

Features

- Complete video level restoration system
- 0.02% differential gain and 0.05° differential phase accuracy at NTSC
- 60 MHz bandwidth
- 0.1 dB flatness to 10 MHz
- $V_S = \pm 5V$ to $\pm 15V$
- TTL/CMOS hold signal

Applications

- Input amplifier in video equipment
- Restoration amplifier in video mixers

Ordering Information

Part No.	Temp. Range	Package	Outline #
EL4089CN	0°C to +75°C	8-Pin P-DIP	MDP0031
EL4089CS	0°C to +75°C	8-Lead SO	MDP0027

General Description

The EL4089C is an 8-pin complete DC-restored monolithic video amplifier sub-system. It contains a high quality video amplifier and a nulling, sample-and-hold amplifier specifically designed to stabilize video performance.

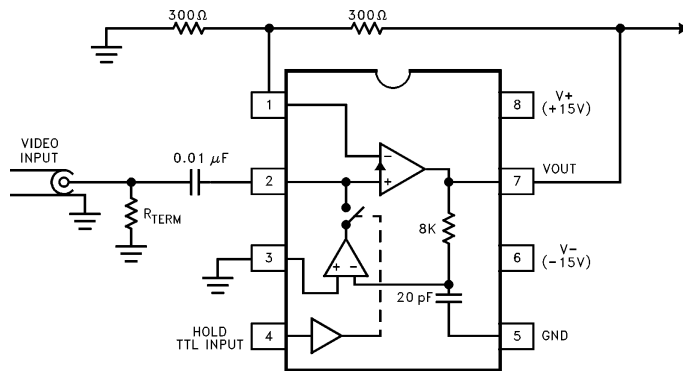
When the HOLD logic input is set to a TTL/CMOS logic 0, the sample- and-hold amplifier can be used to null the DC offset of the video amplifier.

When the HOLD input goes to a TTL/CMOS logic 1, the correcting voltage is stored on the video amplifier's input coupling capacitor. The correction voltage can be further corrected as need be, on each video line.

The video amplifier is optimized for video performance and low power. Its current feedback design allows the user to maintain essentially the same bandwidth over a gain range of nearly 10:1. The amplifier drives back-terminated 75Ω lines.

The EL4089C is fabricated in Elantec's proprietary Complementary Bipolar process which produces NPN and PNP transistors with equivalent AC and DC performance. The EL4089C is specified for operation over 0°C to +75°C temperature range.

Connection Diagram



DC restoring amplifier with a gain of 2, restoring to ground.

Note: All information contained in this data sheet has been carefully checked and is believed to be accurate as of the date of publication; however, this data sheet cannot be a "controlled document". Current revisions, if any, to these specifications are maintained at the factory and are available upon your request. We recommend checking the revision level before finalization of your design documentation.

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Absolute Maximum Ratings ($T_A = 25^\circ\text{C}$)

Voltage between V_+ and V_-	33V	Operating Ambient Temperature Range	0°C to $+75^\circ\text{C}$
Voltage between V_{IN+} , S/ H_{IN+} , and GND pins	$(V_+) + 0.5\text{V}$ to $(V_-) - 0.5\text{V}$	Operating Junction Temperature	150°C
V_{OUT} Current	60 mA	Plastic DIP or SOL	150°C
Current into V_{IN-} and HOLD Pins	5 mA	Storage Temperature Range	-65°C to $+150^\circ\text{C}$
Internal Power Dissipation	See Curves		

Important Note:

All parameters having Min/Max specifications are guaranteed. The Test Level column indicates the specific device testing actually performed during production and Quality inspection. Elantec performs most electrical tests using modern high-speed automatic test equipment, specifically the LTX77 Series system. Unless otherwise noted, all tests are pulsed tests, therefore $T_J = T_C = T_A$.

Test Level	Test Procedure
I	100% production tested and QA sample tested per QA test plan QCX0002.
II	100% production tested at $T_A = 25^\circ\text{C}$ and QA sample tested at $T_A = 25^\circ\text{C}$, T_{MAX} and T_{MIN} per QA test plan QCX0002.
III	QA sample tested per QA test plan QCX0002.
IV	Parameter is guaranteed (but not tested) by Design and Characterization Data.
V	Parameter is typical value at $T_A = 25^\circ\text{C}$ for information purposes only.

Open Loop DC Electrical Characteristics

Provisional Supplies at $\pm 15\text{V}$, Load = 1 k Ω ; $T_A = +25^\circ\text{C}$

Parameter	Description	Temp	Min	Typ	Max	Test Level	Units
Amplifier Section (HOLD = 5V)							
V_{OS}	Input Offset Voltage	$+25^\circ\text{C}$		12	25	II	mV
I_{b+}	IN+ Input Bias Current	$+25^\circ\text{C}$		1	5	II	μA
I_{b-}	IN- Input Bias Current	$+25^\circ\text{C}$		18	150	II	μA
R_{OL}	Transimpedance (Note 1)	$+25^\circ\text{C}$	180	800		II	k Ω
R_{IN-}	IN- Resistance	$+25^\circ\text{C}$		20		V	Ω
CMRR	Common Mode Rejection Ratio (Note 2)	$+25^\circ\text{C}$	44	60		II	dB
V_O	Output Voltage Swing	$+25^\circ\text{C}$	± 12	± 13		II	V
I_{SC}	Short Circuit Current (IN+ Only Driven to 0.5V)	$+25^\circ\text{C}$	45	100		II	mA
Restore Section							
$V_{OS, Comp}$	Composite Input Offset Voltage (Note 3)	$+25^\circ\text{C}$		3	7	II	mV
$I_{b+,r}$	Restore IN+ Input Bias Current	$+25^\circ\text{C}$		3	12	II	μA
I_{OUT}	Restoring Current Available	$+25^\circ\text{C}$	180	300		II	μA
CMRR	Common Mode Rejection Ratio (Note 2)	$+25^\circ\text{C}$	60	70		II	dB

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Open Loop DC Electrical Characteristics — Contd.

Provisional Supplies at $\pm 15V$, Load = 1 k Ω ; $T_A = +25^\circ C$

Parameter	Description	Temp	Min	Typ	Max	Test Level	Units
Restore Section —Contd.							
PSRR	Power Supply Rejection Ratio (Note 4)	+25°C	60	90		II	dB
V _{THRESHOLD}	HOLD Logic Threshold	+25°C	0.8		2.0	II	V
I _{IH, Hold}	HOLD Input Current @ Logic High	+25°C		1	5	II	μA
I _{IL, Hold}	HOLD Input Current @ Logic Low	+25°C		5	15	II	μA
Supply Current							
I _{sy, Hold}	Supply Current (HOLD = 5V)	+25°C	4.8	6.0	9.0	II	mA
I _{sy, Sampling}	Supply Current (HOLD = 0V)	+25°C	5.0	6.5	11.0	II	mA

Closed Loop AC Electrical Characteristics

Provisional Supplies at $\pm 15V$, Load = 150 Ω and 15 pF. R_f and $R_g = 300\Omega$; $A_V = 2$, $T_A = 25^\circ C$. (See Note 7 about Test Fixture)

Parameter	Description	Min	Typ	Max	Test Level	Units
Amplifier Section						
SR	Slew Rate (Note 5)		500		V	V/ μs
SR	Slew Rate with $\pm 5V$ Supplies (Note 5)		275		V	V/ μs
BW	Bandwidth $\pm 5V$ Supplies	-3 dB	60		V	MHz
		-3 dB	55		V	MHz
BW	Bandwidth $\pm 5V$ Supplies	± 0.1 dB	25		V	MHz
		± 0.1 dB	23		V	MHz
dG	Differential Gain at 3.58 MHz (Note 6)	$V_S = \pm 15V$	0.02		V	%
		$V_S = \pm 5V$	0.03		V	%
dPh	Differential Phase at 3.58 MHz (Note 6)	$V_S = \pm 15V$	0.05		V	°
		$V_S = \pm 5V$	0.06		V	°
Restore Section						
SR	Restore Amplifier Slew Rate (Test Circuit) 20%–80%		25		V	V/ μs
T _{HE}	Time to Enable Hold		25		V	ns
T _{HD}	Time to Disable Hold		40		V	ns

Note 1: For current feedback amplifiers, $A_{VOL} = R_{OL}/R_{IN}$.

Note 2: $V_{CM} = \pm 10V$ for $V_S = \pm 15V$.

Note 3: Measured from S/H Input to amplifier output, while restoring.

Note 4: V_{OS} is measured at $V_S = \pm 4.5V$ and $V_S = \pm 16V$, both supplies are changed simultaneously.

Note 5: SR measured at 20% to 80% of a 4V pk-pk square wave.

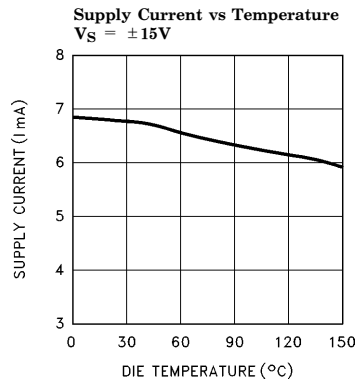
Note 6: DC offset from $-0.714V$ through $+0.714V$, ac amplitude is 286 mVp-p, equivalent to 40 ire.

Note 7: Test fixture was designed to minimize capacitance at the IN- input. A "good" fixture should have less than 2 pF of stray capacitance to ground at this very sensitive pin. See application notes for further details.

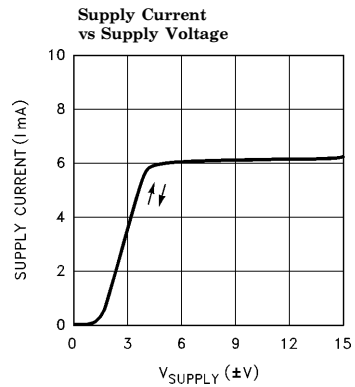
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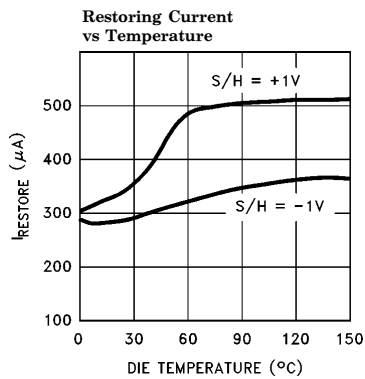
Typical Performance Curves



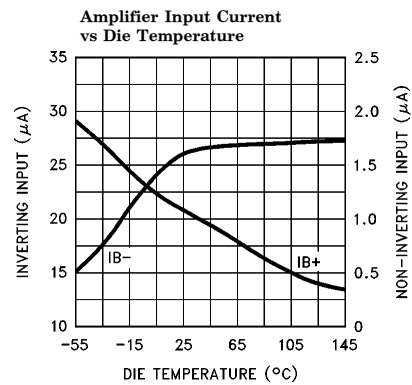
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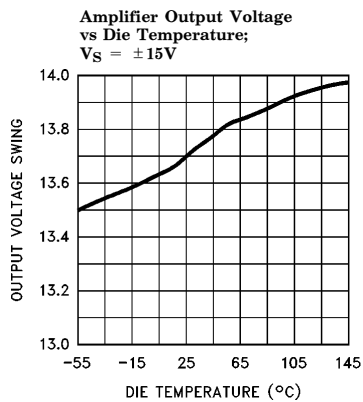
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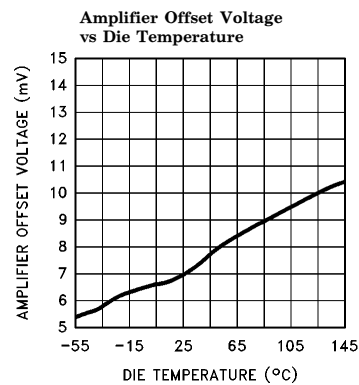
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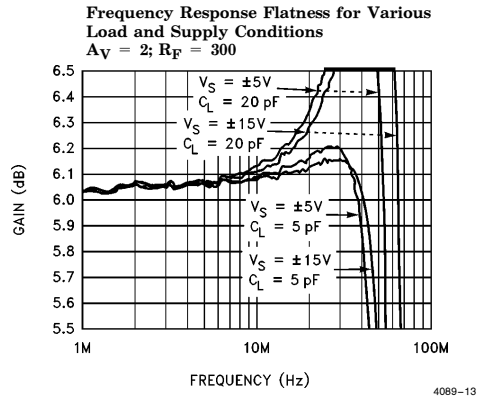
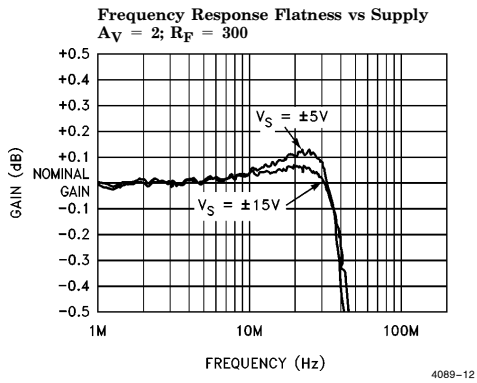
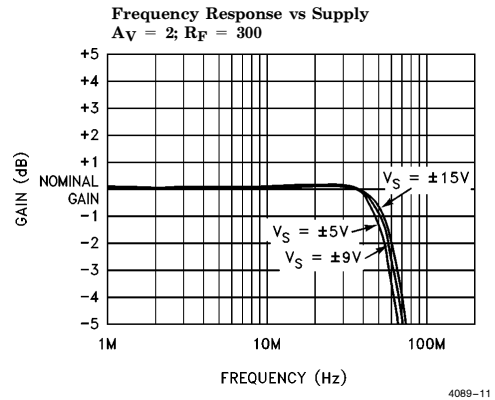
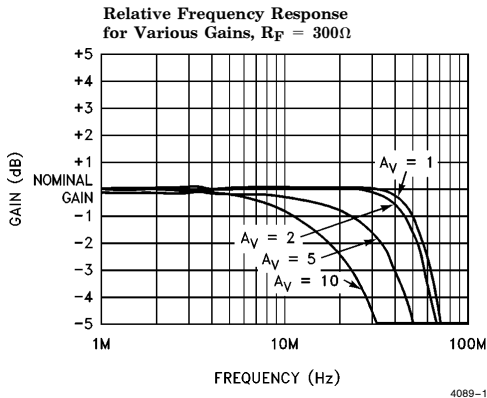
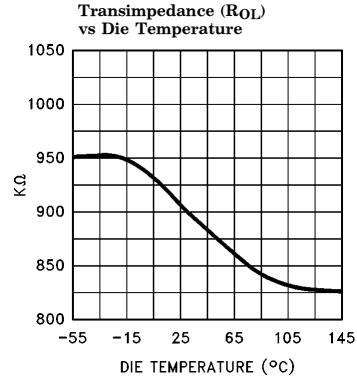
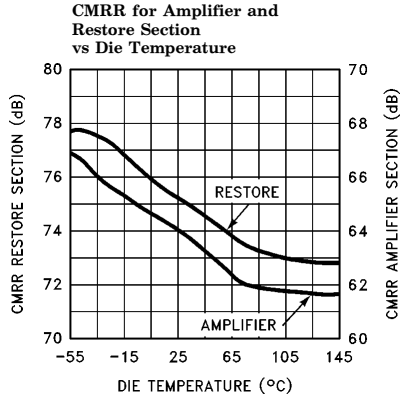


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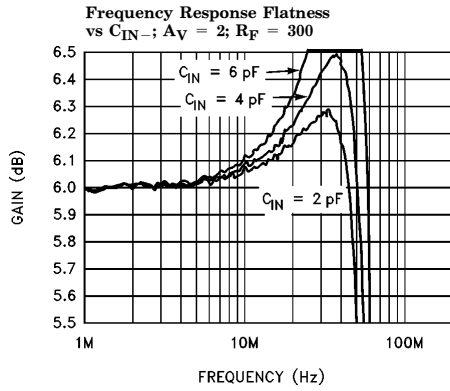
Typical Performance Curves — Contd.



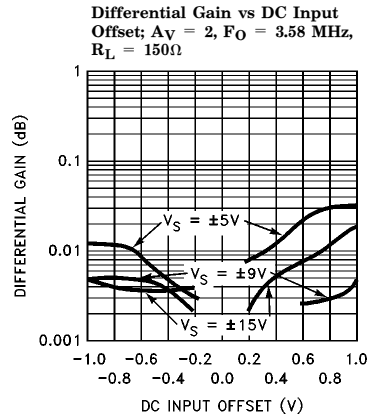
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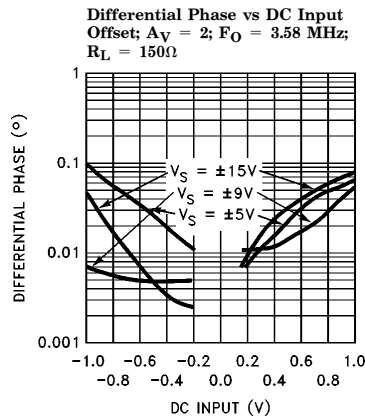
Typical Performance Curves — Contd.



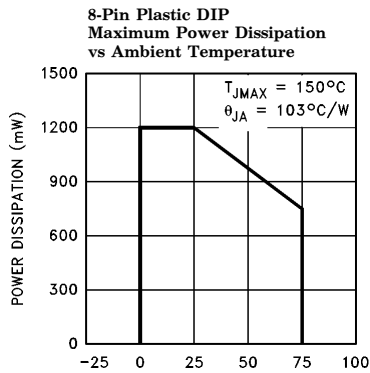
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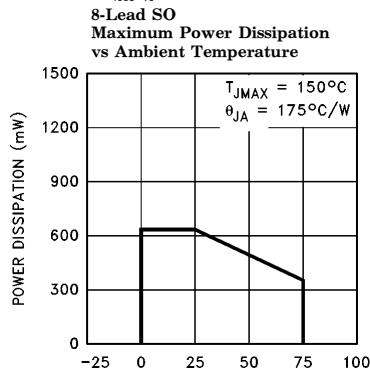
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Typical Application

The EL4089 can be used to DC-restore a video waveform (see Fig. 1). The above circuit forces the cable driving video amplifier's output to ground when the HOLD pin is at a logic low.

The "correction voltage" is stored on capacitor CX1, an external ceramic capacitor. The capacitor value is chosen from the system requirements. The typical input bias current to the video amplifier is 1 μA , so for a 62 μs hold time, and a 0.01 μF capacitor, the output voltage drift is 6.2 mV in one line.

The S/H amplifier can provide a typical current of 300 μA to charge capacitor CX1, so with a 1.2 μs sampling time, the output can be corrected by 36 mV in each line.

Using a smaller value of CX1 increases both the voltage that can be corrected, and the drift while being held, likewise, using a larger value of CX1, reduces the voltages.

The RX1 resistor is in the circuit purely to simulate some external source impedance, and is not needed as a real component. Likewise for RX2. The 75 Ω back terminating resistor RXT is recommended when driving 75 Ω cables.

The board layout should have a ground plane underneath the EL4089, with the ground plane cut away from the vicinity of the $V_{\text{IN-}}$ pin, (pin 1). This helps to minimize the stray capacitance on pin 1.

Power supply bypassing is important, and a 0.1 μF ceramic capacitor, from each power pin to ground, placed very close to the power pins, together with a 4.7 μF tantalum bead capacitor, is recommended.

When both digital and Analog grounds are on the same board, the EL4089 should be on the Analog ground. The digital ground can be connected to the Analog ground through a 100 Ω –300 Ω resistor, near the EL4089. This allows the digital signal a return path, while preventing the digital noise from corrupting the analog ground.

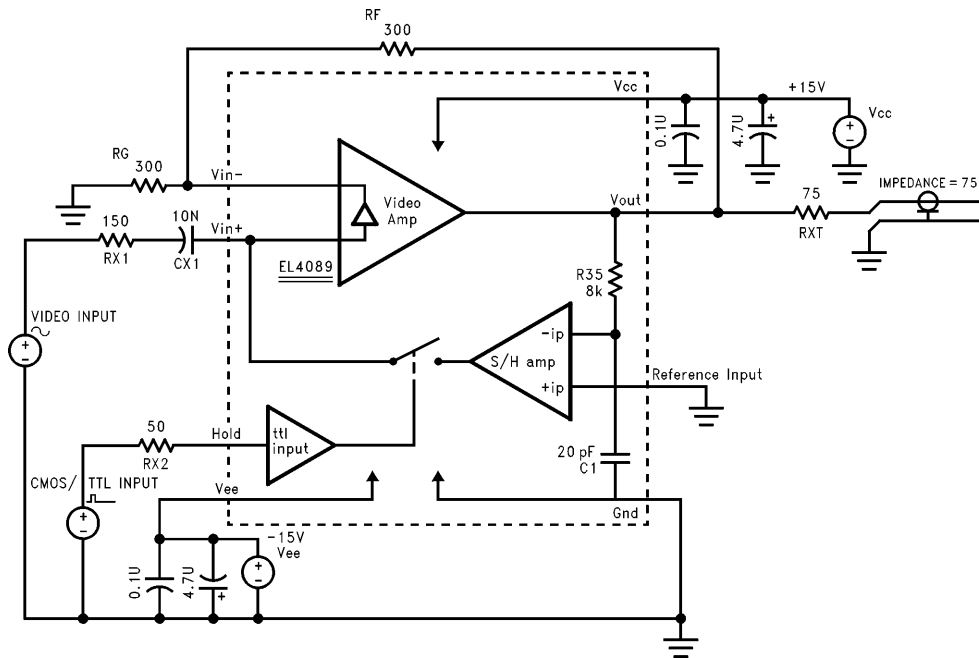


Figure 1

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Table of Charge Storage Capacitor vs Droop Charging Rates

Cap Value nF	Droop in 60 μ s mV	Charge in 1.2 μ s mV	Charge in 4 μ s mV
10	6	36	120
33	1.8	11	36
100	0.6	3.6	12

Basic formulae are:

$$V(\text{droop}) = I_{b+} * (\text{Line time} - \text{Sample time}) / \text{Capacitor}$$

$$\text{and } V(\text{charge}) = I_{OUT} * \text{Sample time} / \text{Capacitor}$$

For best results the source impedance should be kept low, using a buffer for example.

Because the S/H effectively shorts the input signal during Sample, the input should not be sam-

pled during active video. Typically the sample is made during the back porch period of horizontal blanking. For this reason color composite signals, which have color burst on the back porch, can not be passed. See EL2090 or EL4093 for this application.

General Disclaimer

Specifications contained in this data sheet are in effect as of the publication date shown. Elantec, Inc. reserves the right to make changes in the circuitry or specifications contained herein at any time without notice. Elantec, Inc. assumes no responsibility for the use of any circuits described herein and makes no representations that they are free from patent infringement.

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