## Power Factor Controllers

The are active power factor controllers specifically designed for use as a preconverter in electronic ballast and in off-line power converter applications.

These integrated circuits feature an internal startup timer for stand-alone applications, a one quadrant multiplier for near unity power factor, zero current detector to ensure critical conduction operation, transconductance error amplifier, quick start circuit for enhanced startup, trimmed internal bandgap reference, current sensing comparator, and a totem pole output ideally suited for driving a power MOSFET.

Also included are protective features consisting of an overvoltage comparator to eliminate runaway output voltage due to load removal, input undervoltage lockout with hysteresis, cycle-by-cycle current limiting, multiplier output clamp that limits maximum peak switch current, an RS latch for single pulse metering, and a drive output high state clamp for MOSFET gate protection. These devices are available in dual-in-line and surface mount plastic packages.

- Overvoltage Comparator Eliminates Runaway Output Voltage
- Internal Startup Timer
- One Quadrant Multiplier
- Zero Current Detector
- Trimmed 2\% Internal Bandgap Reference
- Totem Pole Output with High State Clamp
- Undervoltage Lockout with 6.0 V of Hysteresis
- Low Startup and Operating Current
- Supersedes Functionality of SG3561, TDA4817 and MC34262

IL34262


## MAXIMUM RATINGS

| Rating | Symbol | Value | Unit |
| :---: | :---: | :---: | :---: |
| Total Power Supply and Zener Current | (Icc + Iz) | 30 | mA |
| Output Current, Source or Sink | lo | 500 | mA |
| Current Sense, Multiplier, and Voltage Feedback Inputs | Vin | -1.0 to +10 | V |
| Zero Current Detect Input <br> High State Forward Current <br> Low State Reverse Current | Iin | $\begin{aligned} & 50 \\ & -10 \end{aligned}$ | mA |
| Power Dissipation and Thermal Characteristics N Suffix, Plastic Package <br> Maximum Power Dissipation @ $\mathrm{TA}=70^{\circ} \mathrm{C}$ <br> Thermal Resistance, Junction-to-Air <br> D Suffix, Plastic Package <br> Maximum Power Dissipation @ $\mathrm{TA}=70^{\circ} \mathrm{C}$ <br> Thermal Resistance, Junction-to-Air | $\begin{array}{\|l} \mathrm{PD} \\ \mathrm{R}_{\theta \mathrm{JA}} \\ \mathrm{PD}^{2} \\ \mathrm{R}_{\theta \mathrm{JIA}} \end{array}$ | $\begin{aligned} & 800 \\ & 100 \\ & 450 \\ & 178 \end{aligned}$ | $\begin{aligned} & \mathrm{mW} \\ & { }^{\circ} \mathrm{C} / \mathrm{W} \\ & \mathrm{~mW} \\ & { }^{0} \mathrm{C} / \mathrm{W} \end{aligned}$ |
| Operating Junction Temperature | TJ | +150 | ${ }^{\circ} \mathrm{C}$ |
| Operating Ambient Temperature | TA | 0 to +85 | ${ }^{\circ} \mathrm{C}$ |
| Storage Temperature | Tstg | -65 to +150 | ${ }^{\circ} \mathrm{C}$ |

ELECTRICAL CHARACTERISTICS (Vcc $=12 \mathrm{~V}$, for $\min /$ max values $T A$ is the operating ambient
temperature range that applies unless otherwise noted.)

| Characteristic | Symbol | Min | Max | Unit |
| :---: | :---: | :---: | :---: | :---: |
| ERROR AMPLIFIER |  |  |  |  |
| Voltage Feedback Input Threshold $\begin{aligned} & \mathrm{TA}=25^{\circ} \mathrm{C} \\ & \mathrm{TA}=\text { Tlow to Thigh }(\mathrm{Vcc}=12 \mathrm{~V} \text { to } 28 \mathrm{~V}) \\ & \hline \end{aligned}$ | VFb | $\begin{gathered} 2.465 \\ 2.44 \\ \hline \end{gathered}$ | $\begin{gathered} 2.535 \\ 2.54 \\ \hline \end{gathered}$ | V |
| Line Regulation (Vcc $=12 \mathrm{~V}$ to $28 \mathrm{~V}, \mathrm{TA}=25^{\circ} \mathrm{C}$ ) | Regline | - | 10 | mV |
| Input Bias Current (VFB $=0 \mathrm{~V}$ ) | IIB | - | -0.5 | $\mu \mathrm{A}$ |
| Transconductance ( $\mathrm{TA}=25^{\circ} \mathrm{C}$ ) | gm | 80 | 130 | $\mu \mathrm{mho}$ |
| Output Current <br> Source (VFB = 2.3 V) <br> Sink (Vfb = 2.7 V) | lo | - | - | $\mu \mathrm{A}$ |
| Output Voltage Swing <br> High State $(\mathrm{VFB}=2.3 \mathrm{~V})$ <br> Low State $(\mathrm{VFB}=2.7 \mathrm{~V})$ | $\begin{aligned} & \mathrm{V}_{\mathrm{OH}}(\mathrm{ea}) \\ & \mathrm{V}_{\mathrm{OL}}(\mathrm{ea}) \\ & \hline \end{aligned}$ | $5.8$ | $\overline{2.4}$ | V |


| Characteristic | Symbol | Min | Max | Unit |
| :---: | :---: | :---: | :---: | :---: |
| OVERVOLTAGE COMPARATOR |  |  |  |  |
| Voltage Feedback Input Threshold | $\mathrm{V}_{\mathrm{FB}}(\mathrm{OV})$ | 1.065 VFB | 1.095 VFB | V |
| MULTIPLIER |  |  |  |  |
| Input Bias Current, Pin 3 (VFB = 0 V ) | ІІв | - | -0.5 | $\mu \mathrm{A}$ |
| Input Threshold, Pin 2 | Vth(M) | $1.05 \mathrm{~V}_{\text {OL(EA) }}$ | - | V |
| Dynamic Input Voltage Range <br> Multiplier Input (Pin 3) <br> Compensation (Pin 2) | $\begin{aligned} & \text { Vpin3 } \\ & \text { Vpin2 } \end{aligned}$ | $\begin{array}{\|c} 0 \text { to } 2.5 \mathrm{Vth}(\mathrm{M}) \text { to } \\ (\mathrm{Vth}(\mathrm{M})+1.0) \end{array}$ | - | V |
| $\begin{aligned} & \text { Multiplier Gain (Vpin } 3=0.5 \text { V, Vpin } 2=\text { Vth(M) + } \\ & 1.0 \mathrm{~V} \text { ) } \end{aligned}$ | K | 0.43 | 0.87 | 1/V |
| ZERO CURRENT DETECTOR |  |  |  |  |
| Input Threshold Voltage (Vjn Increasing) | Vth | 1.33 | 1.87 | V |
| Hysteresis (Vin Decreasing) | VH | 100 | 300 | mV |
| Input Clamp Voltage <br> High State (IDET $=+3.0 \mathrm{~mA}$ ) <br> High State ( $\mathrm{IdET}=-3.0 \mathrm{~mA}$ ) | VIH <br> VIL | $\begin{aligned} & 6.1 \\ & 0.3 \end{aligned}$ | $\overline{1.0}$ | V |
| CURRENT SENSE COMPARATOR |  |  |  |  |
| Input Bias Current (Vpin $4=0 \mathrm{~V}$ ) | $\mathrm{I}_{\text {IB }}$ | - | -1.0 | $\mu \mathrm{A}$ |
| Input Offset Voltage (Vpm $2=1.6 \mathrm{~V}$, Vpm $3=0 \mathrm{~V}$ ) | $\mathrm{V}_{\text {IO }}$ | - | 25 | mV |
| Maximum Current Sense Input Threshold (Note 1) | $\mathrm{V}_{\text {th(max }}$ | 1.3 | 1.8 | V |
| Delay to Output | $\mathrm{t}_{\text {PHL (in/out) }}$ | - | 400 | ns |
| DRIVE OUTPUT |  |  |  |  |
| $\begin{aligned} & \text { Output Voltage }\left(\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}\right) \\ & \text { Low State }\left(\mathrm{I}_{\text {sink }}=20 \mathrm{~mA}\right) \\ & \left(\mathrm{I}_{\text {sink }}=200 \mathrm{~mA}\right) \\ & \text { High State }\left(\mathrm{I}_{\text {source }}=20 \mathrm{~mA}\right) \\ & \left(\mathrm{I}_{\text {source }}=200 \mathrm{~mA}\right) \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{OL}} \\ & \mathrm{~V}_{\mathrm{OH}} \end{aligned}$ | $\begin{aligned} & - \\ & 9.8 \\ & 7.8 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.8 \\ & 3.3 \\ & 0.8 \\ & 3.3 \\ & \hline \end{aligned}$ | V |
| Output Voltage $\left(\mathrm{V}_{\mathrm{CC}}=30 \mathrm{~V}\right)$ <br> High State $\left(\mathrm{I}_{\text {source }}=20 \mathrm{~mA}, \mathrm{C}_{\mathrm{L}}=15 \mathrm{pF}\right.$ ) | $\mathrm{V}_{\mathrm{O}(\text { max })}$ | 14 | 18 | V |
| Output Voltage Rise Time ( $\mathrm{C}_{\mathrm{L}} 1.0 \mathrm{nF}$ ) | $\mathrm{t}_{\mathrm{r}}$ | - | 120 | ns |
| Output Voltage Fall Time ( $\mathrm{C}_{\mathrm{L}} 1.0 \mathrm{nF}$ ) | $\mathrm{t}_{\mathrm{f}}$ | - | 120 | ns |
| Output Voltage with UVLO Activated $\left(\mathrm{Vcc}=7.0 \mathrm{~V}, \mathrm{l}_{\text {Sink }}=1.0 \mathrm{~mA}\right)$ | $\mathrm{V}_{\mathrm{O} \text { (UVLO) }}$ | - | 0.5 | V |
| RESTART TIMER |  |  |  |  |
| Restart Time Delay | tDLY | 200 | - | $\mu \mathrm{s}$ |

Note 1: This parameter is measured with $\mathrm{V}_{\mathrm{FB}}=0 \mathrm{~V}$, and $\mathrm{V}_{\text {Pin3 }}=3.0 \mathrm{~V}$

| Characteristic | Symbol | Min | Max | Unit |
| :---: | :---: | :---: | :---: | :---: |
| UNDERVOLTAGE LOCKOUT |  |  |  |  |
| Startup Threshold ( $\mathrm{V}_{\mathrm{CC}}$ Increasing) | $\mathrm{V}_{\text {th(on) }}$ | 11.5 | 14.5 | V |
| Minimum Operating Voltage After Turn-On ( $\mathrm{V}_{\mathrm{CC}}$ Decreasing) | $\mathrm{V}_{\text {Shutdown }}$ | 7.0 | 9.0 | V |
| Hysteresis | $\mathrm{V}_{\mathrm{H}}$ | 3.8 | 6.2 | V |
| TOTAL DEVICE |  |  |  |  |
| Power Supply Current <br> Startup (Vcc = 7.0 V) <br> Operating Dynamic Operating ( $50 \mathrm{kHz}, \mathrm{C}_{\mathrm{L}}=1.0 \mathrm{nF}$ ) | $\mathrm{I}_{\text {CC }}$ | - | $\begin{gathered} 0.4 \\ 12 \\ 20 \\ \hline \end{gathered}$ | mA |
| Power Supply Zener Voltage (Ice = 25 mA ) | $\mathrm{V}_{\mathrm{Z}}$ | 30 | - | V |



| Notes | Calculation | Formula |
| :---: | :---: | :---: |
| Calculate the maximum required output power. | Required Converter Output Power | $\mathrm{P}_{\mathrm{O}}=\mathrm{V}_{\mathrm{O}} \mathrm{l}_{0}$ |
| Calculated at the minimum required ac line voltage for output regulation. Let the efficiency $\eta=0.92$ for low line operation. | Peak Inductor Current | $\mathrm{I}_{\mathrm{L}(\mathrm{pk})}=\frac{2 \sqrt{2} \mathrm{P}_{\mathrm{O}}}{\eta \operatorname{Vac}_{(\mathrm{LL})}}$ |
| Let the switching cycle $\mathrm{t}=40 \mu \mathrm{~s}$ for universal input ( 85 to 265 Vac ) operation and $20 \mu$ s for fixed input ( 92 to 138 Vac , or 184 to 276 Vac ) operation. | Inductance | $L_{p}=\frac{t\left(\frac{\mathrm{~V}_{\mathrm{O}}}{\sqrt{2}}-\mathrm{Vac}_{(\mathrm{LL})}\right) \eta \mathrm{Vac}_{(\mathrm{LL})}{ }^{2}}{\sqrt{2} \mathrm{~V}_{\mathrm{O}} \mathrm{P}_{\mathrm{O}}}$ |
| In theory the on-time $\mathrm{t}_{\text {on }}$ is constant. In practice $\mathrm{t}_{\text {on }}$ tends to increase at the ac line zero crossings due to the charge on capacitor $\mathrm{C}_{5}$. Let $\mathrm{Vac}=\mathrm{Vac}_{(\mathrm{LL})}$ for initial $\mathrm{t}_{\mathrm{on}}$ and $\mathrm{t}_{\text {off }}$ calculations. | Switch On-Time | $\mathrm{t}_{\mathrm{on}}=\frac{2 \mathrm{P}_{\mathrm{O}} \mathrm{~L}_{\mathrm{p}}}{\eta \mathrm{Vac}^{2}}$ |
| The off-time $t_{\text {off }}$ is greatest at the peak of the ac line voltage and approaches zero at the ac line zero crossings. Theta ( $\theta$ ) represents the angle of the ac line voltage. | Switch Off-Time | $\mathrm{t}_{\text {off }}=\frac{\mathrm{t}_{\text {on }}}{\frac{\mathrm{V}_{\mathrm{O}}}{\sqrt{2} \mathrm{Vac}\|\operatorname{Sin} \theta\|}-1}$ |
| The minimum switching frequency occurs at the peak of the ac line voltage. As the ac line voltage traverses from peak to zero, $\mathrm{t}_{\text {off }}$ approaches zero producing an increase in switching frequency. | Switching Frequency | $f=\frac{1}{t_{\text {on }}+t_{\text {off }}}$ |
| Set the current sense threshold $\mathrm{V}_{\mathrm{CS}}$ to 1.0 V for universal input ( 85 Vac to 265 Vac ) operation and to 0.5 V for fixed input ( 92 Vac to 138 Vac , or 184 Vac to 276 Vac ) operation. Note that $\mathrm{V}_{\mathrm{CS}}$ must be $<1.4 \mathrm{~V}$. | Peak Switch Current | $\mathrm{R}_{7}=\frac{\mathrm{V}_{\mathrm{CS}}}{\mathrm{I}_{\mathrm{L}(\mathrm{pk})}}$ |
| Set the multiplier input voltage $\mathrm{V}_{\mathrm{M}}$ to 3.0 V at high line. Empirically adjust $\mathrm{V}_{\mathrm{M}}$ for the lowest distortion over the ac line voltage range while guaranteeing startup at minimum line. | Multiplier Input Voltage | $\mathrm{V}_{\mathrm{M}}=\frac{\operatorname{Vac} \sqrt{2}}{\left(\frac{R_{5}}{R_{3}}+1\right)}$ |
| The $\mathrm{I}_{\mathrm{IB}} \mathrm{R}_{1}$ error term can be minimized with a divider current in excess of $50 \mu \mathrm{~A}$. | Converter Output Voltage | $\mathrm{V}_{\mathrm{O}}=\mathrm{V}_{\text {ref }}\left(\frac{\mathrm{R}_{2}}{\mathrm{R}_{1}}+1\right)-\mathrm{I}_{\mathrm{IB}} \mathrm{R}_{2}$ |
| The calculated peak-to-peak ripple must be less than $16 \%$ of the average dc output voltage to prevent false tripping of the Overvoltage Comparator. Refer to the Overvoltage Comparator text. ESR is the equivalent series resistance of $\mathrm{C}_{3}$ | Converter Output Peak to Peak Ripple Voltage | $\Delta \mathrm{V}_{\mathrm{O}(\mathrm{pp})}=\mathrm{I}_{\mathrm{O}} \sqrt{\left(\frac{1}{2 \pi \mathrm{f}_{\mathrm{ac}} \mathrm{C}_{3}}\right)^{2}+\mathrm{ESR}^{2}}$ |
| The bandwidth is typically set to 20 Hz . When operating at high ac line, the value of $\mathrm{C}_{1}$ may need to be increased. (See Figure 25) | Error Amplifier Bandwidth | $\mathrm{BW}=\frac{\mathrm{gm}}{2 \pi \mathrm{C}_{1}}$ |

The following converter characteristics must be chosen:

| $\mathrm{V}_{\mathrm{O}}$ - Desired output voltage | Vac -AC RMS line voltage |
| :---: | :---: |
| $\mathrm{I}_{\mathrm{O}}$ - Desired output current | $\mathrm{Vac}_{(\mathrm{LL})}$ - AC RMS low line voltage |
| $\Delta \mathrm{V}_{\mathrm{O}}$ - Converter output peak-to-peak ripple voltage |  |

## <Design Equations>

## APPLICATION INFORMATION

The application circuits shown in Figures 19, 20 and 21 reveal that few external components are required for a complete power factor preconverter. Each circuit is a peak detecting current-mode boost converter that operates in critical conduction mode with a fixed on-time and variable off-time. A major benefit of critical conduction operation is that the current loop is inherently stable, thus elimination the need for ramp compensation. The application in Figure 19 operates over an input voltage range if 90 Vac to 138 Vac and provides an output power of $80 \mathrm{~W}(230 \mathrm{~V}$ at 350 mA ) with an associated power factor of approximately 0.998 at
nominal line. Figures 20 and 21 are universal input preconverter examples that operate over a continuous input voltage range of 90 Vac to 268Vac. Figure 20 provides an output power of 175 W ( 400 V at 440 mA ) while Figure 21 provides 450 W ( 400 V at 1.125 A ). Both circuits have an observed worst-case power factor of approximately 0.989 . The input current and voltage waveforms of Figure 20 are shown in Figure 22 with operation at 115 Vac and 230 Vac. The data for each of the applications was generated with the test set-up shown in Figure 24.

## 80W Power Factor Controller



Power Factor Controller Test Data

| AC Line Input |  |  |  |  |  |  |  |  | DC Output |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Current Harmonic Distortion (\% $1_{\text {fund }}$ ) |  |  |  |  |  |  |  |  |  |
| $\mathrm{V}_{\text {rms }}$ | $\mathrm{P}_{\text {in }}$ | PF | 1 fund | THD | 2 | 3 | 5 | 7 | $\mathrm{V}_{\mathrm{O}(\mathrm{pp})}$ | $\mathrm{V}_{0}$ | 10 | Po | $\eta(\%)$ |
| 90 | 85.9 | 0.999 | 0.93 | 2.6 | 0.08 | 1.6 | 0.84 | 0.95 | 4.0 | 230.7 | 0.350 | 80.8 | 94.0 |
| 100 | 85.3 | 0.999 | 0.85 | 2.3 | 0.13 | 1.0 | 1.2 | 0.73 | 4.0 | 230.7 | 0.350 | 80.8 | 94.7 |
| 110 | 85.1 | 0.998 | 0.77 | 2.2 | 0.10 | 0.58 | 1.5 | 0.59 | 4.0 | 230.7 | 0.350 | 80.8 | 94.9 |
| 120 | 84.7 | 0.998 | 0.71 | 3.0 | 0.09 | 0.73 | 1.9 | 0.58 | 4.1 | 230.7 | 0.350 | 80.8 | 95.3 |
| 130 | 84.4 | 0.997 | 0.65 | 3.9 | 0.12 | 1.7 | 2.2 | 0.61 | 4.1 | 230.7 | 0.350 | 80.8 | 95.7 |
| 138 | 84.1 | 0.996 | 0.62 | 4.6 | 0.16 | 2.4 | 2.3 | 0.60 | 4.1 | 230.7 | 0.350 | 80.8 | 96.0 |

This data was taken with the test set-up shown in Figure 24.
$\mathrm{T}=$ Coilcraft N2881-A
Primary: 62 turns of \# 22 AWG
Secondary: 5 turns of \# 22 AWG
Core: Coilcraft PT2510, EE 25
Gap: $0.072^{\prime \prime}$ total for a primary inductance ( $L_{p}$ ) of $320 \mu \mathrm{H}$
Heatsink = AAVID Engineering Inc. 590302B03600, or 593002B03400

## 175W Universal Input Power Factor Controller



Power Factor Controller Test Data

| AC Line Input |  |  |  |  |  |  |  |  | DC Output |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Current Harmonic Distortion (\% $\mathrm{l}_{\text {fund }}$ ) |  |  |  |  | $\mathrm{V}_{\mathrm{O}(\mathrm{pp})}$ | $\mathrm{V}_{0}$ | 10 | Po | $\eta(\%)$ |
| $\mathrm{V}_{\mathrm{rms}}$ | $P_{\text {in }}$ | PF | 1 fund | THD | 2 | 3 | 5 | 7 |  |  |  |  |  |
| 90 | 193.3 | 0.991 | 2.15 | 2.8 | 0.18 | 2.6 | 0.55 | 1.0 | 3.3 | 402.1 | 0.44 | 176.9 | 91.5 |
| 120 | 190.1 | 0.998 | 1.59 | 1.6 | 0.10 | 1.4 | 0.23 | 0.72 | 3.3 | 402.1 | 0.44 | 176.9 | 93.1 |
| 138 | 188.2 | 0.999 | 1.36 | 1.2 | 0.12 | 1.3 | 0.65 | 0.80 | 3.3 | 402.1 | 0.44 | 176.9 | 94.0 |
| 180 | 184.9 | 0.998 | 1.03 | 2.0 | 0.10 | 0.49 | 1.2 | 0.82 | 3.4 | 402.1 | 0.44 | 176.9 | 95.7 |
| 240 | 182.0 | 0.993 | 0.76 | 4.4 | 0.09 | 1.6 | 2.3 | 0.51 | 3.4 | 402.1 | 0.44 | 176.9 | 97.2 |
| 268 | 180.9 | 0.989 | 0.69 | 5.9 | 0.10 | 2.3 | 2.9 | 0.46 | 3.4 | 402.1 | 0.44 | 176.9 | 97.8 |

This data was taken with the test set-up shown in Figure 24.

$$
T=\text { Coilcraft N2880-A }
$$

Primary: 78 turns of \# 16 AWG
Secondary: 6 turns of \# 18 AWG
Core: Coilcraft PT4215, EE 42-15
Gap: 0.104" total for a primary inductance ( $L_{p}$ ) of $870 \mu \mathrm{H}$
Heatsink = AAVID Engineering Inc. 590302B03600

450W Universal Input Power Factor Controller


Power Factor Controller Test Data

| AC Line Input |  |  |  |  |  |  |  |  | DC Output |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Current Harmonic Distortion (\% $\mathrm{l}_{\text {fund }}$ ) |  |  |  |  |  |  |  |  |  |
| $\mathrm{V}_{\text {rms }}$ | $\mathrm{P}_{\text {in }}$ | PF | $1_{\text {fund }}$ | THD | 2 | 3 | 5 | 7 | $\mathrm{V}_{\mathrm{O}(\mathrm{pp})}$ | $\mathrm{V}_{0}$ | 10 | Po | $\eta(\%)$ |
| 90 | 489.5 | 0.990 | 5.53 | 2.2 | 0.10 | 1.5 | 0.25 | 0.83 | 8.8 | 395.5 | 1.14 | 450.9 | 92.1 |
| 120 | 475.1 | 0.998 | 3.94 | 2.5 | 0.12 | 0.29 | 0.62 | 0.52 | 8.8 | 395.5 | 1.14 | 450.9 | 94.9 |
| 138 | 470.6 | 0.998 | 3.38 | 2.1 | 0.06 | 0.70 | 1.1 | 0.41 | 8.8 | 395.5 | 1.14 | 450.9 | 95.8 |
| 180 | 463.4 | 0.998 | 2.57 | 4.1 | 0.21 | 2.0 | 1.6 | 0.71 | 8.9 | 395.5 | 1.14 | 450.9 | 97.3 |
| 240 | 460.1 | 0.996 | 1.91 | 4.8 | 0.14 | 4.3 | 2.2 | 0.63 | 8.9 | 395.5 | 1.14 | 450.9 | 98.0 |
| 268 | 459.1 | 0.995 | 1.72 | 5.8 | 0.10 | 5.0 | 2.5 | 0.61 | 8.9 | 395.5 | 1.14 | 450.9 | 98.2 |

This data was taken with the test set-up shown in Figure 24.
$\mathrm{T}=$ Coilcraft P3657-A
Primary: 38 turns Litz wire, 1300 strands of \#48 AWG, Kerrigan-Lewis, Chicago, IL
Secondary: 3 turns of \# 20 AWG
Core: Coilcraft PT4220, EE 42-20
Gap: $0.180^{\prime \prime}$ total for a primary inductance ( $L_{P}$ ) of $190 \mu \mathrm{H}$
Heatsink = AAVID Engineering Inc. 604953B04000 Extrusion

## N SUFFIX PLASTIC DIP



| $\phi \mid 0.25(0.010)(1)$ | T |
| :--- | :--- | :--- |

## NOTES:

1. Dimensions "A", "B" do not include mold flash or protrusions. Maximum mold flash or protrusions $0.25 \mathrm{~mm}(0.010)$ per side.

|  | Dimension, mm |  |
| :---: | :---: | :---: |
| Symbol | MIN | MAX |
| A | 8.51 | 10.16 |
| B | 6.1 | 7.11 |
| C |  | 5.33 |
| D | 0.36 | 0.56 |
| F | 1.14 | 1.78 |
| G | 2.54 |  |
| H | 7.62 |  |
| J | $0^{\circ}$ | $10^{\circ}$ |
| K | 2.92 | 3.81 |
| L | 7.62 | 8.26 |
| M | 0.2 | 0.36 |
| N | 0.38 |  |

