May 1999

### LMC6462 Dual/LMC6464 Quad Micropower, Rail-to-Rail Input and Output CMOS Operational Amplifier

### **General Description**

The LMC6462/4 is a micropower version of the popular LMC6482/4, combining Rail-to-Rail Input and Output Range with very low power consumption.

The LMC6462/4 provides an input common-mode voltage range that exceeds both rails. The rail-to-rail output swing of the amplifier, guaranteed for loads down to 25 k $\Omega$ , assures maximum dynamic sigal range. This rail-to-rail performance of the amplifier, combined with its high voltage gain makes it unique among rail-to-rail amplifiers. The LMC6462/4 is an excellent upgrade for circuits using limited common-mode range amplifiers.

The LMC6462/4, with guaranteed specifications at 3V and 5V, is especially well-suited for low voltage applications. A quiescent power consumption of 60  $\mu W$  per amplifier (at  $V_{\rm S}=3V)$  can extend the useful life of battery operated systems. The amplifier's 150 fA input current, low offset voltage of 0.25 mV, and 85 dB CMRR maintain accuracy in battery-powered systems.

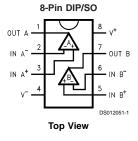
### **Features**

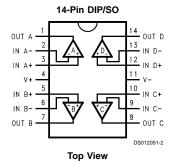
(Typical unless otherwise noted)

- Ultra Low Supply Current 20 µA/Amplifier
- Guaranteed Characteristics at 3V and 5V
- Rail-to-Rail Input Common-Mode Voltage Range
- Rail-to-Rail Output Swing (within 10 mV of rail,  $V_S = 5V$  and  $R_L = 25 \text{ k}\Omega$ )
- Low Input Current 150 fA
- Low Input Offset Voltage 0.25 mV

### **Applications**

- Battery Operated Circuits
- Transducer Interface Circuits
- Portable Communication Devices
- Medical Applications
- Battery Monitoring





Package	Temp	Temperature Range				
	Military	Industrial	Drawing	Media		
	-55°C to +125°C	-40°C to +85°C				
8-Pin Molded DIP	LMC6462AMN	LMC6462AIN, LMC6462BIN	N08E	Rails		
8-Pin SO-8		LMC6462AIM, LMC6462BIM	M08A	Rails		
		LMC6462AIMX, LMC6462BIMX	M08A	Tape and Ree		
14-Pin Molded DIP	LMC6464AMN	LMC6464AIN, LMC6464BIN	N14A	Rails		
14-Pin SO-14		LMC6464AIM, LMC6464BIM	M14A	Rails		
		LMC6464AIMX, LMC6464BIMX	M14A	Tape and Ree		
8-Pin Ceramic DIP	LMC6462AMJ-QML		J08A	Rails		
14-Pin Ceramic DIP	LMC6464AMJ-QML		J14A	Rails		
14-Pin Ceramic SOIC	LMC6464AMWG-QML		WG14A	Trays		

### **Absolute Maximum Ratings** (Note 1)

If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/ Distributors for availability and specifications.

ESD Tolerance (Note 2) 2.0 kV Differential Input Voltage ±Supply Voltage Voltage at Input/Output Pin  $(V^{+}) + 0.3V, (V^{-}) - 0.3V$ Supply Voltage (V<sup>+</sup> – V<sup>-</sup>) 16V Current at Input Pin (Note 12) ±5 mA

Current at Output Pin (Notes 3, 8)

±30 mA Current at Power Supply Pin Lead Temp. (Soldering, 10 sec.) -65°C to +150°C Storage Temperature Range

Junction Temperature (Note 4)

40 mA 260°C

150°C

# **Operating Ratings** (Note 1)

Supply Voltage  $3.0V \le V^+ \le 15.5V$ 

Junction Temperature Range

LMC6462AM, LMC6464AM  $-55^{\circ}C \le T_{J} \le +125^{\circ}C$ LMC6462AI, LMC6464AI  $-40^{\circ}\text{C} \le \text{T}_{\text{J}} \le +85^{\circ}\text{C}$ LMC6462BI, LMC6464BI  $-40^{\circ}\text{C} \le \text{T}_{\text{J}} \le +85^{\circ}\text{C}$ 

Thermal Resistance ( $\theta_{JA}$ )

N Package, 8-Pin Molded DIP 115°C/W 193°C/W M Package, 8-Pin Surface Mount N Package, 14-Pin Molded DIP 81°C/W

M Package, 14-Pin

Surface Mount 126°C/W

### **5V DC Electrical Characteristics**

Unless otherwise specified, all limits guaranteed for  $T_J = 25^{\circ}C$ ,  $V^+ = 5V$ ,  $V^- = 0V$ ,  $V_{CM} = V_O = V^+/2$  and  $R_L > 1M$ . **Boldface** limits apply at the temperature extremes.

				LMC6462AI	LMC6462BI	LMC6462AM	
Symbol	Parameter	Conditions	Тур	LMC6464AI	LMC6464BI	LMC6464AM	Units
			(Note 5)	Limit	Limit	Limit	
				(Note 6)	(Note 6)	(Note 6)	
Vos	Input Offset Voltage		0.25	0.5	3.0	0.5	mV
				1.2	3.7	1.5	max
TCVos	Input Offset Voltage		1.5				μV/°C
	Average Drift						
I <sub>B</sub>	Input Current	(Note 13)	0.15	10	10	200	pA max
Ios	Input Offset Current	(Note 13)	0.075	5	5	100	pA max
C <sub>IN</sub>	Common-Mode		3				pF
	Input Capacitance						
R <sub>IN</sub>	Input Resistance		>10				Tera Ω
CMRR	Common Mode	$0V \le V_{CM} \le 15.0V$ ,	85	70	65	70	dB
	Rejection Ratio	V+ = 15V		67	62	65	min
		$0V \le V_{CM} \le 5.0V$	85	70	65	70	]
		V+ = 5V		67	62	65	
+PSRR	Positive Power Supply	5V ≤ V <sup>+</sup> ≤ 15V,	85	70	65	70	dB
	Rejection Ratio	$V^{-} = 0V, V_{O} = 2.5V$		67	62	65	min
-PSRR	Negative Power Supply	$-5V \le V^- \le -15V$ ,	85	70	65	70	dB
	Rejection Ratio	$V^{+} = 0V, V_{O} = -2.5V$		67	62	65	min
V <sub>CM</sub>	Input Common-Mode	V+ = 5V	-0.2	-0.10	-0.10	-0.10	V
	Voltage Range	For CMRR ≥ 50 dB		0.00	0.00	0.00	max
			5.30	5.25	5.25	5.25	V
				5.00	5.00	5.00	min
		V+ = 15V	-0.2	-0.15	-0.15	-0.15	V
		For CMRR ≥ 50 dB		0.00	0.00	0.00	max
			15.30	15.25	15.25	15.25	V
				15.00	15.00	15.00	min

### **5V DC Electrical Characteristics** (Continued)

Unless otherwise specified, all limits guaranteed for  $T_J$  = 25°C,  $V^+$  = 5V,  $V^-$  = 0V,  $V_{CM}$  =  $V_O$  = V+/2 and  $R_L$  > 1M. **Boldface** limits apply at the temperature extremes.

Symbol A <sub>V</sub>	Parameter  Large Signal	Conditions $R_{L} = 100 \text{ k}\Omega \qquad \text{Sourcing}$		<b>Typ</b> (Note 5)	LMC6462AI LMC6464AI Limit (Note 6)	LMC6464BI LMC6464BI Limit (Note 6)	LMC6462AM LMC6464AM Limit (Note 6)	Units V/mV
	Voltage Gain	(Note 7)						min
			Sinking	400				V/mV
								min
		$R_L = 25 \text{ k}\Omega$	Sourcing	2500				V/mV
		(Note 7)						min
			Sinking	200				V/mV
								min
Vo	Output Swing	V+ = 5V		4.995	4.990	4.950	4.990	V
		$R_L = 100 \text{ k}\Omega \text{ to}$	o V+/2		4.980	4.925	4.970	min
				0.005	0.010	0.050	0.010	V
					0.020	0.075	0.030	max
		V <sup>+</sup> = 5V		4.990	4.975	4.950	4.975	V
		$R_L = 25 \text{ k}\Omega \text{ to}$	$R_L = 25 \text{ k}\Omega \text{ to V}^+/2$		4.965	4.850	4.955	min
				0.010	0.020	0.050	0.020	V
					0.035	0.150	0.045	max
		V+ = 15V		14.990	14.975	14.950	14.975	V
		$R_L = 100 \text{ k}\Omega \text{ to}$	) V+/2		14.965	14.925	14.955	min
				0.010	0.025	0.050	0.025	V
					0.035	0.075	0.050	max
		V+ = 15V		14.965	14.900	14.850	14.900	V
		$R_L = 25 \text{ k}\Omega \text{ to}$	V+/2	0.025	14.850	14.800	14.800	min
					0.050	0.100	0.050	V
				27	0.150	0.200	0.200	max
$I_{SC}$	Output Short Circuit	Sourcing, V <sub>O</sub> =	Sourcing, V <sub>O</sub> = 0V		19	19	19	mA
	Current				15	15	15	min
	V+ = 5V	Sinking, V <sub>O</sub> =	5V	27	22	22	22	mA
				38	17	17	17	min
I <sub>SC</sub>	Output Short Circuit	Sourcing, V <sub>O</sub> =	Sourcing, V <sub>O</sub> = 0V		24	24	24	mA
	Current				17	17	17	min
	V <sup>+</sup> = 15V	Sinking, V <sub>O</sub> =	12V	75	55	55	55	mA
		(Note 8)	_		45	45	45	min
Is	Supply Current	Dual, LMC6462		40	55	55	55 	μA
		$V^{+} = +5V, V_{O}$			70	70	75	max
		Quad, LMC646		80	110	110	110	μΑ
		$V^{+} = +5V, V_{O}$		50	140	140	150	max
		Dual, LMC6462		50	60	60	60	μΑ
		$V^{+} = +15V, V_{C}$			70	70	75	max
		Quad, LMC646		90	120	120	120	μΑ
		$V^{+} = +15V, V_{C}$	, = V <sup>+</sup> /2		140	140	150	max

### **5V AC Electrical Characteristics**

Unless otherwise specified, all limits guaranteed for  $T_J$  = 25°C,  $V^+$  = 5V,  $V^-$  = 0V,  $V_{CM}$  =  $V_O$  = V+/2 and  $R_L$  > 1M. **Boldface** limits apply at the temperature extremes.

				LMC6462AI	LMC6462BI	LMC6462AM	
Symbol	Parameter	Conditions	Тур	LMC6464AI	LMC6464BI	LMC6464AM	Units
			(Note 5)	Limit	Limit	Limit	
				(Note 6)	(Note 6)	(Note 6)	
SR	Slew Rate	(Note 9)	28	15	15	15	V/ms
				8	8	8	min
GBW	Gain-Bandwidth Product	V+ = 15V	50				kHz
φ <sub>m</sub>	Phase Margin		50				Deg
G <sub>m</sub>	Gain Margin		15				dB
	Amp-to-Amp Isolation	(Note 10)	130				dB
e <sub>n</sub>	Input-Referred	f = 1 kHz	80				nV/√ <del>Hz</del>
	Voltage Noise	V <sub>CM</sub> = 1V					, ,,,,
i <sub>n</sub>	Input-Referred	f = 1 kHz	0.03				pA/√Hz
	Current Noise						F: :: V

**3V DC Electrical Characteristics**Unless otherwise specified, all limits guaranteed for  $T_J = 25^{\circ}C$ ,  $V^+ = 3V$ ,  $V^- = 0V$ ,  $V_{CM} = V_O = V^+/2$  and  $R_L > 1M$ . Boldface limits apply at the temperature extremes.

				LMC6462AI	LMC6462BI	LMC6462AM	
Symbol	Parameter	Conditions	Тур	LMC6464AI	LMC6464BI	LMC6464AM	Units
			(Note 5)	Limit	Limit	Limit	
				(Note 6)	(Note 6)	(Note 6)	
Vos	Input Offset Voltage		0.9	2.0	3.0	2.0	mV
				2.7	3.7	3.0	max
TCVos	Input Offset Voltage		2.0				μV/°C
	Average Drift						
I <sub>B</sub>	Input Current	(Note 13)	0.15	10	10	200	pА
I <sub>os</sub>	Input Offset Current	(Note 13)	0.075	5	5	100	pА
CMRR	Common Mode	0V ≤ V <sub>CM</sub> ≤ 3V	74	60	60	60	dB
	Rejection Ratio						min
PSRR	Power Supply	3V ≤ V <sup>+</sup> ≤ 15V, V <sup>-</sup> = 0V	80	60	60	60	dB
	Rejection Ratio						min
V <sub>CM</sub>	Input Common-Mode	For CMRR ≥ 50 dB	-0.10	0.0	0.0	0.0	V
	Voltage Range						max
			3.0	3.0	3.0	3.0	V
							min
Vo	Output Swing	$R_L = 25 \text{ k}\Omega \text{ to V}^{+}/2$	2.95	2.9	2.9	2.9	V
							min
			0.15	0.1	0.1	0.1	V
							max
Is	Supply Current	Dual, LMC6462	40	55	55	55	μA
		$V_{O} = V^{+}/2$		70	70	70	
		Quad, LMC6464	80	110	110	110	μA
		$V_{O} = V^{+}/2$		140	140	140	max

### **3V AC Electrical Characteristics**

Unless otherwise specified,  $V^+ = 3V$ ,  $V^- = 0V$ ,  $V_{CM} = V_O = V^+/2$  and  $R_L > 1M$ . Boldface limits apply at the temperature extremes.

				LMC6462AI	LMC6462BI	LMC6462AM	
Symbol	Parameter	Conditions	Тур	LMC6464AI	LMC6464BI	LMC6464AM	Units
			(Note 5)	Limit	Limit	Limit	
				(Note 6)	(Note 6)	(Note 6)	
SR	Slew Rate	(Note 11)	23				V/ms
GBW	Gain-Bandwidth Product		50				kHz

Note 1: Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but specific performance is not guaranteed. For guaranteed specifications and the test conditions, see the Electrical Characteristics.

Note 2: Human body model, 1.5 kΩ in series with 100 pF. All pins rated per method 3015.6 of MIL-STD-883. This is a class 2 device rating.

Note 3: Applies to both single supply and split-supply operation. Continuous short circuit operation at elevated ambient temperature can result in exceeding the maximum allowed junction temperature of 150°C. Output currents in excess of ±30 mA over long term may adversely affect reliability.

Note 4: The maximum power dissipation is a function of  $T_{J(max)}$ ,  $\theta_{JA}$ , and  $T_A$ . The maximum allowable power dissipation at any ambient temperature is  $P_D = (T_{J(max)} - T_A)/\theta_{JA}$ . All numbers apply for packages soldered directly into a PC board.

Note 5: Typical Values represent the most likely parametric norm.

Note 6: All limits are guaranteed by testing or statistical analysis.

Note 7:  $V^+$  = 15V,  $V_{CM}$  = 7.5V and  $R_L$  connected to 7.5V. For Sourcing tests,  $7.5V \le V_O \le 11.5V$ . For Sinking tests,  $3.5V \le V_O \le 7.5V$ .

Note 8: Do not short circuit output to V+, when V+ is greater than 13V or reliability will be adversely affected.

Note 9: V+ = 15V. Connected as Voltage Follower with 10V step input. Number specified is the slower of either the positive or negative slew rates.

Note 10: Input referred, V<sup>+</sup> = 15V and R<sub>L</sub> = 100 k $\Omega$  connected to 7.5V. Each amp excited in turn with 1 kHz to produce V<sub>O</sub> = 12 V<sub>PP</sub>.

Note 11: Connected as Voltage Follower with 2V step input. Number specified is the slower of either the positive or negative slew rates.

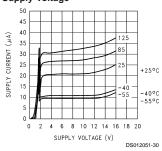
Note 12: Limiting input pin current is only necessary for input voltages that exceed absolute maximum input voltage ratings.

Note 13: Guaranteed limits are dictated by tester limitations and not device performance. Actual performance is reflected in the typical value.

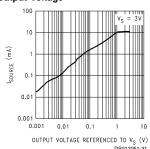
Note 14: For guaranteed Military Temperature Range parameters see RETSMC6462/4X.

### Typical Performance Characteristics V<sub>S</sub> = +5V, Single Supply, T<sub>A</sub> = 25°C unless otherwise specified

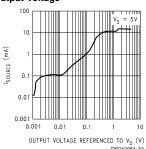
### Supply Current vs Supply Voltage



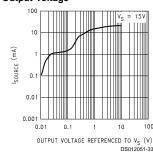
### Sourcing Current vs Output Voltage



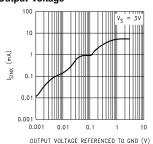
### Sourcing Current vs Output Voltage



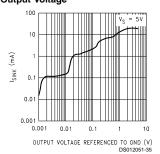
### Sourcing Current vs Output Voltage



### Sinking Current vs Output Voltage

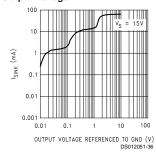


#### Sinking Current vs Output Voltage

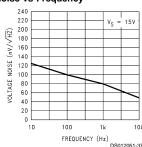


## **Typical Performance Characteristics** $V_S = +5V$ , Single Supply, $T_A = 25^{\circ}C$ unless otherwise specified (Continued)

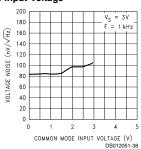
### Sinking Current vs Output Voltage



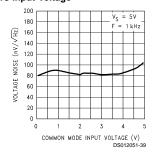
### Input Voltage Noise vs Frequency



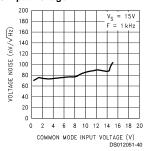
## Input Voltage Noise vs Input Voltage



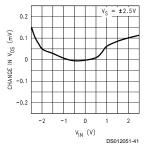
# Input Voltage Noise vs Input Voltage



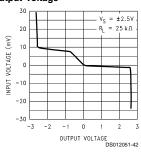
## Input Voltage Noise vs Input Voltage



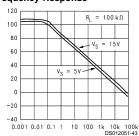
 $\Delta \text{V}_{\text{OS}}$  vs CMR



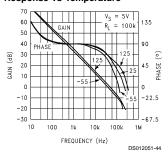
### Input Voltage vs Output Voltage



### Open Loop Frequency Response

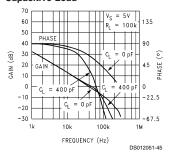


### Open Loop Frequency Response vs Temperature

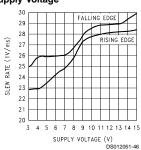


# Typical Performance Characteristics $V_S = +5V$ , Single Supply, $T_A = 25$ °C unless otherwise specified (Continued)

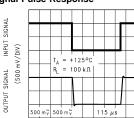
### Gain and Phase vs Capacitive Load



### Slew Rate vs Supply Voltage

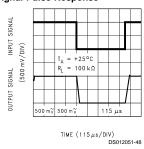


### Non-Inverting Large Signal Pulse Response

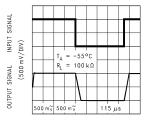


TIME (115 μs/DIV)
DS012051-47

### Non-Inverting Large Signal Pulse Response

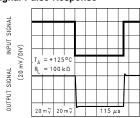


### Non-Inverting Large Signal Pulse Response



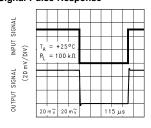
TIME (115 µs/DIV)
DS012051-49

### Non-Inverting Small Signal Pulse Response



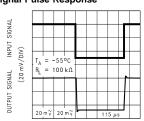
TIME (115 μs/DIV)
DS012051-50

### Non-Inverting Small Signal Pulse Response



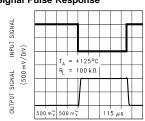
TIME (115 µs/DIV) DS012051-51

### Non-Inverting Small Signal Pulse Response



TIME (115 μs/DIV)
DS012051-52

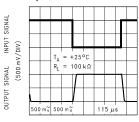
### Inverting Large Signal Pulse Response



TIME (115 μs/DIV) DS012051-53

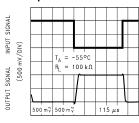
## **Typical Performance Characteristics** $V_S = +5V$ , Single Supply, $T_A = 25^{\circ}C$ unless otherwise specified (Continued)

### Inverting Large Signal Pulse Response



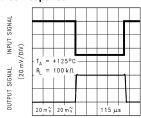
TIME (115 μs/DIV) DS012051-54

## Inverting Large Signal Pulse Response



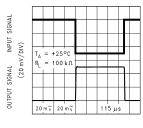
TIME (115 μs/DIV)
DS012051-55

## Inverting Small Signal Pulse Response



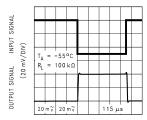
TIME (115 μs/DIV) DS012051-56

### Inverting Small Signal Pulse Response



TIME (115 μs/DIV) DS012051-57

### Inverting Small Signal Pulse Response



TIME (115 µs/DIV) DS012051-58

### **Application Information**

### 1.0 Input Common-Mode Voltage Range

The LMC6462/4 has a rail-to-rail input common-mode voltage range. *Figure 1* shows an input voltage exceeding both supplies with no resulting phase inversion on the output.

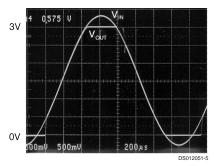


FIGURE 1. An Input Voltage Signal Exceeds the LMC6462/4 Power Supply Voltage with No Output Phase Inversion

The absolute maximum input voltage at  $V^+ = 3V$  is 300 mV beyond either supply rail at room temperature. Voltages greatly exceeding this absolute maximum rating, as in *Figure 2*, can cause excessive current to flow in or out of the input

pins, possibly affecting reliability. The input current can be externally limited to  $\pm 5$  mA, with an input resistor, as shown in *Figure 3*.

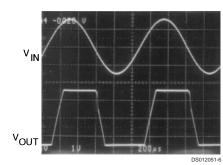


FIGURE 2. A ±7.5V Input Signal Greatly Exceeds the 3V Supply in Figure 3 Causing No Phase Inversion Due to R<sub>I</sub>

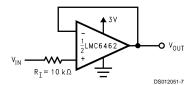


FIGURE 3. Input Current Protection for Voltages Exceeding the Supply Voltage

#### 2.0 Rail-to-Rail Output

The approximated output resistance of the LMC6462/4 is  $180\Omega$  sourcing, and  $130\Omega$  sinking at  $V_S=3V$ , and  $110\Omega$  sourcing and  $83\Omega$  sinking at  $V_S=5V$ . The maximum output swing can be estimated as a function of load using the calculated output resistance.

#### 3.0 Capacitive Load Tolerance

The LMC6462/4 can typically drive a 200 pF load with  $V_{\rm S}=5$ V at unity gain without oscillating. The unity gain follower is the most sensitive configuration to capacitive load. Direct capacitive loading reduces the phase margin of op-amps. The combination of the op-amp's output impedance and the capacitive load induces phase lag. This results in either an underdamped pulse response or oscillation.

Capacitive load compensation can be accomplished using resistive isolation as shown in *Figure 4*. If there is a resistive component of the load in parallel to the capacitive component, the isolation resistor and the resistive load create a voltage divider at the output. This introduces a DC error at the output.

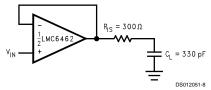


FIGURE 4. Resistive Isolation of a 300 pF Capacitive Load

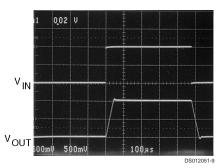


FIGURE 5. Pulse Response of the LMC6462 Circuit Shown in Figure 4

Figure 5 displays the pulse response of the LMC6462/4 circuit in Figure 4.

Another circuit, shown in *Figure 6*, is also used to indirectly drive capacitive loads. This circuit is an improvement to the circuit shown in *Figure 4* because it provides DC accuracy as well as AC stability. R1 and C1 serve to counteract the loss of phase margin by feeding the high frequency component of the output signal back to the amplifiers inverting input, thereby preserving phase margin in the overall feedback loop. The values of R1 and C1 should be experimentally determined by the system designer for the desired pulse response. Increased capacitive drive is possible by increasing the value of the capacitor in the feedback loop.

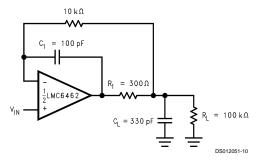


FIGURE 6. LMC6462 Non-Inverting Amplifier, Compensated to Handle a 300 pF Capacitive and 100 k $\Omega$  Resistive Load

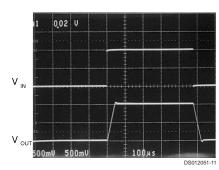


FIGURE 7. Pulse Response of LMC6462 Circuit in Figure 6

The pulse response of the circuit shown in Figure 6 is shown in Figure 7.

### 4.0 Compensating for Input Capacitance

It is quite common to use large values of feedback resistance with amplifiers that have ultra-low input current, like the LMC6462/4. Large feedback resistors can react with small values of input capacitance due to transducers, photodiodes, and circuits board parasitics to reduce phase margins.

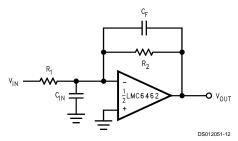


FIGURE 8. Canceling the Effect of Input Capacitance

The effect of input capacitance can be compensated for by adding a feedback capacitor. The feedback capacitor (as in *Figure 8*),  $C_F$ , is first estimated by:

$$\frac{1}{2\pi R_1\,C_{IN}} \geq \frac{1}{2\pi R_2\,C_F}$$

or

$$R_1 C_{IN} \leq R_2 C_F$$

which typically provides significant overcompensation.

Printed circuit board stray capacitance may be larger or smaller than that of a breadboard, so the actual optimum value for  $C_F$  may be different. The values of  $C_F$  should be checked on the actual circuit. (Refer to the LMC660 quad CMOS amplifier data sheet for a more detailed discussion.)

### 5.0 Offset Voltage Adjustment

Offset voltage adjustment circuits are illustrated in *Figure 9* and *Figure 10*. Large value resistances and potentiometers are used to reduce power consumption while providing typically  $\pm 2.5$  mV of adjustment range, referred to the input, for both configurations with V<sub>S</sub> =  $\pm 5$ V.

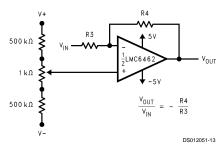


FIGURE 9. Inverting Configuration Offset Voltage Adjustment

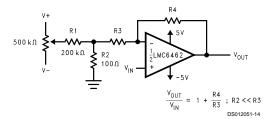


FIGURE 10. Non-Inverting Configuration
Offset Voltage Adjustment

#### 6.0 Spice Macromodel

A Spice macromodel is available for the LMC6462/4. This model includes a simulation of:

- · Input common-mode voltage range
- · Frequency and transient response
- · GBW dependence on loading conditions
- · Quiescent and dynamic supply current
- · Output swing dependence on loading conditions

and many more characteristics as listed on the macromodel

Contact the National Semiconductor Customer Response Center to obtain an operational amplifier Spice model library disk

## 7.0 Printed-Circuit-Board Layout for High-Impedance Work

It is generally recognized that any circuit which must operate with less than 1000 pA of leakage current requires special layout of the PC board. When one wishes to take advantage of the ultra-low input current of the LMC6462/4, typically 150 fA, it is essential to have an excellent layout. Fortunately, the techniques of obtaining low leakages are quite simple. First, the user must not ignore the surface leakage of the PC board, even though it may sometimes appear acceptably low, because under conditions of high humidity or dust or contamination, the surface leakage will be appreciable.

To minimize the effect of any surface leakage, lay out a ring of foil completely surrounding the LMC6462's inputs and the terminals of capacitors, diodes, conductors, resistors, relay terminals, etc. connected to the op-amp's inputs, as in Figure 11. To have a significant effect, guard rings should be placed in both the top and bottom of the PC board. This PC foil must then be connected to a voltage which is at the same voltage as the amplifier inputs, since no leakage current can flow between two points at the same potential. For example, a PC board trace-to-pad resistance of  $10^{12}\Omega$ , which is normally considered a very large resistance, could leak 5 pA if the trace were a 5V bus adjacent to the pad of the input. This would cause a 30 times degradation from the LMC6462/4's actual performance. However, if a guard ring is held within 5 mV of the inputs, then even a resistance of  $10^{11}\Omega$  would cause only 0.05 pA of leakage current. See Figure 12 for typical connections of guard rings for standard op-amp configurations.

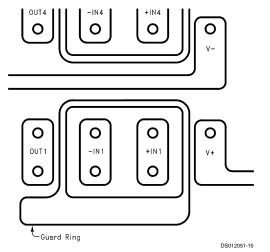
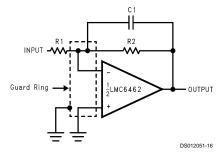
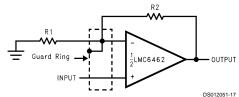


FIGURE 11. Example of Guard Ring in P.C. Board Layout



### **Inverting Amplifier**



### Non-Inverting Amplifier

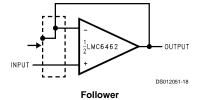
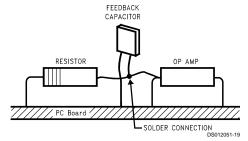


FIGURE 12. Typical Connections of Guard Rings

The designer should be aware that when it is inappropriate to lay out a PC board for the sake of just a few circuits, there is another technique which is even better than a guard ring on a PC board: Don't insert the amplifier's input pin into the

board at all, but bend it up in the air and use only air as an insulator. Air is an excellent insulator. In this case you may have to forego some of the advantages of PC board construction, but the advantages are sometimes well worth the effort of using point-to-point up-in-the-air wiring. See *Figure* 13



(Input pins are lifted out of PC board and soldered directly to components. All other pins connected to PC board.)  $\,$ 

FIGURE 13. Air Wiring

#### 8.0 Instrumentation Circuits

The LMC6464 has the high input impedance, large common-mode range and high CMRR needed for designing instrumentation circuits. Instrumentation circuits designed with the LMC6464 can reject a larger range of common-mode signals than most in-amps. This makes instrumentation circuits designed with the LMC6464 an excellent choice for noisy or industrial environments. Other appli-

cations that benefit from these features include analytic medical instruments, magnetic field detectors, gas detectors, and silicon-based transducers.

A small valued potentiometer is used in series with Rg to set the differential gain of the three op-amp instrumentation circuit in *Figure 14*. This combination is used instead of one large valued potentiometer to increase gain trim accuracy and reduce error due to vibration.

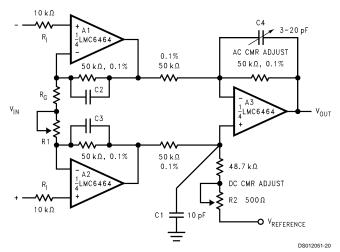


FIGURE 14. Low Power Three Op-Amp Instrumentation Amplifier

A two op-amp instrumentation amplifier designed for a gain of 100 is shown in *Figure 15*. Low sensitivity trimming is made for offset voltage, CMRR and gain. Low cost and low power consumption are the main advantages of this two op-amp circuit.

Higher frequency and larger common-mode range applications are best facilitated by a three op-amp instrumentation amplifier.

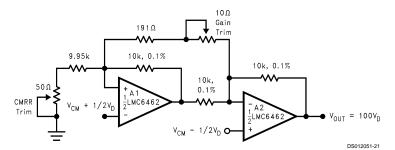


FIGURE 15. Low-Power Two-Op-Amp Instrumentation Amplifier

### **Typical Single-Supply Applications**

### TRANSDUCER INTERFACE CIRCUITS

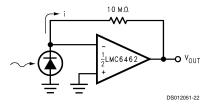


FIGURE 16. Photo Detector Circuit

Photocells can be used in portable light measuring instruments. The LMC6462, which can be operated off a battery, is an excellent choice for this circuit because of its very low input current and offset voltage.

### LMC6462 AS A COMPARATOR

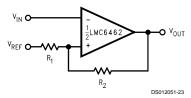


FIGURE 17. Comparator with Hysteresis

Figure 17 shows the application of the LMC6462 as a comparator. The hysteresis is determined by the ratio of the two resistors. The LMC6462 can thus be used as a micropower comparator, in applications where the quiescent current is an important parameter.

### HALF-WAVE AND FULL-WAVE RECTIFIERS

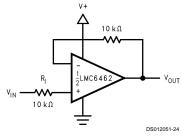


FIGURE 18. Half-Wave Rectifier with Input Current Protection (R<sub>I</sub>)

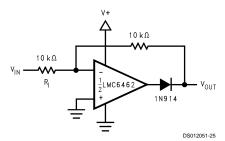


FIGURE 19. Full-Wave Rectifier with Input Current Protection (R<sub>I</sub>)

In Figure 18 Figure 19,  $\rm R_1$  limits current into the amplifier since excess current can be caused by the input voltage exceeding the supply voltage.

### PRECISION CURRENT SOURCE

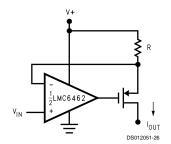


FIGURE 20. Precision Current Source

The output current  $I_{\text{OUT}}$  is given by:

$$I_{OUT} = \left(\frac{V^+ - V_{IN}}{R}\right)$$

### **OSCILLATORS**

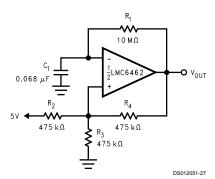


FIGURE 21. 1 Hz Square-Wave Oscillator

For single supply 5V operation, the output of the circuit will swing from 0V to 5V. The voltage divider set up  $R_2,\,R_3$  and  $R_4$  will cause the non-inverting input of the LMC6462 to move from 1.67V ( $1\!\!/3$  of 5V) to 3.33V ( $2\!\!/3$  of 5V). This voltage behaves as the threshold voltage.

 $\rm R_1$  and  $\rm C_1$  determine the time constant of the circuit. The frequency of oscillation,  $\rm f_{OSC}$  is

### **Typical Single-Supply Applications**

(Continued)

$$\left(\frac{1}{2\Delta t}\right)$$

where  $\Delta t$  is the time the amplifier input takes to move from 1.67V to 3.33V. The calculations are shown below.

$$1.67 = 5\left(1 - e^{-\frac{t_1}{\tau}}\right)$$

where  $\tau$  = RC = 0.68 seconds

 $\rightarrow$ t<sub>1</sub> = 0.27 seconds.

and

$$3.33 = 5\left(1 - e^{-\frac{t_2}{\tau}}\right)$$

 $\rightarrow$ t<sub>2</sub> = 0.75 seconds

Then,

$$f_{OSC} = \left(\frac{1}{2\Delta t}\right)$$

$$=\frac{1}{2(0.75-0.27)}$$

= 1 Hz

### LOW FREQUENCY NULL

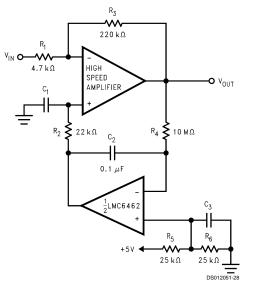
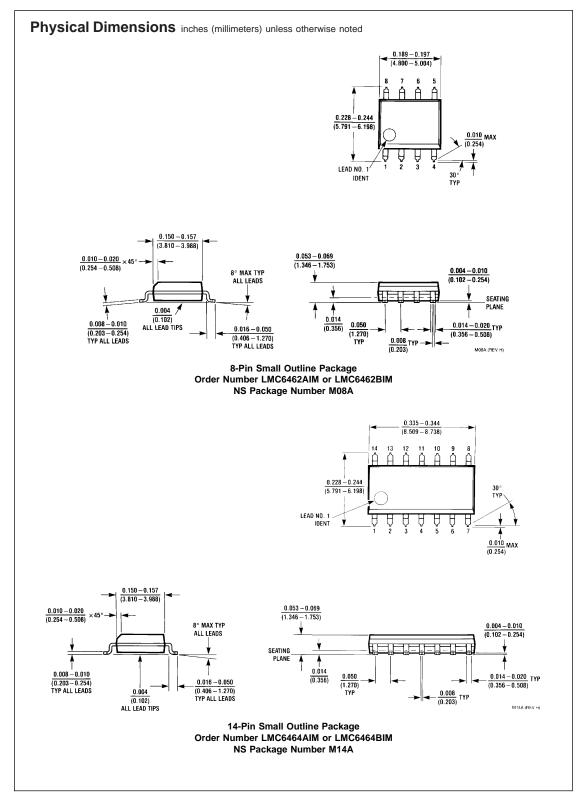


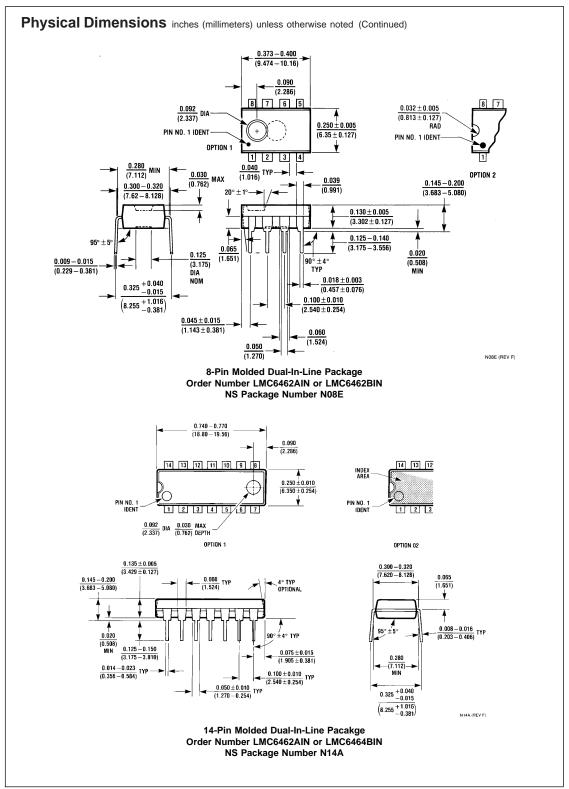
FIGURE 22. High Gain Amplifier with Low Frequency Null

Output offset voltage is the error introduced in the output voltage due to the inherent input offset voltage  $V_{\rm OS}$ , of an amplifier.

Output Offset Voltage = (Input Offset Voltage) (Gain)

In the above configuration, the resistors  $R_{\rm 5}$  and  $R_{\rm 6}$  determine the nominal voltage around which the input signal,  $V_{\rm IN}$  should be symmetrical. The high frequency component of the input signal  $V_{\rm IN}$  will be unaffected while the low frequency component will be nulled since the DC level of the output will be the input offset voltage of the LMC6462 plus the bias voltage. This implies that the output offset voltage due to the top amplifier will be eliminated.





### **Notes**

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National Semiconductor Corporation

Tel: 1-800-272-9959 Fax: 1-800-737-7018 Email: support@nsc.com

www.national.com

National Semiconductor Europe

Europe
Fax: +49 (0) 1 80-530 85 86
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Deutsch Tel: +49 (0) 1 80-530 85 85
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