4 \mathrm{~V}$ |  | 4.9 |  | V |
| $V_{\text {REFADJ }}$ | Internal Reference Voltage Adjustment Range | $2 \mathrm{~V}<\mathrm{V}_{39}<6 \mathrm{~V}$ |  | $\pm 14$ |  | \% |

## EAST WEST PARABOLA GENERATOR

Electrical Characteristics ( $\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$ )

| Symbol | Parameter | Test conditions | Min. | Typ. | Max. | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vsym | Parabola Symetry Adjustment Capability (for Keystone Adjustment ; with Pin 38) | See Figure 2 ; internal voltage $\begin{aligned} & V_{38}=2 \mathrm{~V} \\ & V_{38}=4 \mathrm{~V} \\ & V_{38}=6 \mathrm{~V} \end{aligned}$ |  | $\begin{aligned} & 3.2 \\ & 3.5 \\ & 3.8 \end{aligned}$ |  | V |
| Kadj | Keystone Adjustment Capability B/A ratio A/B ratio | $\begin{aligned} & \text { See Figure } 2 ; V_{37}=4 V \\ & V_{38}=2 V \\ & V_{38}=6 V \end{aligned}$ |  | $\begin{aligned} & 2.3 \\ & 2.0 \end{aligned}$ |  |  |
| Paramp | Parabola Amplitude Adjustment Capability Maximum Amplitude on Pin 36 Maximum Ratio between Max and Min | $\begin{aligned} & V_{38}=4.3 V, V_{28}=2 V \\ & V_{37}=2 V \\ & 2 V<V_{37}<6 V \end{aligned}$ | $\begin{aligned} & 3.3 \\ & 2.4 \end{aligned}$ | $\begin{gathered} 3.8 \\ 3 \end{gathered}$ | 4.3 | V |

VERTICAL SECTION
Operating Conditions

| Symbol | Parameter | Test conditions | Min. | Typ. | Max. | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| VSVR | Vertical Sync Input Voltage Range | On Pin 34 | 0 |  | 5.5 | V |

Electrical Characteristics (Vcc $=12 \mathrm{~V}, \mathrm{~T}_{\text {amb }}=25^{\circ} \mathrm{C}$ )

| Symbol | Parameter | Test conditions | Min. | Typ. | Max. | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{I}_{\text {BIASP }}$ | Pin 23-28-29 Bias Current (Current Sourced by PNP Base) | For $\mathrm{V}_{23-28-29}=2 \mathrm{~V}$ |  | 2 |  | $\mu \mathrm{A}$ |
| IBIASN | Pin 31 Bias Current (Current Sunk by NPN Base) | For $\mathrm{V}_{31}=6 \mathrm{~V}$ |  | 0.5 |  | $\mu \mathrm{A}$ |
| VSth | Vertical Sync Input Threshold Voltage | Pin 34; High-level Low-level | 2 |  | 0.8 | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \end{aligned}$ |
| VSBI | Vertical Sync Input Bias Current (Current Sourced by PNP Base) | $\mathrm{V}_{34}=0.8 \mathrm{~V}$ |  | 1 |  | $\mu \mathrm{A}$ |
| VRB | Voltage at Ramp Bottom Point | On Pin 27 |  | 2/8 |  | $V_{\text {REF-V }}$ |
| $\mathrm{V}_{\text {RT }}$ | Voltage at Ramp Top Point (with Sync) | On Pin 27 |  | 5/8 |  | $\mathrm{V}_{\text {REF-V }}$ |
| $V_{\text {RTF }}$ | Voltage at Ramp Top Point (without Sync) | On Pin 27 |  | VRT-0.1 |  | V |
| IR27 | Output Current Range on Pin 27 during Ramp Charging Time. Current to Charge Capacitor between Pin 27 and Ground | $\begin{aligned} & \mathrm{V}_{28}=2 \mathrm{~V}(\text { Note } 2), \\ & 2 \mathrm{~V}<\mathrm{V}_{27}<55 \mathrm{~V} \\ & \text { Min current } \\ & \text { Max current } \end{aligned}$ | 100 | $\begin{gathered} 15 \\ 135 \end{gathered}$ | 20 | $\mu \mathrm{A}$ <br> $\mu \mathrm{A}$ |
| VSW | Minimum Vertical Sync Pulse Width | Pin 34 | 5 |  |  | $\mu \mathrm{S}$ |
| VSmDut | Vertical Sync Input Maximum Duty-cycle | Pin 34 |  |  | 15 | \% |
| VSTD | Vertical Sawtooth Discharge Time Duration | On Pin 27, with 150nF cap |  | 85 |  | $\mu \mathrm{S}$ |
| VFRF | Vertical Free Running Frequency ( $\mathrm{V}_{28}=2 \mathrm{~V}$ ) | Measured on Pin 27 $\operatorname{Cosc}(\text { Pin27 })=150 \mathrm{nF}$ |  | 100 |  | Hz |
| ASFR | AUTO-SYNC Frequency Range (see Note 3) | With $\mathrm{C}_{27}=150 \mathrm{nF} \pm 5 \%$ | 50 |  | 150 | Hz |
| RATD | Ramp Amplitude Thermal Drift | On Pin 30 (see Note 1) $\left(0^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{amb}}<70^{\circ} \mathrm{C}\right)$ |  | 100 |  | ppm $/{ }^{\circ} \mathrm{C}$ |
| RAFD | Ramp Amplitude Drift Versus Frequency | $\begin{aligned} & V_{31}=6 \mathrm{~V}, \mathrm{C}_{27}=150 \mathrm{nF} \\ & 50 \mathrm{~Hz}<\mathrm{F}<120 \mathrm{~Hz} \end{aligned}$ |  | 200 |  | $\mathrm{ppm} / \mathrm{Hz}$ |
| Rlin | Ramp Linearity on Pin $27 \Delta \mathrm{l}_{27} / \mathrm{I}_{27}$ | $\begin{aligned} & \mathrm{V}_{28}=2 \mathrm{~V}, \mathrm{~V}_{25}=4.3 \mathrm{~V} \\ & 2.5 \mathrm{~V}<\mathrm{V}_{27}<4.5 \mathrm{~V} \end{aligned}$ |  | 0.5 |  | \% |
| Rload | Minimum Load on Pin 25 for less than 1\% Vertical Amplitude Drift |  | 50 |  |  | $\mathrm{M} \Omega$ |
| Vpos | Vertical Position Adjustment Range Voltage on Pin 32 | $\begin{aligned} & V_{33}=2 \mathrm{~V} \\ & V_{33}=4 \mathrm{~V} \\ & V_{33}=6 \mathrm{~V} \end{aligned}$ | 3.65 | $\begin{aligned} & 3.2 \\ & 3.5 \\ & 3.8 \\ & \hline \end{aligned}$ | 3.3 | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \\ & \mathrm{~V} \end{aligned}$ |
| Ivpos | Max Current on Vertical Position Control Output (Pin 32) |  |  | $\pm 2$ |  | mA |
| Vor | Vertical Output Voltage Range (on Pin 30) (Peak to Peak Voltage on Pin 30) | $\begin{aligned} & V_{31}=2 \mathrm{~V} \\ & V_{31}=4 \mathrm{~V} \\ & V_{31}=6 \mathrm{~V} \end{aligned}$ | 3.75 | $\begin{aligned} & 2 \\ & 3 \\ & 4 \end{aligned}$ | 2.2 | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \\ & \mathrm{~V} \end{aligned}$ |
| $\mathrm{V}_{\text {OUTDC }}$ | DC Voltage on Vertical Output (Pin30) | See Note 4 |  | 7/16 |  | $\mathrm{V}_{\text {REF-V }}$ |
| V OI | Vertical Output Maximum Output Current | On Pin 30 |  | $\pm 5$ |  | mA |
| dVS | Max Vertical S-Correction Amplitude ( $\mathrm{V}_{28}=2 \mathrm{~V}$ Inhibits S-CORR; $\mathrm{V}_{28}=6 \mathrm{~V}$ gives Maximum S-CORR) (see Figure 3) | $\Delta \mathrm{V} / \mathrm{V} 30 \mathrm{pp}$ at $\mathrm{T} / 4$ $\Delta \mathrm{V} / \mathrm{V} 30 \mathrm{pp}$ at $3 \mathrm{~T} / 4$ |  | $\begin{aligned} & -4 \\ & +4 \end{aligned}$ |  | $\begin{aligned} & \hline \% \\ & \% \end{aligned}$ |
| Ccorr | C-Correction Adjustment Range Voltage on Pin 27 for Maximum Slope on the Ramp (with S-Correction) (see Figure 4) | $\begin{aligned} & \mathrm{V}_{29}=2 \mathrm{~V} \\ & \mathrm{~V}_{29}=4 \mathrm{~V} \\ & \mathrm{~V}_{29}=6 \mathrm{~V} \end{aligned}$ |  | $\begin{gathered} 3 \\ 3.5 \\ 4 \\ \hline \end{gathered}$ |  | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \\ & \mathrm{~V} \end{aligned}$ |

Notes: 1. These parameters are not tested on each unit. They are measured during our internal qualification procedure which includes characterization on batches comming from comers of our processes and also temperature characterization.
2. When 2 V are applied on Pin 28 (Vertical S-Correction control), then the S-Correction is inhibited, consequently the sawtooth have a linear shape.
3. It is the frequency range for which the VERTICAL OSCILLATOR will automatically synchronize, using a single capacitor value on Pin 27 and with a constant ramp amplitude.
4. Typically 3.5 V for Vertical reference voltage typical value ( 8 V ).

Figure 1 : Testing Circuit


Figure 2 : Keystone Adjustment


Figure 3 : S Amplitude Adjustment


Figure 4 : C Correction Adjustment


## OPERATING DESCRIPTION

## GENERAL CONSIDERATIONS Power Supply

The typical value of the power supply voltage $\mathrm{V}_{\mathrm{CC}}$ is 12 V . Perfect operation is obtained if $\mathrm{V}_{\mathrm{cc}}$ is maintained in the limits : $10.8 \mathrm{~V} \rightarrow 13.2 \mathrm{~V}$.
In order to avoid erratic operation of the circuit during the transient phase of $\mathrm{V}_{\mathrm{cc}}$ switching on, or switching off, the value of $\mathrm{V}_{\mathrm{cc}}$ is monitored and the outputs of the circuit are inhibited if it is too low. In order to have a very good power supply rejection, the circuit is internally powered by several internal voltage references (The unique typical value of which is 8 V ). Two of these voltage references are externally accessible, one for the vertical part and one for the horizontal part. These voltage references can be used for the DC control voltages applied on the concerned pins by the way of potentiometers or digital to analog converters (DAC's). Furthermore it is possible to filter the a.m. voltage references by the use of external capacitor connected to ground, in order to minimize the noise and consequently the "jitter" on vertical and horizontal output signals.

## DC Control Adjustments

The circuit has 10 adjustment capabilities: 3 for the horizontal part, 1 for the SMPS part, 2 for the E/W correction, 4 for the vertical part.
The corresponding inputs of the circuit has to be driven with a DC voltage typically comprised between 2 and 6 V for a value of the internal voltage reference of 8V.
More precisely, the control voltages have to be maintained between Vref/4 and 3/4 . Vref. The application of control voltages outside this range is not dangerousfor the circuit but the good operation is not guaranted (except for Pin 2 : duty cycle adjusment. See outputs inhibition paragraph).

Figure 5 : Example of Practical DC Control Voltage Generation


The input currents of the DC control inputs are typically very low (about a few $\mu \mathrm{A}$ ). Depending on the internal structure of the inputs, the input currents can be positive or negative (sink or source).

## HORIZONTAL PART

 Input sectionThe horizontal input is designed to be sensitive to TTL signals typically comprised between 0 and 5 V . The typical threshold of this input is 1.6 V . This input stage uses an NPN differential stage and the input current is very low.
Concerning the duty cycle of the input signal, the following signals may be applied to the circuit.

Figure 6


Using internal integration, both signals are recognized on condition that $Z / T \leq 25 \%$. Synchronisation occurs on the leading edge of the rectified signal. The minimum value of $Z$ is $0.7 \mu \mathrm{~s}$.

Figure 7 : Input Structure


## PLL1

The PLL1 is composed of a phase comparator, an external filter and a Voltage Controlled Oscillator (VCO).
The phase comparatoris a "phase frequency" type, designed in CMOS technology. This kind of phase detector avoids locking on false frequencies. It is followed by a "charge pump", composed of 2 current sources sink and source ( $1=1 \mathrm{~mA}$ typ.)

Figure 8 : Principle Diagram


The dynamic behaviour of the PLL is fixed by an external filter which integrates the current of the charge pump. A "CRC" filter is generally used.
PLL1 is inhibited by applying a high level on Pin 35 (PLLinhib) which is a TL compatible input. The inhibition results from the opening of a switch located between the charge pump and the filter (see Figure 8). The VCO uses an external RC network. It delivers a linear sawtooth obtained by charge and discharge of the capacitor, by a current proportionnal to the current in the resistor. typical thresholds of sawtooth are 1.6 V and 6.4 V .

Figure 9


The control voltage of the VCO is typically comprised between 1.6 V and 6 V . The theoretical frequency range of this VCO is in the ratio $1 \rightarrow 3.75$, but due to spread and thermal drift of external components and the circuit itself, the effective frequency range has to be smaller (e.g. $30 \mathrm{kHz} \rightarrow$ 82 kHz ). Inthe absence of synchronisationsignal the control voltage is equal to 1.6 V typ. and the VCO oscillates on its lowest frequency (free frequency). The synchro frequency has to be always higher than the free frequency and a margin has to be taken. As an example for a synchro range from 30 kHz to 82 kHz , the suggested free frequency is 27 kHz . To compensate for the spread of external components and of the circuit itself, the free frequency may be adjusted by a DC voltage on Pin 14 (Fmin adjust) (see Figure10 for details).

The PLL1 ensures the coincidence between the leading edge of the synchro signal and a phase reference obtained by comparison between the sawtooth of the VCO and an internal DC voltage adjustable between 2.4 V and 4 V (by Pin 15). So a $\pm 45^{\circ}$ phase adjustment is possible.

Figure 10 : Details of VCO and Fhmin Adjustment


Figure 11 : Safety Functions Block Diagram


Figure 12 : LOCK/UNLOCK Block Diagram


The TDA9103 also includes a LOCK/UNLOCK identification block which sense in real-time wheather the PLL is locked on the incomming horizontal sync signal or not. The resulting information is available on safety blanking output (Pin 23) where it is mixed with others information (see Figure 11). The block diagram of the LOCK/UNLOCK function is described in Figure 12.
The NOR1 gate is receiving the phase comparator output pulses (which also drives the charge pump). When the PLL is locked, on point A there is a very small negative pulse ( 100 ns ) at each horizontal cycle, so after R-C filter, there is a high level on Pin 13 which force SBLK to high level (provided other inputs on NOR2 are also at low level).
When the PLL is unlocked, the 100 ns negative pulse on $\mathbf{A}$ becomes much larger and consequently the average level on Pin 13 will decrease. When it reaches 6.5 V , point $\mathbf{B}$ goes to high level forcing NOR2 open collector output to " 0 ".
The status of Pin 13 is approximately the following :

- Near OV when there is no H -SYNC,
- Between 0 and 4 V with H -SYNC frequency differ-
ent from VCO,
- Between 4 and 8 V when H -SYNC frequency = VCO frequency but not in phase, - Near to 8 V when PLL is locked.

It is important to notice that Pin 13 is not an output pin and must only be used for filtering purpose (see Figure 12).

Figure 13 : PLL1 Timing Diagram


## PLL2

Figure 14 : Dual PLL Block Diagram


The PLL2 ensures the coincidence between the leading edge of the shaped flyback signal and a phase reference signal obtained by comparison of the sawtooth of the VCO and a constant DC voltage (3.2V) (see Figure 15).

Figure 15 : PLL2 Timing Diagram


The phase comparator of PLL2 is similar to the one of PLL1, it is followed by a charge pump with a
$\pm 0.5 \mathrm{~mA}$ (typ.) output current.
The flyback input is composed of an NPN transistor. This input has to be current driven. The maximum recommanded input current is 2 mA (see Figure 16).

Figure 16 : Flyback Input Electrical Diagram


## Output Section

The H -drive signal is transmitted to the output through a shaping block ensuring a duty cycle adjustable from $30 \%$ to $50 \%$. In order to ensure a reliable operation of the scanning power part, the output is inhibited in the following circumstances:

- Vcc too low.
- Xray protection activated.
- During the flyback.
- Output voluntarily inhibited.

The output stage is composed of a Darlington NPN bipolar transistor. Both the collector and the emitter are accessible.

Figure 17 : Output stage simplified diagram, showing the two possibilities of connection


The outputDarlington is in off-state when the power scanning transistor is also in off-state.
The maximum output current is 20 mA , and the correspondingvoltage drop of the outputdarlington is 1.1 V typically.
It is evident that the power scanning transistor cannot be directly driven by the integrated circuit. An interface has to be designed betweenthe circuit and the power transistor which can be of bipolar or MOS type.
Outputs inhibition: the application of a voltage lower than 1V (typ.) on Pin 2 (duty cycle adjust) inhibits the horizontal, vertical and SMPS outputs. This is not memorised.
X-ray protection : the activation of the X-ray protection is obtained by application of a high level on the X -ray input ( $>1.6 \mathrm{~V}$ ). Consequences of X -ray protection are :

- Inhibition of H drive output.
- Inhibition of SPMS output.
- Activation of safety blanking output.

The reset of this protection is obtained by $\mathrm{V}_{\mathrm{cc}}$ switch off.

## S Correction. S Outputs

In the case where the "S correction" of the horizontal scanning is performed using capacitors, it is necessary to switch capacitors when the frequency changes.
For this the outputsS1, 2, 3 and 4 (Pins 9, 8, 7 and 16) give an indication about the horizontal frequency by monitoring the control voltage of the VCO (Pin 12).
The switching of the S outputs occurs for the following value of the control voltage.

| S 1 | 2 V |
| :---: | :---: |
| S 2 | 2.4 V |
| S 3 | 3 V |
| S 4 | 3.7 V |

The use of comparators with hysteresis avoids erratic switching of the Sout outputs if the control voltage of the VCO remains very close to a switching reference level.

## SMPS

This unit generates the supply voltage for the horizontal scanning system. This supply voltage is approximately proportional to the H frequency in order to keep the scanning amplitude constant when the frequency changes. More precisely the amplitude regulation is obtained by detecting and regulating the "flyback" amplitude or EHT value.
The power supply is a step-up converter and it uses the "current-mode" regulation principle.
The power supply works in synchronism with the horizontal scanning. The switching power transistor (external to the TDA9103) is switched on at the beginning of the positive slope of the horizontal sawtooth. It is switched off as required by the integrated regulator. The current in the switching power transistor is monitored and limited, and the ratio Ton/Ton+Toff of the power transistor is limited to $75 \%$ typically providing a very good reliability to the power supply.

Figure 18 : SMPS Block Diagram


Figure 19 : SMPS Timing Diagram


Figure 20 : H Scanning Amplitude Regulation Example


The following functions are implemented in the TDA9103:

- ADC controlled variable gain amplifier allowing a variation of $\pm 14 \%$ of the voltage reference.
This is used to set the horizontal image amplitude.
- An erroramplifier, the non inverting input of which is connected to the above mentioned adjustable voltage reference.
The inverting input and the output of the error
amplifier are externally accessible.
- A comparator which determines the conduction of the external transistor by comparing the output voltage of the error amplifier and the voltage applied on Pin 42 (Isense), which is the image of the current in the power transistor (current mode principle).
- A flip-flop which memorizes the on or off state of the power transistor.
- An output buffer stage (open collector).


## PARABOLA GENERATION FOR EAST-WEST CORRECTION (see Figure 21)

Starting from the vertical ramp a parabola is generated for E/W correction.
The core of the parabola generator is an analog multiplier which generates a current in the form :

$$
\mathrm{I}=\mathrm{k}\left(\mathrm{~V}_{\mathrm{RAMP}}-\mathrm{V}_{\mathrm{MID}}\right)^{2}
$$

Where $V_{\text {RAMP }}$ is the vertical ramp, typically comprised between 2 and 5 V , $\mathrm{V}_{\text {MID }}$ is a DC voltage with a nominal value of 3.5 V , but adjustable in the range $3.2 \mathrm{~V} \rightarrow 3.8 \mathrm{~V}$ in order to generate a dissymmetric parabola if required (keystone adjustment).
The current is converted into voltage through a variable gain transresistance amplifier. The gain, controlled by the voltage on Pin 37 (E/W-AMP) can be adjusted in the ratio $3 / 1$.
The parabola is available on Pin 36 by the way of an emitter follower which has to be biased by an external resistor ( $10 \mathrm{k} \Omega$ ). It must be AC coupled with external circuitry.
The typical parabola amplitude (AC), with the DC
control voltages $\mathrm{V}_{37}$ and $\mathrm{V}_{38}$ set to 4 V , is 2 V .
It is important to note that the parasitic parabola during the discharge of the vertical oscillator capacitor is suppressed.

## VERTICAL PART (see Figure 22)

The vertical part generates a fixed amplitude ramp which can be affected by a $S$ correction shape. Then, the amplitude of this ramp is adjusted to drive an external power stage.
The internal reference voltage used for the vertical part is available between Pin 26 and Pin 24. It can be used as voltage reference for any DC adjusment to keep a high accuracy to each adjustment. Its typical value is :

$$
\mathrm{V}_{26}=\mathrm{V}_{\text {REF }}=8 \mathrm{~V} .
$$

The charge of the external capacitor on Pin 27 ( $\mathrm{V}_{\text {CAP }}$ generates a fixed amplitude ramp between the internal voltages, $\mathrm{V}_{\mathrm{L}}\left(\mathrm{V}_{\mathrm{L}}=\mathrm{V}_{\text {REF }} / 4\right)$ and $\mathrm{V}_{\mathrm{H}}$ ( $\mathrm{V}_{\mathrm{H}}=5 / 8 \cdot \mathrm{~V}_{\mathrm{REF}}$ ).

Figure 21 : Parabola Generation Principle


Figure 22 : Vertical Part Block Diagram


17/27

## Function

When the synchronisation pulse is not present, an internal current source sets the free running frequency. For an external capacitor, Cosc $=180 \mathrm{nF}$, the typical free running frequency is 84 Hz .

Typical free running frequency can be calculated by :

$$
f_{0}(H z)=1.5 \cdot 10^{-5} \cdot \frac{1}{\operatorname{Cosc}(n F)}
$$

A negative or positive TTL level pulse applied on Pin 34 (VSYNC) can synchronise the ramp in the frequency range [fmin, fmax]. This frequency range dependson the external capacitor connected on Pin 27. A capacitor in the range $[150 \mathrm{nF}, 220 \mathrm{nF}]$ is recommanded for application in the following range: 50 Hz to 120 Hz .

Typical maximum and minimum frequency, at $25^{\circ} \mathrm{C}$ and without any correction (S correction or C correction), can be calculated by :
$f_{\max }=2.5 \cdot \mathrm{f}_{0}$
$\mathrm{f}_{\text {min }}=0.33 \cdot \mathrm{f}_{0}$
If $S$ or $C$ corrections are applied, these values are slighty affected.
If an external synchronisation pulse is applied, the internal oscillator is automaticaly caught but the amplitude is no more constant. An internal correction is activated to adjust it in less than half a second: the highest voltage of the ramp on Pin 27 is sampled on the sampling capacitor connected on Pin 25 (VAGCCAP) at each clock pulse and a transconductance amplifier generates the charge current of the capacitor. The ramp amplitude becomes again constant.
It is recommanded to use a AGC capacitor with low leakage current. A value lower than 100 nA is mandatory.

## DC Control Adjustments

Then, a S correction shape can be added to this ramp. This frequency independent $S$ correction is generated internally; its amplitude is DC adjustable on Pin 28 (VSAMP) and it can be centered to generate C correction, according to the voltage applied on Pin 29 (Vscent).
It is non effective for $\mathrm{V}_{\text {Samp }}$ lower than $\mathrm{V}_{\text {Ref }} / 4$ and maximum for $\mathrm{V}_{\text {SAMP }}=3 / 4 \cdot \mathrm{~V}_{\text {REF }}$.

Endly, the amplitude of this S corrected ramp can be adjusted by the voltage applied on Pin 31 ( $\mathrm{V}_{\text {AMP }}$ ). The adjusted ramp is available on Pin 30 (Vout) to drive an external power stage. The gain of this stage is typically $\pm 30 \%$ when voltage applied on Pin 31 is in the range $V_{\text {ref }} / 4$ to $3 / 4$. Vref. The DC value of this ramp is kept constant in the frequency range, for any correction applied on it. Its typical value is :

$$
\mathrm{V}_{\mathrm{DCOUT}}=\mathrm{V}_{\mathrm{MID}}=7 / 16 \cdot \mathrm{~V}_{\mathrm{REF}}
$$

A DC voltage is available on Pin 32 ( $\mathrm{V}_{\text {DCOUT }}$ ). It is driven by the voltage applied on Pin 33 (VPOs). For a voltage control range between $\mathrm{V}_{\text {REF }} / 4$ and $3 / 4$. $V_{\text {REF }}$, the voltage available on Pin 32 is :

$$
\text { VDCOUT }=7 / 16 \cdot V_{\text {REF }} \pm 300 \mathrm{mV}
$$

So, the Vdcout voltage is correlated with DC value of $V_{\text {OUt }}$. It increases the accuracy when temperature varies.

## Basic Equations

In first approximation, the amplitude of the ramp on Pin 30 (Vout) is :
$\mathrm{V}_{\text {OUT }}-\mathrm{V}_{\text {MID }}=\left(\mathrm{V}_{\text {CAP }}-\mathrm{V}_{\text {MID }}\right)\left[1+0.16 \cdot\left(\mathrm{~V}_{\text {AMP }}-\mathrm{V}_{\text {REF }} / 2\right)\right]$
with $\mathrm{V}_{\mathrm{MID}}=7 / 16 \cdot \mathrm{~V}_{\text {REF }}$; typically 3.5 V $\mathrm{V}_{\text {MID }}$ is the middle value of the ramp on Pin 27 $V_{C A P}=V_{27}$, ramp with fixed amplitude.
On Pin 32 (Vdcout), the voltage (in volts) is calculated by :

$$
\mathrm{V}_{\mathrm{DCOUT}}=\mathrm{V}_{\text {MID }}+0.16 \cdot\left(\mathrm{~V}_{\mathrm{POS}}-\mathrm{V}_{\mathrm{REF}} / 2\right)
$$

Vpos is the voltage applied on Pin 33.
The center of the $S$ correction can be approximatively calculated according to the voltage applied on Pin 29 ( $V_{\text {SCENT }}$ ) :
$\mathrm{V}_{\text {CENTER }}=\mathrm{V}_{\text {MID }}+0.25 \cdot\left(\mathrm{~V}_{\text {SCENT }}-\mathrm{V}_{\text {REF }} / 2\right)$
This is an internal voltage used to adjust the $C$ correction. The S correction can be adjusted along the ramp according to this parameter. It is ineffective when VSAMP is lower than VREF/4.
The current available on Pin 27
(when $\mathrm{V}_{\text {SAMP }}=\mathrm{V}_{\mathrm{REF}} / 4$ ) is : losc $=3 / 8 \cdot V_{\text {REF }} \cdot$ Cosc $\cdot f$
Cosc : capacitor connected on Pin 27
f synchronisation frequency
The recommanded capacitor value on Pin 25 $\left(\mathrm{V}_{\mathrm{AGC}}\right)$ is 470 nF . Its assumes a good stability of the internal closed loop.

## INTERNAL SCHEMATICS

Figure 23


Figure 25


Figure 27


Figure 24

HDUTY
Figure 26


Figure 28


INTERNAL SCHEMATICS (continued)
Figure 29


Figure 31


Figure 33


Figure 35


Figure 30


Figure 32


Figure 34


Figure 36


INTERNAL SCHEMATICS (continued)
Figure 37
VAGCCAP

Figure 38


Figure 39


Figure 40


Figure 41


## INTERNAL SCHEMATICS (continued)

Figure 42


Figure 44


Figure 46


Figure 43


Figure 45


Figure 47


## INTERNAL SCHEMATICS (continued)

Figure 48


Figure 50


Figure 52


Figure 49


Figure 51


Figure 53


APPLICATION DIAGRAM


A demonstration board has been developped by SGS-THOMSON and is available through your usual SGS-THOMSON office.
This board has been designed in order to give first the possibility to evaluate the TDA9103 in STAND ALONE, and then to be easily connected to an existing monitor.
In stand alone evaluation, for exemple, flyback simulator is implemented in order to be able to
close the 2nd PLL loop, potentiometers are also present to easily adjust all functions.
Then for testing in a real application, the upper part of the board can be detached and the remaining part can be connected to real application.
In addition to this, the application board has been volontary designed separating clearly all the blocks. This led to quite large PCB but give much more space for measuring anything on the board.

Figure 54


Figure 55


PACKAGE MECHANICAL DATA


| Dimensions | Millimeters |  |  | Inches |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Min. | Typ. | Max. | Min. | Typ. | Max. |
| A |  |  | 5.08 |  |  | 0.200 |
| A1 | 0.51 |  |  | 0.020 |  |  |
| A2 | 3.05 | 3.81 | 4.57 | 0.120 | 0.150 | 0.180 |
| B | 0.36 | 0.46 | 0.56 | 0.0142 | 0.0181 | 0.0220 |
| B1 | 0.76 | 1.02 | 1.14 | 0.030 | 0.040 | 0.045 |
| C | 0.23 | 0.25 | 0.38 | 0.0090 | 0.0098 | 0.0150 |
| D | 37.85 | 38.10 | 38.35 | 1.490 | 1.5 | 1.510 |
| E | 15.24 |  | 16.00 | 0.60 |  | 0.629 |
| E1 | 12.70 | 13.72 | 14.48 | 0.50 | 0.540 | 0.570 |
| e |  | 1.778 |  |  | 0.070 |  |
| e1 |  | 15.24 |  |  | 0.60 |  |
| e2 |  |  | 18.54 |  |  | 0.730 |
| e3 |  | 3.30 | 3.56 | 0.10 | 0.130 | 0.140 |

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