

Triple, Low Cost, Gain of 2, Video Op Amp

Features

- Optimized for 5V operation
- Stable at gain of 2
- 100 MHz Gain bandwidth product
- 130 V/µs slew rate
- Drives 150Ω load to video levels
- Input and outputs operate at negative supply rail
- -60 dB isolation at 4.2 MHz

Applications

- Consumer video amplifier
- Active filters/integrators
- Cost sensitive applications
- Single supply amplifiers

Ordering Information

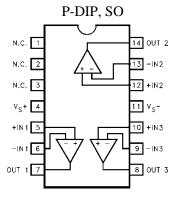
| Part No | Temp. Range | Package | Outline # | | |
|----------|----------------|---------------|-----------|--|--|
| EL2321CN | -40°C to +85°C | 14-lead P-DIP | MDP0031 | | |
| EL2321CS | -40°C to +85°C | 14-lead SO | MDP0027 | | |

General Description

The EL2321C operational amplifier, built using Elantec's complementary bipolar process, offers unprecedented high frequency performance at a very low cost. It is suitable for any application, such as consumer video, where traditional DC performance specifications are of secondary importance to the high frequency specifications. On a 5V supply at a gain of +2 the EL2321C will drive a 150Ω load to +2V, with a bandwidth of 100~MHz. This device achieves 0.1~dB bandwidth at 5~MHz.

The recommended power supply voltage is 5V. At zero and 5V supplies, the inputs will operate to ground. When the outputs are at 0V the amplifier draws only 2.4 mA of supply current.

Connection Diagram



Note: All information contained in this data sheet has been carefully checked and is believed to be accurate as of the date of publication; however, this data sheet cannot be a "controlled document". Current revisions, if any, to these specifications are maintained at the factory and are available upon your request. We recommend checking the revision level before finalization of your design documentation.

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Absolute Maximum Ratings (TA = 25 °C)

Total Supply Voltage 18V Power Dissipation See Curves Input Voltage -6V_S Storage Temperature Range -65°C to +150°C Differential Input Voltage 6V Operating Temperature Range -40°C to +85°C

Peak Output Current 75 mA per amplifier

Important Note:

All parameters having Min/Max specifications are guaranteed. The Test Level column indicates the specific device testing actually performed during production and Quality inspection. Elantec performs most electrical tests using modern high-speed automatic test equipment, specifically the LTX77 Series system. Unless otherwise noted, all tests are pulsed tests, therefor $T_J = T_C = T_A$.

| Test Level | Test Procedure |
|--------------|--|
| I | 100% production tested and QA sample tested per QA test plan QCX0002. |
| II | 100% production tested at T_A = 25°C and QA sample tested at T_A = 25°C, T_{MAX} and T_{MIN} per QA test plan QCX0002. |
| III | QA sample tested per QA test plan QCX0002. |
| IV | Parameter is guaranteed (but not tested) by Design and Characterization Data. |
| \mathbf{v} | Parameter is typical value at $T_A = 25$ °C for information purposes only. |

DC Characteristics

 $V_S\!\!=\!\!+5V,$ $R_L\!\!=\!\!1K$ $\Omega,$ $V_{IN}\!\!=\!\!1V,$ $T_A\!\!=\!\!25^{\circ}C$ unless otherwise specified.

| Parameter | Description | Conditions | Min | Тур | Max | Test Level | Units |
|-------------------|------------------------------|-------------------------------------|-----|-------|-----|---------------|-------|
| V _{OS} | Input Offset Voltage | | -20 | 10 | 20 | I | mV |
| TCV _{OS} | Average Offset Voltage Drift | [1] | | -50 | | V | μV/°C |
| I _B | Input Bias Current | | -15 | -7 | -3 | I | μΑ |
| I _{OS} | Input Offset Current | | | 0.3 | 1.0 | I | μΑ |
| TCI _{OS} | Average Offset Current Drift | [1] | -1 | -3 | | V | nA/°C |
| A _{VOL} | Open Loop Gain | $V_{OUT=5}, 25, R_{L}=1K\Omega$ | 160 | 250 | | I | V/V |
| | | $V_{OUT=5}, 2.5, R_L = 150K\Omega$ | 160 | 250 | | V | V/V |
| PSRR | Power Supply Rejection Ratio | $V_S = 4.5 V \text{ to } 5.5 V$ | 43 | 50 | | I | dB |
| CMRR | Common Mode Rejection Ratio | VCM = 0V to +3.8V | 60 | 65 | | I | dB |
| CMIR | Common Mode Input Range | | 0.0 | | 3.0 | I | V |
| V _{OUT} | Output Voltage Swing | $RFB = R_G = 1K, R_L = 150\Omega$ | 2.8 | 3.2 | | I | V |
| I _{SC} | Output Short Circuit Current | Output to Ground [2] | 75 | 125 | | I | mA |
| I _S | Supply Current | No Load (per channel) $V_{IN} = 0V$ | 2.0 | 2.4 | 3.0 | I | mA |
| R _{IN} | Input Resistance | Differential | | 150 | | V | ΚΩ |
| | | Common Mode | | 1.5 | | V | ΜΩ |
| C _{IN} | Input Capacitance | $A_V = +1 @ 10 MHz$ | | 1 | | V | pF |
| R _{OUT} | Output Resistance | | | 0.150 | | V | Ω |
| PSOR | Power Supply Operating Range | Single Supply | 4 | | 6 | V | V |

- 1. Measured from T_{MIN} to T_{MAX} .
- $2. \quad A \ heat\text{-sink is required to keep junction temperature below absolute maximum when an output is shorted.}$

Closed Loop AC Electrical Characteristics

 V_S =5V, AC Test Figure, T_A = 25°C unless otherwise specified

| Parameter | Description | Conditions | Min | Тур | Max | Test Level | Units |
|---------------------------------|--|------------------|-----|-----|-----|---------------|-----------|
| BW | -3dB Bandwidth (V _{OUT} = 0.4 mVp-p) | $A_V = +1$ | | 100 | | V | MHz |
| | ± 0.1 dB Bandwidth ($V_{OUT} = 0.4 \text{ mVp-p}$) | $A_V = +1$ | | 10 | | V | MHz |
| GBWP | Gain Bandwidth Product | | | 50 | | V | MHz |
| PM | Phase Margin | | | 55 | | V | (°) |
| SR | Slew Rate | | 85 | 130 | | V | V/µs |
| FBWP | Full Power Bandwidth | [1] | 8 | 11 | | V | MHz |
| t _R , t _F | Rise Time, Fall Time | 0.1V step | | 2 | | V | ns |
| OS | Overshoot | 0.1V step | | 15 | | V | % |
| t _{PD} | Propagation Delay | | | 3.5 | | V | ns |
| ts | Settling to 0.1% ($A_V = 1$) | VS = 5V, 2V Step | | 80 | | V | ns |
| dG | Differential Gain [2] | NTSC/PAL | | 0.1 | | V | % |
| dP | Differential Phase [2] | NTSC/PAL | | 0.2 | | V | (°) |
| e _N | Input Noise Voltage | 10 KHz | | 15 | | V | nV/rt(Hz) |
| i _N | Input Noise Current | 10 KHz | | 1.5 | | V | nV/rt(Hz) |
| CS | Channel Separation | P = 5 MHz | | 55 | | V | dB |

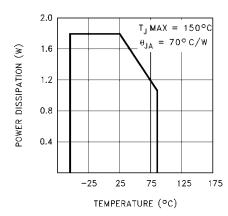
 $^{1. \}quad \text{For } V_S = 5V, \ V_{OUT} = 4V_{pp}. \ \text{Full power bandwidth is based on slew rate measurement using: } \\ \text{FPBW} = SR/(2pi*V_{peak}) \\ \text{For } V_S = 5V, \ V_{OUT} = 4V_{pp}. \\ \text{Full power bandwidth is based on slew rate measurement using: } \\ \text{FPBW} = SR/(2pi*V_{peak}) \\ \text{Full power bandwidth is based on slew rate measurement using: } \\ \text{FPBW} = SR/(2pi*V_{peak}) \\ \text{Full power bandwidth is based on slew rate measurement using: } \\ \text{FPBW} = SR/(2pi*V_{peak}) \\ \text{FULL power bandwidth is based on slew rate measurement using: } \\ \text{FPBW} = SR/(2pi*V_{peak}) \\ \text{FULL power bandwidth is based on slew rate measurement using: } \\ \text{FPBW} = SR/(2pi*V_{peak}) \\ \text{FULL power bandwidth is based on slew rate measurement using: } \\ \text{FULL power bandwidth is based on slew rate measurement using: } \\ \text{FULL power bandwidth is based on slew rate measurement using: } \\ \text{FULL power bandwidth is based on slew rate measurement using: } \\ \text{FULL power bandwidth is based on slew rate measurement using: } \\ \text{FULL power bandwidth is based on slew rate measurement using: } \\ \text{FULL power bandwidth is based on slew rate measurement using: } \\ \text{FULL power bandwidth is based on slew rate measurement using: } \\ \text{FULL power bandwidth is based on slew rate measurement using: } \\ \text{FULL power bandwidth is based on slew rate measurement using: } \\ \text{FULL power bandwidth is based on slew rate measurement using: } \\ \text{FULL power bandwidth is based on slew rate measurement using: } \\ \text{FULL power bandwidth is based on slew rate measurement using: } \\ \text{FULL power bandwidth is based on slew rate measurement using: } \\ \text{FULL power bandwidth is based on slew rate measurement using: } \\ \text{FULL power bandwidth is based on slew rate measurement using: } \\ \text{FULL power bandwidth is based on slew rate measurement using: } \\ \text{FULL power bandwidth is based on slew rate measurement using: } \\ \text{FULL power bandwidth is based on slew rate measurement using: } \\ \text{FULL power bandwidth is bandwidth is bandwidth is bandwidth is bandwidth is$

^{2.} Video performance measured at V_S = 5V, A_V = +2 with 2 times normal video level across R_L = 150 Ω

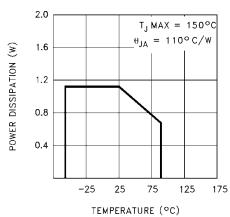
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Typical Performance Curves

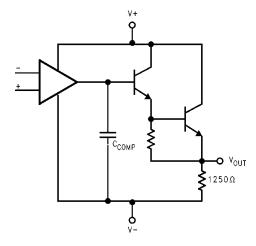
14-Pin Plastic DIP Maximum Power Dissipation vs Ambient Temperature



14-Lead SO Maximum Power Dissipation vs Ambient Temperature



Simplified Block Diagram



Applications Information

Product Description

The EL2321C operational amplifier is stable at a gain of 1. It is built on Elantec's proprietary complimentary bipolar process. This topology allows it to be used in a variety of applications where current mode amplifiers are not appropriate because of restrictions placed on the feedback elements. This product is especially designed for applications where high bandwidth and good video performance characteristics are desired but the higher cost of more flexible and sophisticated products are prohibitive.

Power Supplies

The EL2321C is designed to work at a supply voltage difference of 4.5V to 5.5V. It will work on any combination of \pm supplies. All electrical characteristics are measured with a 5V supply.

Output Swing vs Load

Please refer to the simplified block diagram. This amplifier provides an NPN pull-up transistor output and a passive 1250Ω pull-down resistor to the most negative supply. In a application where the load is connected to V_S- the output voltage can swing to within 200 mV of V_S- .

Output Drive Capability

This device does not have short circuit protection. Each output is capable of than 100 mA into a shorted output. Care must be used in the design to limit the output current with a series resistor.

Single 5 Volt Supply Video Cable Driver

These amplifiers may be used as a direct coupled video cable driver with a gain of 2. With a 75 Ω back matching resistor driving a terminated 75Ω cable the output at the cable load will be original video level (1V NTSC). The best operating mode is with direct coupling. The input signal must be offset to keep the entire signal within the range of the amplifier. The required offset voltage can be set with a resistor divider and a bypass capacitor in the video path (Figure 1). The input DC offset should be between 3V and .5V. With R_A =68K and R_B =4.7K the input offset will be .32V. Since these amplifiers require a DC load at their outputs it is good design practice to add a 250 Ω resistor to ground directly at the amplifier output. Then if the 75Ω cable termination resistor were inadvertently removed there would still be an output signal. The values in figure 1 give an output range of 0V to 2.6V

Output capacitive coupling also has some restrictions. These amplifiers require a DC load at their outputs. A 75Ω back matching resistor to a cable and a 75Ω load to ground at the end of the cable provide a 150Ω DC load. But output capacitive coupling opens this DC path so an extra pulldown resistor on the amplifier output to ground is required. Figure 4 shows a 250Ω resistor. Capacitively coupling the output will require that we shift the output offset voltage higher than in the direct coupled case. Using R_A =43K and R_B =4.7K will make the quiescent output offset voltage about 1V. The output dynamic range will be .6V to 3V.

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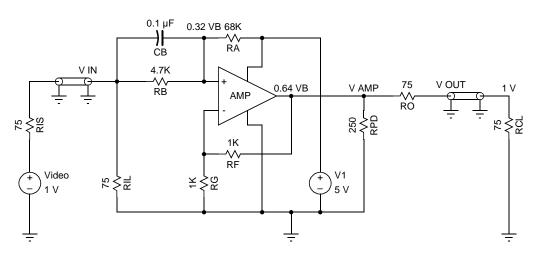


Figure 1.

Input capacitive coupling will increase the needed dynamic range of the amplifier. The standard NTSC video signal is 1V peak to peak plus 143 mV for the color AC peak. The video signal is made up of the -286 mV sync pulse plus the 714 mV picture signal which may very from 0V to 714 mV. The video signal average value for a black picture is about 28 mV (*Figure 2*) and with a white picture level is about 583 mV (*Figure 3*). This gives a maximum change in average value of about

555 mV. A direct coupled amplifier with an standard NTSC video signal needs a dynamic range of 1.143V. But with input capacitance coupling the dynamic range requirements are the sum of the 1.143V video plus the average picture value change of 0.555V or 1.698V_{P-P}. At a gain of two this doubles to 3.394V. These amplifiers do not have this much dynamic range so a gain of less than 2 must be used to avoid waveform compression under all conditions.

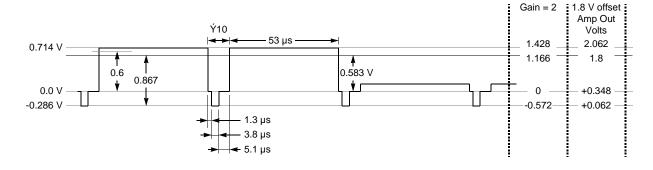


Figure 2. White Level Video

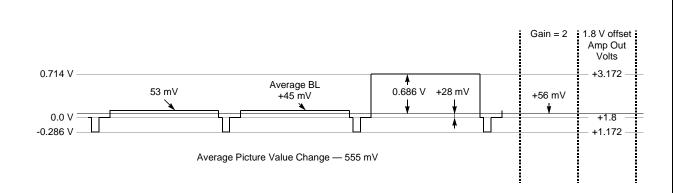


Figure 3. Black Level Video

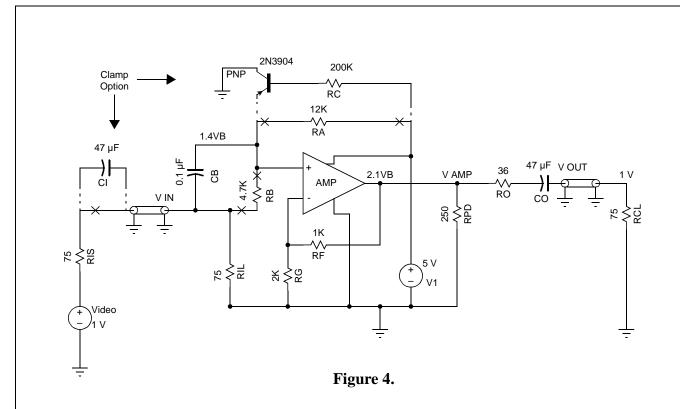
Capacitively coupling the input and output is worse than a capacitor only on the input. Without any special compromises you can only take a gain of one. But if the backmatch resistor is reduced to 36Ω , reducing the output range requirement 25% and the output offset is shifted to 2.1V you can take a gain of 1.5 and have a standard NTSC 1Vat the 75 Ω load.

A simple transistor, capacitor and resistor sync tip clamp may be used when the input is already AC coupled to set the sync tip to ground. This gives the input a fixed DC level and can be used like a direct coupled input. The clamp uses a PNP transistor with the collector at ground and the base has a 200 K Ω resistor to 5V. The emitter connects to the amplifier input and a capacitor from the video input. The clamp functions as an inverted Beta current source for input bias current with plus inputs and a clamp to ground for minus inputs. The RA and RB resistors are removed for the clamp option (Figure 4).

Printed Circuit Layout

The EL2321C is well behaved, and easy to apply in most applications. However, a few simple techniques will help assure rapid, high quality results. As with any high frequency device, good PCB layout is necessary for optimum performance. Ground-plane construction is highly recommended, as is good power supply bypassing. A 0.1 µF ceramic capacitor is recommended for bypassing both supplies. Lead lengths should be as short as possible, and bypass capacitors should be as close to the device pins as possible. For good AC performance, parasitic capacitances should be kept to a minimum at both inputs and at the output. Resistor values should be kept under 5 K Ω because of the RC time constants associated with the parasitic capacitance. Metal-film and carbon resistors are both acceptable, use of wire-wound resistors is not recommended because of their parasitic inductance. Similarly, capacitors should be low-inductance for best performance.

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General Disclaimer

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Elantec, Inc.

1996 Tarob Court Milpitas, CA 95035

Telephone: (408) 945-1323

(800) 333-6314

Fax: (408) 945-9305 European Office: 44-71-482-4596

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