## -Description

BD9524MUV is a switching regulator controller with high output current which can achieve low output voltage ( $2.0 \mathrm{~V} \sim 5.5 \mathrm{~V}$ ) from a wide input voltage range ( $7 \mathrm{~V} \sim 25 \mathrm{~V}$ ). High efficiency for the switching regulator can be realized by utilizing an external N-MOSFET power transistor. A new technology called $\mathrm{H}^{3} \mathrm{Reg}^{\top \mathrm{TM}}$ is a Rohm proprietary control method to realize ultra high transient response against load change. SLLM (Simple Light Load Mode) technology is also integrated to improve efficiency in light load mode, providing high efficiency over a wide load range. For protection and ease of use, the soft start function, variable frequency function, short circuit protection function with timer latch, over voltage protection with timer latch, and Power good function are all built in. This switching regulator is specially designed for Main Power Supply.

## - Features

1) $2 \mathrm{ch} \mathrm{H}^{3} \mathrm{Reg}^{\mathrm{TM}}$ Switching Regulator Controller
2) Adjustable Simple Light Load Mode (SLLM), Quiet Light Load Mode (QLLM) and Forced continuous Mode
3) Thermal Shut Down (TSD), Under Voltage LockOut (UVLO), Over Current Protection (OCP), Over Voltage Protection (OVP), Short circuit protection with timer-latch (SCP)
4) Soft start function to minimize rush current during startup
5) Switching Frequency Variable ( $\mathrm{f}=200 \mathrm{KHz} \sim 500 \mathrm{KHz}$ )
6) Power good circuit
7) 2ch Linear regulator
8) VQFN032V5050 package
-Applications
Laptop PC, Desktop PC, LCD-TV, Digital Components

- Maximum Absolute Ratings ( $\mathrm{Ta}=25^{\circ} \mathrm{C}$ )

| Parameter | Symbol | Limits | Unit |
| :---: | :---: | :---: | :---: |
| Terminal voltage | VIN, CTL | $30{ }^{* *}{ }^{*}$ | V |
|  | EXTVCC, PGOOD1, PGOOD2FB1, FB2, Is+1, Is+2, MCTL | $7^{* *}{ }^{*}$ | V |
|  | FS1, FS2, REF1, REF2, SS1, SS2, LG1, LG2 | REG1+0.3 ${ }^{* 1^{*} 2}$ | V |
|  | BOOT1, BOOT2 | $35^{* 1_{1}{ }^{2}}$ | V |
|  | BOOT1-SW1, BOOT2-SW2, HG1-SW1, HG2-SW2 | $7^{* 1^{*}}$ | V |
|  | HG1 | BOOT1+0.3 ${ }^{* *}{ }^{*}$ | V |
|  | HG2 | BOOT2+0.3 ${ }^{* *^{*} 2}$ | V |
|  | EN1, EN2 | 6 1*2 | V |
|  | DGND, PGND1, PGND2 | AGND $\pm 0.3{ }^{* * 2}$ | V |
| Power dissipation 1 | Pd1 | $0.38{ }^{* 3}$ | W |
| Power dissipation 2 | Pd2 | $0.88{ }^{* 4}$ | W |
| Power dissipation 3 | Pd3 | $2.06{ }^{* 5}$ | W |
| Power dissipation 4 | Pd4 | 4.56 * 6 | W |
| Operating temperature range | Topr | -10~+100 | ${ }^{\circ} \mathrm{C}$ |
| Storage temperature range | Tstg | $-55 \sim+150$ | ${ }^{\circ} \mathrm{C}$ |
| Junction Temperature | Tjmax | +150 | ${ }^{\circ} \mathrm{C}$ |

*1 Do not however exceed Pd.
*2 Instantaneous surge voltage, back electromotive force and voltage under less than $10 \%$ duty cycle.
*3 Reduced by 3.0 mW for each increase in Ta of $1^{\circ} \mathrm{C}$ over $25^{\circ} \mathrm{C}$ (when don't mounted on a heat radiation board)
${ }^{*} 4$ Reduced by 7.0 mW for increase in Ta of $1^{\circ} \mathrm{C}$ over $25^{\circ} \mathrm{C}$. (when mounted on a board $70.0 \mathrm{~mm} \times 70 \mathrm{~mm} \times 1.6 \mathrm{~mm}$ Glass-epoxy PCB which has 1 layer. (Copper foil area: $0 \mathrm{~mm}^{2}$ ))
*5 Reduced by 16.5 mW for increase in Ta of $1^{\circ} \mathrm{C}$ over $25^{\circ} \mathrm{C}$. (when mounted on a board $70.0 \mathrm{~mm} \times 70 \mathrm{~mm} \times 1.6 \mathrm{~mm}$ Glass-epoxy PCB which has 4 layers. ( $1^{\text {st }}$ and $4^{\text {th }}$ copper foil area : $20.2 \mathrm{~mm}^{2}, 2^{\text {nd }}$ and $3^{\text {rd }}$ copper foil area : $5505 \mathrm{~mm}^{2}$ ))
*6 Reduced by 36.5 mW for increase in Ta of $1^{\circ} \mathrm{C}$ over $25^{\circ} \mathrm{C}$. (when mounted on a board $70.0 \mathrm{~mm} \times 70 \mathrm{~mm} \times 1.6 \mathrm{~mm}$ Glass-epoxy PCB which has 4 layers. (All copper foil area : $5505 \mathrm{~mm}^{2}$ ))

- Operating Conditions $\left(\mathrm{Ta}=25^{\circ} \mathrm{C}\right)$

| Parameter | Symbol | MIN. | MAX. | Unit |
| :---: | :---: | :---: | :---: | :---: |
| Terminal voltage | VIN | 7 | 25 | V |
|  | EXTVCC | 4.5 | 5.5 | V |
|  | CTL | -0.3 | 25 | V |
|  | EN1, EN2 | -0.3 | 5.5 | V |
|  | BOOT1, BOOT2 | 4.5 | 30 | V |
|  | BOOT1-SW1, BOOT2-SW2, HG1-SW1, HG2-SW2 | -0.3 | 5.5 | V |
|  | PGOOD1, PGOOD2 | -0.3 | 5.5 | V |
|  | FS1, FS2 | 0.09 | 1.25 | V |
|  | REF1, REF2 | 1 | 2.75 | V |
|  | Is+1, Is+2, FB1, FB2 | 1.9 | 5.6 | V |
|  | MCTL | -0.3 | REG1+0.3 | V |

*This product should not be used in a radioactive environment.

- Electrical characteristics
(unless otherwise noted, $\mathrm{Ta}=25^{\circ} \mathrm{C} \mathrm{VIN}=12 \mathrm{~V}, \mathrm{CTL}=5 \mathrm{~V}, \mathrm{EN} 1=\mathrm{EN} 2=5 \mathrm{~V}, \mathrm{REF} 1=2.5 \mathrm{~V}, \mathrm{REF} 2=1.65 \mathrm{~V}, \mathrm{FS} 1=\mathrm{FS} 2=0.582 \mathrm{~V}$ )

| Parameter | Symbol | Standard Value |  |  | Unit | Conditions |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN. | TYP. | MAX. |  |  |
| VIN standby current | ISTB | 70 | 150 | 250 | $\mu \mathrm{A}$ | CTL=5V, EN1 $=\mathrm{EN} 2=0 \mathrm{~V}$ |
| VIN bias current | IIN | 0 | 45 | 130 | $\mu \mathrm{A}$ | EXTVCC=5V |
| Shut down mode current | ISHD | -10 | 0 | 10 | $\mu \mathrm{A}$ | $\mathrm{CTL}=0 \mathrm{~V}$ |
| CTL Low voltage | VCTLL | -0.3 | - | 0.8 | V |  |
| CTL High voltage | VCTLH | 2.3 | - | 25 | V |  |
| CTL bias current | ICTL | - | 1 | 3 | $\mu \mathrm{A}$ | $\mathrm{VCTL}=5 \mathrm{~V}$ |
| EN Low voltage | VENL | -0.3 | - | 0.8 | V |  |
| EN High voltage | VENH | 2.3 | - | 5.5 | V |  |
| EN bias current | IEN | - | 1 | 3 | $\mu \mathrm{A}$ | $\mathrm{VEN}=3 \mathrm{~V}$ |
| [5V linear regulator] |  |  |  |  |  |  |
| REG1 output voltage | VREG1 | 4.90 | 5.00 | 5.10 | V | IREG1=1mA |
| Maximum current | IREG1 | 200 | - | - | mA | IREG2=0mA |
| Line Regulation | REG1I | - | 90 | 180 | mV | VIN=7.5 to 25 V |
| Load Regulation | REG1L | - | 30 | 50 | mV | IREG1=0 to 30mA |
| [3.3V linear regulator] |  |  |  |  |  |  |
| REG2 output voltage | VREG2 | 3.27 | 3.30 | 3.33 | V | IREG2=1mA |
| Maximum current | IREG2 | 100 | - | - | mA |  |
| Line regulation | REG2I | - | - | 20 | mV | VIN=7.5 to 25 V |
| Load regulation | REG2L | - | - | 30 | mV | IREG2=0 to 100mA |

[5V switch block]

| EXTVCC input threshold voltage | VCC_UVLO | 4.2 | 4.4 | 4.6 | V | EXTVCC: Sweep up |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| EXTVCC input delay time | TVCC | 2 | 4 | 8 | ms |  |
| Switch Resistance | RVCC |  | 1.0 | 2.0 | $\Omega$ |  |

[Under voltage lock out block for DC/DC]

| REG1 threshold voltage | REG1_UVLO | 4.0 | 4.2 | 4.4 | V | REG1: Sweep up |
| :--- | :---: | :---: | :---: | :---: | :---: | :--- |
| REG2 threshold voltage | REG2_UVLO | 2.45 | 2.65 | 2.85 | V | REG2: Sweep up |
| Hysteresis voltage | dV_UVLO | 50 | 100 | 200 | mV | REG1, REG2: Sweep down |

[Error amplifier block]

| Feed back voltage 1 | VFB1 | REF1 $\times 2$ <br> -25 m | REF1 $\times 2$ | REF1 $\times 2$ <br> +25 m | V |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| FB1 bias current | IFB1 | 20 | 45 | 90 | $\mu \mathrm{~A}$ | FB1 $=5 \mathrm{~V}$ |
| Output discharge resistance 1 | RDISOUT1 | 0.5 | 1 | 3 | $\mathrm{k} \Omega$ |  |
| Feed back voltage 2 | VFB2 | REF2 $\times 2$ <br> -25 m | REF2 $\times 2$ | REF2 $\times 2$ <br> +25 m | V |  |
| FB2 bias current | IFB2 | 10 | 30 | 60 | $\mu \mathrm{~A}$ | FB2=3.3V |
| Output discharge resistance 2 | RDISOUT2 | 0.5 | 1 | 3 | $\mathrm{k} \Omega$ |  |
| REF1, REF2 bias current | IREF1, IREF2 | -10 | - | 10 | $\mu \mathrm{~A}$ |  |

- Electrical characteristics - Continued
(unless otherwise noted, $\mathrm{Ta}=25^{\circ} \mathrm{C}$ VIN=12V, CTL=5V, EN1 $=\mathrm{EN} 2=5 \mathrm{~V}, \mathrm{REF} 1=2.5 \mathrm{~V}$, REF2 $=1.65 \mathrm{~V}, \mathrm{FS} 1=\mathrm{FS} 2=0.582 \mathrm{~V}$ )

| Parameter | Symbol | Standard Value |  |  | Unit | Conditions |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN. | TYP. | MAX. |  |  |
| [ $\mathrm{H}^{3} \mathrm{Reg}^{\text {TM }}$ block] |  |  |  |  |  |  |
| On Time 1 | TON1 | 0.810 | 0.960 | 1.110 | $\mu \mathrm{s}$ | REF=2.5V |
| On Time 2 | TON2 | 0.520 | 0.670 | 0.820 | $\mu \mathrm{s}$ | REF=1.65V |
| Maximum On Time | TONMAX | 3.5 | 7 | 14 | $\mu \mathrm{s}$ |  |
| Minimum Off Time | TOFFMIN | - | 0.2 | 0.4 | $\mu \mathrm{s}$ |  |
| FS1, FS2 bias current | IFS | -10 | 0 | 10 | $\mu \mathrm{A}$ |  |
| [FET driver block] |  |  |  |  |  |  |
| HG higher side ON resistor | HGHON | - | 3.0 | 6.0 | $\Omega$ |  |
| HG lower side ON resistor | HGLON | - | 2.0 | 4.0 | $\Omega$ |  |
| LG higher side ON resistor | LGHON | - | 2.0 | 4.0 | $\Omega$ |  |
| LG lower side ON resistor | LGLON | - | 0.5 | 1.0 | $\Omega$ |  |

## [Over Voltage Protection block]

| Latch Type OVP Threshold voltage | VLOVP | REF $\times 2$ <br> $\times 1.15$ | REF $\times 2$ <br> $\times 1.175$ | REF $\times 2$ <br> $\times 1.20$ | V |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| Latch Type OVP delay time | TLOVP | 50 | 150 | 300 | $\mu \mathrm{~s}$ |  |

[Short circuit protection block]

| SCP Threshold voltage | VSCP | REF $\times 2 \times$ <br> 0.66 | REF $\times 2$ <br> $\times 0.7$ | REF $\times 2$ <br> $\times 0.74$ | V |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Delay time | TSCP | 0.5 | 1 | 2 | ms |

[Current limit protection block]

| Maximum offset voltage | dVSMAX | 50 | 65 | 80 | mV |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Is +1 bias current | IISP1 | - | 2.5 | 10 | $\mu \mathrm{~A}$ |  |
| Is +2 bias current | IISP2 | - | 2.5 | 10 | $\mu \mathrm{~A}$ |  |

[Power good block]

| Power good low threshold | VPGTHL | $\mathrm{REF} \times 2$ <br> $\times 0.87$ | $\mathrm{REF} \times 2$ <br> $\times 0.90$ | $\mathrm{REF} \times 2$ <br> $\times 0.93$ | V |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Power good high threshold | VPGTHH | $\mathrm{REF} \times 2$ <br> $\times 1.07$ | $\mathrm{REF} \times 2$ <br> $\times 1.10$ | $\mathrm{REF} \times 2$ <br> $\times 1.13$ | V |  |
| Power good low voltage | VPGL | - | 0.1 | 0.2 | V | IPGOOD $=1 \mathrm{~mA}$ |
| Power good leakage current | ILEAKPG | -2 | 0 | 2 | $\mu \mathrm{~A}$ | VPGOOD $=5 \mathrm{~V}$ |

## [Soft Start block]

| Charge current | ISS | 1.8 | 2.5 | 3.2 | $\mu \mathrm{~A}$ |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Standby voltage | VSS_STB | - | - | 50 | mV |  |

[SLLM mode control block]

| MCTL terminal voltage 1 | VCONT | -0.3 | - | 0.3 | V | Continuous mode |
| :--- | :---: | :---: | :---: | :---: | :---: | :--- |
| MCTL terminal voltage 2 | VQLLM | 1.5 | - | 3.0 | V | QL' <br> $($ Maximum LG off time $: 50 \mu \mathrm{~s})$ |
| MCTL terminal voltage 3 | VSLLM | 4.5 | - | REG1+0.3 | V | SL <br> $\left(L^{2} \mathrm{M}\right.$ mode <br> (Maximum LG off time $: \infty)$ |
| MCTL float level | VMCTL | 1.5 | - | 3.0 | V |  |

Output condition table

| Input |  |  | Output |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CTL | EN1 | EN2 | REG1 5 V$)$ | REG2 $(3.3 V)$ | DC/DC1 | DC/DC2 |
| Low | Low | Low | OFF | OFF | OFF | OFF |
| Low | Low | High | OFF | OFF | OFF | OFF |
| Low | High | Low | OFF | OFF | OFF | OFF |
| Low | High | High | OFF | OFF | OFF | OFF |
| High | Low | Low | ON | ON | OFF | OFF |
| High | Low | High | ON | ON | OFF | ON |
| High | High | Low | ON | ON | ON | OFF |
| High | High | High | ON | ON | ON | ON |


*Apply the supply voltage EXTVCC pin after REG1 pin is operated.

- Pin Configuration

- Pin Function Table

| PIN No. | PIN name | PIN Function |
| :---: | :---: | :---: |
| 1 | SW2 | Highside FET source pin 2 |
| 2 | HG2 | Highside FET gate drive pin 2 |
| 3 | BOOT2 | HG Driver power supply pin 2 |
| 4 | EN2 | Vo2 ON/OFF pin (High=ON, Low=OFF) |
| 5 | PGOOD2 | Vo2 Power Good Open Drain Output pin |
| 6 | SS2 | Vo2 soft start pin |
| 7 | DGND | Ground |
| 8 | REF2 | Vo2 output voltage setting pin |
| 9 | Is+2 | Current sense pin +2 |
| 10 | FB2 | Vo2 output voltage sense pin, current sense pin -2 |
| 11 | FS2 | Input pin for setting Vo2 frequency |
| 12 | MCTL | Mode shift pin (Low=continuous, Middle=QLLM, High=SLLM) |
| 13 | AGND | Input pin Ground |
| 14 | FS1 | Input pin for setting Vo1 frequency |
| 15 | FB1 | Vo2 output voltage sense pin, current sense pin -1 |
| 16 | Is+1 | Current sense pin +1 |
| 17 | REF1 | Vo1 output voltage setting pin |
| 18 | CTL | Linear regulator ON/OFF pin (High=ON, Low=OFF) |
| 19 | SS1 | Vo1 soft start pin |
| 20 | PGOOD1 | Vo1 Power Good Open Drain Output pin |
| 21 | EN1 | Vo1 ON/OFF pin (High=ON, Low=OFF) |
| 22 | BOOT1 | HG Driver power supply pin 1 |
| 23 | HG1 | Highside FET gate drive pin 1 |
| 24 | SW1 | Highside FET source pin 1 |
| 25 | PGND1 | Lowside FET source pin 1 |
| 26 | LG1 | Lowside FET gate drive pin 1 |
| 27 | EXTVCC | Outside power supply input pin |
| 28 | REG2 | 3.3 V linear regulator output pin |
| 29 | REG1 | 5 V linear regulator output pin |
| 30 | VIN | Power supply input pin |
| 31 | LG2 | Lowside FET gate drive pin 2 |
| 32 | PGND2 | Lowside FET source pin 2 |
| Reverse | FIN | Exposed Pad, Connect to GND |

## - Reference data



Fig. 1 wake up (Vo=5.0V)


Fig. 2 wake up (Vo=3.3V)


Fig. 3 wake up (REG1, REG2)


Fig. 4 CONT Mode ( $\mathrm{Io}=0 \mathrm{~A}$ )


Fig. 5 CONT Mode ( $\mathrm{lo}=0.4 \mathrm{~A}$ )


Fig. 6 CONT Mode ( $\mathrm{Io}=1.4 \mathrm{~A}$ )


Fig. 7 QLLM $(\mathrm{lo}=0 \mathrm{~A})$


Fig. 8 QLLM ( $\mathrm{Io}=0.4 \mathrm{~A}$ )


Fig. 9 QLLM ( $\mathrm{lo}=1.4 \mathrm{~A}$ )


Fig. 10 SLLM ( $\mathrm{Io}=0 \mathrm{~A}$ )


Fig. 11 SLLM ( $\mathrm{Io}=0.4 \mathrm{~A}$ )


Fig. 12 SLLM ( $\mathrm{lo}=1.4 \mathrm{~A}$ )

## - Reference data



Fig. 13 FS-ON TIME


Fig. 15 lo-frequency (Vo1=5.0V)

Fig. 16 Io-efficiency (VIN=12V, Vo1=5.0V)


边


Fig. 14 FS-freqency

Fig. 17 VIN-Ivin (Io=0A, Vo1=5.0V)

- VIN

This is the main power supply pin. The input supply voltage range is 7 V to 25 V . The duty cycle of BD9524MUV is determined by input voltage and control output voltage. Therefore, when VIN voltage fluctuated, the output voltage also becomes unstable. Since VIN line is also the input voltage of switching regulator, stability depends on the impedance of the voltage supply. It is recommended to establish bypass capacitor and CR filter suitable for the actual application.

- CTL

When CTL pin voltage is at least 2.3 V the status of the linear regulator output becomes active ( $\mathrm{REG1}=5 \mathrm{~V}, \mathrm{REG2}=3.3 \mathrm{~V}$ ). Conversely, the status switches off when CTL pin voltage goes lower than 0.8 V . The switching regulator doesn't become active when the status of CTL pin is low, if the status of EN pin is high.

- EN

When EN pin voltage is at least 2.3 V , the status of the switching regulator becomes active. Conversely, the status switches off when EN pin voltage goes lower than 0.8 V .

- REG1

This is the output pin for 5 V linear regulator and also active in power supply for driver and control circuit of the inside. The standby function for REG1 is determined by CTL pin. The voltage is 5 V , with 100 mA current ability. It is recommended that a 10uF capacitor (X5R or X7R) be established between REG1 and GND.

- REG2

This is the output pin for 3.3 V linear regulator. The standby function for REG2 is determined by CTL. The voltage is 3.3 V , with 100 mA current ability. It is recommended that a 10 uF capacitor (X5R or X7R) be established between REG2 and GND. It is available to set REF and SS by the resistance division value from REG2 in case REF are not set from an external power supply.

- EXTVCC

This is the external input pin to REG1. When EXTVCC is beyond 4.4V, it supplies REG1 as EXTVCC is the power supply.

- REF

This is the setting pin for output voltage of switching regulator. It is so convenient to be synchronized to outside power supply.
This IC controls the voltage in the status of $2 \times R E F \fallingdotseq F B$.

- FB

This is the feedback pin from the output of switching regulator. This IC controls the voltage in the status of $2 \times$ REF $\doteqdot$ FB.

- SS

This is the setting pin for soft start. The rising time is determined by the capacitor connected between SS and GND, and the fixed current inside IC after it is the status of low in standby mode. It controls the output voltage till SS voltage catch up the REF pin to become the double of the SS terminal voltage.

- FS

This is the input pin for setting the frequency. It is available to set it in frequency range is 200 KHz to 500 kHz .

- Is+

This is the sense pin for output current. In case it is connected to side of the coil resistance for sense current and the voltage is set $65 \mathrm{mV}(\mathrm{typ})$ or more higher than FB pin voltage, the switching operation turns OFF.

- PGOOD

This is the open drain pin for deciding the output of switching regulator.

- MCTL

This is the switching shift pin for SLLM (Simple Light Load Mode). The efficiency in SLLM mode improves in setting MCTL pin to 1.5 V or more. In case MCTL terminal voltage range is from 1.5 to 3.0 V , LG maximum OFF time is 40 usec, from 4.5 V to REG1 +0.3 V , LG maximum OFF time is to infinity. It is in continuous mode that MCTL pin voltage is set 0.3 V or less.

- AGND,DGND

This is the ground pin.

- BOOT

This is the power supply pin for high side FET driver. The maximum voltage range to GND pin is to 35 V , to SW pin is to 7 V . In switching operations, the voltage swings from (VIN+REG1) to REG1 by BOOT pin operation.

- HG

This is the highside FET gate drive pin. It is operated in switching between BOOT to SW. In case the output MOS is 3ohm /the status of Hi , 2ohm/the status of Low, it is operated hi-side FET gate in high speed.

- SW

This is the ground pin for high side FET drive. The maximum voltage range to GND pin is to 30 V . Switching operation swings from the status of BOOT to the status of GND.

- LG

This is the lowside FET gate drive pin. It is operated in switching between REG1 to PGND. In case the output MOS is 2ohm /the status of $\mathrm{Hi}, 0.50 \mathrm{hm} /$ the status of Low, it is operated low-side FET gate in high speed.

- PGND

This is the ground pin for low side FET drive.

- Explanation of Operation

The BD9524MUV is a 2 ch synchronous buck regulator controller incorporating ROHM's proprietary $\mathrm{H}^{3} \mathrm{Reg}^{\text {TM }}$ CONTROLLA control system. When VOUT drops due to a rapid load change, the system quickly restores VOUT by extending the TON time interval. Thus, it serves to improve the regulator's transient response. Activating the Light Load Mode will also exercise Simple Light Load Mode (SLLM) control when the load is light, to further increase efficiency.
$H^{3} \mathrm{Reg}^{\mathrm{TM}}$ control
(Normal operation)


When VOUT falls to a reference voltage ( $2 \times$ REF), the drop is detected, activating the $\mathrm{H}^{3} \mathrm{Reg}^{\text {TM }}$ CONTROLLA system.

$$
\text { ton }=\frac{2 \times R E F}{V I N} \times \frac{1}{f}[\mathrm{sec}] \cdot \cdots(1)
$$

HG output is determined by the formula above.
(VOUT drops due to a rapid load change)


When Vout drops due to a rapid load change, and the voltage remains below reference voltage after the programmed ton time interval has elapsed, the system quickly restores Vout by extending the ton time, improving the transient response.

Light Load Control
(SLLM)


In SLLM (MCTL="High voltage"), when the status of LG is OFF and the coil current is within OA (it flows to SW from VOUT.), SLLM function is operated to prevent output next HG. The status of HG is ON, when VOUT falls below reference voltage again.

In QLLM (MCTL="Hiz or Middle voltage"), when the status of LG is OFF and the coil current is within OA (it flows to SW from VOUT.), QLLM function is operated to prevent output next HG.
Then, VOUT falls below the output programmed voltage within the programmed time (typ $=40 \mu \mathrm{~s}$ ), the status of HG is ON. In case VOUT doesn't fall in the programmed time, the status of LG is ON forcedly and VOUT falls. As a result, he status of next HG is ON.
*Attention: $\mathrm{H}^{3} \mathrm{Reg}^{\text {TM }}$ CONTROLLA monitors the supplying current from capacitor to load, using the ESR of output capacitor, and realize the rapid response. Bpass capacitor used at each load (Ex. Ceramic capacitor) exercise the effect with connecting to each load side. Do not put a ceramic capacitor on Cout side of power supply.


Timing Chart

- Soft Start Function

- Timer Latch Type Short Circuit Protection

- Over Voltage Protection

- Over current protection circuit


Soft start is exercised with the EN pin set high. Current control takes effect at startup, enabling a moderate output voltage "ramping start." Soft start timing and incoming current are calculated with formulas (2) and (3) below.

Soft start time

$$
\text { Tss }=\frac{R E F \times \text { Css }}{2 \mu \mathrm{~A}(\mathrm{typ})}[\mathrm{sec}] \cdots(2)
$$

Incoming current

$$
\mathrm{IIN}=\frac{\mathrm{Co} \times \text { Vout }}{\text { Tss }}
$$

[A]
(Css: Soft start capacitor; Co: Output capacitor)

Short protection kicks in when output falls to or below REF $\times 1.4$ (setting voltage $\times 0.7$ ).
When the programmed time period elapses, output is latched OFF to prevent destruction of the IC. Output voltage can be restored either by reconnecting the EN pin or disabling UVLO.

When output rise to or above REF $\times 2.35$ (output setting voltage $\times 1.175$ ), output over voltage protection is exercised, and low side FET goes up maximum for reducing output. (LG=High, HG=Low). When output falls within the programmed time (typ=150 $\mu$ s), it returns to the standard mode. When the programmed time period elapses, output is latched OFF to prevent destruction of the IC. Output voltage can be restored either by reconnecting the EN pin or disabling UVLO.

During the normal operation, when VOUT becomes less than reference voltage, HG becomes High during the time tON. However, when inductor current exceeds ILIMIT threshold, HG becomes OFF.
After $2.5 \mu \mathrm{sec}($ typ $)$, HG becomes ON again if the output voltage is lower than the specific voltage level and IL is lower than ILIMIT level.

## - External Component Selection

1. Inductor (L) selection


The inductor value is a major influence on the output ripple current. As formula (4) below indicates, the greater the inductor or the switching frequency, the lower the ripple current.

$$
\Delta I L=\frac{(\text { VIN-VOUT }) \times \text { VoUT }}{L \times \operatorname{VIN} \times f}[A] \cdot \cdots(4)
$$

The proper output ripple current setting is about $30 \%$ of maximum output current.

$$
\begin{aligned}
\Delta \mathrm{IL}= & 0.3 \times \text { Ioutmax. }[\mathrm{A}] \cdot \cdots(5) \\
\mathrm{L} & =\frac{(\text { VIN-VouT }) \times \text { Vout }}{\Delta \mathrm{IL} \times \operatorname{VIN} \times f}[\mathrm{H}] \cdot(6)
\end{aligned}
$$

( $\Delta \mathrm{IL}$ : output ripple current; f: switch frequency)
※Passing a current larger than the inductor's rated current will cause magnetic saturation in the inductor and decrease system efficiency. In selecting the inductor, be sure to allow enough margin to assure that peak current does not exceed the inductor rated current value.
※To minimize possible inductor damage and maximize efficiency, choose a inductor with a low (DCR, ACR) resistance.

## 2.Output Capacitor (Co) Selection



Output Capacitor

When determining the proper output capacitor, be sure to factor in the equivalent series resistance required to smooth out ripple volume and maintain a stable output voltage range.
Output ripple voltage is determined as in formula (7) below.
$\Delta$ Vout $=\Delta$ IL $\times$ ESR [V] • • • (7)
( $\Delta \mathrm{IL}$ : Output ripple current; ESR: Co equivalent series resistance)
※ In selecting a capacitor, make sure the capacitor rating allows sufficient margin relative to output voltage. Note that a lower ESR can minimize output ripple voltage.

Please give due consideration to the conditions in formula (8) below for output capacity, bear in mind that output rise time must be established within the soft start time frame.

$$
\text { Co+CEXT } \leqq \frac{\text { Tss } \times(\text { Limit-lout })}{\text { Vout }} \cdots \cdot(8)
$$

Tss: Soft start time
Limit: Over current detection 2A(Typ)

Note: Improper capacitor may cause startup malfunctions.

## 3. Input Capacitor (Cin) Selection



Input Capacitor

The input capacitor selected must have low enough ESR resistance to fully support large ripple output, in order to prevent extreme over current. The formula for ripple current IRMS is given in (9) below.

IRMS $=$ Iout $\times \frac{\sqrt{\operatorname{VIN}(\mathrm{VIN}-\mathrm{VoUT})}}{\operatorname{VIN}} \quad[\mathrm{A}] \cdots \cdot(9)$
Where VIN $=2 \times$ Vout, IRMS $=\frac{\text { IOUT }}{2}$

A low ESR capacitor is recommended to reduce ESR loss and maximize efficiency.
4. MOSFET Selection


Loss on the main MOSFET
Pmain=Pron+Pgate+Ptran
$=\frac{\text { VOUT }}{\text { VIN }} \times$ RON $\times$ IOUT $^{2}+$ Ciss $\times f \times$ VDD $+\frac{\text { VIN }^{2} \times \text { Crss } \times \text { IOUT } \times f}{\text { IDRIVE }} \cdots($
(Ron: On-resistance of FET; Ciss: FET gate capacitance;
f: Switching frequency Crss: FET inverse transfer function; IDRIVE: Gate peak current)

Loss on the synchronous MOSFET
Psyn=Pron+Pgate
$=\frac{\text { VIN-VOUT }}{\text { VIN }} \times$ RON $\times$ IOUT $^{2}+$ Ciss $\times f \times$ VDD $\cdots(11)$
5. Setting Detection Resistance (Detect ILIMIT at the peak current)
(A) High accuracy current detective circuit (use the low resistance)


The over current protection function detects the output ripple current peak value. This parameter (setting value) is determined as in formula (13) below.

ILMIT $=\frac{65 \mathrm{mV} \text { (typ) }}{\mathrm{R}}[\mathrm{A}] \cdots(12)$
(R: Detection resistance)
(B) Low loss current detective circuit (use the DCR value of inductor)


When the over current protection is detected by DCR of inductor $L$, this parameter (setting value) is determined as in formula (13) below.
(Application circuit:P18)
ILMIT $=65 \mathrm{mV}(\mathrm{typ}) \times \frac{\mathrm{r} \times \mathrm{C}}{\mathrm{L}}[\mathrm{A}] \cdot \cdots(13)$
$\left(R L=\frac{L}{r \times C}\right)$
(RL: the DCR value of inductor)
(C) Low loss current detective circuit (the DCR value of inductor : high)

6. Setting standard voltage (REF)


It is available to set the reference voltage (REF) with outside supply voltage $\times 2$ [V] by using outside power supply voltage.


It is available to set the reference voltage (REF) by the resistance division value from REG2 in case REF is not set from an external power supply.

$$
R E F=\frac{R 2}{R 1+R 2} \times R E G 2[V] \cdot \cdots(15)
$$

## 7. Setting output voltage

This IC is operated that output voltage is REF $\times 2 \fallingdotseq \mathrm{FB}$. And it is operated that output voltage is feed back to FB pin.


## -I/O Equivalent Circuit



## - I/O Equivalent Circuit



## - Evaluation Board Circuit (Vo1=5V f1 $=300 \mathrm{kHz}$ Vo2 $=3.3 \mathrm{~V}$ f2 $=400 \mathrm{kHz}$ )



| DESIGNATION | RATING | PART No. | COMPANY |
| :---: | :---: | :---: | :---: |
| R1 | $0 \Omega$ | MCR03EZHJ000 | ROHM |
| R2 | $0 \Omega$ | MCR03EZHJO00 | ROHM |
| R3 | $0 \Omega$ | MCR03EZHJ000 | ROHM |
| R4 | $0 \Omega$ | MCR03EZHJ000 | ROHM |
| R5 | $0 \Omega$ | MCR03EZHJ000 | ROHM |
| R6 | $15 \mathrm{k} \Omega$ | MCR03PZHZF1502 | ROHM |
| R7 | 47k $\Omega$ | MCR03PZHZF4702 | ROHM |
| R8 | 30 k ת | MCR03PZHZF3002 | ROHM |
| R9 | 30k $\Omega$ | MCR03PZHZF3002 | ROHM |
| R10* | - | - | - |
| R11 * | - | - | - |
| R12 | - | - | - |
| R13 | 1M $\Omega$ | MCR03PZHZF1004 | ROHM |
| R14 | $51 \mathrm{k} \Omega$ | MCR03PZHZF5102 | ROHM |
| R15* | - | - | - |
| R16 | - | - | - |
| R17 | 36kת | MCR03PZHZF3602 | ROHM |
| R18* | - | - | - |
| R19* | - | - | - |
| R20 | 100k $\Omega$ | MCR03PZHZF1003 | ROHM |
| R21 | $0 \Omega$ | MCR03EZHJ000 | ROHM |
| R22 * | - | - | - |
| R24 | $0 \Omega$ | MCR03EZHJ000 | ROHM |
| R25 | $0 \Omega$ | MCR03EZHJO00 | ROHM |
| R26 * | - | - | - |
| R27* | - | - | - |
| R28 | $0 \Omega$ | MCR03EZHJ000 | ROHM |
| R29 | $0 \Omega$ | MCR03EZHJ000 | ROHM |
| R30 | $0 \Omega$ | MCR03EZHJ000 | ROHM |
| R31 * | - | - | - |
| R32 | $0 \Omega$ | MCR03EZHJO00 | ROHM |
| R33 | $5 \mathrm{~m} \Omega$ | PMR100HZPFU5L00 | ROHM |
| R34 | $0 \Omega$ | MCR03EZHJO00 | ROHM |
| R35 | $0 \Omega$ | MCR03EZHJO00 | ROHM |
| R36 | 100k $\Omega$ | MCR03PZHZF1003 | ROHM |
| R37 | $0 \Omega$ | MCR03EZHJO00 | ROHM |
| R39 | $0 \Omega$ | MCR03EZHJ000 | ROHM |
| R40 | $0 \Omega$ | MCR03EZHJ000 | ROHM |
| R41* | - | - | - |
| R42* | - | - | - |
| R43 | $0 \Omega$ | MCR03EZHJ000 | ROHM |
| R44 | $0 \Omega$ | MCR03EZHJ000 | ROHM |
| R45* | - | - | - |
| R46 | $0 \Omega$ | MCR03EZHJ000 | ROHM |
| R47 | $0 \Omega$ | MCR03EZHJ000 | ROHM |
| R48 | $5 \mathrm{~m} \Omega$ | PMR100HZPFU5L00 | ROHM |
| R49 | $0 \Omega$ | MCR03EZHJ000 | ROHM |
| R50 | $0 \Omega$ | MCR03EZHJ000 | ROHM |
| R52 | - | - | - |
| R54 | - | - | - |
| R55 | - | - | - |
| R56 | - | - | - |
| R57 | - | - | - |


| DESIGNATION | RATING | PART No. | COMPANY |
| :---: | :---: | :---: | :---: |
| R58 | $1 \mathrm{M} \Omega$ | MCR03PZHZF1004 | ROHM |
| R63 | - | - | - |
| C1 | 10uF(25V) | CM32X7R106M25A | KYOCERA |
| C2 | 10uF(6.3V) | GRM21BB10J106KD | MURATA |
| C3 | 10uF(6.3V) | GRM21BB10J106KD | MURATA |
| C4 | 10uF(6.3V) | GRM21BB10J106KD | MURATA |
| C5 | $0.01 \mathrm{uF}(50 \mathrm{~V})$ | GRM188B11H103KD | MURATA |
| C6 | $0.01 \mathrm{uF}(50 \mathrm{~V})$ | GRM188B11H103KD | MURATA |
| C7 | 1000pF(50 V) | GRM188B11H102KD | MURATA |
| C8 | 1000pF(50V) | GRM188B11H102KD | MURATA |
| C9 | - | - | - |
| C10 | - | - | - |
| C11 | 220uF | 6TPE220MI | SANYO |
| C12 | - | - | - |
| C13* | - | - | - |
| C14 | $0.47 \mathrm{uF}(10 \mathrm{~V})$ | GRM188B11A474KD | MURATA |
| C15 | 10uF(25V) | CM32XR7106M25A | KYOCERA |
| C16 | 10uF(25V) | CM32XR7106M25A | KYOCERA |
| C17 | 10uF(6.3V) | GRM21BB10J106KD | MURATA |
| C18 | - | - | - |
| C19 | - | - | - |
| C20 | - | - | - |
| C21 | 220uF | 6TPE220MI | SANYO |
| C22 | - | - | - |
| C23* | - | - | - |
| C24 | $0.47 \mathrm{uF}(10 \mathrm{~V})$ | GRM188B11A474KD | MURATA |
| C25 | 10uF(25V) | CM32XR7106M25A | KYOCERA |
| C26 | 10uF(25V) | CM32XR7106M25A | KYOCERA |
| C27 | 10uF(6.3V) | GRM21BB10J106KD | MURATA |
| C28 | - | - | - |
| C29 | - | - | - |
| C30 | - | - | - |
| C31 | - | - | - |
| C32 | - | - | - |
| C33 | - | - | - |
| C34* | - | - | - |
| C35* | - | - | - |
| C36 * | - | - | - |
| C37* | - | - | - |
| D1 | Diode | RSX501L-20 | ROHM |
| D2 | Diode | RSX501L-20 | ROHM |
| D3 | Diode | RB520S-30 | ROHM |
| D4 | Diode | RB520S-30 | ROHM |
| L1 | 2.5uH | CDEP105NP-2R5MC- $32$ | Sumida |
| L2 | 2.5uH | CDEP105NP-2R5MC- $32$ | Sumida |
| Q1 | FET | uPA2702 | NEC |
| Q2 | FET | uPA2702 | NEC |
| Q3 | FET | uPA2702 | NEC |
| Q4 | FET | uPA2702 | NEC |
| Q5 | - | - | - |
| Q6 | - | - | - |
| U1 | - | BD9524MUV | ROHM |

* Patterns for over current detection used DCR.
- Handling method of unused pin during using only 1ch DC/DC.

If using only 1 ch DC/DC and 2ch pin is set to be off at all times, please manage the unused pin as diagram below.

| PIN No, | PIN Name | Management |
| :---: | :---: | :---: |
| 1 | SW2 | GND |
| 2 | HG2 | OPEN |
| 3 | BOOT2 | GND |
| 4 | EN2 | GND |
| 5 | PGOOD2 | GND |
| 6 | SS2 | GND |
| 8 | REF2 | GND |
| 9 | Is+2 | GND |
| 10 | FB2 | GND |
| 11 | FS2 | GND |
| 31 | LG2 | OPEN |



- Notes for use

1. This integrated circuit is a monolithic IC, which (as shown in the figure below), has $P$ isolation in the $P$ substrate and between the various pins. A P-N junction is formed from this P layer and N layer of each pin, with the type of junction depending on the relation between each potential, as follows:

- When GND> element $A>$ element $B$, the $P-N$ junction is a diode.
- When element $\mathrm{B}>G \mathrm{GN}$ element A , the $\mathrm{P}-\mathrm{N}$ junction operates as a parasitic transistor.

Parasitic diodes inevitably occur in the structure of the IC. The operation of parasitic diodes can result in mutual interference among circuits, as well as operating malfunctions and physical damage. Therefore, be careful to avoid methods by which parasitic diodes operate, such as applying a voltage lower than the GND ( P substrate) voltage to an input pin.

2. In some modes of operation, power supply voltage and pin voltage are reversed, giving rise to possible internal circuit damage. For example, when the external capacitor is charged, the electric charge can cause a VCC short circuit to the GND. In order to avoid these problems, inserting a VCC series countercurrent prevention diode or bypass diode between the various pins and the VCC is recommended.

3. Absolute maximum rating

Although the quality of this IC is rigorously controlled, the IC may be destroyed when applied voltage or operating temperature exceeds its absolute maximum rating. Because short mode or open mode cannot be specified when the IC is destroyed, it is important to take physical safety measures such as fusing if a special mode in excess of absolute rating limits is to be implemented.
4.GND potential Make sure the potential for the GND pin is always kept lower than the potentials of all other pins, regardless of the operating mode.
5. Thermal design

In order to build sufficient margin into the thermal design, give proper consideration to the allowable loss (Power Dissipation) in actual operation.
6. Short-circuits between pins and incorrect mounting position

When mounting the IC onto the circuit board, be extremely careful about the orientation and position of the IC. The IC may be destroyed if it is incorrectly positioned for mounting. Do not short-circuit between any output pin and supply pin or ground, or between the output pins themselves. Accidental attachment of small objects on these pins will cause shorts and may damage the IC.
7. Operation in strong electromagnetic fields

Use in strong electromagnetic fields may cause malfunctions. Use extreme caution with electromagnetic fields.
8. Thermal shutdown circuit

This IC is provided with a built-in thermal shutdown (TSD) circuit, which is activated when the operating temperature reaches $175^{\circ} \mathrm{C}$ (standard value), and has a hysteresis range of $15^{\circ} \mathrm{C}$ (standard). When the IC chip temperature rises to the threshold, all the inputs automatically turn OFF. Note that the TSD circuit is provided for the exclusive purpose shutting down the IC in the presence of extreme heat, and is not designed to protect the IC per se or guarantee performance when or after extreme heat conditions occur. Therefore, do not operate the IC with the expectation of continued use or subsequent operation once the TSD is activated.
9. Capacitor between output and GND

When a larger capacitor is connected between the output and GND, Vcc or VIN shorted with the GND or OV line - for any reason - may cause the charged capacitor current to flow to the output, possibly destroying the IC. Do not connect a capacitor larger than 1000uF between the output and GND.
10. Precautions for board inspection

Connecting low-impedance capacitors to run inspections with the board may produce stress on the IC. Therefore, be certain to use proper discharge procedure before each process of the operation. To prevent electrostatic accumulation and discharge in the assembly process, thoroughly ground yourself and any equipment that could sustain ESD damage, and continue observing ESD-prevention procedures in all handling, transfer and storage operations. Before attempting to connect components to the test setup, make certain that the power supply is OFF. Likewise, be sure the power supply is OFF before removing any component connected to the test setup.
11. GND wiring pattern

When both a small-signal GND and high current GND are present, single-point grounding (at the set standard point) is recommended, in order to separate the small-signal and high current patterns, and to be sure the voltage change stemming from the wiring resistance and high current does not cause any voltage change in the small-signal GND. In the same way, care must be taken to avoid wiring pattern fluctuations in any connected external component GND.
-Power Dissipation


- Ordering part number


Part No.


Part No.



Packaging and forming specification E2: Embossed tape and reel

## VQFN032V5050



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