

# Dual, Matched Picoampere, Microvolt Input, Low Noise Op Amp

## FEATURES

- *Guaranteed Offset Voltage*      50 $\mu$ V Max.
- *Guaranteed Bias Current*  
 25°C      120pA Max.  
 -55°C to 125°C      700pA Max.
- *Guaranteed Drift*      1.5 $\mu$ V/°C Max.
- *Low Noise, 0.1Hz to 10Hz*      0.5 $\mu$ Vp-p
- *Guaranteed Supply Current*      600 $\mu$ A Max.
- *Guaranteed CMRR*      112dB Min.
- *Guaranteed PSRR*      112dB Min.
- *Guaranteed Voltage Gain with 5mA Load Current*
- *Guaranteed Matching Characteristics*

## APPLICATIONS

- Strain Gauge Signal Conditioner
- Dual Limit Precision Threshold Detection
- Charge Integrators
- Wide Dynamic Range Logarithmic Amplifiers
- Light Meters
- Low Frequency Active Filters
- Standard Cell Buffers
- Thermocouple Amplifiers

## DESCRIPTION

The LT1024 dual, matched internally compensated universal precision operational amplifier can be used in practically all precision applications requiring multiple op amps. The LT1024 combines picoampere bias currents (which are maintained over the full -55°C to 125°C temperature range), microvolt offset voltage (and low drift with time and temperature), low voltage and current noise, and low power dissipation. Extremely high common-mode and power supply rejection ratios, practically immeasurable warm-up drift, and the ability to deliver 5mA load current with a voltage gain of a million round out the LT1024's superb precision specifications.

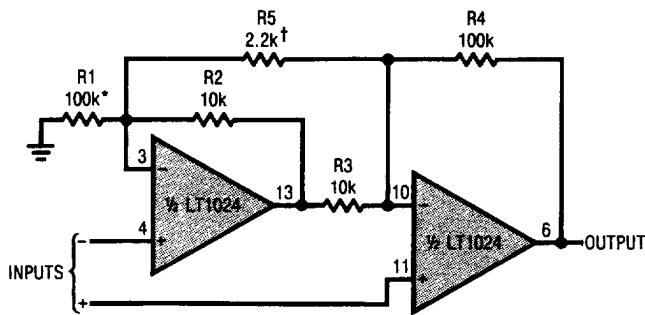
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Tight matching is guaranteed on offset voltage, non-inverting bias currents and common-mode and power supply rejections.

The all-around excellence of the LT1024 eliminates the necessity of the time-consuming error analysis procedure of precision system design in many dual applications; the LT1024 can be stocked as the universal dual op amp in the 14-pin DIP configuration.

For a single op amp with similar specifications, see the LT1012 data sheet; for a single supply dual precision op amp in the 8-pin configuration, see the LT1013 data sheet.

**Two Op Amp Instrumentation Amplifier**



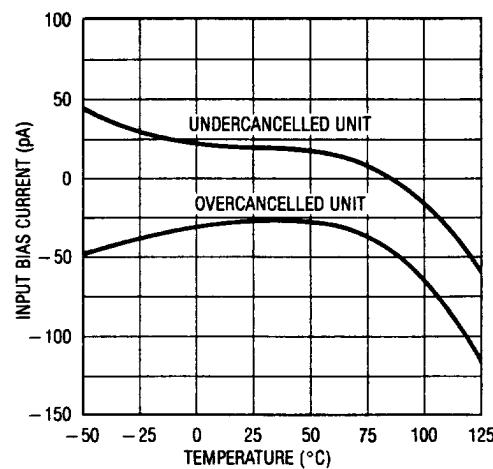
$$\text{GAIN} = \frac{R_4}{R_3} \left[ 1 + \frac{1}{2} \left( \frac{R_2 + R_3}{R_1} \right) + \frac{R_2 + R_3}{R_5} \right] = 100$$

\*TRIM FOR COMMON-MODE REJECTION

†TRIM FOR GAIN

TYPICAL PERFORMANCE:  
 OFFSET VOLTAGE = 20 $\mu$ V  
 BIAS CURRENT =  $\pm$ 30pA  
 OFFSET CURRENT = 30pA

**Input Bias Current vs Temperature**

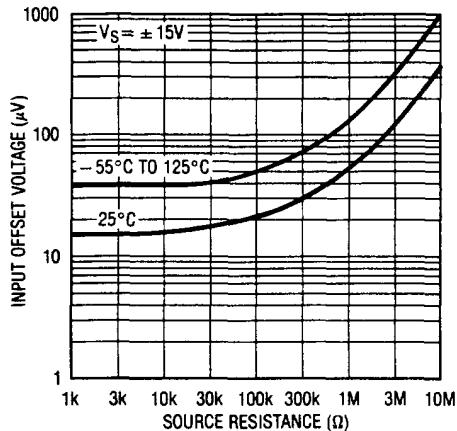




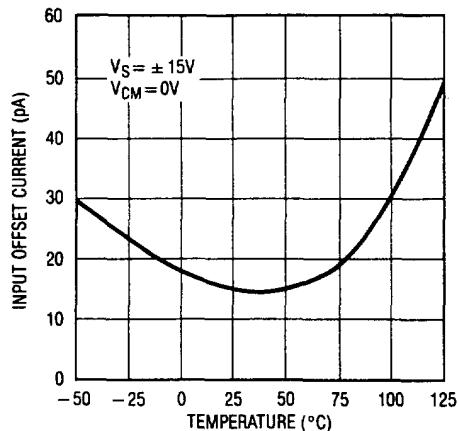


## TYPICAL PERFORMANCE CHARACTERISTICS

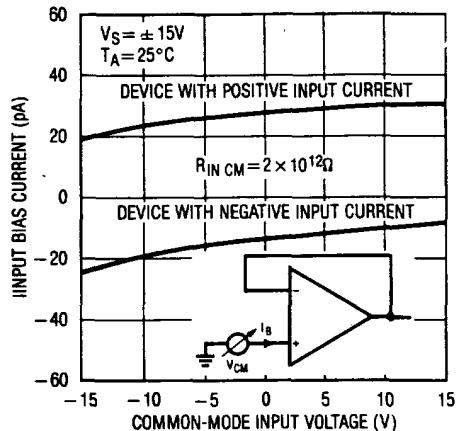
**Offset Voltage vs Source Resistance (Balanced or Unbalanced)**



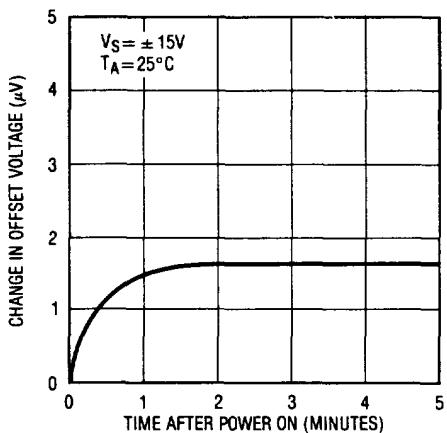
**Input Offset Current vs Temperature**



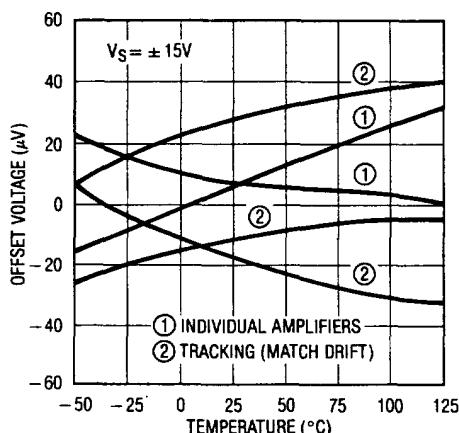
**Input Bias Current Over Common-Mode Range**



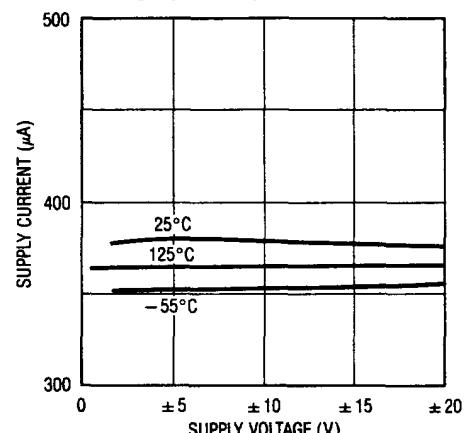
**Warm-Up Drift**



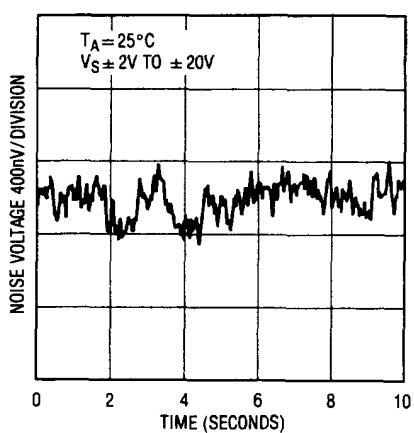
**Offset Voltage Drift and Tracking with Temperature of Representative Units**



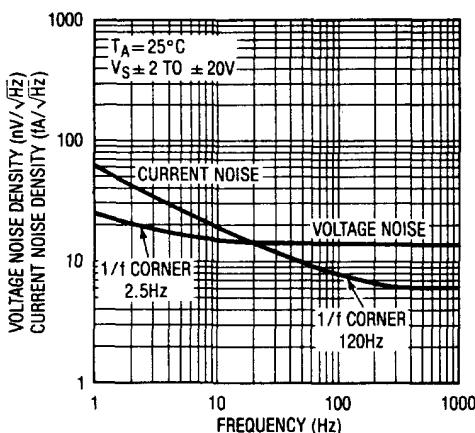
**Supply Current vs Supply Voltage per Amplifier**



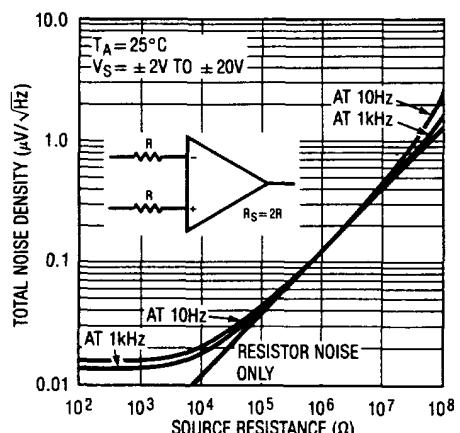
**0.1Hz to 10Hz Noise**



**Noise Spectrum**

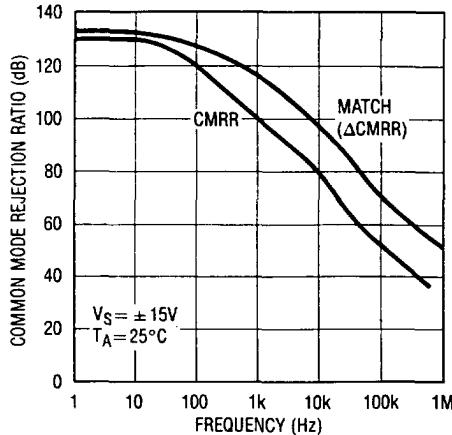


**Total Noise vs Source Resistance**

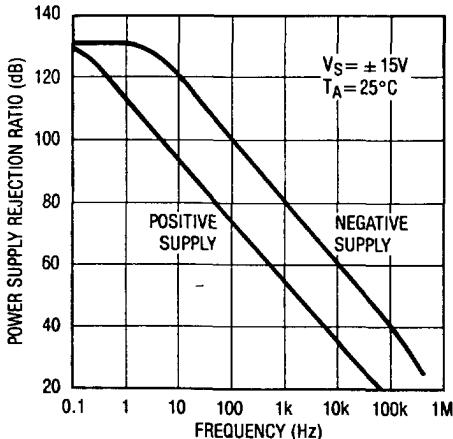


## TYPICAL PERFORMANCE CHARACTERISTICS

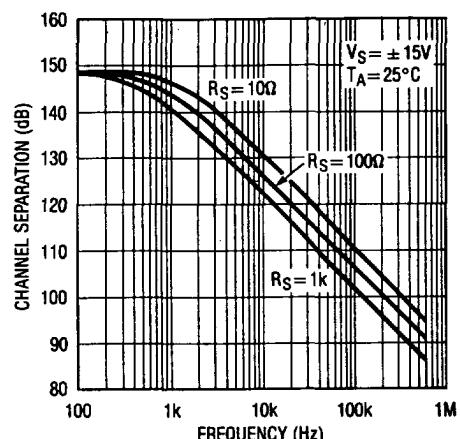
**Common-Mode Rejection and CMRR Match vs Frequency**



**Power Supply Rejection vs Frequency**

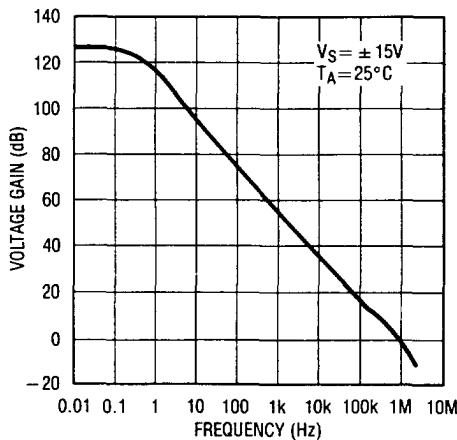


**Channel Separation vs Frequency**

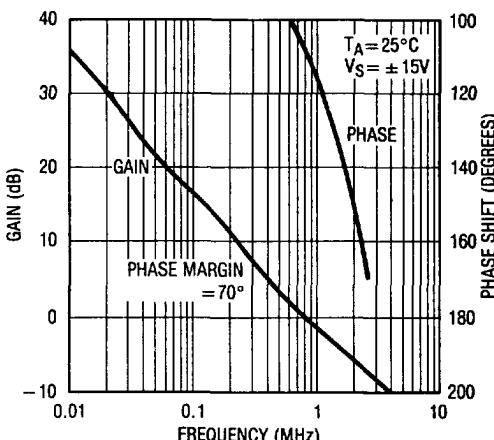


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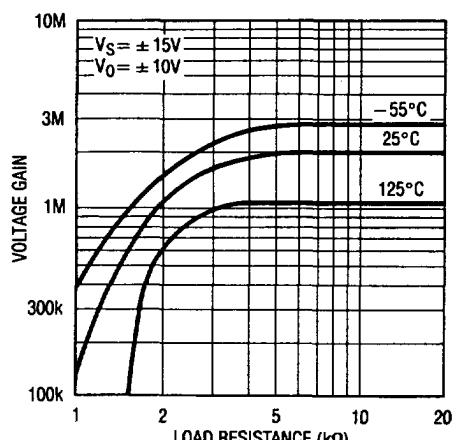
**Voltage Gain vs Frequency**



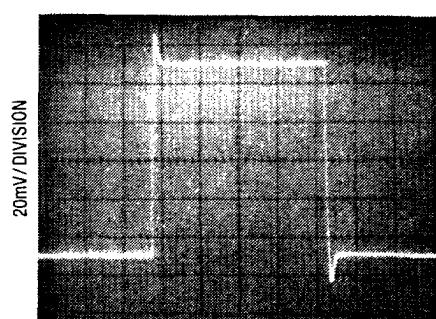
**Gain, Phase Shift vs Frequency**



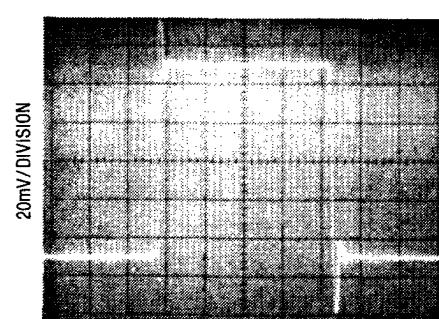
**Voltage Gain vs Load Resistance**



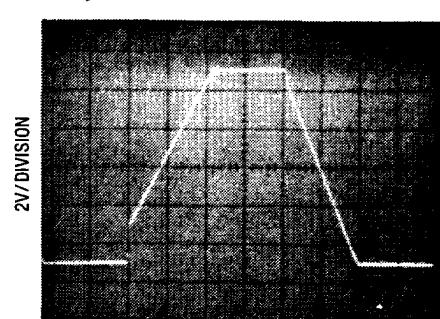
**Small Signal Transient Response**



**Small Signal Transient Response**



**Large Signal Transient Response**



**APPLICATIONS INFORMATION**

The LT1024 may be inserted directly into OP-10, OP-207 or OP227 sockets with or without removal of external nulling components.

The LT1024 is specified over a wide range of power supply voltages from  $\pm 2V$  to  $\pm 18V$ . Operation with lower supplies is possible down to  $\pm 1.2V$  (two NiCad batteries).

**Advantages of Matched Dual Op Amps**

In many applications, the performance of a system depends on the matching between two operational amplifiers rather than the individual characteristics of the two op amps. Two or three op amp instrumentation amplifiers, tracking voltage references, and low drift active filters are some of the circuits requiring matching between two op amps.

The well-known triple op amp configuration illustrates these concepts. Output offset is a function of the difference between the offsets of the two halves of the LT1024. This error cancellation principle holds for a considerable number of input-referred parameters in addition to offset voltage and its drift with temperature. Input bias current will be the average of the two non-inverting input currents ( $I_B^+$ ). The difference between these two cur-

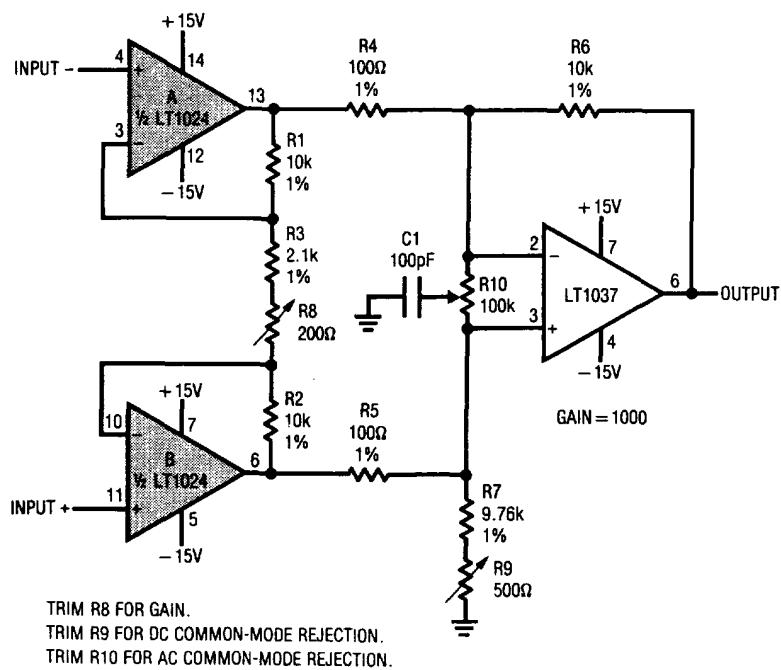
rents ( $I_{OS}^+$ ) is the offset current of the instrumentation amplifier. Common-mode and power supply rejections will be dependent only on the match between the two amplifiers (assuming perfect resistor matching).

The concepts of common-mode and power supply rejection ratio match ( $\Delta CMRR$  and  $\Delta PSRR$ ) are best demonstrated with a numerical example:

Assume  $CMRR_A = +1.0\mu V/V$  or  $120dB$  and  $CMRR_B = +0.5\mu V/V$  or  $126dB$ , then  $\Delta CMRR = 0.5\mu V/V$  or  $126dB$   
if  $CMRR_B = -0.5\mu V/V$ , which is still  $126dB$ , then  $\Delta CMRR = 1.5\mu V/V$  or  $116.5dB$ .

Typical performance of the instrumentation amplifier:  
Input offset voltage =  $25\mu V$ .  
Input bias current =  $30pA$ .  
Input resistance =  $10^{12}\Omega$ .  
Input offset current =  $30pA$ .  
Input noise =  $0.7\mu Vp-p$ .  
Power bandwidth ( $V_o = \pm 10V$ ) =  $80kHz$ .

Clearly, the LT1024, by specifying and guaranteeing all of these matching parameters, can significantly improve the performance of matching dependent circuits.

**Three Op Amp Instrumentation Amplifier**

## APPLICATIONS INFORMATION

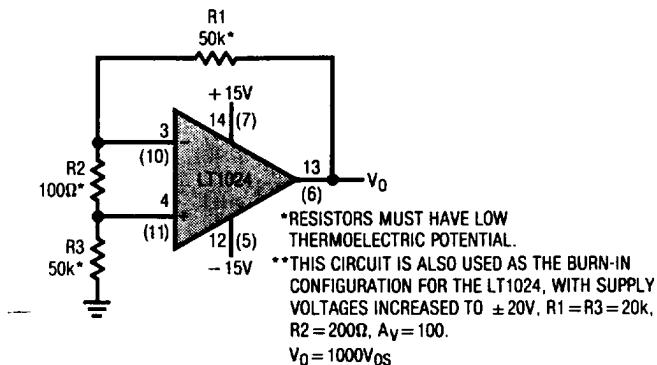
### Achieving Picoampere/Microvolt Performance

In order to realize the picoampere/microvolt level accuracy of the LT1024, proper care must be exercised. For example, leakage currents in circuitry external to the op amp can significantly degrade performance. High quality insulation should be used (e.g., Teflon, Kel-F); cleaning of all insulating surfaces to remove fluxes and other residues will probably be required. Surface coating may be necessary to provide a moisture barrier in high humidity environments.

Board leakage can be minimized by encircling the input circuitry with a guard ring operated at a potential close to that of the inputs: in inverting configurations, the guard ring should be tied to ground, in non-inverting connections, to the inverting input. Guarding both sides of the printed circuit board is required. Bulk leakage reduction depends on the guard ring width. Nanoampere level leakage into the offset trim terminals can affect offset voltage and drift with temperature.

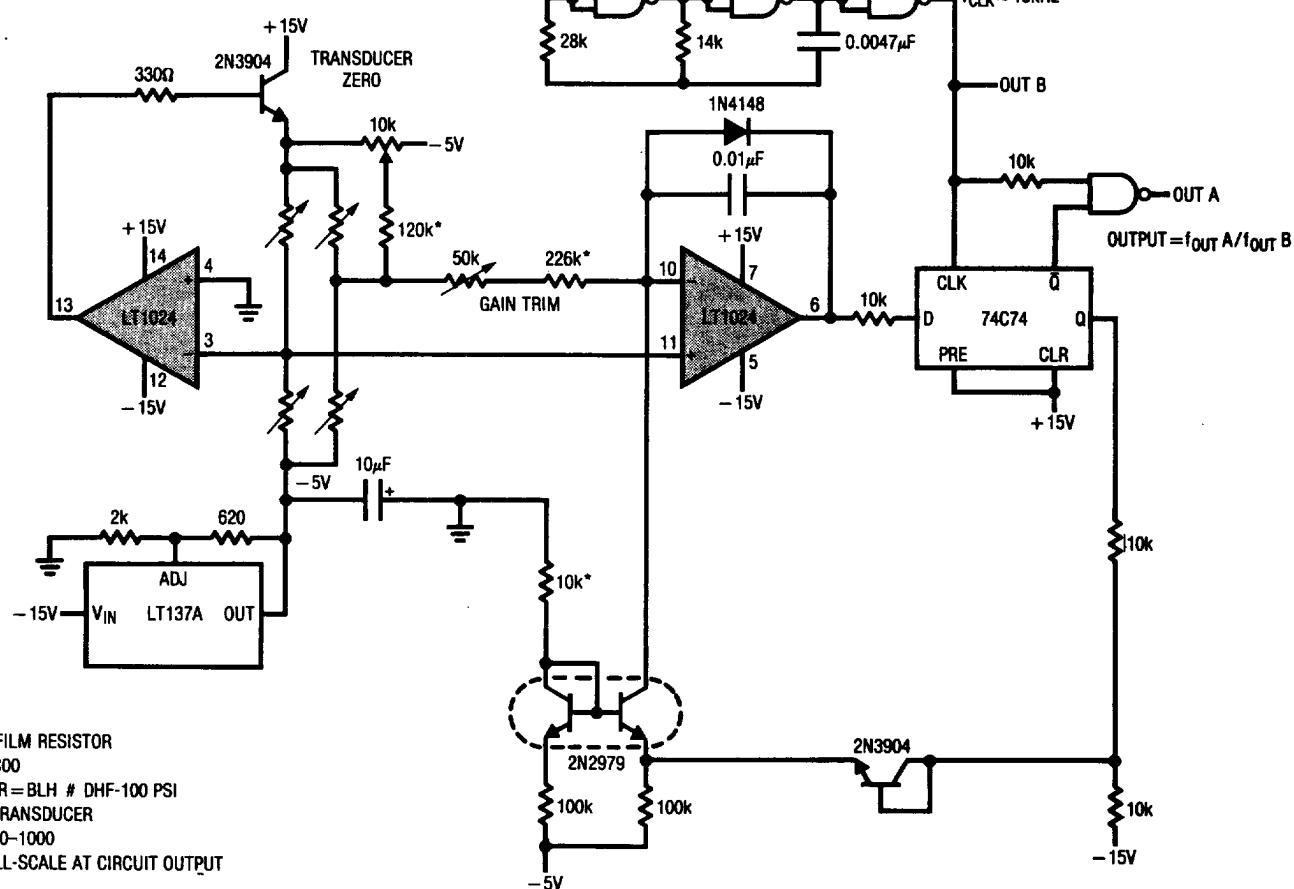
Microvolt level error voltages can also be generated in the external circuitry. Thermocouple effects caused by temperature gradients across dissimilar metals at the contacts to the input terminals can exceed the inherent drift of the amplifier. Air currents over device leads should be minimized, package leads should be short, and the two input leads should be as close together as possible and maintained at the same temperature.

### Test Circuit for Offset Voltage and its Drift with Temperature



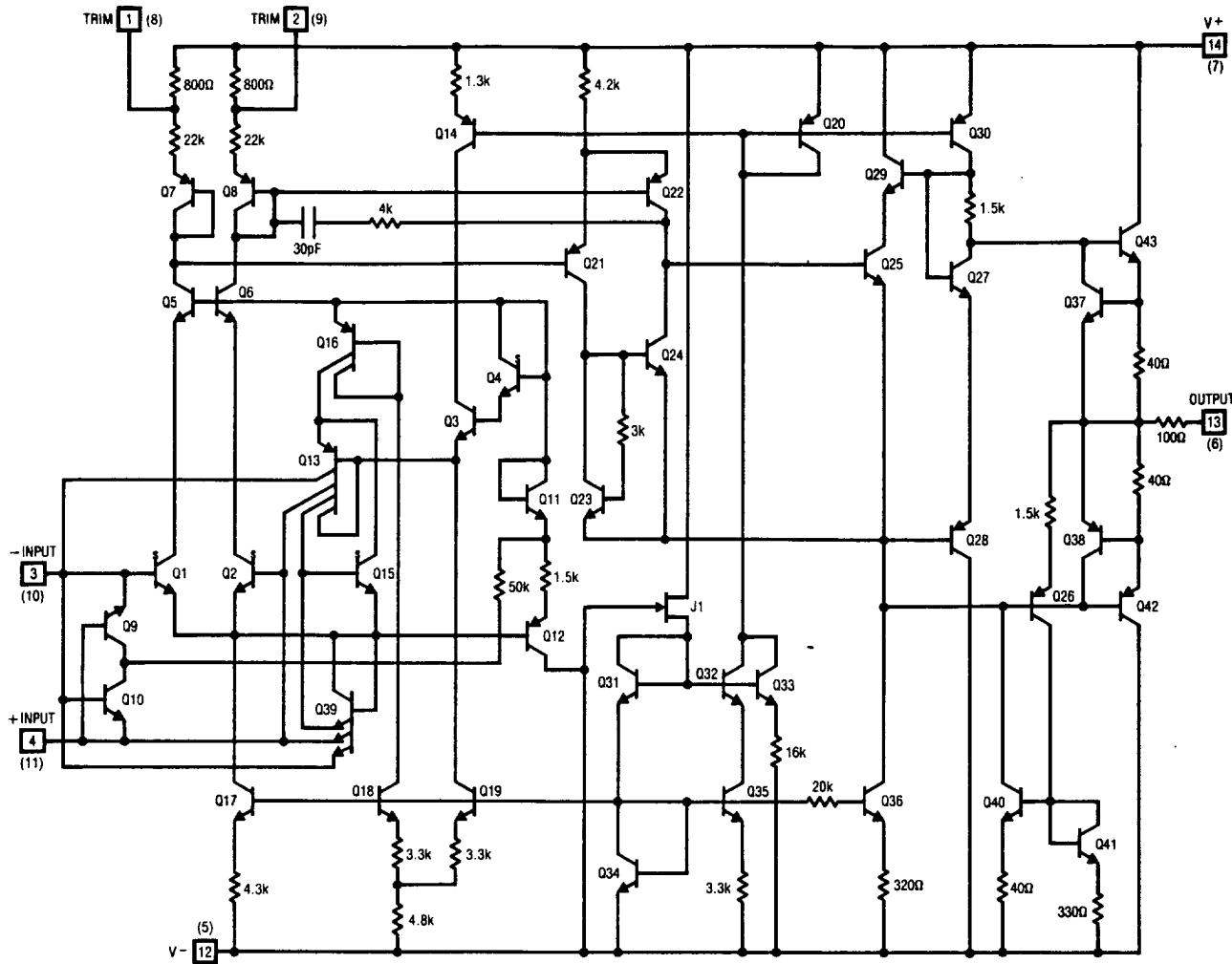
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### Direct Pressure Transducer to Digital Output Signal Conditioner



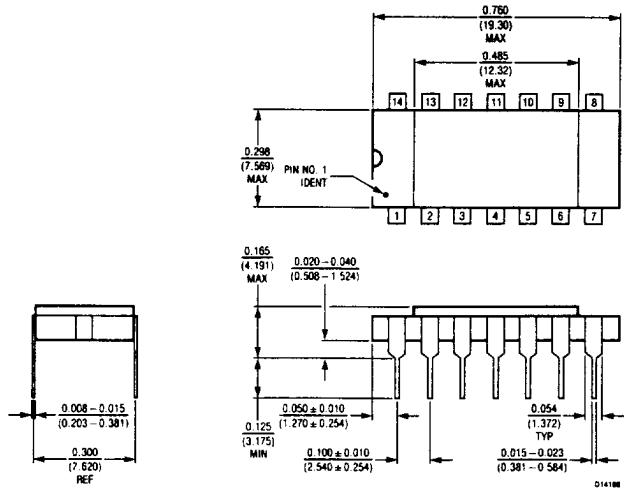
## SCHEMATIC DIAGRAM

1/2 LT1024



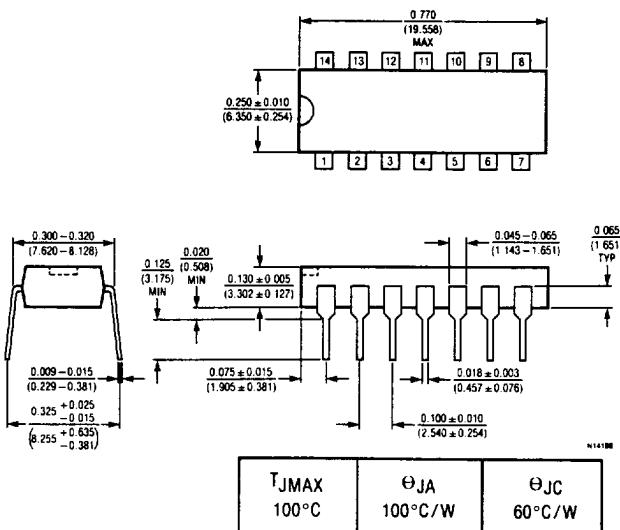
## PACKAGE DESCRIPTION

D14 Package 14-Lead Hermetic DIP (Sidebrazed)



T <sub>JMAX</sub> 150°C	θ <sub>JA</sub> 100°C/W	θ <sub>JC</sub> 60°C/W
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N14 Package 14-Lead Plastic



T <sub>JMAX</sub> 100°C	θ <sub>JA</sub> 100°C/W	θ <sub>JC</sub> 60°C/W
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