

SANYO Semiconductors **DATA SHEET**

LB1975 — Monolithic Digital IC
For Fan Motor
3-phase Brushless Motor Driver

Overview

The LB1975 is a 3-phase brushless motor driver IC suited for use in direct PWM driving of DC fan motors for air conditioners, water heaters, and other similar equipment. Since a shunt regulator circuit is built in, single power supply operation sharing the same power supply for the motor is supported.

Features

- Withstand voltage 46V, output current 2.5A
- Direct PWM drive output
- 3 built-in output top-side diodes
- Built-in current limiter
- Built-in FG output circuit

Specifications

Absolute Maximum Ratings at Ta = 25°C

Parameter	Symbol	Conditions	Ratings	Unit
Supply voltage	V _{CC} max		7	V
	V _M max		46	V
Output current	I _O max		2.5	Α
Maximum input current	I _{REG} max	V _{REG} pin	10	mA
Allowable power dissipation	Pd max1	Independent IC	3	W
	Pd max2	With infinite hear sink	20	W
Operating temperature	Topr		-20 to +100	°C
Storage temperature	Tstg		-55 to +150	°C

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LB1975

Allowable Operating Ranges at Ta = 25°C

Parameter	Symbol	Conditions	Ratings	Unit
Supply voltage range	Vcc		4.5 to 6.7	V
	VΜ		20 to 42	V
Input current range	I _{REG}	V _{REG} pin	1 to 5	mA
FG pin applied voltage	V _{FG}		0 to V _{CC}	V
FG pin output current	I _{FG}		0 to 10	mA

Electrical Characteristics at Ta = 25 °C, $V_{CC} = 5V$, $V_{M} = 30V$

Parameter	Symbol	Conditions	Ratings			Unit
1 drameter	Cyribor		min	typ	max	Offic
Supply current	ICC		10	14	18	mA
Output Block						
Output saturation voltage	V _O sat1(L)	$I_O = 1.0A$, $V_O(sink)$		1.1	1.4	V
	V _O sat1(H)	I _O = 1.0A, V _O (source)		0.9	1.3	V
	V _O sat1	$I_O = 1.0A$, $V_O(sink) + V_O(source)$		2.0	2.6	V
	V _O sat2(L)	$I_O = 2.0A$, $V_O(sink)$		1.4	1.8	V
	V _O sat2(H)	I _O = 2.0A, V _O (source)		1.2	1.7	>
	V _O sat2	$I_O = 2.0A$, $V_O(sink) + V_O(source)$		2.6	3.4	>
Output leak current	I _O Leak(L)				100	μА
	I _O Leak(H)		-100			μΑ
Upper side diode forward voltage	V _{FH} 1	I _O = 1.0A		1.2	1.6	V
	V _{FH} 2	I _O = 2.0A		2.1	2.6	V
Hall Amplifier						
Input bias current	I _{HB}		-4	-1		μА
Common-mode input voltage range	VICM		1.5		V _{CC} -1.5	٧
Hall input sensitivity	VHIN		60			mVp-p
Hysteresis width	ΔV _{IN} (HA)		23	32	39	mV
Input voltage (low to high)	VSLH		6	16	25	mV
Input voltage (high to low)	VSHL		-25	-16	-6	mV
FG Pin (speed pulse output)			'	'		l.
Output low-level voltage	V _{FGL}	I _{FG} = 5mA			0.5	V
Pull-up resistor value	R _{FG}		7.5	10	12.5	kΩ
Current Limiter			l.			
Limiter	V _{RF}		0.45	0.50	0.55	V
Thermal Shutdown			l.			
Thermal shutdown operating temperature	TSD	Design target Value (junction temperature)	150	180		°C
Hysteresis width	ΔTSD	Design target Value (junction temperature)		40		°C
Low-Voltage Protection			I.			
Operating voltage	V _{LVSD}		3.5	3.8	4.1	V
Non-operating voltage	V _{LVSD} (OFF)			4.3	4.5	V
Hysteresis width	ΔV _{LVSD}		0.4	0.5	0.6	٧
PWM Oscillator		l	I			
Output high-level voltage	V _{OH} (OSC)		2.95	3.10	3.25	V
Output low-level voltage	V _{OL} (OSC)		1.38	1.45	1.59	V
Amplitude	Vosc		1.50	1.65	1.71	Vp-p
Oscillator frequency	fosc	C = 2200pF	19.6	23.0	27.6	kHz
Charge current	ICHG		-110	-94	-83	μА
Discharge resistance	R _{DCHG}		1.6	2.1	2.6	kΩ
V _{REG} Pin	20110	l		l		
Pin voltage	V _{REG}	I _{REG} = 1.5mA	6.6	7.0	7.2	V

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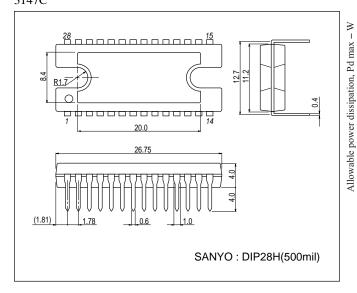
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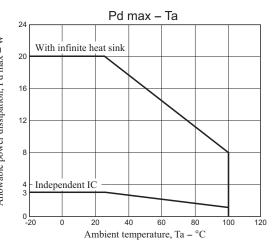
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Devenuetes	C. mah al	Conditions		Ratings			
Parameter	Symbol	Conditions	min	typ	max	Unit	
V _{CTL} Pin							
Input voltage	V _{CTL} 1	Output duty 0%	1.1	1.4	1.7	V	
	V _{CTL} ²	Output duty 100%	3.2	3.5	3.8	V	
Input bias current	I _B 1(CTL)	V _{CTL} = 0V	-82			μА	
	I _B 2(CTL)	V _{CTL} = 5V			92	μА	
V _{CTL} Amplifier							
Reference voltage	VCREF		2.23	2.35	2.46	V	
Output voltage	V _{COUT} 1	V _{CTL} = 0V	3.90	4.20	4.40	V	
	V _{COUT} 2	V _{CTL} = 5V	0.60	0.80	1.10	٧	
Start/Stop Pin							
High-level input voltage range	V _{IH} (S/S)		V _{CC} -1.5		Vcc	V	
Low-level input voltage range	V _{IL} (S/S)		0		1.5	V	
Input open voltage	V _{IO} (S/S)		V _{CC} -0.5		Vcc	V	
Hysteresis width	ΔV _{IN} (S/S)		0.35	0.50	0.65	V	
High-level input current	I _{IH} (S/S)	$V(S/S) = V_{CC}$	-10	0	+10	μА	
Low-level input current	I _{IL} (S/S)	V(S/S) = 0V	-280	-210		μА	
Forward/Reverse Pin							
High-level input voltage range	V _{IH} (F/R)		V _{CC} -1.5		Vcc	V	
Low-level input voltage range	V _{IL} (F/R)		0		1.5	V	
Input open voltage	V _{IO} (F/R)		V _{CC} -0.5		Vcc	V	
Hysteresis width	ΔV _{IN} (F/R)		0.35	0.50	0.65	V	
High-level input current	I _{IH} (F/R)	$V(F/R) = V_{CC}$	-10	0	+10	μА	
Low-level input current	I _{IL} (F/R)	V(F/R) = 0V	-280	-210		μΑ	

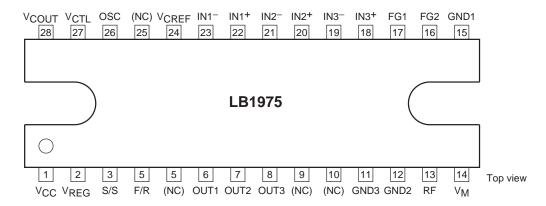
Package Dimensions

unit : mm (typ) 3147C





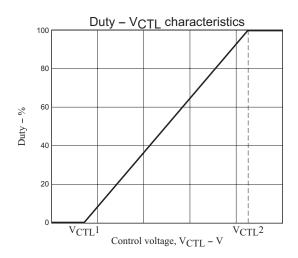
Pin Assignment



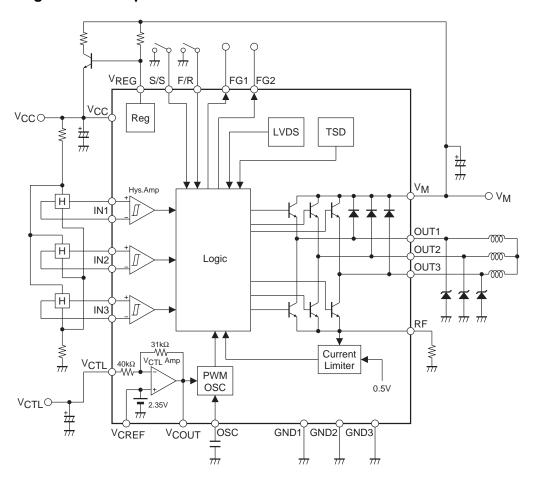
Truth Table

		Input		Forward/reverse control	Output	FG o	utput				
	IN1	IN2	IN3	F/R	$Source \to Sink$	FG1	FG2				
4		L	Н	L	OUT2 → OUT1		L				
'	Н	L	П	Н	OUT1 → OUT2		L				
2	Н	L		L	OUT3 → OUT1		Н				
2	П	L	L	Н	OUT1 → OUT3	L	П				
3	н	ш		ш	ш	н	L	L	OUT3 → OUT2		
3		П	L	Н	OUT2 → OUT3	L	L				
4	,	н	l	L	L	OUT1 → OUT2	Н	н			
4	L		L	Н	OUT2 → OUT1	П	П				
5	L	н н		L	OUT1 → OUT3	Н	_				
5			Н	OUT3 → OUT1	П	L					
6		L L H L H		L	OUT2 → OUT3	Н	Н				
0			Н	OUT3 → OUT2							





Block Diagram and Peripheral Circuit



Pin Functions

	unctions			
Pin No.	Pin name	Pin voltage	Function	Equivalent circuit
1	VCC	4.5V to 6.7V	Power supply for blocks other than the output block.	
2	VREG	0.0V to 7.3V	Shunt regulator output pin (7V).	2
3	S/S	0.0V to VCC	Start/stop control pin. Low: start High or Open: stop Typical threshold voltage for VCC = 5V: approx. 2.8V (low to high) approx. 2.3V (high to low)	V _{CC} \$20kΩ 3.8kΩ 3.8kΩ 3

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Pin No.	Pin name	Pin voltage	Function	Equivalent circuit
4	F/R	0.0V to V _{CC}	Forward/reverse pin. Low: forward High or Open: reverse Typical threshold voltage for VCC = 5V: approx. 2.8V (low to high) approx. 2.3V (high to low)	V _{CC} 20kΩ 3.8kΩ 4
6 7 8 13	OUT1 OUT2 OUT3 RF	0.0V to VCC	Output pin 1. Output pin 2. Output pin 3. Output current detect pin. Connect resistor Rf between this pin and ground. Output current is limited to value set	V _{CC} (14) (6) (7) (7)
14	V _M		with V _{RF} /Rf. (Current limiter operation) Output block power supply.	0.5V
11	GND3		Output block ground.	
15	GND3 GND1		Ground for blocks other than the output	
12	GND2		block.	
17	FG1	0.0V to V _{CC}	Speed pulse output pin 1 with built-in pull-up resistor.	V _{CC}
16	FG2	0.0V to V _{CC}	Speed pulse output pin 2 with built-in pull-up resistor.	
22	IN1+	1.5V to	Hall input pin.	Vcc
23	IN1 ⁻	V _{CC} – 1.5V	IN ⁺ > IN⁻ : High input	
20 21	IN2 ⁺		IN ⁺ < IN⁻ : Low input	* * * *
18 19	IN3+ IN3-			(18) 300Ω (19) (21) (23) (23)
26	osc	1.0V to VCC	This pin sets the PWM oscillation frequency. Connect a capacitor between this pin and ground.	VCC 2V 94μΑ 200Ω 2.1kΩ \$ 2.1kΩ \$

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Pin No.	Pin name	Pin voltage	Function	Equivalent circuit			
27	VCTL	0.0V to 6.7V	Output duty cycle control pin. • VCTL ≤ VCTL1 Duty cycle 0% • VCTL1 < VCTL < VCTL2 Duty cycle is controlled by VCTL • VCTL ≥ VCTL2 Duty cycle 100%	31kΩ W VCC 40kΩ 2.35V 40kΩ 27)			
24	VCREF	0.0V to V _{CC} – 2.0V	V _{CTL} amplifier internal reference voltage pin (2.35V).	V _{CC} 100μA 200Ω 23.5kΩ § 777 777 777 777 777 777 777 777 777 7			
28	VCOUT	0.7V to V _{CC} – 0.7V	V _{CTL} amplifier output pin.	VCC 200Ω 31kΩ W 200Ω W 7 M 7 M 7 M 7 M 7 M 7 M 7 M 7 M 7 M 7			

IC Description

1. Direct PWM Drive

The LB1975 employs the direct PWM drive principle. Motor rotation speed is controlled by varying the output duty cycle according to an analog voltage input (V_{CTL}). This eliminates the need to alter the motor power supply voltage. Compared to previous ICs using the PAM principle (such as the Sanyo LB1690), this allows simplification of the power supply circuitry. The V_{CTL} input can be directly supplied by a microcontroller, motor speed can, therefore, be controlled directly from the microcontroller.

For PWM, the source-side output transistors are switched on and off so that the ON duty tracks the V_{CTL} input. The output duty cycle can be controlled over the range of 0% to 100% by the V_{CTL} input.

2. PWM Frequency

The PWM oscillator frequency fp_{WM} [Hz] is set by the capacitance C [pF] connected between the OSC pin and GND. The following equation applies:

$$fpwm \approx 1 / (1.97 \times C) \times 10^8$$

Because output transistor on/off switching is subject to a delay, setting the PWM frequency to a very high value will cause the delay to become noticeable. The PWM frequency therefore should normally be kept below 40kHz (typ.), which is achieved with a capacitance C of 1300pF or higher. For reference, the source-side output transistor switching delay time is about 2µs for ON and about 4µs for OFF.

3. Output Diodes

Because the PWM switching operation is carried out by the source-side output transistors, Schottky barrier diodes must be connected between the OUT pins and GND (OUT1 to OUT3). Use diodes with an average forward current rating in the range of 1.0 to 2.0A, in accordance with the motor type and current limiting requirements.

If no Schottky barrier diodes are connected externally, or if Schottky barrier diodes with high forward voltage (V_F) are used, the internal parasitic diode between OUT and GND becomes active. When this happens, the output logic circuit may malfunction, resulting in feed-through current in the output which can destroy the output transistors. To prevent this possibility, Schottky barrier diodes must be used and dimensioned properly.

The larger the V_F of the externally connected Schottky barrier diodes, or the hotter the IC is, the more likely are the parasitic diodes between OUT and GND to become active and the more likely is malfunction to occur. The V_F of the Schottky barrier diodes must be determined so that output malfunction does not occur also when the IC becomes hot. If malfunction occurs, choose a Schottky barrier diode with lower V_F .

4. Protection circuits

4-1. Low voltage protection circuit

When the V_{CC} voltage falls below a stipulated level (V_{LVSD}), the low voltage protection circuit cuts off the source-side output transistors to prevent V_{CC} related malfunction.

4-2. Thermal shutdown circuit (overheat protection circuit)

When the junction temperature rises above a stipulated value (TSD), the thermal shutdown circuit cuts off the sourceside output transistors to prevent IC damage due to overheating. Design the application heat characteristics so that the protection circuit will not be triggered under normal circumstances.

4-3. Current limiter

The current limiter cuts off the source-side output transistors when the output current reaches a preset value (limiter value). This interrupts the source current and thereby limits the output current peak value. By connecting the resistance Rf between the RF pin and ground, the output current can be detected as a voltage. When the RF pin voltage reaches 0.5V (typ.), the current limiter is activated. It performs on/off control of the source-side output transistors, thereby limiting the output current to the value determined by 0.5/Rf.

5. Hall Input Circuit

The Hall input circuit is a differential amplifier with a hysteresis of 32mV (typ.). The operation DC level must be within the common-mode input voltage range (1.5V to $V_{CC}-1.5V$). To prevent noise and other adverse influences, the input level should be at least 3 times the hysteresis (120 to $16mV_{p-p}$). If noise at the Hall input is a problem, a noise-canceling capacitor (about $0.01\mu F$) should be connected across the Hall input IN⁺ and IN⁻ pins.

6. FG Output Circuit

The Hall input signal at IN1, IN2, and IN3 is combined and subject to waveform shaping before being output. The signal at FG1 has the same frequency as the FG1 Hall input, and the signal at FG2 has a frequency that is three times higher.

7. Start/Stop Control Circuit

The start/stop control circuit turns the source-side output transistors OFF (motor stop) when a High signal is input at the S/S pin or when the pin is Open. When a Low signal is input at the S/S pin, the source-side output transistors are turned ON, and the normal operation state is established (motor start).

8. Forward/Reverse Switching

The LB1975 is designed under the assumption that forward/reverse switching is not carried out while the motor is running. If switching is carried out while the motor is running, reverse torque braking occurs, leading to a high current flow. If the current limiter is triggered, the source-side output transistors are switched off, and the sink-side output transistors go into the short brake condition. However, because the current limiter of this IC cannot control the current flowing in the sink-side output transistors, these may be destroyed by the short brake current. Therefore F/R switching while the motor is running is permissible only if the output current (I_O) is limited to a maximum of 2.5A using the motor coil resistance or other suitable means.

F/R switching should be carried out only while a High signal is input to the S/S pin or the pin is Open (stop condition), or while the VCTL pin conforms to the following condition: $V_{CTL} \le V_{CTL} 1$ (duty cycle 0%). In any other condition, F/R switching will result in feed-through current. The F/R pin should therefore be fixed to Low (forward) or High or Open (reverse) during use.

9. VCC, VM Power Supplies

When the power supply voltage (V_{CC} , V_{M}) rises very quickly when a power is first applied, a feed-through current may occur at the output. If the current remains below about 0.2A to 0.3A, it does not pose a problem, but such a possibility should still be prevented by slowing down the voltage rise at power-on. Especially if the F/R pin is set to High or Open (reverse), a quick rise in V_{CC} is likely to cause feed-through current. This should be prevented by ensuring that ΔV_{CC} / $\Delta t = 0.2V/\mu s$ or less. Feed-through current can also be prevented by first switching on V_{CC} and then V_{M} during power-on.

The sequence at power-down should be as follows. Provide a stop input to the S/S pin or a duty ratio 0% input to the V_{CTL} pin. When the motor has come to a full stop, switch off V_{M} and then V_{CC} . If power is switched off while the motor is still rotating or a current is flowing in the motor coil (including motor restraint or inertia rotation), a counter electromotive current or kickback current may flow on the V_{M} side, depending on the motor type and power-off procedure. If this current cannot be absorbed by the V_{M} power supply or a capacitor, V_{M} voltage may rise and exceed the absolute maximum V_{M} rating for the IC. Ensure that this does not happen through proper design of the V_{M} power supply or through use of a capacitor.

Because the LB1975 incorporates a shunt regulator, it can be used on a single power supply. In this case, supply V_{CC} (6.3V typ.) to the V_{REG} pin via an external NPN transistor and resistor. When not using the regulator, leave the V_{REG} pin open.

10. Power Supply Stabilizing Capacitors

If the V_{CC} line fluctuates drastically, the low-voltage protection circuit may be activated by mistake, or other malfunctions may occur. The V_{CC} line must therefore be stabilized by connecting a capacitor of at least several μF between V_{CC} and GND. Because a large switching current flows in the V_M line, wiring inductance and other factors can lead to V_M voltage fluctuations. As the GND line also fluctuates, the V_M line must be stabilized by connecting a capacitor of at least several μF between V_M and GND, to prevent exceeding V_M max or other problems. Especially when long wiring runs (V_M , V_{CC} , GND) are used, sufficient capacitance should be provided to ensure power supply stability.

11. VCREF Pin, VCOUT Pin

These pins are always used in the Open condition. If chattering occurs in the PWM switching output, connect a capacitor (about $0.1\mu F$) between V_{CREF} and ground or between V_{COUT} and GND.

12. IC Heat Dissipation Fins

A heat sink may be mounted to the heat dissipation fins of this IC, but it may not be connected to GND. The sink should be electrically open.

13. Sample calculation for internal power dissipation (approximate)

The calculation assumes the following parameters:

 $V_{CC} = 5V$

 $V_{\mathbf{M}} = 30V$

Source-side output transistor ON duty cycle 80% (PWM control)

Output current $I_O = 1A$ (RF pin average current)

(1) ICC power dissipation P1

$$P1 = V_{CC} \times I_{CC} = 5V \times 14mA = 0.07W$$

(2) Output drive current power dissipation P2

$$P2 = V_M \times 11mA = 30V \times 11mA = 0.33W$$

(3) Source-side output transistor power dissipation P3

$$P3 = V_O(source) \times I_O \times Duty(on) = 0.9V \times 1A \times 0.8 = 0.72W$$

(4) Sink-side output transistor power dissipation P4

$$P4 = V_O(\sin k) \times I_O = 1.1V \times 1A = 1.10W$$

(5) Total internal power dissipation P

$$P = P1 + P2 + P3 + P4 = 2.22W$$

14. IC temperature Rise Measurement

Because the chip temperature of the IC cannot be measured directly, measurement according to one of the following procedures should always be carried out.

14-1. Thermocouple measurement

A thermocouple element is mounted to the IC heat dissipation fin. This measurement method is easy to implement, but it will be subject to measurement errors if the temperature is not stable.

14-2. Measurement using internal diode characteristics of IC

This is the recommended measurement method. It makes use of the parasitic diode incorporated in the IC between FG1 and GND. Set FG1 to High and measure the voltage V_F of the parasitic diode to calculate the temperature. (Sanyo data: for $I_F = -1$ mA, V_F temperature characteristics are about -2mV/ $^{\circ}$ C)

15. NC Pins

Because NC pins are electrically open, they may be used for wiring purpose etc.

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