

# SANYO Semiconductors **DATA SHEET**

# LB1991V — For Fan Motor 3-phase Brushless Motor Driver

#### Overview

The LB1991V is a 3-phase brushless motor driver IC that is optimal for driving the DC fan motor.

### **Functions**

- 3-phase full-wave voltage drive technique (120° voltage-linear technique)
- Torque ripple correction circuit (overlap correction)
- Speed control technique based on motor voltage and current control
- Built-in FG comparators
- Built-in thermal shutdown circuit

#### **Specifications**

**Absolute Maximum Ratings** at Ta = 25°C

Parameter	Symbol	Conditions	Ratings	Unit
Maximum supply voltage	V <sub>CC</sub> 1 max		10	V
	V <sub>CC</sub> 2 max		11	V
	V <sub>S</sub> max		11	V
Applied output voltage	V <sub>O</sub> max		V <sub>S</sub> +2	V
Maximum output current	I <sub>O</sub> max		1.0	Α
Allowable power dissipation	Pd max	Independent IC	440	mW
Operating temperature	Topr		-20 to +75	°C
Storage temperature	Tstg		-55 to +150	°C

#### Allowable Operating Ranges at Ta = 25°C

Parameter	Symbol	Conditions	Ratings	Unit
Supply voltage	V <sub>CC</sub> 1	V <sub>CC</sub> 1 ≤ V <sub>CC</sub> 2	2.7 to 6.0	٧
	V <sub>CC</sub> <sup>2</sup>		3.5 to 9.0	V
	٧s		Up to V <sub>CC</sub> 2	V
Hall input amplitude	VHALL	Between Hall effect element inputs	±20 to ±80	mVp-p

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#### **LB1991V**

# **Electrical Characteristics** at Ta = 25°C, $V_{CC}1 = 3V$ , $V_{CC}2 = 4.75V$ , $V_S = 1.5V$

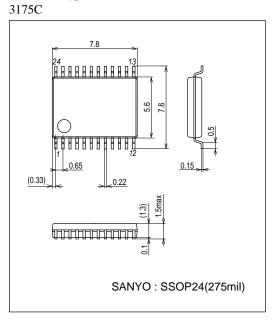
Parameter	Symbol	Conditions		Ratings			
Farameter	Symbol	Conditions	min	typ	max	Unit	
Supply Current							
V <sub>CC</sub> 1 current drain	I <sub>CC</sub> 1	I <sub>OUT</sub> = 100mA		3	5	mA	
V <sub>CC</sub> 2 current drain	I <sub>CC</sub> 2	I <sub>OUT</sub> = 100mA		7.0	10.0	mA	
V <sub>CC</sub> 1 quiescent current	I <sub>CC</sub> 1Q	V <sub>STBY</sub> = 0V		1.5	3.0	mA	
V <sub>CC</sub> 2 quiescent current	I <sub>CC</sub> 2Q	V <sub>STBY</sub> = 0V			100	μΑ	
V <sub>S</sub> quiescent current	I <sub>S</sub> Q	V <sub>STBY</sub> = 0V		75	100	μΑ	
VX1							
High side residual voltage	V <sub>XH</sub> 1	I <sub>OUT</sub> = 0.2A	0.15	0.22	0.29	V	
Low side residual voltage	V <sub>XL</sub> 1	I <sub>OUT</sub> = 0.2A	0.15	0.20	0.25	V	
VX2							
High side residual voltage	V <sub>XH</sub> 2	I <sub>OUT</sub> = 0.5A		0.25	0.40	V	
Low side residual voltage	V <sub>XL</sub> 2	I <sub>OUT</sub> = 0.5A		0.25	0.40	٧	
Output saturation voltage	V <sub>O</sub> (sat)	I <sub>OUT</sub> = 0.8A, Sink + Source			1.4	V	
Overlap	O.L	$R_L = 39\Omega \times 3$ , Rangle = $20k\Omega *2$	72	80	87	%	
High/low overlap difference	ΔΟ.L	(Average upper side overlap) – (Average lower side overlap) *2	-8		+8	%	
Hall Amplifiers				L			
Input offset voltage	VHOFF	Design target *1	-5		+5	mV	
Common-mode input voltage range	VHCM	Rangle = 20kΩ	0.95		2.1	V	
I/O voltage gain	V <sub>GVH</sub>	Rangle = 20kΩ	25.5	28.5	31.5	dB	
Standby Pin	• • • • • • • • • • • • • • • • • • • •	-	l l	ı.			
High-level voltage	V <sub>STH</sub>		2.5			V	
Low-level voltage	V <sub>STL</sub>				0.4	V	
Input current	ISTIN	V <sub>STBY</sub> = 3V		25	40	μА	
Leakage current	ISTLK	V <sub>STBY</sub> = 0V			-30	μА	
FRC Pin	OTER	1 0151				,	
High-level voltage	VFRCH		2.5			V	
Low-level voltage	VFRCL				0.4	V	
Input current	IFRCIN	VFRC = 3V		25	30	μА	
Leakage current	IFRCLK	VFRC = 0V			-30	μА	
VH	TROLK	THO					
Hall supply voltage	VHALL	I <sub>H</sub> = 5mA, VH(+) – VH(–)	0.85	0.95	1.05	V	
****			0.81	0.88	0.95	V	
(-) pin voltage   V <sub>H</sub> (-)   I <sub>H</sub> = 5mA   0.81   0.88   0.95   V <b>FG Comparator</b>						•	
Input offset voltage	V <sub>FGOFF</sub>		-3		+3	mV	
Input bias voltage	l <sub>bFG</sub>	$V_{\text{FGIN}}^+ = V_{\text{FGIN}}^- = 1.5V$			500	nA	
Input bias current offset		V <sub>FGIN</sub> <sup>+</sup> = V <sub>FGIN</sub> <sup>-</sup> = 1.5V	-100		+100	nA	
Common-mode input voltage range	∆l <sub>bFG</sub>	*FGIN = *FGIN = 1.5*	1.2		2.5	V	
Output high-level voltage	VEGCH	At the internal pull-up resistors	2.8		2.0	V	
Output high-level voltage  Output low-level voltage	VFGOH	At the internal pull-up resistors  At the internal pull-up resistors	2.0		0.2	V	
1 0	VFGOL			100	0.2	dB	
Voltage gain	VGFG	Design target *1		100	-		
Output current (sink)	IFGOS	For the output pin low level			5	mA	
Thermal shutdown	TCD	Decima toward *4	1 1	400		^^	
Operating temperature	TSD	Design target *1		180		°C	
Temperature hysteresis	ΔTSD	Design target *1		20		°C	

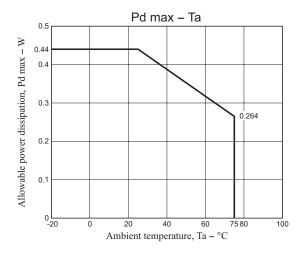
 $<sup>\</sup>ensuremath{^{\star}}\xspace$  1: Design target values in the conditions column are not tested.

 $<sup>^{*}2</sup>$ : The standard for overlap is the value as measured.

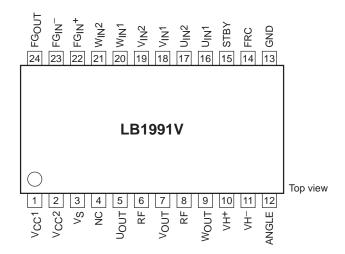
# **Package Dimensions**

unit: mm (typ)





# **Pin Assignment**

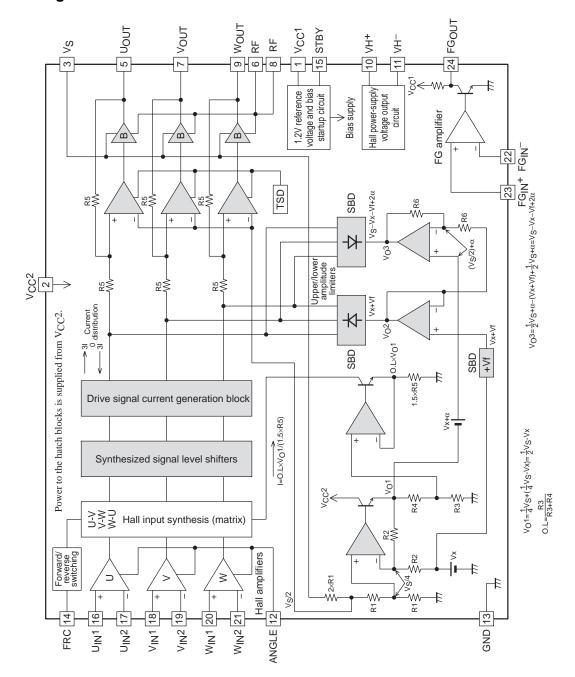


# **Truth Table**

5	Source phase → Sink phase	Hall input			- FDO
		U	V	W	FRC
	$V \rightarrow W$			٦	Н
1	$W \to V$	Н	Н		L
•	$U\toW$	Н	L	L	Н
2	$W \to U$	П			L
3	$U \to V$			н	Н
	$V \to U$	Н	L		L
4	$W \to V$	L		Н	Н
	$V \rightarrow W$	L	L		L
5	$W \to U$	L		н	Н
	$U\toW$	L	Н		L
6	$V \rightarrow U$	L	Н	L -	Н
	$U \rightarrow V$	L			L

Note: The "H" entries in the FRC column indicate a voltage of 2.50V or higher, and the "L" entries indicate a voltage of 0.4V or lower. (When V<sub>CC</sub>1 is 3V.) At the Hall inputs, for each phase a high-level input is the state where the (+) input is 0.02V or higher than the (-) input. Similarly, a low-level input is the state where the (+) input is 0.02V or lower than the (-) input.

# **Block Diagram**

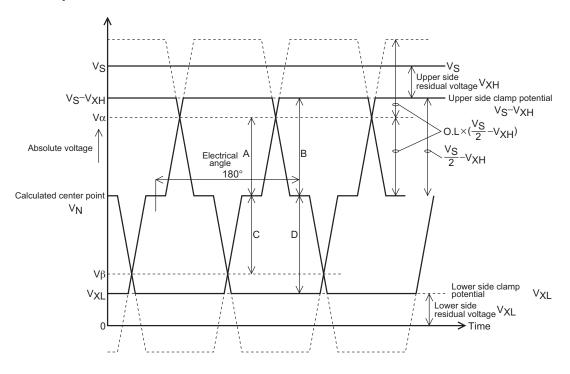


# **LB1991V**

# **Pin Function**

FIIII	unction		
Pin No.	Pin name	Pin function	Equivalent circuit
1	V <sub>CC</sub> 1	Supply voltage for all circuits other than the IC internal output block and the amplitude control block.	
2	V <sub>CC</sub> 2	Supply voltage for the IC internal output control block and the amplitude control block.	
3	٧S	Motor drive power supply. The voltage applied to this pin must not exceed V <sub>CC</sub> 2.	2 VCC <sup>2</sup> 3 Vs
5	U <sub>OUT</sub>	U phase output.	1/2/15
7	VOUT	V phase output.	$ \begin{array}{c c} 5K\Omega \geqslant \\ 1/4 \times VS \qquad $
9	W <sub>OUT</sub>	W phase output. (These outputs include built-in spark killer diodes.)	\$5kΩ (1,5) (1,6) RF
6,8	RF	Ground for the output power transistors.	(8)
10	VH+	Hall element bias voltage supply. A voltage that is typically 0.95V is generated between the VH+ and VH- pins (When I <sub>H</sub> is 5mA).	About (1) VH-
			About 1.9V VH+ S G N N N N N N N N N N N N N N N N N N
13	GND	Ground for circuits other than the output transistor.  The RF pin potential is the lowest output transistor potential.	
14	FRC	Forward/reverse selection. Applications can select motor forward or reverse direction rotation using this pin. (This pin has hysteresis characteristics.)	V <sub>CC1</sub> V <sub>CC1</sub>
15	STBY	Selects the bias supply for all circuits other than the FG comparators.  The bias supply is cut when this pin is set to the low level.	FRC 50kΩ STBY 100kΩ 15 W T T T T T T T T T T T T T T T T T T
16 17	U <sub>IN</sub> 1 U <sub>IN</sub> 2	U phase Hall element input.  The logic high level is the state where the IN+ voltage is greater than the IN- voltage.	1) Vcc1
18 19	V <sub>IN</sub> 1 V <sub>IN</sub> 2	V phase Hall element input.  The logic high level is the state where the IN <sup>+</sup> voltage is greater than the IN <sup>-</sup> voltage.	$4k\Omega \geqslant 4k\Omega \geqslant 200\Omega \qquad (18,20)$ $V_{CC1} \qquad W \qquad (16)$ $Each input of 1$
20 21	W <sub>IN</sub> 1 W <sub>IN</sub> 2	W phase Hall element input.  The logic high level is the state where the IN <sup>+</sup> voltage is greater than the IN <sup>-</sup> voltage.	ANGLE (17)
12	ANGLE	Hall input/output gain control. The gain is controlled by the resistor connected between this pin and ground.	ANGLE (I) A A A A A A A A A A A A A A A A A A A
22	FG <sub>IN</sub> +	FG comparator non-inverting inputs. There is no internally applied bias.	Vcc1
23	FG <sub>IN</sub> <sup>-</sup>	FG comparator inverting inputs. There is no internally applied bias.	FG <sub>IN</sub> - 200Ω 23 - W- 200Ω 200Ω 200Ω 400 - 20
24	FG <sub>OUT</sub>	FG comparator outputs. There is an internal $20k\Omega$ resistor load.	

# **Overlap Generation and Calculation Method**



## **Overlap Generation**

Since the voltage generated in the amplitude control block is, taking the center point as the reference,  $2 \times \text{coverlap} \times (1/2 \text{ V}_S - \text{V}_X)$  on one side, the intersection point of the waveform will be  $\text{coverlap} \times (1/2 \text{ V}_S - \text{V}_X)$  from the center point.

To clamp that waveform at  $(1/2 \text{ V}_S - \text{V}_X)$  referenced to the center point the overlap must be:  $A/B \times 100 = \text{coverlap} \times 100 \text{ (\%)}$ .

### **Overlap Calculation**

• Upper side overlap

Calculated center point: 
$$V_N = \frac{(V_S - V_{XH} - V_{XL})}{2} + V_{XL} = \frac{(V_S - V_{XH} + V_{XL})}{2}$$

Since  $A = V\alpha - V_N$ ,  $B = V_S - V_{XH} - V_N$ , the upper side overlap will be:

$$<$$
overlap $> = \frac{A}{B} = \frac{V\alpha - ((V_S - V_{XH} + V_{XL})/2)}{V_S - V_{XH} - ((V_S - V_{XH} + V_{XL})/2)} \times 100$ 

Which can be calculated as:

$$=\frac{2V\alpha-(V_{S}-V_{XH})-V_{XL}}{(V_{S}-V_{XH})-V_{XL}}\times100(\%)$$

Lower side overlap

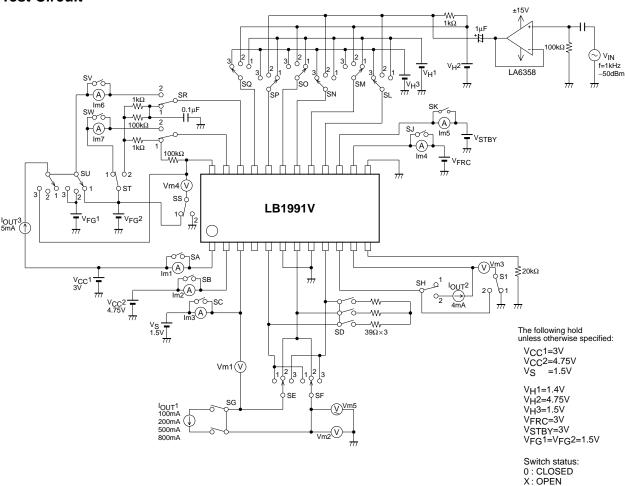
Since  $C = V_N - V\beta$ , and  $D = V_N - V_{XL}$ , the lower side overlap will be:

$$<$$
overlap $> = \frac{C}{D} = \frac{((V_S - V_{XH} + V_{XL})/2) - V_{\beta}}{((V_S - V_{XH} + V_{XL})/2) - V_{XL}} \times 100$ 

Which can be calculated as:

$$= \frac{(V_S - V_{XH}) + V_{XL} - 2V\beta}{(V_S - V_{XH}) - V_{XL}} \times 100(\%)$$

#### **Test Circuit**



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