PWM STEP-UP DC/DC CONVERTER RH5RH××1A/××2B/××3B SERIES

APPLICATION MANUAL

RIGOM

PWM STEP-UP DC/DC CONVERTER

RH5RH××1A/××2B/××3B SERIES

OUTLINE

The RH5RH××1A/××2B/××3B Series are PWM Step-up DC/DC converter ICs by CMOS process.

The RH5RH××1A IC consists of an oscillator, a PWM control circuit, a driver transistor (Lx switch), a reference voltage unit, an error amplifier, a phase compensation circuit, resistors for voltage detection, a soft-start circuit, and an Lx switch protection circuit. A low ripple, high efficiency step-up DC/DC converter can be constructed of this RH5RH××1A IC with only three external components, that is, an inductor, a diode and a capacitor.

These RH5RH××1A/××2B/××3B ICs can achieve ultra-low supply current (no load) –TYP. 15µA –by a newly developed PWM control circuit, equivalent to the low supply current of a VFM (chopper) Step-up DC/DC converter.

Furthermore, these ICs can hold down the supply current to TYP. $2\mu A$ by stopping the operation of the oscillator when the input voltage > (the output voltage set value + the dropout voltage by the diode and the inductor).

These RH5RH××1A/××2B/××3B Series ICs are recommendable to the user who desires a low ripple PWM DC/DC converter, but cannot adopt a conventional PWM DC/DC converter because of its too large supply current.

The RH5RH××2B/××3B Series ICs use the same chip as that employed in the RH5RH××1A IC and are provided with a drive pin (EXT) for an external transistor. Because of the use of the drive pin (EXT), an external transistor with a low saturation voltage can be used so that a large current can be caused to flow through the inductor and accordingly a large output current can be obtained. Therefore, these RH5RH××2B/××3B Series ICs are recommendable to the user who need a current as large as several tens mA to several hundreds mA.

The RH5RH $\times \times 3B$ IC also includes an internal chip enable circuit so that it is possible to set the standby supply current at MAX. $0.5\mu A$.

These RH5RH××1A/××2B/××3B ICs are suitable for use with battery-powered instruments with low noise and low supply current.

FEATURES

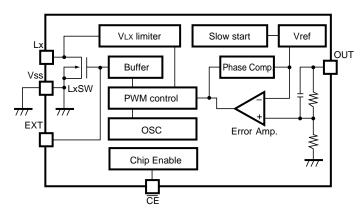
- Small Number of External Components ······Only an inductor, a diode and a capacitor (RH5RH××1A)
- Low Supply CurrentTYP. 15µA (RH5RH301A)
- Low Ripple and Low Noise
- Low Start-up Voltage (when the output current is 1mA) ········MAX. 0.9V
- High Output Voltage Accuracy ------±2.5%
- High Efficiency ······TYP. 85%
- Low Temperature-Drift Coefficient of Output Voltage ······TYP. ±50 ppm/°C
- Soft-Start ······MIN. 500µs
- Small Packages ·········SOT-89 (RH5RH××1A, RH5RH××2B), SOT-89-5 (RH5RH××3B)

APPLICATIONS

- Power source for battery-powered equipment.
- Power source for cameras, camcorders, VCRs, PDAs, electronic data banks, and hand-held communication equipment.
- Power source for instruments which require low noise and low supply current, such as hand-held audio equipment.
- Power source for appliances which require higher cell voltage than that of batteries used in the appliances.



BLOCK DIAGRAM



Error Amp. (Error Amplifier) has a DC gain of 80dB, and Phase Comp. (Phase Compensation Circuit) provides the frequency characteristics including the 1st pole (fp=0.25Hz) and the zero point (fz=2.5kHz). Furthermore, another zero point (fz=1.0kHz) is also obtained by the resistors and a capacitor connected to the OUT pin.

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(Note) Lx Pin ·······only for RH5RH××1A and RH5RH××3B

EXT Pin ······only for RH5RH××2B and RH5RH××3B

CE Pin ······only for RH5RH××3B
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SELECTION GUIDE

In RH5RH Series, the output voltage, the driver, and the taping type for the ICs can be selected at the user's request. The selection can be made by designating the part number as shown below:

$$\begin{array}{ccc} RH5RH \underset{\frown}{\times} \underset{\frown}{\times} \underset{\frown}{\times} -\underset{\frown}{\times} \underset{\frown}{\times} \leftarrow Part \ Number \\ & a \quad b \quad c \end{array}$$

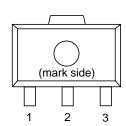
Code	Description
a	Setting Output Voltage (Vout): Stepwise setting with a step of 0.1V in the range of 2.7V to 7.5V is possible.
b	Designation of Driver: 1A: Internal Lx Tr. Driver (Oscillator Frequency 50kHz) 2B: External Tr. Driver (Oscillator Frequency 100kHz) 3B: Internal Tr./External Tr. (selectively available) (Oscillator Frequency 100kHz, with chip enable function)
c	Designation of Taping Type: Ex. SOT-89 : T1, T2 SOT-89-5 : T1, T2 (refer to Taping Specifications) "T1" is prescribed as a standard.

For example, the product with Output Voltage 5.0V, the External Driver (the Oscillator Frequency 100kHz) and Taping Type T1, is designated by Part Number RH5RH502B-T1.

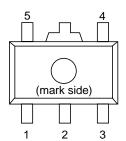


PIN CONFIGURATION

• SOT-89







PIN DESCRIPTION

	Pin No.		Pin No.			
××1B	××2B	××3B	Symbol	Description		
1	1	5	Vss	Ground Pin		
2	2	2	OUT	Step-up Output Pin, Power Supply (for device itself)		
3	_	4	Lx	Switching Pin (Nch Open Drain)		
_	3	3	EXT	External Tr. Drive Pin (CMOS Output)		
_	_	1	$\overline{ ext{CE}}$	Chip Enable Pin (Active Low)		

ABSOLUTE MAXIMUM RATINGS

Vss=0V

Symbol	Item	Rating	Unit	Note
Vout	Output Pin Voltage	+12	V	
VLX	Lx Pin Voltage	+12	V	Note1
VEXT	EXT Pin Voltage	– 0.3 to Vout+0.3	V	Note2
VCE	CE Pin Voltage	-0.3 to Vout+0.3	V	Note3
Ilx	Lx Pin Output Current	250	mA	Note1
IEXT	EXT Pin Current	±50	mA	Note2
PD	Power Dissipation	500	mW	
Topt	Operating Temperature Range	-30 to +80	°C	
Tstg	Storage Temperature Range	−55 to +125	°C	
Tsolder	Lead Temperature(Soldering)	$260^{\circ}\mathrm{C},\!10\mathrm{s}$		

(Note 1) Applicable to RH5RH××1A and RH5RH××3B. (Note 2) Applicable to RH5RH××2B and RH5RH××3B.

(Note 3) Applicable to RH5RH××3B.

ABSOLUTE MAXIMUM RATINGS

Absolute Maximum ratings are threshold limit values that must not be exceeded even for an instant under any conditions. Moreover, such values for any two items must not be reached simultaneously. Operation above these absolute maximum ratings may cause degradation or permanent damage to the device. These are stress ratings only and do not necessarily imply functional operation below these limits.

ELECTRICAL CHARACTERISTICS

• RH5RH301A V_{OUT=3.0}V

Symbol	Item	Conditions	MIN.	TYP.	MAX.	Unit	Note
Vout	Output Voltage		2.925	3.000	3.075	V	
Vin	Input Voltage				8	V	
Vstart	Start-up Voltage	Iout=1mA,Vin : 0→2V		0.8	0.9	V	
Vhold	Hold-on Voltage	Iout=1mA,Vin : 2→0V	0.7			V	
Idd1	Supply Current 1	To be measured at OUT Pin (excluding Switching Current)		15	25	μA	
Idd2	Supply Current 2	To be measured at OUT Pin (excluding Switching Current) VIN=3.5V		2	5	μA	
ILX	Lx Switching Current	VLX=0.4V	60			mA	
ILXleak	Lx Leakage Current	VLX=6V,VIN=3.5V			0.5	μA	
fosc	Oscillator Frequency		40	50	60	kHz	
Maxdty	Oscillator Maximum Duty Cycle	on (VLx "L") side	70	80	90	%	
η	Efficiency		70	85		%	
tstart	Soft-Start Time	Time required for the rising of Vout up to 3V.	0.5	2.0		ms	Note1
VLXlim	VLX Voltage Limit	Lx Switch ON	0.65	0.8	1.0	V	Note2

Unless otherwise provided, Vin=1.8V, Vss=0V, Iout=10mA, Topt=25°C, and use External Circuit of Typical Application (FIG. 1).

- (Note 1) Soft-Start Circuit is operated in the following sequence :
 - (1) Vin is applied
 - (2) The voltage (Vref) of the reference voltage unit is maintained at 0V for about 200µs after the application of VIN.
 - (3) The output of Error Amp. is raised to "H" level during the maintenance of the voltage (Vref) of the reference voltage unit.
 - (4) After the rise of Vref, the output of Internal Error Amp. is gradually decreased to an appropriate value by the function of Internal Phase Compensation Circuit, and the Output Voltage is gradually increased in accordance with the gradual decrease of the output of Internal Error Amp.
- (Note 2) Lx is gradually increased after Lx Switch is turned ON. In accordance with the increase of Lx, VLx is also increased. When VLx reaches VLxlim, Lx Switch is turned OFF by an Lx Switch Protection Circuit.



• RH5RH501A V_{OUT=5.0}V

Symbol	Item	Conditions	MIN.	TYP.	MAX.	Unit	Note
Vout	Output Voltage		4.875	5.000	5.125	V	
Vin	Input Voltage				8	V	
Vstart	Start-up Voltage	Iout=1mA,Vin:0→2V		0.8	0.9	V	
Vhold	Hold-on Voltage	Iout=1mA,Vin:2→0V	0.7			V	
Idd1	Supply Current 1	To be measured at OUT Pin (excluding Switching Current)		30	45	μА	
Idd2	Supply Current 2	To be measured at OUT Pin (excluding Switching Current) VIN=5.5V		2	5	μА	
ILX	Lx Switching Current	VLX=0.4V	80			mA	
ILXleak	Lx Leakage Current	VLX=6V,VIN=5.5V			0.5	μA	
fosc	Oscillator Frequency		40	50	60	kHz	
Maxdty	Oscillator Maximum Duty Cycle	on (VLX "L") side	70	80	90	%	
η	Efficiency		70	85		%	
tstart	Soft-Start Time	Time required for the rising of Vout up to 5V.	0.5	2.0		ms	Note1
VLXlim	VLX Voltage Limit	Lx Switch ON	0.65	0.8	1.0	V	Note2

Unless otherwise provided, Vin=3V, Vss=0V, Iout=10mA, Topt=25°C, and use External Circuit of Typical Application (FIG. 1).

- (Note 1) Soft-Start Circuit is operated in the following sequence :
 - (1) Vin is applied.
 - (2) The voltage (Vref) of the reference voltage unit is maintained at 0V for about 200µs after the application of VIN.
 - (3) The output of Error Amp. is raised to "H" level during the maintenance of the voltage (Vref) of the reference voltage unit.
 - (4) After the rise of Vref, the output of Internal Error Amp. is gradually decreased to an appropriate value by the function of Internal Phase Compensation Circuit, and the Output Voltage is gradually increased in accordance with the gradual decrease of the output of Internal Error Amp.
- (Note 2) Lx is gradually increased after Lx Switch is turned ON. In accordance with the increase of lxx, Vxx is also increased. When Vxx reaches Vxxiim, Lx Switch is turned OFF by an Lx Switch Protection Circuit.



• RH5RH302B V_{OUT=3.0}V

Symbol	Item	Conditions	MIN.	TYP.	MAX.	Unit	Note
Vout	Output Voltage		2.925	3.000	3.075	V	
Vin	Input Voltage				8	V	
Vstart	Oscillator Start-up Voltage	EXT no load,Vou⊤ :0→2V		0.7	0.8	V	
IDD1	Supply Current 1	EXT no load,VOUT=2.88V		30	50	μA	
IDD2	Supply Current 2	EXT no load,VOUT=3.5V		2	5	μA	
IEXTH	EXT "H" Output Current	VEXT=VOUT-0.4V			-1.5	mA	
IEXTL	EXT "L" Output Current	Vext=0.4V	1.5			mA	
fosc	Oscillator Frequency		80	100	120	kHz	
Maxdty	Oscillator Maximum Duty Cycle	Vext "H" side	70	80	90	%	
tstart	Soft-Start Time	Time required for the rising of Vout up to 3V	0.5	2.0		ms	Note1

Unless otherwise provided, Vin=1.8V, Vss=0V, Iout=10mA, Topt=25 $^{\circ}$ C, and use External Circuit of Typical Application (FIG. 2).

• RH5RH502B Vout=5.0V

Symbol	Item	Conditions	MIN.	TYP.	MAX.	Unit	Note
Vout	Output Voltage		4.875	5.000	5.125	V	
Vin	Input Voltage				8	V	
Vstart	Oscillator Start-up Voltage	EXT no load,Vou⊤ :0→2V		0.7	0.8	V	
IDD1	Supply Current 1	EXT no load,Vout=4.8V		60	90	μА	
IDD2	Supply Current 2	EXT no load,VOUT=5.5V		2	5	μA	
IEXTH	EXT "H" Output Current	VEXT=VOUT-0.4V			-2	mA	
IEXTL	EXT "L" Output Current	Vext=0.4V	2			mA	
fosc	Oscillator Frequency		80	100	120	kHz	
Maxdty	Oscillator Maximum Duty Cycle	VEXT "H" side	70	80	90	%	
tstart	Soft-Start Time	Time required for the rising of Vout up to 5V	0.5	2.0		ms	Note1

Unless otherwise provided, Vin=3V, Vss=0V, Iout=10mA, Topt=25 $^{\circ}$ C and use External Circuit of Typical Application (FIG. 2).

Note 1) refer to page 5 (Note 1)



• RH5RH303B

Symbol	Item	Conditions	MIN.	TYP.	MAX.	Unit	Note
Vout	Output Voltage		2.925	3.000	3.075	V	
Vin	Input Voltage				8	V	
Vstart	Start-up Voltage	IOUT=1mA,VIN: 0→2V		0.8	0.9	V	
Vhold	Hold-on Voltage	IOUT=1mA,VIN: 2→0V	0.7			V	
η	Efficiency		70	85		%	
Idd1	Supply Current 1	To be measured at OUT pin		30	50	μA	
Idd2	Supply Current 2	To be measured at OUT pin VIN=3.5V		2	5	μA	
Ilx	Lx Switching Current	VLX=0.4V	60			mA	
ILXleak	Lx Leakage Current	VLX=6V,VIN=3.5V			0.5	μA	
Іехтн	EXT "H" Output Current	VEXT=VOUT-0.4V			-1.5	mA	
IEXTL	EXT "L" Output Current	Vext=0.4V	1.5			mA	
VCEH1	CE "H" Level 1	Vout≥1.5V	Vout-0.4			V	
VCEL1	CE "L" Level 1	Vout≥1.5V			0.4	V	
VCEH2	CE "H" Level 2	0.8V≤Vout<1.5V	Vout-0.1			V	
VCEL2	CE "L" Level 2	0.8V≤Vout<1.5V			0.1	V	
Ісен	CE "H" Input Current	CE=3V			0.5	μA	
ICEL	CE "L" Input Current	CE=0V	-0.5			μA	
fosc	Oscillator Frequency		80	100	120	kHz	
Maxdty	Oscillator Maximum Duty Cycle	on (VLX "L")side	70	80	90	%	
tstart	Soft-Start Time	Time required for the rising of Vout up to 3V.	0.5	2.0		ms	Note1
VLXlim	VLX Voltage Limit	Lx Switch ON	0.65	0.8	1.0	V	Note2

Unless otherwise provided, Vin=1.8V, Vss=0V, Iout=10mA, Topt=25°C, and use External Circuit of Typical Application (FIG. 3).

(Note 1) Soft-Start Circuit is operated in the following sequence:

- (1) Vin is applied
- (2) The voltage (Vref) of the reference voltage unit is maintained at 0V for about 200µs after the application of VIN.
- (3) The output of Error Amp. is raised to "H" level during the maintenance of the voltage (Vref) of the reference voltage unit.
- (4) After the rise of Vref, the output of Internal Error Amp. is gradually decreased to an appropriate value by the function of Internal Phase Compensation Circuit, and the Output Voltage is gradually increased in accordance with the gradual decrease of the output of Internal Error Amp.
- (Note 2) Lx is gradually increased after Lx Switch is turned ON. In accordance with the increase of Lx, VLx is also increased. When VLx reaches VLxlim, Lx Switch is turned OFF by an Lx Switch Protection Circuit.



• RH5RH503B Vout=5.0V

Symbol	Item	Conditions	MIN.	TYP.	MAX.	Unit	Note
Vout	Output Voltage		4.875	5.000	5.125	V	
Vin	Input Voltage				8	V	
Vstart	Start-up Voltage	IOUT=1mA,VIN: 0→2V		0.8	0.9	V	
Vhold	Hold-on Voltage	IOUT=1mA,VIN: 2→0V	0.7			V	
η	Efficiency		70	85		%	
Idd1	Supply Current 1	To be measured at OUT pin		60	90	μA	
IDD2	Supply Current 2	To be measured at OUT pin VIN=5.5V		2	5	μA	
Ilx	Lx Switching Current	VLX=0.4V	80			mA	
ILXleak	Lx Leakage Current	VLX=6V,VIN=5.5V			0.5	μA	
Іехтн	EXT "H" Output Current	VEXT=VOUT-0.4V			-2.0	mA	
IEXTL	EXT "L" Output Current	Vext=0.4V	2.0			mA	
VCEH1	CE "H" Level 1	Vout≥1.5V	Vout-0.4			V	
VCEL1	CE "L" Level 1	Vout≥1.5V			0.4	V	
VCEH2	CE "H" Level 2	0.8V≤Vout<1.5V	Vout-0.1			V	
VCEL2	CE "L" Level 2	0.8V≤Vout<1.5V			0.1	V	
Ісен	CE "H" Input Current	CE=5V			0.5	μA	
ICEL	CE "L" Input Current	CE=0V	-0.5			μA	
fosc	Oscillator Frequency		80	100	120	kHz	
Maxdty	Oscillator Maximum Duty Cycle	on (VLX "L")side	70	80	90	%	
tstart	Soft-Start Time	Time required for the rising of Vout up to 5V.	0.5	2.0		ms	Note1
VLXlim	VLX Voltage Limit	Lx Switch ON	0.65	0.8	1.0	V	Note2

Unless otherwise provided, Vin=3V, Vss=0V, Iout=10mA, Topt=25°C, and use External Circuit of Typical Application (FIG. 3).

- (Note 1) Soft-Start Circuit is operated in the following sequence :
 - (1) Vin is applied.
 - (2) The voltage (Vref) of the reference voltage unit is maintained at 0V for about 200µs after the application of VIN.
 - (3) The output of Error Amp. is raised to "H" level during the maintenance of the voltage (Vref) of the reference voltage unit.
 - (4) After the rise of Vref, the output of Internal Error Amp. is gradually decreased to an appropriate value by the function of Internal Phase Compensation Circuit, and the Output Voltage is gradually increased in accordance with the gradual decrease of the output of Internal Error Amp.
- (Note 2) Lx is gradually increased after Lx Switch is turned ON. In accordance with the increase of Lx, VLx is also increased. When VLx reaches VLxlim, Lx Switch is turned OFF by an Lx Switch Protection Circuit.

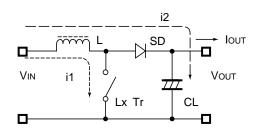


OPERATION OF STEP-UP DC/DC CONVERTER

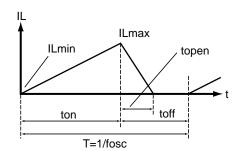
Step-up DC/DC Converter charges energy in the inductor when Lx Transistor (LxTr) is on, and discharges the energy with the addition of the energy from Input Power Source thereto, so that a higher output voltage than the input voltage is obtained.

The operation will be explained with reference to the following diagrams:

< Basic Circuits >



< Current through L >



- Step 1 : LxTr is turned ON and current IL (= i1) flows, so that energy is charged in L. At this moment, IL(=i1) is increased from ILmin (= 0) to reach ILmax in proportion to the on-time period (ton) of LxTr.
- Step 2: When LxTr is turned OFF, Schottky diode (SD) is turned ON in order that L maintains IL at ILmax, so that current IL (= i2) is released.
- Step 3: IL (=i2) is gradually decreased, and in the case of discontinuous mode, IL reaches ILmin (=0) after a time period of topen, so that SD is turned OFF. However, in the case of a continuous mode which will be mentioned later, the time period (toff) runs out before IL reaches ILmin (=0), so that LxTr is turned ON in the next cycle, and SD is turned OFF. In this case, ILmin does not reach zero, and IL (=i1) increases from ILmin (>0).

In the case of PWM control system, the output voltage is maintained constant by controlling the on-time period (ton), with the oscillator frequency (fosc) being maintained constant.

Discontinuous Conduction Mode and Continuous Conduction Mode

In the above two diagrams, the maximum value (ILmax) and the minimum value (ILmin) of the current which flows through the inductor are the same as those when LxTr is ON and also when LxTr is OFF.

The difference between ILmax and ILmin, which is represented by ΔI , is:

wherein T=1/fosc=ton+toff $duty (\%) = ton/T \cdot 100 = ton \cdot fosc \cdot 100$ $topen \leq toff$

In Equation 1, $Vin \cdot ton/L$ and $(Vout-Vin) \cdot topen/L$ are respectively show the change in the current at ON, and the change in the current at OFF.



When the output current (IOUT) is relatively small, topen<toff as illustrated in the above diagram. In this case, the energy charged in the inductor during the time period of ton is discharged in its entirely during the time period of toff, so that ILmin becomes zero (ILmin=0). When IOUT is gradually increased, topen eventually becomes equal to toff (topen=toff), and when IOUT is further increased. ILmin becomes larger than zero (ILmin>0). The former mode is referred to as the discontinuous mode and the latter mode is referred to as the continuous mode.

In the continuous mode, when Equation 1 is solved for ton and the solution is tonc,

$$tonc = T \cdot (1 - V_{IN}/V_{OUT})$$
 Equation 2

When ton<tonc, the mode is the discontinuous mode, and when ton=tonc, the mode is the continuous mode.

Output Current in Discontinuous Mode

In the discontinuous mode, when LxTr is on, the energy PoN charged in the inductor is provided by Equation 3 as follows:

$$\begin{split} Pon = & \int_{0}^{ton} Vin \cdot IL \ (t) \ dt = & \int_{0}^{ton} (Vin^2 \cdot t/L) \ dt \\ = & Vin^2 \cdot ton^2/(2 \cdot L) \cdot \dots \cdot Equation \ 3 \end{split}$$

In the case of the step-up DC/DC converter, the energy is also supplied from the input power source at the time of OFF.

Thus, Poff=
$$\int_0^{\text{topen}} \text{Vin} \cdot \text{IL}(t) dt = \int_0^{\text{topen}} ((\text{Vout-Vin}) \cdot t/\text{L}) dt$$

=Vin \cdot (Vout-Vin) \cdot topen^2/(2 \cdot L)

Here, topen=VIN · ton/(VOUT-VIN) from Equation 1, and when this is substituted into the above equation.

$$=V_{IN}^3 \cdot ton^2/(2 \cdot L \cdot (V_{OUT}-V_{IN})$$
.....Equation 4

Input power is (PON+POFF)/T. When this is converted in its entirely to the output.

Equation 6 can be obtained as follows by solving Equation 5 for IOUT by substituting Equations 3 and 4 into Equation 5:

$$IOUT=VIN^2 \cdot ton^2/(2 \cdot L \cdot T \cdot (VOUT-VIN))$$
 Equation 6

The peak current which flows through $L \cdot LxTr \cdot SD$ is



Therefore it is necessary that the setting of the input/output conditions and the selection of peripheral components should be made with ILmax taken into consideration.

Output Current in Continuous Conduction Mode

When the operation enters into the continuous conduction mode by increasing the IOUT, ILmin becomes equal to Iconst (> 0), and this current always flows through the inductor. Therefore, VIN · Iconst is added to PIN in Equation 5.

Thus, $PIN=VIN \cdot Iconst+(PON+POFF)/T=VOUT \cdot IOUT=POUT$

When the above Equation is solved for IOUT,

 $Iout = Vin^2 \cdot tonc^2/(2 \cdot L \cdot T \cdot (Vout - Vin)) + Vin \cdot Iconst/Vout \cdots Equation 8$

The peak current which flows through $L \cdot LxTr \cdot SD$ is

ILmax=VIN · ton/L+Iconst · · · · · Equation 9

From Equations 6 and 9, the larger the value of L, the smaller the load current at which the operation enters into the continuous mode, and the smaller the difference between ILmax and ILmin, and the smaller the value of ILmax.

Therefore, when the load current is the same, the larger the value of L, the easier the selection of peripheral components with a small allowable current becomes, and the smaller the ripple of the peripheral components can be made. In this case, however, it must be noted from Equation 6 that IOUT becomes small when the allowable current of the inductor is small or when VIN is so small that the operation cannot enter into the continuous mode.

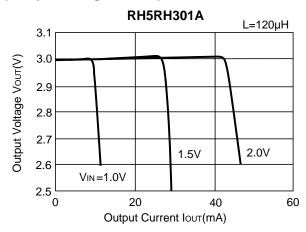
HINTS

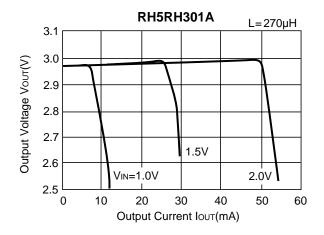
The above explanation is directed to the calculation in an ideal case where there is no energy loss caused by the resistance in the external components and LxSW. In an actual case, the maximum output current will be 50 to 80% of the above calculated maximum output current. In particular, care must be taken because VIN is decreased in an amount corresponding to the voltage drop caused by LxSW when IL is large or VIN is low. Furthermore, it is required that with respect to VOUT, Vf of the diode (about 0.3V in the case of a Schottky type diode) be taken into consideration.

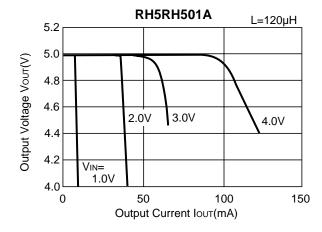


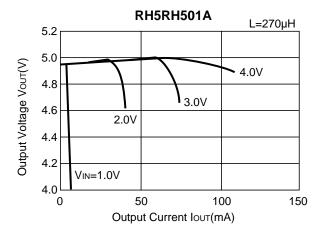
TYPICAL CHARACTERISTICS

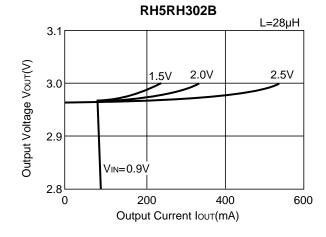
1) Output Voltage vs. Output Current

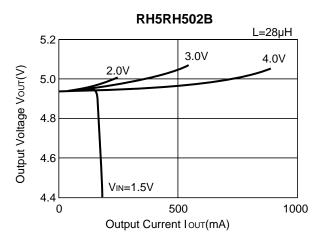




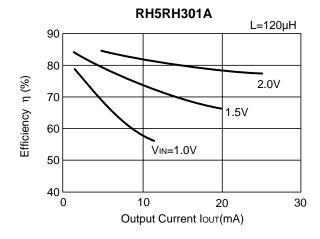


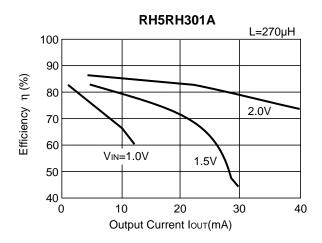


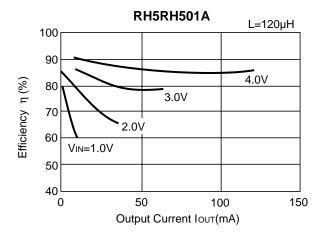


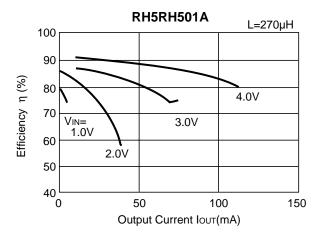


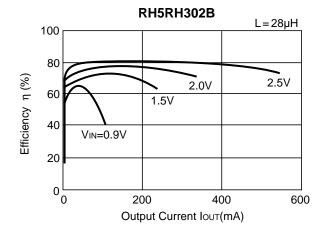
2) Efficiency vs. Output Current

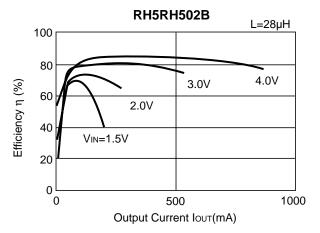




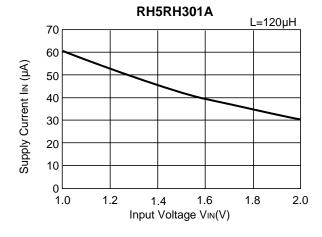


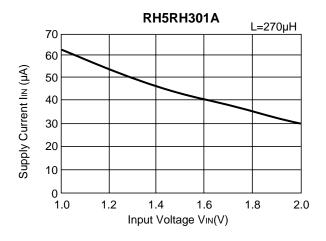


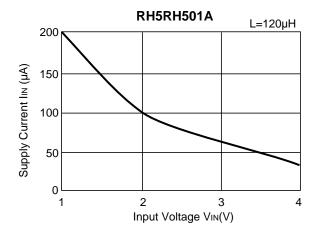


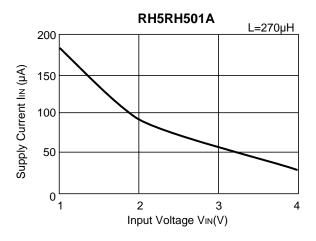


3) Supply Curret (No Load) vs. Input Voltage

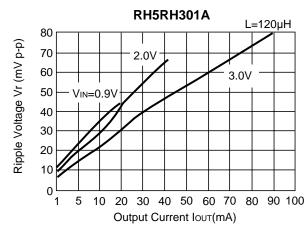


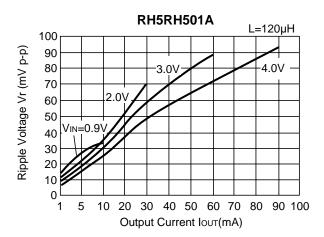


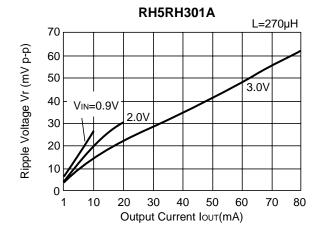


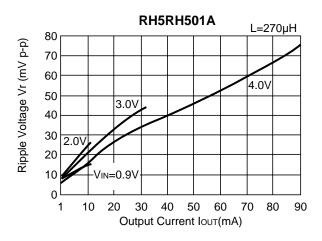


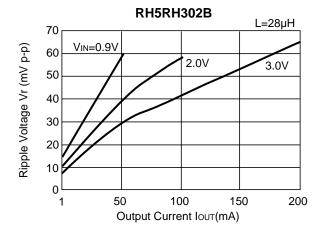
4) Output Current vs.Ripple Voltage

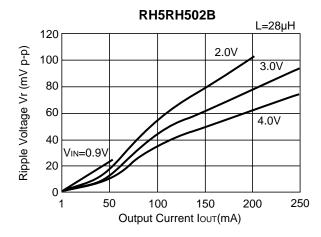




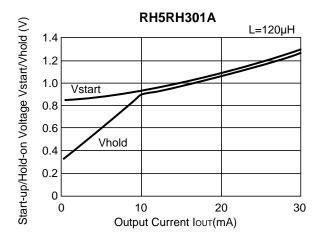


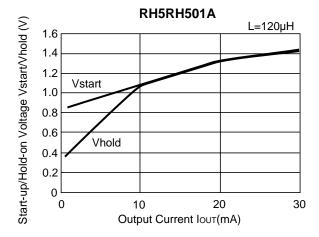


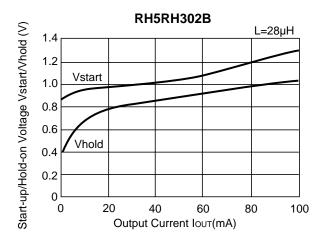


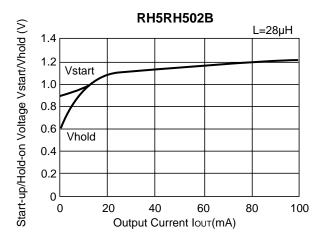


5) Start-up/Hold-on Voltage vs. Output Current (Topt=25°C)

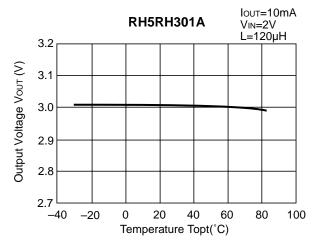


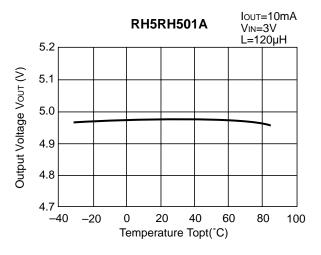


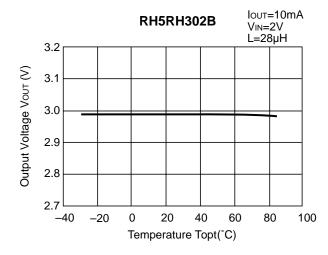


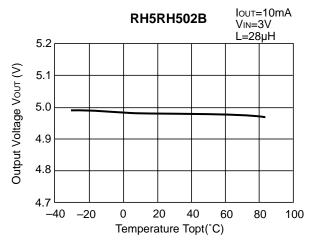


6) Output Voltage vs. Temperature

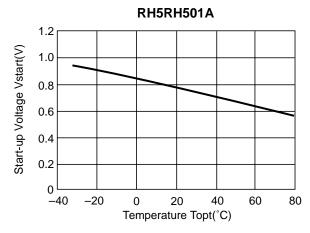




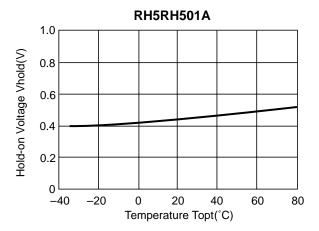




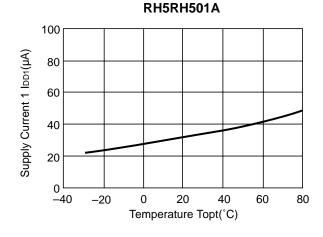
7) Start-up Voltage vs. Temperature



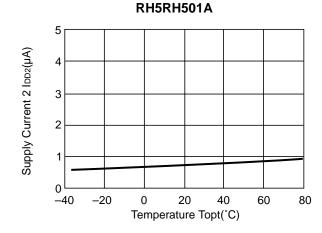
8) Hold-on Voltage vs. Temperature



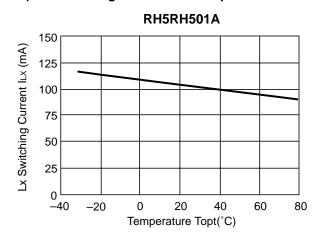
9) Supply Current 1 vs.Temperature



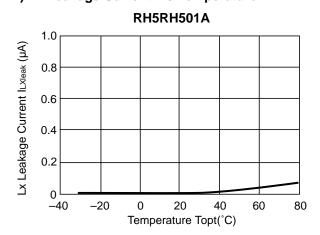
10) Supply Current 2 vs.Temperature



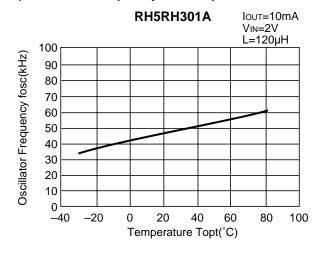
11) Lx Switching Current vs.Temperature

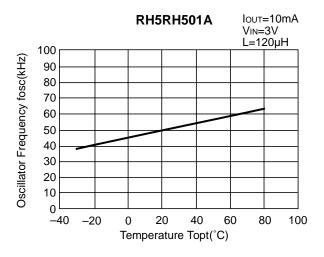


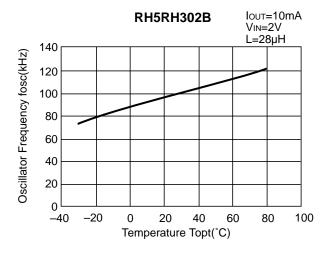
12) Lx Leakage Current vs.Temperature

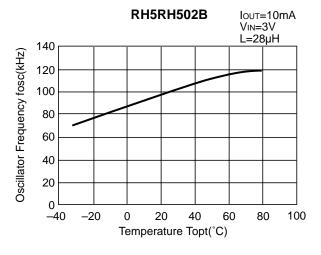


13) Oscillator Frequency vs. Temperature

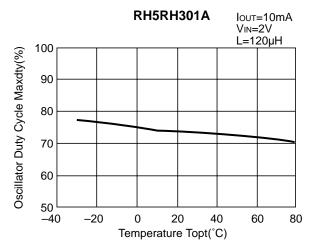


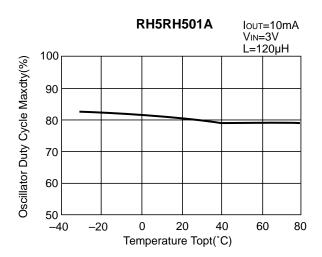


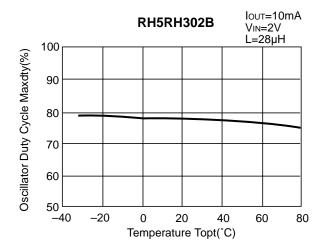


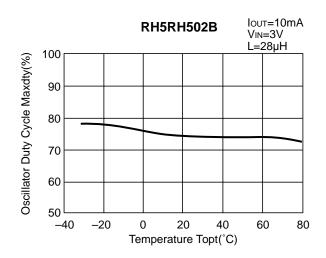


14) Oscillator Duty Cycle vs. Temperature



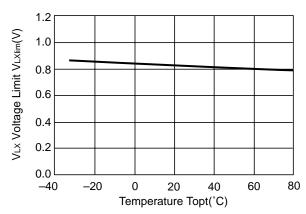






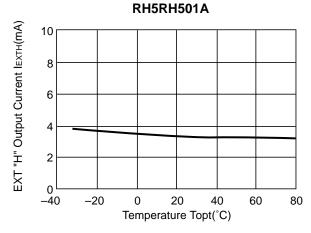
15) VLX Voltage Limit vs. Temperature



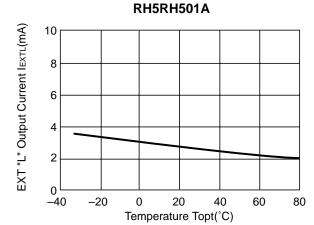




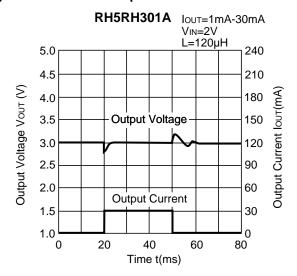
DUEDUEOA

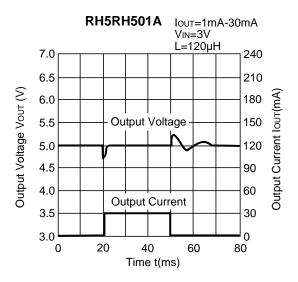


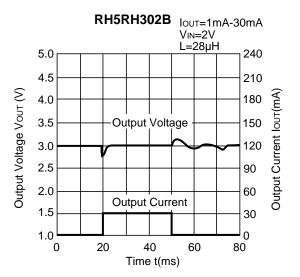
17) EXT "L" Output Current vs. Temperature

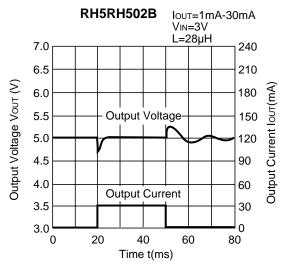


18) Load Transient Response

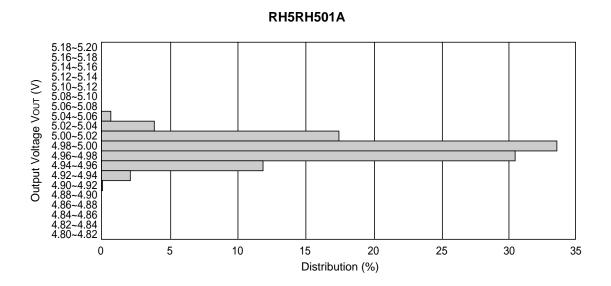






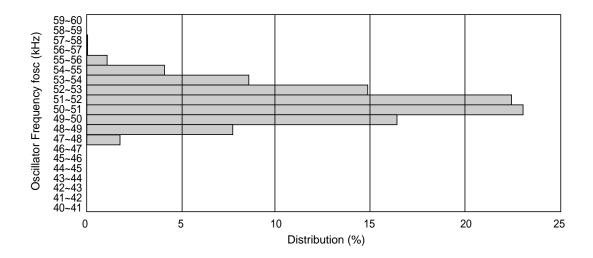


19) Distribution of Output Voltage



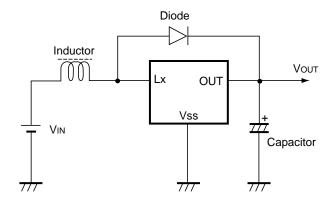
20) Distribution of Oscillator Frequency

RH5RH501A



TYPICAL APPLICATIONS

• RH5RH××1A



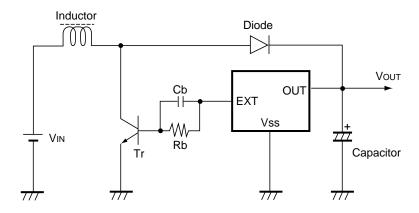
Components Inductor (L) : 120µH (Sumida Electric Co., Ltd.)

Diode (D) : MA721 (Matsushita Electronics Corporation, Schottky Type)

Capacitor (CL) $: 22\mu F$ (Tantalum Type)

FIG. 1

• RH5RH××2B



 $Components\ Inductor\ (L) \\ \hspace{2cm} : 28\mu H\ (Troidal\ Core)$

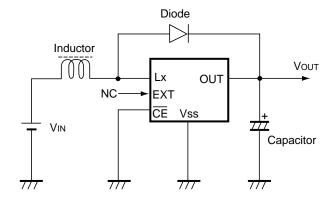
 $Diode\left(D\right) \\ \hspace{1.5cm} : HRP22\left(Hitachi, Schottky \, Type\right)$

 $Capacitor \, (CL) \hspace{1.5cm} : 100 \mu F \, (Tantalum \, Type)$

$$\begin{split} & Transistor \, (Tr) & : 2SD1628G \\ & Base \, Resistor \, (Rb) & : 300\Omega \\ & Base \, Capacitor \, (Cb) & : 0.01 \mu F \end{split}$$

FIG. 2

• RH5RH××3B

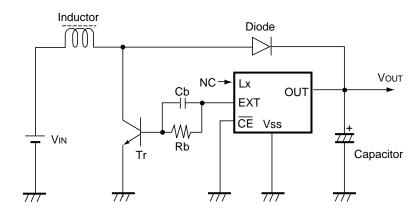


Components Inductor (L) : 120µH (Sumida Electric Co., Ltd.)

 $Diode \, (D) \\ \hspace*{1.5cm} : MA721 \, (Matsushita \, Electronics \, Corporation, \, Schottky \, Type)$

 $Capacitor \, (CL) \hspace{1.5cm} : 22 \mu F \, (Tantalum \, Type)$

FIG. 3



 $Components\ Inductor\ (L) \qquad \qquad :28\mu H\ (Troidal\ Core)$

Diode (D) : HRP22 (Hitachi, Schottky Type)

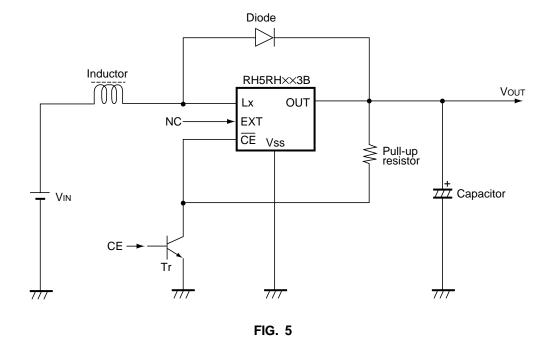
Capacitor (CL) : 100µF (Tantalum Type)

Transistor (Tr) : 2SD1628G

 $\begin{aligned} & Base \ Resistor \ (Rb) & : 300 \Omega \\ & Base \ Capacitor \ (Cb) & : 0.01 \mu F \end{aligned}$

FIG. 4

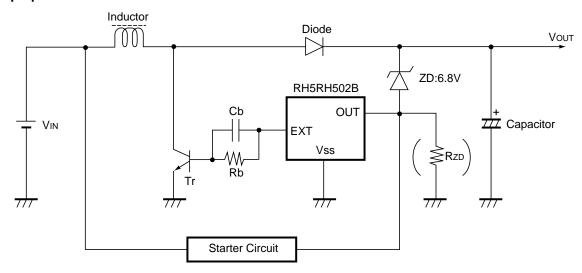
• $\overline{\text{CE}}$ pin Drive Circuit



RIGON

APPLICATION CIRCUITS

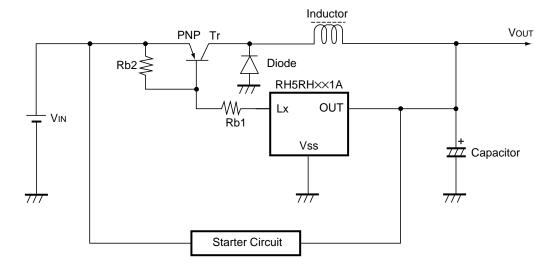
• 12V Step-up Circuit



(Note) When the Output Current is small or the Output Voltage is unstable, use the Rzd for flowing the bias current through the Zener diode ZD.

FIG. 6

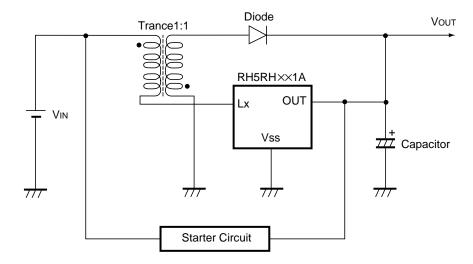
• Step-down Circuit



(Note) When the Lx pin Voltage is over the rating at the time PNP Tr is OFF, use a RH5RH××2B and drive the PNP Tr. by the external NPN Tr.

FIG. 7

• Step-up/Step-down Circuit with Flyback

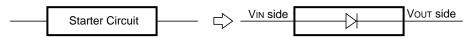


(Note) Use a RH5RH××2B, depend on the Output Current.

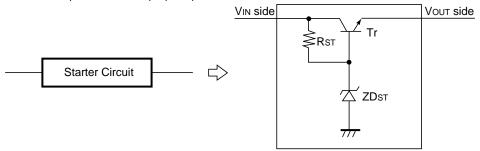
FIG. 8

*The Starter Circuit is necessary for all above circuits.

1.for Step-up Circuit.



2.for Step-down and Step-up/Step-down Circuit.



ZDst $2.5V \le ZDst \le Designation of Output Voltage$ Rst Input Bias Current of ZDst and Tr. (several $k\Omega$ to several hundreds $k\Omega$)

APPLICATION HINTS

When using these ICs, be sure to take care of the following points:

- Set external components as close as possible to the IC and minimize the connection between the components and the IC. In particular, when an external component is connected to OUT Pin, make minimum connection with the capacitor.
- Make sufficient grounding. A large current flows through Vss Pin by switching. When the impedance of the
 Vss connection is high, the potential within the IC is varied by the switching current. This may result in
 unstable operation of the IC.
- Use capacitor with a capacity of 10µF or more, and with good high frequency characteristics such as tantalum capacitor. We recommend the use of a capacitor with a resistance to the voltage being at least three times the output set voltage. This is because there may be the case where a spike-shaped high voltage is generated by the inductor when Lx transistor is turned OFF.
- Take the utmost care when choosing a inductor. Namely, choose such an inductor that has sufficiently small d.c. resistance and large allowable current, and hardly reaches magnetic saturation. When the inductance value of the inductor is small, there may be the case where ILX exceeds the absolute maximum ratings at the maximum load. Use an inductor with an appropriate inductance.
- Use a diode of a Schottky type with high switching speed, and also take care of the rated current.
- These ICs are provided with a soft-start circuit. However, there may be the case where the overshoot of the out put voltage takes place depending upon the peripheral circuits employed and the input/output conditions. In particular, when the input voltage is increased slowly, the occurrence of the overshoot of the output voltage becomes conspicuous. Therefore in the case where the overshoot becomes a problem, take a countermeasure against this problem, for example, by clamping the output (OUT Pin) by use of a Zener diode.
- The transient response characteristics corresponding to the variations in the input and output are set so as to be slightly delayed by an internal phase compensation circuit in order to prevent the oscillation. because of such setting of the transient response characteristics, take care of the occurrence of the overshoot and/or undershoot of the output voltage.
- The internal phase compensation circuit is designed with the avoidance of the problem of the occurrence of the oscillation fully taken into consideration. However, there may be the case the oscillation takes place depending upon the conditions for the attachment of external components. In particular, take the utmost care when an inductor with a large inductance is used.

The performance of power source circuits using these ICs largely depends upon the peripheral components. Take the utmost care in the selection of the peripheral components. In particular, design the peripheral circuits in such a manner that the values such as voltage, current and power of each component, PCB patterns and the IC do not exceed their respective rated values.

