

SEMICONDUCTOR

September 2011

FDMS3604AS

PowerTrench[®] Power Stage

30 V Asymmetric Dual N-Channel MOSFET

Features

Q1: N-Channel

- Max r_{DS(on)} = 8 mΩ at V_{GS} = 10 V, I_D = 13 A
- Max $r_{DS(on)}$ = 11 m Ω at V_{GS} = 4.5 V, I_D = 11 A

Q2: N-Channel

- Max r_{DS(on)} = 2.6 mΩ at V_{GS} = 10 V, I_D = 23 A
- Max $r_{DS(on)}$ = 3.5 m Ω at V_{GS} = 4.5 V, I_D = 21 A
- Low inductance packaging shortens rise/fall times, resulting in lower switching losses
- MOSFET integration enables optimum layout for lower circuit inductance and reduced switch node ringing
- RoHS Compliant

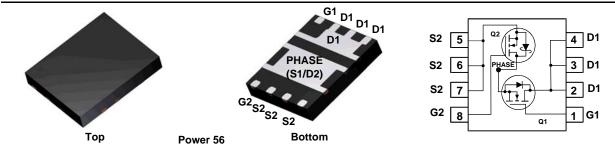


General Description

This device includes two specialized N-Channel MOSFETs in a dual PQFN package. The switch node has been internally connected to enable easy placement and routing of synchronous buck converters. The control MOSFET (Q1) and synchronous SyncFET (Q2) have been designed to provide optimal power efficiency.

Applications

- Computing
- Communications
- General Purpose Point of Load
- Notebook VCORE
- Sever



MOSFET Maximum Ratings T_A = 25 °C unless otherwise noted

Symbol	Parameter			Q2	Units	
V _{DS}	Drain to Source Voltage		30	30	V	
V _{GS}	Gate to Source Voltage	(Note 3)	±20	±20	V	
	Drain Current -Continuous (Package limited)	T _C = 25 °C	30	40	- A	
	-Continuous (Silicon limited)	T _C = 25 °C	60	130		
D	-Continuous	T _A = 25 °C	13 ^{1a}	23 ^{1b}		
	-Pulsed		40	100		
E _{AS}	Single Pulse Avalanche Energy		40 ⁴	112 ⁵	mJ	
P _D	Power Dissipation for Single Operation	T _A = 25 °C	2.2 ^{1a}	2.5 ^{1b}	14/	
	Power Dissipation for Single Operation $T_A = 25 \text{ °C}$		1.0 ^{1c}	1.0 ^{1d}	W	
T _J , T _{STG}	Operating and Storage Junction Temperature Range			+150	°C	

Thermal Characteristics

$R_{ ext{ heta}JA}$	Thermal Resistance, Junction to Ambient	57 ^{1a}	50 ^{1b}		
R_{\thetaJA}	Thermal Resistance, Junction to Ambient	125 ^{1c}	120 ^{1d} °C/W		
$R_{ extsf{ heta}JC}$	Thermal Resistance, Junction to Case	3.5	2		

Package Marking and Ordering Information

Γ	Device Marking	Device	Package	Reel Size	Tape Width	Quantity
	22CA N7CC	FDMS3604AS	Power 56	13 "	12 mm	3000 units
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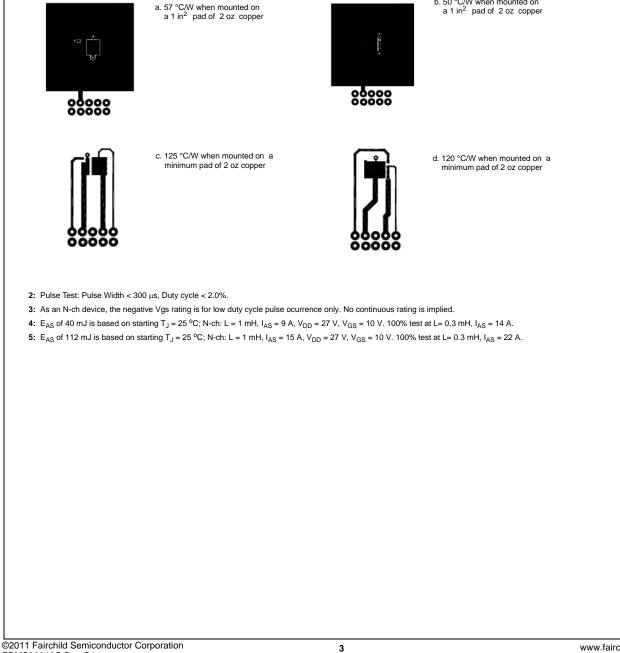
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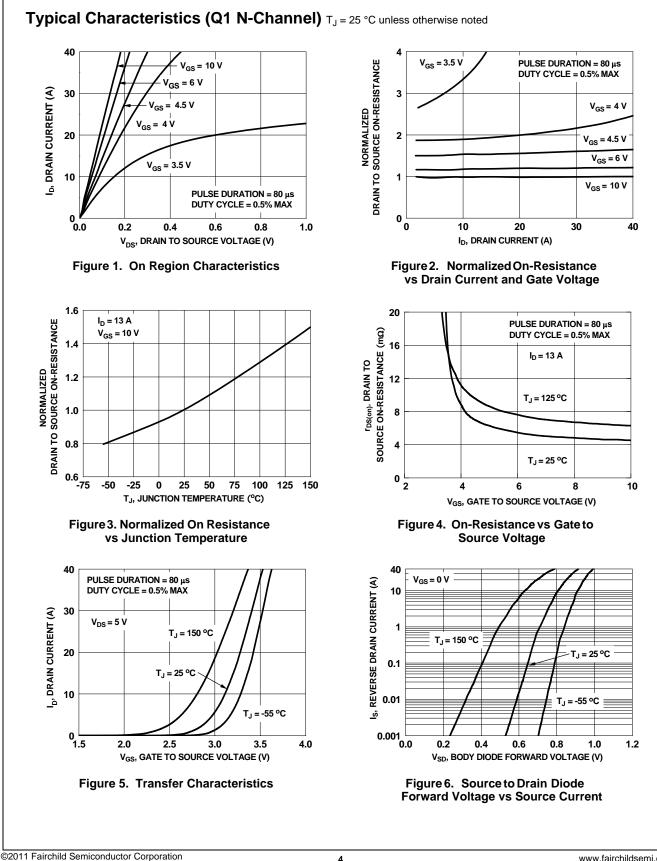
Symbol	Parameter	Test Conditions	Туре	Min	Тур	Max	Units	
Off Chara	acteristics							
BV _{DSS}	Drain to Source Breakdown Voltage	$I_D = 250 \ \mu A, \ V_{GS} = 0 \ V$ $I_D = 1 \ mA, \ V_{GS} = 0 \ V$	Q1 Q2	30 30			V	
ΔΒV _{DSS} ΔΤ _J	Breakdown Voltage Temperature Coefficient	$I_D = 250 \ \mu$ A, referenced to 25 °C $I_D = 10 \ m$ A, referenced to 25 °C	Q1 Q2		15 12		mV/°C	
I _{DSS}	Zero Gate Voltage Drain Current	$V_{DS} = 24 V, V_{GS} = 0 V$	Q1 Q2			1 500	μΑ μΑ	
I _{GSS}	Gate to Source Leakage Current, Forwad	V_{GS} = 20 V, V_{DS} = 0 V	Q1 Q2			100 100	nA nA	
On Chara	octeristics							
V _{GS(th)}	Gate to Source Threshold Voltage	$V_{GS} = V_{DS}, I_D = 250 \ \mu A$ $V_{GS} = V_{DS}, I_D = 1 \ m A$	Q1 Q2	1.1 1.1	2 1.8	2.7 3	V	
$\frac{\Delta V_{GS(th)}}{\Delta T_J}$	Gate to Source Threshold Voltage Temperature Coefficient	$I_D = 250 \ \mu$ A, referenced to 25 °C $I_D = 10 \ m$ A, referenced to 25 °C	Q1 Q2		-6 -5		mV/°C	
		$ \begin{array}{l} V_{GS} = 10 \; V, \; I_D = 13 \; A \\ V_{GS} = 4.5 \; V, \; I_D = 11 \; A \\ V_{GS} = 10 \; V, \; I_D = 13 \; A \; , \; T_J = 125 \; ^\circ C \end{array} $	Q1		5.8 8.5 7.8	8 11 10.8		
r _{DS(on)}	Drain to Source On Resistance		Q2		2 2.6 2.6	2.6 3.5 4	.5	
9 _{FS}	Forward Transconductance	$V_{DS} = 5 V$, $I_D = 13 A$ $V_{DS} = 5 V$, $I_D = 23 A$	Q1 Q2		61 130		S	
Dynamic	Characteristics							
C _{iss}	Input Capacitance	Q1: V _{DS} = 15 V, V _{GS} = 0 V, f = 1 MHZ	Q1 Q2		1273 3078	1695 4095	pF	
C _{oss}	Output Capacitance	Q2: $V_{DS} = 15 \text{ V}, \text{ V}_{GS} = 0 \text{ V}, \text{ f} = 1 \text{ MHZ}$			461 1169	615 1555	pF	
C _{rss}	Reverse Transfer Capacitance				50 98	75 150	pF	
R _g	Gate Resistance		Q1 Q2	0.2 0.2	0.6 0.8	2 3	Ω	
Switching	g Characteristics							
t _{d(on)}	Turn-On Delay Time		Q1 Q2		8.2 13	16 23	ns	
t _r	Rise Time	Q1: V _{DD} = 15 V, I _D = 13 A, R _{GEN} = 6 Ω	Q1 Q2		2.5 4.8	10 10	ns	
t _{d(off)}	Turn-Off Delay Time	Q2:	Q1 Q2		20 31	32 50	ns	
t _f	Fall Time	$V_{DD} = 15 \text{ V}, \text{ I}_{D} = 23 \text{ A}, \text{ R}_{GEN} = 6 \Omega$	Q1 Q2		2.2 3.4	10 10	ns	
Qg	Total Gate Charge	$V_{GS} = 0$ V to 10 V Q1	Q1 Q2		21 47	29 66	nC	
Qg	Total Gate Charge	$V_{GS} = 0 V \text{ to } 4.5 V V_{DD} = 15 V,$ $V_{D} = 13 A$	Q1 Q2		10 22	14 31	nC	
Q _{gs}	Gate to Source Gate Charge	Q2	Q1 Q2		3.9 9		nC	
Q _{gd}	Gate to Drain "Miller" Charge	$V_{DD} = 15 V,$ $I_{D} = 23 A$	Q1 Q2		3.1 5.5		nC	
			~	1		-		

Electrical Characteristics T_J = 25 °C unless otherwise noted

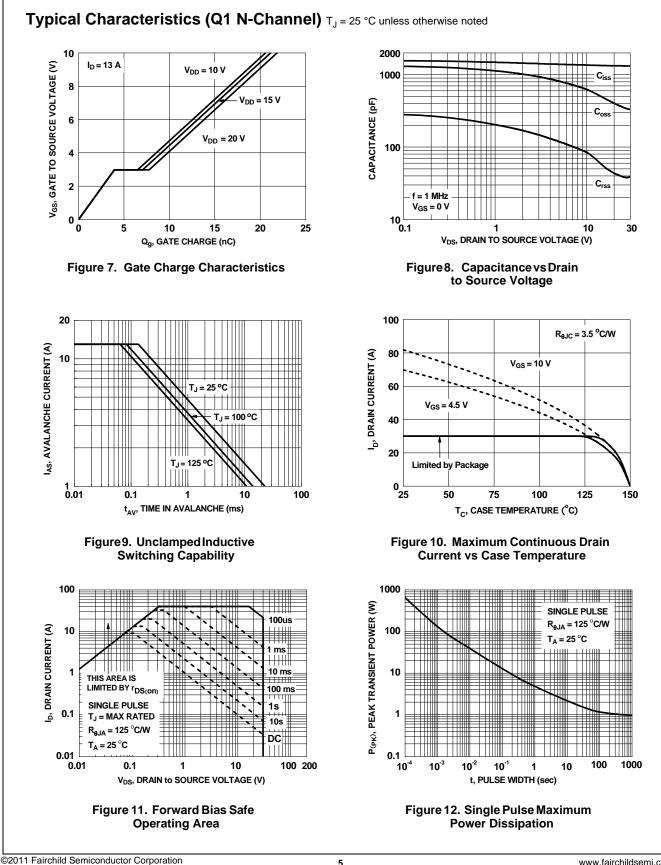
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Symbol	Parameter	Test Conditions	Туре	Min	Тур	Max	Units
Drain-So	urce Diode Characteristics						
V _{SD}	Source to Drain Diode Forward Voltage		Q1 Q2		0.8 0.8	1.2 1.2	V
t _{rr}	Reverse Recovery Time	Q1 I _F = 13 A, di/dt = 100 A/µs	Q1 Q2		25 32	40 51	ns
Q _{rr}	Reverse Recovery Charge	Q2 I _F = 23 A, di/dt = 300 A/µs	Q1 Q2		9 39	18 62	nC
	mined with the device mounted on a 1 in ² pad 2 oz copp board design. a. 57 °C/W when mounted on a 1 in ² pad of 2 oz copper	b. 50 °	R _{0JC} is gu C/W when in ² pad of	mounted of	on	hile R _{θCA} is	determin
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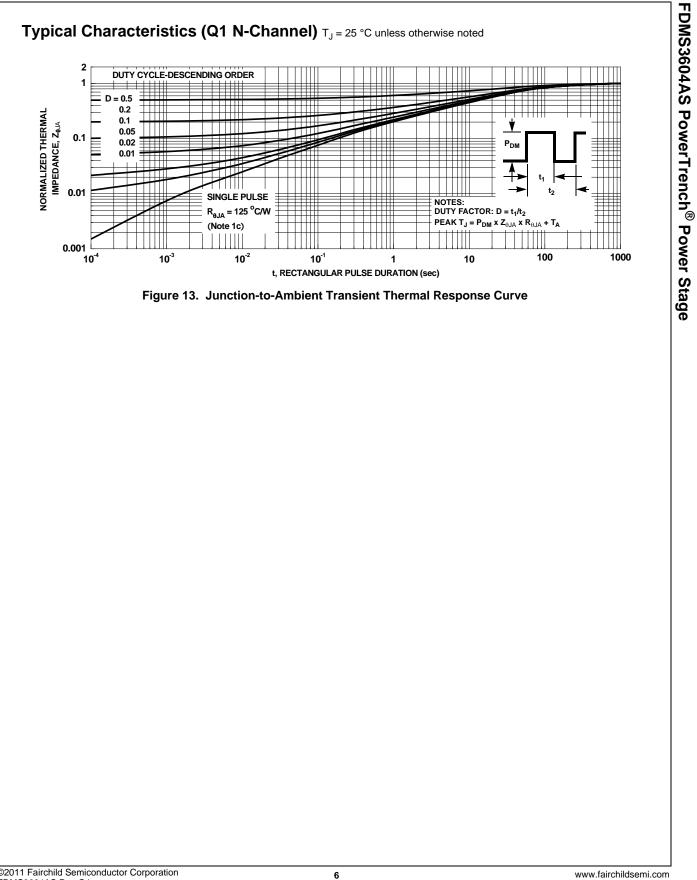


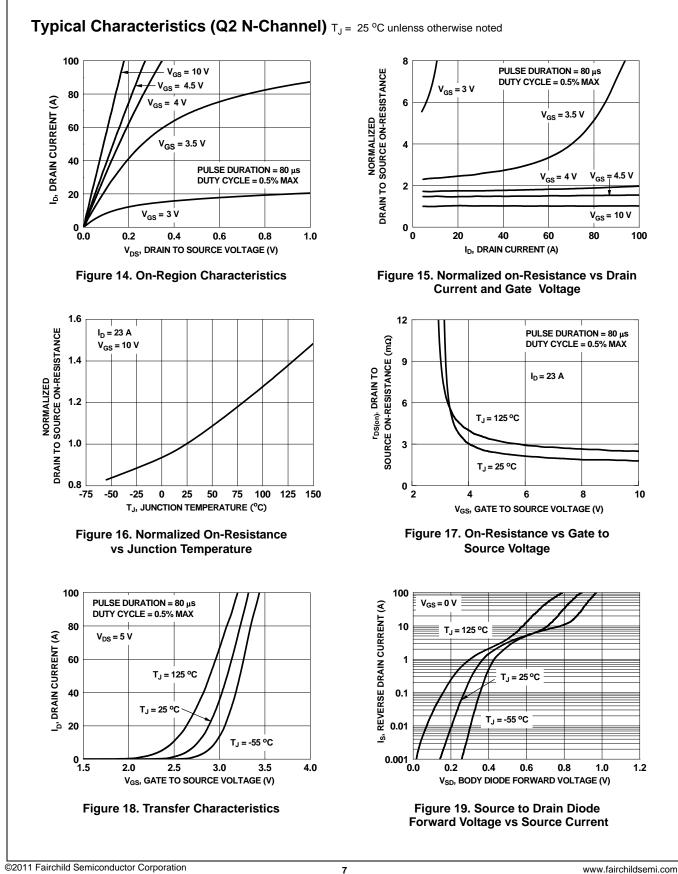


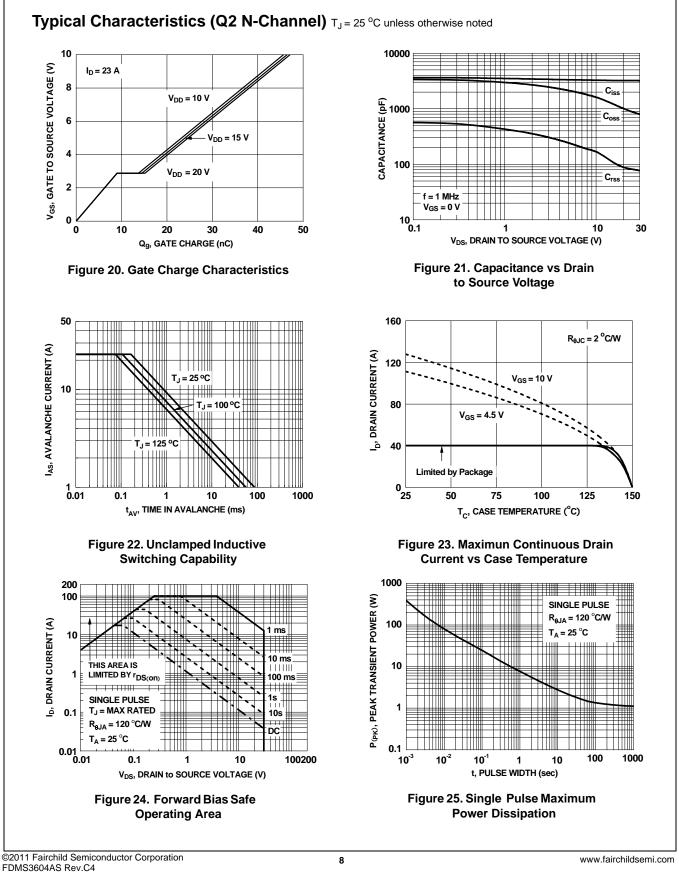


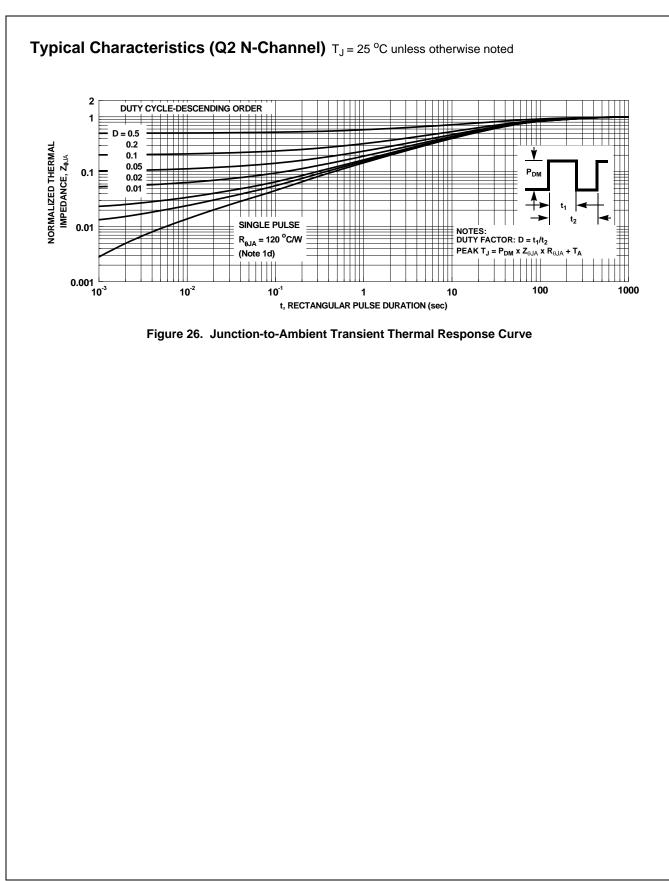
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Typical Characteristics (continued)

SyncFET Schottky body diode Characteristics

Fairchild's SyncFET process embeds a Schottky diode in parallel with PowerTrench MOSFET. This diode exhibits similar characteristics to a discrete external Schottky diode in parallel with a MOSFET. Figure 27 shows the reverse recovery characteristic of the FDMS3604AS.

25 20 didt = 300 A/µs 15 CURRENT (A) 10 5 0 -5 0 50 100 150 200 TIME (ns) Figure 27. FDMS3604AS SyncFET body diode reverse recovery characteristic

Schottky barrier diodes exhibit significant leakage at high temperature and high reverse voltage. This will increase the power in the device.

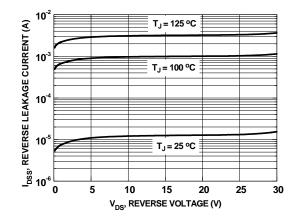
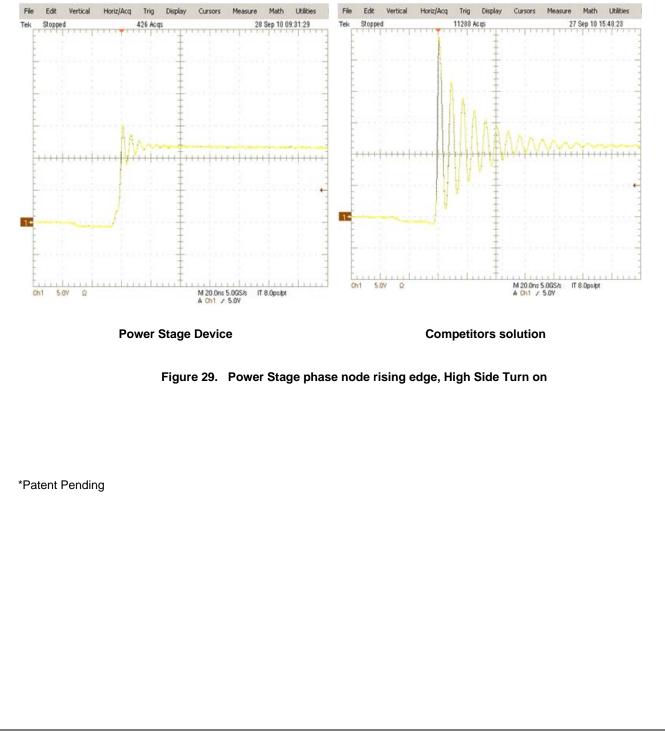


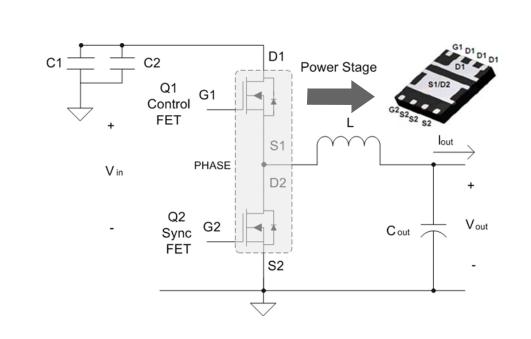
Figure 28. SyncFET body diode reverse leakage versus drain-source voltage

Application Information

1. Switch Node Ringing Suppression

Fairchild's Power Stage products incorporate a proprietary design* that minimizes the peak overshoot, ringing voltage on the switch node (PHASE) without the need of any external snubbing components in a buck converter. As shown in the figure 29, the Power Stage solution rings significantly less than competitor solutions under the same set of test conditions.

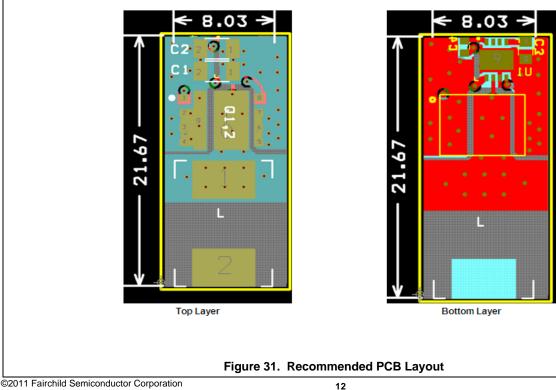






2. Recommended PCB Layout Guidelines

As a PCB designer, it is necessary to address critical issues in layout to minimize losses and optimize the performance of the power train. Power Stage is a high power density solution and all high current flow paths, such as VIN (D1), PHASE (S1/D2) and GND (S2), should be short and wide for better and stable current flow, heat radiation and system performance. A recommended layout procedure is discussed below to maximize the electrical and thermal performance of the part.



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Following is a guideline, not a requirement which the PCB designer should consider:

1. Input ceramic bypass capacitors C1 and C2 must be placed close to the D1 and S2 pins of Power Stage to help reduce parasitic inductance and high frequency conduction loss induced by switching operation. C1 and C2 show the bypass capacitors placed close to the part between D1 and S2. Input capacitors should be connected in parallel close to the part. Multiple input caps can be connected depending upon the application.

2. The PHASE copper trace serves two purposes; In addition to being the current path from the Power Stage package to the output inductor (L), it also serves as heat sink for the lower FET in the Power Stage package. The trace should be short and wide enough to present a low resistance path for the high current flow between the Power Stage and the inductor. This is done to minimize conduction losses and limit temperature rise. Please note that the PHASE node is a high voltage and high frequency switching node with high noise potential. Care should be taken to minimize coupling to adjacent traces. The reference layout in figure 31 shows a good balance between the thermal and electrical performance of Power Stage.

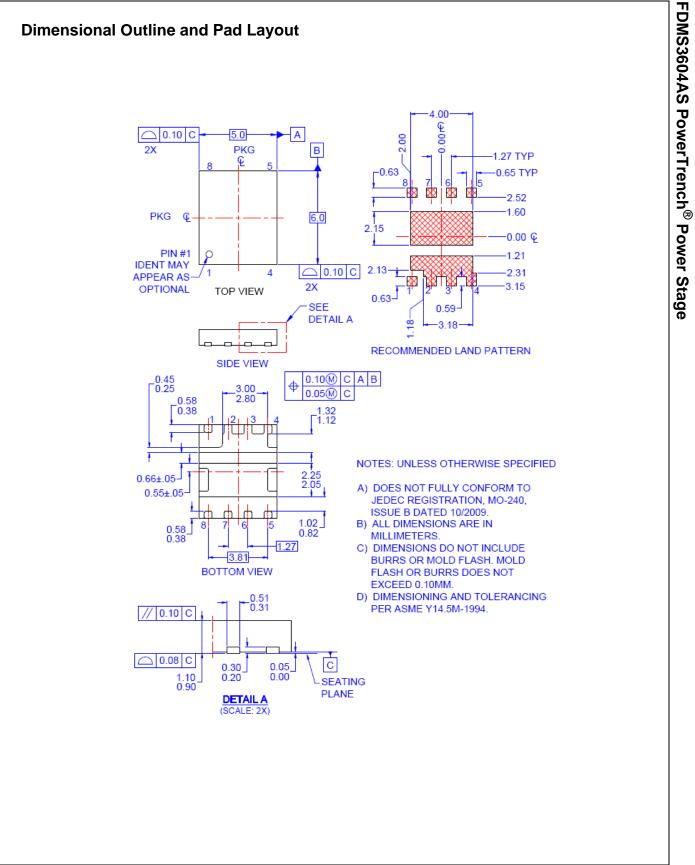
3. Output inductor location should be as close as possible to the Power Stage device for lower power loss due to copper trace resistance. A shorter and wider PHASE trace to the inductor reduces the conduction loss. Preferably the Power Stage should be directly in line (as shown in figure 31) with the inductor for space savings and compactness.

4. The PowerTrench[®] Technology MOSFETs used in the Power Stage are effective at minimizing phase node ringing. It allows the part to operate well within the breakdown voltage limits. This eliminates the need to have an external snubber circuit in most cases. If the designer chooses to use an RC snubber, it should be placed close to the part between the PHASE pad and S2 pins to dampen the high-frequency ringing.

5. The driver IC should be placed close to the Power Stage part with the shortest possible paths for the High Side gate and Low Side gates through a wide trace connection. This eliminates the effect of parasitic inductance and resistance between the driver and the MOSFET and turns the devices on and off as efficiently as possible. At higher-frequency operation this impedance can limit the gate current trying to charge the MOSFET input capacitance. This will result in slower rise and fall times and additional switching losses. Power Stage has both the gate pins on the same side of the package which allows for back mounting of the driver IC to the board. This provides a very compact path for the drive signals and improves efficiency of the part.

6. S2 pins should be connected to the GND plane with multiple vias for a low impedance grounding. Poor grounding can create a noise transient offset voltage level between S2 and driver ground. This could lead to faulty operation of the gate driver and MOSFET.

7. Use multiple vias on each copper area to interconnect top, inner and bottom layers to help smooth current flow and heat conduction. Vias should be relatively large, around 8 mils to 10 mils, and of reasonable inductance. Critical high frequency components such as ceramic bypass caps should be located close to the part and on the same side of the PCB. If not feasible, they should be connected from the backside via a network of low inductance vias.





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