## LB1991V - For Fan Motor 3-phase Brushless Motor Driver

## Overview

The LB1991V is a 3-phase brushless motor driver IC that is optimal for driving the DC fan motor.

## Functions

- 3-phase full-wave voltage drive technique ( $120^{\circ}$ voltage-linear technique)
- Torque ripple correction circuit (overlap correction)
- Speed control technique based on motor voltage and current control
- Built-in FG comparators
- Built-in thermal shutdown circuit


## Specifications

Absolute Maximum Ratings at $\mathrm{Ta}=25^{\circ} \mathrm{C}$

| Parameter | Symbol | Conditions | Ratings | Unit |
| :---: | :---: | :---: | :---: | :---: |
| Maximum supply voltage | $\mathrm{V}_{\mathrm{CC}}{ }^{1 \text { max }}$ |  | 10 | V |
|  | $\mathrm{V}_{\mathrm{CC}}{ }^{2}$ max |  | 11 | V |
|  | $V_{S}$ max |  | 11 | V |
| Applied output voltage | $\mathrm{V}_{\mathrm{O}}$ max |  | $\mathrm{V}_{\mathrm{S}^{+2}}$ | V |
| Maximum output current | IO max |  | 1.0 | A |
| Allowable power dissipation | Pd max | Independent IC | 440 | mW |
| Operating temperature | Topr |  | -20 to +75 | ${ }^{\circ} \mathrm{C}$ |
| Storage temperature | Tstg |  | -55 to +150 | ${ }^{\circ} \mathrm{C}$ |

Allowable Operating Ranges at $\mathrm{Ta}=25^{\circ} \mathrm{C}$

| Parameter | Symbol | Conditions | Ratings | Unit |
| :--- | :--- | :--- | ---: | :---: |
| Supply voltage | $\mathrm{V}_{\mathrm{CC}} 1$ | $\mathrm{~V}_{\mathrm{CC}} 1 \leq \mathrm{V}_{\mathrm{CC}}{ }^{2}$ | 2.7 to 6.0 | V |
|  | $\mathrm{~V}_{\mathrm{CC}}{ }^{2}$ |  | 3.5 to 9.0 | V |
|  | $\mathrm{~V}_{\mathrm{S}}$ |  | Up to $\mathrm{V}_{\mathrm{CC}}{ }^{2}$ | V |
| Hall input amplitude | $\mathrm{V}_{\mathrm{HALL}}$ | Between Hall effect element inputs | $\pm 20$ to $\pm 80$ | $\mathrm{mVp}-\mathrm{p}$ |

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Electrical Characteristics at $\mathrm{Ta}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}} 1=3 \mathrm{~V}, \mathrm{~V}_{\mathrm{CC}} 2=4.75 \mathrm{~V}, \mathrm{~V}_{\mathrm{S}}=1.5 \mathrm{~V}$

| Parameter | Symbol | Conditions | Ratings |  |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | min | typ | max |  |
| Supply Current |  |  |  |  |  |  |
| $\mathrm{V}_{\mathrm{CC}} 1$ current drain | ${ }^{\text {I CC }}{ }^{1}$ | IOUT $=100 \mathrm{~mA}$ |  | 3 | 5 | mA |
| $\mathrm{V}_{\mathrm{CC}}{ }^{2}$ current drain | ${ }^{1} \mathrm{CC}{ }^{2}$ | IOUT $=100 \mathrm{~mA}$ |  | 7.0 | 10.0 | mA |
| $\mathrm{V}_{\text {CC }}{ }^{1}$ quiescent current | ${ }^{1} \mathrm{CC}{ }^{1 Q}$ | $V_{\text {STBY }}=0 \mathrm{~V}$ |  | 1.5 | 3.0 | mA |
| $\mathrm{V}_{C C}$ 2 quiescent current | ${ }^{1} \mathrm{CC} 2 \mathrm{Q}$ | $V_{\text {STBY }}=0 \mathrm{~V}$ |  |  | 100 | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\text {S }}$ quiescent current | ISQ | $V_{\text {STBY }}=0 \mathrm{~V}$ |  | 75 | 100 | $\mu \mathrm{A}$ |
| VX1 |  |  |  |  |  |  |
| High side residual voltage | $\mathrm{V}_{\mathrm{XH}}{ }^{1}$ | ${ }^{\text {I }}$ OUT $=0.2 \mathrm{~A}$ | 0.15 | 0.22 | 0.29 | V |
| Low side residual voltage | $\mathrm{V}_{\mathrm{XL}}{ }^{1}$ | IOUT $=0.2 \mathrm{~A}$ | 0.15 | 0.20 | 0.25 | V |
| VX2 |  |  |  |  |  |  |
| High side residual voltage | $\mathrm{V}_{X H}{ }^{2}$ | IOUT $=0.5 \mathrm{~A}$ |  | 0.25 | 0.40 | V |
| Low side residual voltage | $\mathrm{V}_{\mathrm{XL}}{ }^{2}$ | IOUT $=0.5 \mathrm{~A}$ |  | 0.25 | 0.40 | V |
| Output saturation voltage | $\mathrm{V}_{\mathrm{O}}$ (sat) | IOUT $=0.8 \mathrm{~A}$, Sink + Source |  |  | 1.4 | V |
| Overlap | O.L | $\mathrm{R}_{\mathrm{L}}=39 \Omega \times 3$, Rangle $=20 \mathrm{k} \Omega$ *2 | 72 | 80 | 87 | \% |
| High/low overlap difference | $\Delta \mathrm{O} . \mathrm{L}$ | (Average upper side overlap) (Average lower side overlap) *2 | -8 |  | +8 | \% |
| Hall Amplifiers |  |  |  |  |  |  |
| Input offset voltage | V HOFF | Design target *1 | -5 |  | +5 | mV |
| Common-mode input voltage range | $\mathrm{V}_{\text {HCM }}$ | Rangle $=20 \mathrm{k} \Omega$ | 0.95 |  | 2.1 | V |
| I/O voltage gain | $\mathrm{V}_{\mathrm{GVH}}$ | Rangle $=20 \mathrm{k} \Omega$ | 25.5 | 28.5 | 31.5 | dB |
| Standby Pin |  |  |  |  |  |  |
| High-level voltage | $\mathrm{V}_{\text {STH }}$ |  | 2.5 |  |  | V |
| Low-level voltage | $V_{\text {STL }}$ |  |  |  | 0.4 | V |
| Input current | ISTIN | $V_{\text {STBY }}=3 \mathrm{~V}$ |  | 25 | 40 | $\mu \mathrm{A}$ |
| Leakage current | ISTLK | $V_{\text {STBY }}=0 \mathrm{~V}$ |  |  | -30 | $\mu \mathrm{A}$ |
| FRC Pin |  |  |  |  |  |  |
| High-level voltage | $\mathrm{V}_{\text {FRCH }}$ |  | 2.5 |  |  | V |
| Low-level voltage | $V_{\text {FRCL }}$ |  |  |  | 0.4 | V |
| Input current | $I_{\text {FRCIN }}$ | $V_{\text {FRC }}=3 \mathrm{~V}$ |  | 25 | 30 | $\mu \mathrm{A}$ |
| Leakage current | IFRCLK | $\mathrm{V}_{\mathrm{FRC}}=0 \mathrm{~V}$ |  |  | -30 | $\mu \mathrm{A}$ |
| VH |  |  |  |  |  |  |
| Hall supply voltage | $\mathrm{V}_{\text {HALL }}$ | $\mathrm{I}_{\mathrm{H}}=5 \mathrm{~mA}, \mathrm{VH}(+)-\mathrm{VH}(-)$ | 0.85 | 0.95 | 1.05 | V |
| (-) pin voltage | $\mathrm{V}_{\mathrm{H}^{(-)}}$ | $\mathrm{I}_{\mathrm{H}}=5 \mathrm{~mA}$ | 0.81 | 0.88 | 0.95 | V |
| FG Comparator |  |  |  |  |  |  |
| Input offset voltage | $\mathrm{V}_{\text {FGOFF }}$ |  | -3 |  | +3 | mV |
| Input bias voltage | lbFG | $\mathrm{V}_{\mathrm{FGIN}}{ }^{+}=\mathrm{V}_{\mathrm{FGIN}^{-}}=1.5 \mathrm{~V}$ |  |  | 500 | nA |
| Input bias current offset | $\Delta_{\mathrm{bFG}}$ | $\mathrm{V}_{\mathrm{FGIN}}+=\mathrm{V}_{\mathrm{FGIN}^{-}}=1.5 \mathrm{~V}$ | -100 |  | +100 | nA |
| Common-mode input voltage range | $V_{\text {FGCM }}$ |  | 1.2 |  | 2.5 | V |
| Output high-level voltage | $\mathrm{V}_{\mathrm{FGOH}}$ | At the internal pull-up resistors | 2.8 |  |  | V |
| Output low-level voltage | $\mathrm{V}_{\mathrm{FGOL}}$ | At the internal pull-up resistors |  |  | 0.2 | V |
| Voltage gain | $\mathrm{V}_{\mathrm{GFG}}$ | Design target *1 |  | 100 |  | dB |
| Output current (sink) | ${ }^{\text {I FGOS }}$ | For the output pin low level |  |  | 5 | mA |
| Thermal shutdown |  |  |  |  |  |  |
| Operating temperature | TSD | Design target *1 |  | 180 |  | ${ }^{\circ} \mathrm{C}$ |
| Temperature hysteresis | $\Delta \mathrm{TSD}$ | Design target *1 |  | 20 |  | ${ }^{\circ} \mathrm{C}$ |

*1: Design target values in the conditions column are not tested.
*2: The standard for overlap is the value as measured.

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## Package Dimensions

unit : mm (typ)
3175C



## Pin Assignment



Truth Table

|  | Source phase $\rightarrow$ Sink phase |  | in |  | FRC |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | U | V | W |  |
| 1 | $V \rightarrow W$ | H | H | L | H |
|  | $\mathrm{W} \rightarrow \mathrm{V}$ |  |  |  | L |
| 2 | $\mathrm{U} \rightarrow \mathrm{W}$ | H | L | L | H |
|  | $\mathrm{W} \rightarrow \mathrm{U}$ |  |  |  | L |
| 3 | $\mathrm{U} \rightarrow \mathrm{V}$ | H | L | H | H |
|  | $\mathrm{V} \rightarrow \mathrm{U}$ |  |  |  | L |
| 4 | $\mathrm{W} \rightarrow \mathrm{V}$ | L | L | H | H |
|  | $\mathrm{V} \rightarrow \mathrm{W}$ |  |  |  | L |
| 5 | $\mathrm{W} \rightarrow \mathrm{U}$ | L | H | H | H |
|  | $\mathrm{U} \rightarrow \mathrm{W}$ |  |  |  | L |
| 6 | $V \rightarrow \mathrm{U}$ | L | H | L | H |
|  | $\mathrm{U} \rightarrow \mathrm{V}$ |  |  |  | L |

Note: The " H " entries in the FRC column indicate a voltage of 2.50 V or higher, and the " L " entries indicate a voltage of 0.4 V or lower. (When $\mathrm{V}_{\mathrm{CC}}{ }^{1}$ is 3 V .) At the Hall inputs, for each phase a high-level input is the state where the $(+)$ input is 0.02 V or higher than the $(-)$ input. Similarly, a low-level input is the state where the (+) input is 0.02 V or lower than the (-) input.

## Block Diagram



Pin Function

\begin{tabular}{|c|c|c|c|}
\hline Pin No. \& Pin name \& Pin function \& Equivalent circuit \\
\hline 1 \& \(\mathrm{V}_{\mathrm{CC}}{ }^{1}\) \& Supply voltage for all circuits other than the IC internal output block and the amplitude control block. \& \\
\hline 2 \& \(\mathrm{V}_{\mathrm{CC}}{ }^{2}\) \& Supply voltage for the IC internal output control block and the amplitude control block. \& \\
\hline 3 \& \(\mathrm{V}_{\mathrm{S}}\) \& Motor drive power supply. The voltage applied to this pin must not exceed \(\mathrm{V}_{\mathrm{CC}}{ }^{2}\). \&  \\
\hline 5 \& \& U phase output. \&  \\
\hline 7 \& \(V_{\text {OUT }}\) \& V phase output. \&  \\
\hline 9 \& WOUT \& \begin{tabular}{l}
W phase output. \\
(These outputs include built-in spark killer diodes.)
\end{tabular} \& (6) RF \\
\hline 6,8 \& RF \& Ground for the output power transistors. \& \\
\hline 10

11 \& $$
\mathrm{VH}^{+}
$$

\[
\mathrm{VH}^{-}

\] \& | Hall element bias voltage supply. |
| :--- |
| A voltage that is typically 0.95 V is generated between the $\mathrm{VH}^{+}$and $\mathrm{VH}^{-}$pins (When $\mathrm{I}_{\mathrm{H}}$ is 5 mA ). | \&  <br>


\hline 13 \& GND \& | Ground for circuits other than the output transistor. |
| :--- |
| The RF pin potential is the lowest output transistor potential. | \& <br>

\hline 14 \& FRC \& Forward/reverse selection. Applications can select motor forward or reverse direction rotation using this pin. (This pin has hysteresis characteristics.) \&  <br>

\hline 15 \& STBY \& | Selects the bias supply for all circuits other than the FG comparators. |
| :--- |
| The bias supply is cut when this pin is set to the low level. | \&  <br>

\hline $$
\begin{aligned}
& 16 \\
& 17
\end{aligned}
$$ \& \[

$$
\begin{aligned}
& \mathrm{U}_{\mathrm{IN} 1} \\
& \mathrm{U}_{\mathrm{IN}} 2
\end{aligned}
$$

\] \& | U phase Hall element input. |
| :--- |
| The logic high level is the state where the $\mathrm{IN}^{+}$voltage is greater than the $\mathrm{IN}^{-}$voltage. | \& (1) $v_{C C}{ }^{1}$ <br>

\hline $$
\begin{aligned}
& 18 \\
& 19
\end{aligned}
$$ \& \[

$$
\begin{aligned}
& \mathrm{V}_{\mathrm{IN} 1} \\
& \mathrm{~V}_{\mathrm{IN}}{ }^{2}
\end{aligned}
$$

\] \& | $V$ phase Hall element input. |
| :--- |
| The logic high level is the state where the $\mathrm{IN}^{+}$voltage is greater than the $\mathrm{IN}^{-}$voltage. | \&  <br>

\hline $$
\begin{aligned}
& 20 \\
& 21
\end{aligned}
$$ \& \[

$$
\begin{aligned}
& \mathrm{W}_{\mathrm{IN} 1} \\
& \mathrm{~W}_{\mathrm{IN} 2}{ }^{2}
\end{aligned}
$$

\] \& | W phase Hall element input. |
| :--- |
| The logic high level is the state where the $\mathrm{IN}^{+}$voltage is greater than the $\mathrm{IN}^{-}$voltage. | \&  <br>

\hline 12 \& ANGLE \& Hall input/output gain control. The gain is controlled by the resistor connected between this pin and ground. \& $\pi \pi \quad \pi \quad \pi m$ <br>
\hline 22 \& $\mathrm{FG}_{1 \mathrm{~N}^{+}}$ \& FG comparator non-inverting inputs. There is no internally applied bias. \& $\mathrm{V}_{\mathrm{CC}}{ }^{1}$ <br>

\hline 23 \& $\mathrm{FG}_{1 \mathrm{~N}^{-}}$ \& | FG comparator inverting inputs. |
| :--- |
| There is no internally applied bias. | \&  <br>


\hline 24 \& FGOUT \& | FG comparator outputs. |
| :--- |
| There is an internal $20 \mathrm{k} \Omega$ resistor load. | \&  <br>

\hline
\end{tabular}

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## Overlap Generation and Calculation Method



## Overlap Generation

Since the voltage generated in the amplitude control block is, taking the center point as the reference, $2 \times$ <overlap> $\times$ $\left(1 / 2 \mathrm{~V}_{\mathrm{S}}-\mathrm{V}_{\mathrm{X}}\right)$ on one side, the intersection point of the waveform will be <overlap> $\times\left(1 / 2 \mathrm{~V}_{\mathrm{S}}-\mathrm{VX}\right)$ from the center point.
To clamp that waveform at $\left(1 / 2 \mathrm{~V}_{\mathrm{S}}-\mathrm{V}_{\mathrm{X}}\right)$ referenced to the center point the overlap must be:
$\mathrm{A} / \mathrm{B} \times 100=$ <overlap $>\times 100(\%)$.

## Overlap Calculation

- Upper side overlap

Calculated center point: $\mathrm{V}_{\mathrm{N}}=\frac{\left(\mathrm{V}_{S}-\mathrm{V}_{X H}-\mathrm{V}_{X L}\right)}{2}+\mathrm{V}_{X L}=\frac{\left(\mathrm{V}_{S}-\mathrm{V}_{X H}+\mathrm{V}_{X L}\right)}{2}$
Since $A=V \alpha-V_{N}, B=V_{S}-V_{X H}-V_{N}$, the upper side overlap will be:
<overlap $>=\frac{\mathrm{A}}{\mathrm{B}}=\frac{\mathrm{V} \alpha-\left(\left(\mathrm{V}_{\mathrm{S}}-\mathrm{V}_{\mathrm{XH}}+\mathrm{V}_{\mathrm{XL}}\right) / 2\right)}{\mathrm{V}_{\mathrm{S}}-\mathrm{V}_{\mathrm{XH}}-\left(\left(\mathrm{V}_{\mathrm{S}}-\mathrm{V}_{\mathrm{XH}}+\mathrm{V}_{\mathrm{XL}}\right) / 2\right)} \times 100$
Which can be calculated as:

$$
=\frac{2 \mathrm{~V} \alpha-\left(\mathrm{V}_{\mathrm{S}}-\mathrm{V}_{\mathrm{XH}}\right)-\mathrm{V}_{\mathrm{XL}}}{\left(\mathrm{~V}_{\mathrm{S}}-\mathrm{V}_{\mathrm{XH}}\right)-\mathrm{V}_{\mathrm{XL}}} \times 100(\%)
$$

- Lower side overlap

Since $C=V_{N}-V \beta$, and $D=V_{N}-V_{X L}$, the lower side overlap will be:
<overlap> $=\frac{\mathrm{C}}{\mathrm{D}}=\frac{\left(\left(\mathrm{V}_{\mathrm{S}}-\mathrm{V}_{\mathrm{XH}}+\mathrm{V}_{\mathrm{XL}}\right) / 2\right)-\mathrm{V} \beta}{\left(\left(\mathrm{V}_{\mathrm{S}}-\mathrm{V}_{\mathrm{XH}}+\mathrm{V}_{\mathrm{XL}}\right) / 2\right)-\mathrm{V}_{\mathrm{XL}}} \times 100$
Which can be calculated as:

$$
=\frac{\left(\mathrm{V}_{\mathrm{S}}-\mathrm{V}_{\mathrm{XH}}\right)+\mathrm{V}_{\mathrm{XL}}-2 \mathrm{~V} \beta}{\left(\mathrm{~V}_{\mathrm{S}}-\mathrm{V}_{\mathrm{XH}}\right)-\mathrm{V}_{\mathrm{XL}}} \times 100(\%)
$$

## Test Circuit



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