

## 3A, 21V 500kHz Synchronous Step-Down Converter

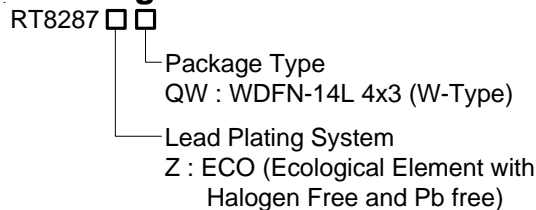
### General Description

The RT8287 is a synchronous step-down regulator with an internal power MOSFET. It achieves 3A of continuous output current over a wide input supply range with excellent load and line regulation. Current mode operation provides fast transient response and eases loop stabilization.

Fault condition protection includes cycle-by-cycle current limiting and thermal shutdown. An adjustable soft-start reduces the stress on the input source at startup.

The RT8287 requires a minimal number of readily available external components, providing a compact solution.

### Ordering Information

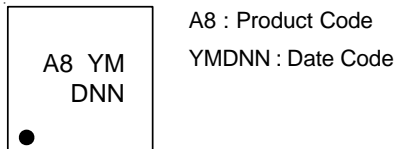


Note :

Richtek products are :

- ▶ RoHS compliant and compatible with the current requirements of IPC/JEDEC J-STD-020.
- ▶ Suitable for use in SnPb or Pb-free soldering processes.

### Marking Information



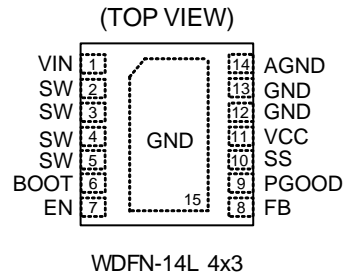
### Features

- 3A Output Current
- Adjustable Soft-Start
- 120mΩ/40mΩ Internal Power MOSFET Switch
- Internal Compensation Minimizes External Parts Count
- Fixed 500kHz Frequency
- Thermal Shutdown Protection
- Cycle-by-Cycle Over Current Protection
- Wide 4.5V to 21V Operating Input Range
- Adjustable Output from 0.808V to 15V
- Small 14-Lead WDFN Package
- RoHS Compliant and Halogen Free

### Applications

- Distributive Power Systems
- Battery Charger
- DSL Modems
- Pre-Regulator for Linear Regulators

### Pin Configurations



## Typical Application Circuit

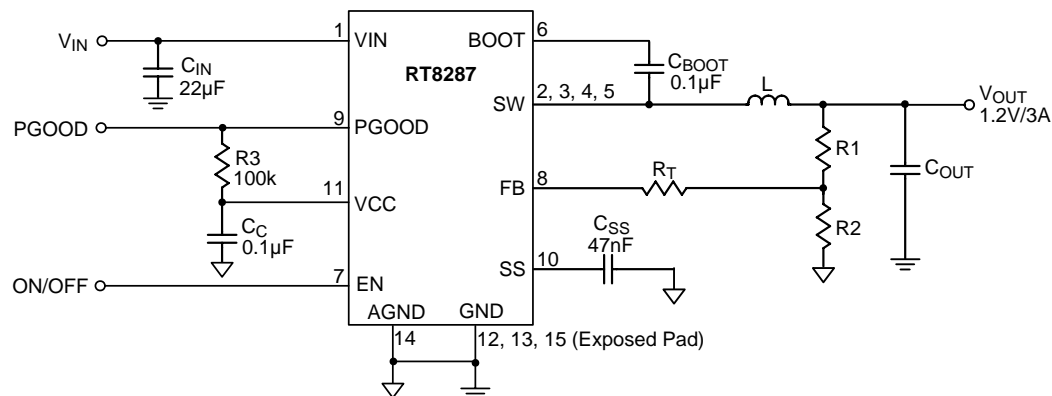


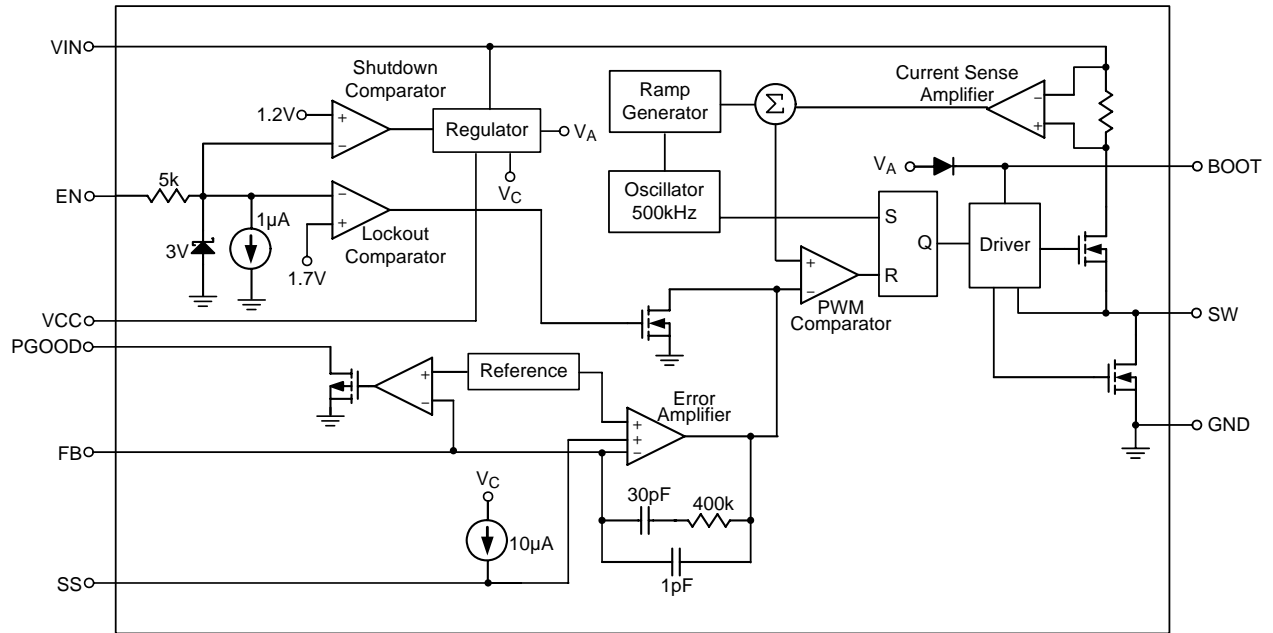
Table 1. Recommended Components Selection

V <sub>OUT</sub> (V)	R <sub>1</sub> (kΩ)	R <sub>2</sub> (kΩ)	R <sub>T</sub> (kΩ)	L (μH)	C <sub>OUT</sub> (μF)
5	75	14.46	0	4.7	22 x 2
3.3	75	24.32	0	3.6	22 x 2
2.5	75	35.82	0	3.6	22 x 2
1.8	5	4.07	30	2	22 x 2
1.5	5	5.84	39	2	22 x 2
1.2	5	10.31	47	2	22 x 2
1.05	5	16.69	47	1.5	22 x 2

## Function Pin Description

Pin No.	Pin Name	Pin Function
1	VIN	Supply Input. VIN supplies the power to the IC, as well as the step-down converter switches. Drive VIN with a 4.5V to 21V power source. Bypass VIN to GND with a suitably large capacitor to eliminate noise on the input to the IC.
2, 3, 4, 5	SW	Switch Node. SW is the switching node that supplies power to the output. Connect the output LC filter from SW to the output load. Note that a capacitor is required from SW to BOOT to power the high side switch.
6	BOOT	High Side Gate Drive Boost Input. BOOT supplies the drive for the high side N-MOSFET switch. Connect a 100nF or greater capacitor from SW to BOOT to power the high side switch.
7	EN	Chip Enable (Active High). For automatic start-up, connect the EN pin to VIN with a 100kΩ resistor.
8	FB	Feedback Input. FB senses the output voltage to regulate said voltage. Drive FB with a resistive voltage divider from the output voltage. The feedback threshold is 0.808V.
9	PGOOD	Power Good Output. The output of this pin is open-drain. Power good threshold is 90% low to high and 70% high to low of regulation value.
10	SS	Soft-Start Control Input. SS controls the soft-start period. Connect a capacitor from SS to GND to set the soft-start period.
11	VCC	Bias Supply. Decouple with 0.1μF to 0.22μF capacitor. The capacitance should be no more than 0.22μF.
12, 13 15 (Exposed Pad)	GND	Ground. The exposed pad must be soldered to a large PCB and connected to GND for maximum power dissipation.
14	AGND	Analog Ground. Connect this pin to the system ground in PCB layout.

**Function Block Diagram**



## Absolute Maximum Ratings (Note 1)

- Supply Input Voltage,  $V_{IN}$  ----- -0.3V to 26V
- Switch Voltage, SW ----- -0.3V to ( $V_{IN} + 0.3V$ )
- Boot Voltage, BOOT ----- ( $SW - 0.3V$ ) to ( $SW + 6V$ )
- All Other Pins ----- -0.3V to 6V
- Power Dissipation,  $P_D$  @  $T_A = 25^\circ C$   
 WDFN-14L 4x3 ----- 1.667W
- Package Thermal Resistance (Note 2)  
 WDFN-14L 4x3,  $\theta_{JA}$  -----  $60^\circ C/W$   
 WDFN-14L 4x3,  $\theta_{JC}$  -----  $7^\circ C/W$
- Junction Temperature -----  $150^\circ C$
- Lead Temperature (Soldering, 10 sec.) -----  $260^\circ C$
- Storage Temperature Range -----  $-65^\circ C$  to  $150^\circ C$
- ESD Susceptibility (Note 3)  
 HBM ----- 2kV  
 MM ----- 200V

## Recommended Operating Conditions (Note 4)

- Supply Input Voltage,  $V_{IN}$  ----- 4.5V to 21V
- Junction Temperature Range -----  $-40^\circ C$  to  $125^\circ C$
- Ambient Temperature Range -----  $-40^\circ C$  to  $85^\circ C$

## Electrical Characteristics

( $V_{IN} = 12V$ ,  $T_A = 25^\circ C$  unless otherwise specified)

Parameter		Symbol	Test Conditions	Min	Typ	Max	Unit
Shutdown Current		$I_{SHDN}$	$V_{EN} = 0$	--	0	1	$\mu A$
Quiescent Current		$I_Q$	$V_{EN} = 2V$ , $V_{FB} = 1V$	--	0.7	--	mA
Upper Switch On Resistance		$R_{DS(ON)1}$		--	120	--	m $\Omega$
Lower Switch On Resistance		$R_{DS(ON)2}$		--	40	--	m $\Omega$
Switch Leakage		$I_{LEAK}$	$V_{EN} = 0V$ , $V_{SW} = 0V$ or $12V$	--	0	10	$\mu A$
Current Limit		$I_{LIMIT}$	$V_{BOOT} - V_{SW} = 4.8V$	5.4	6.5	--	A
Oscillator Frequency		$f_{SW}$	$V_{FB} = 0.75V$	425	500	575	kHz
Short Circuit Frequency			$V_{FB} = 0V$	--	150	--	kHz
Maximum Duty Cycle		$D_{MAX}$	$V_{FB} = 0.8V$	--	90	--	%
Minimum On Time		$t_{ON}$		--	100	--	ns
Feedback Voltage		$V_{FB}$	$4.5V \leq V_{IN} \leq 21V$	0.796	0.808	0.82	V
Feedback Current		$I_{FB}$		--	10	50	nA
EN Threshold Voltage	Logic-High	$V_{IH}$		2	--	5.5	V
	Logic-Low	$V_{IL}$		--	--	0.4	
Enable Current			$V_{EN} = 2V$	--	1	--	$\mu A$
			$V_{EN} = 0V$	--	0	--	

To be continued

Parameter	Symbol	Test Conditions	Min	Typ	Max	Unit
Power Good Rising Threshold			--	90	--	%
Power Good Falling Threshold			--	70	--	%
Power Good Delay			--	20	--	μs
Power Good Sink Current Capability		Sink 4mA	--	--	0.4	V
Power Good Leakage Current			--	10	--	nA
Under Voltage Lockout Threshold	V <sub>UVLO</sub>	V <sub>IN</sub> Rising	3.8	4	4.2	V
Under Voltage Lockout Threshold Hysteresis	ΔV <sub>UVLO</sub>		--	400	--	mV
VCC Regulator			--	5	--	V
VCC Load Regulation		I <sub>CC</sub> = 5mA	--	5	--	%
Soft-Start Period	t <sub>SS</sub>	C <sub>SS</sub> = 47nF	--	4.7	--	ms
Thermal Shutdown	T <sub>SD</sub>		--	150	--	°C

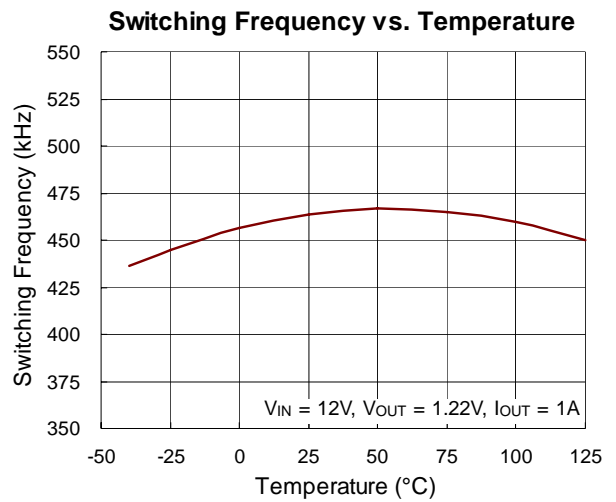
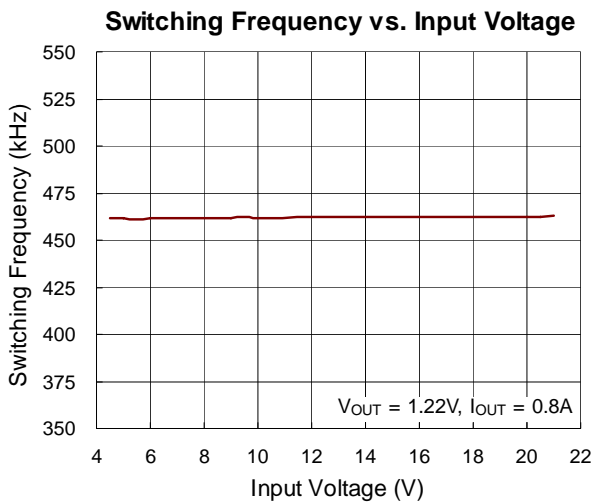
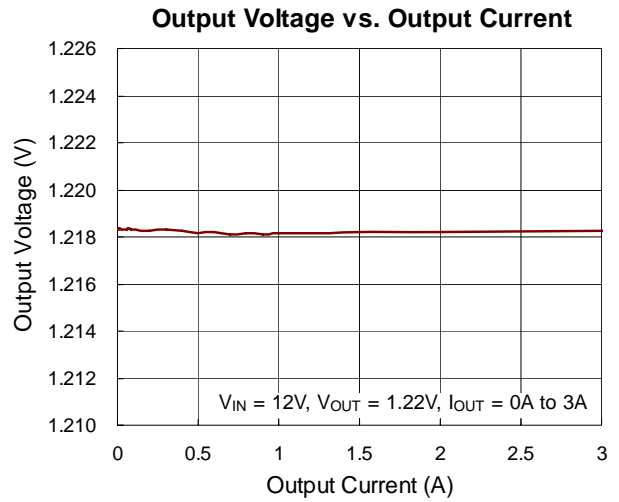
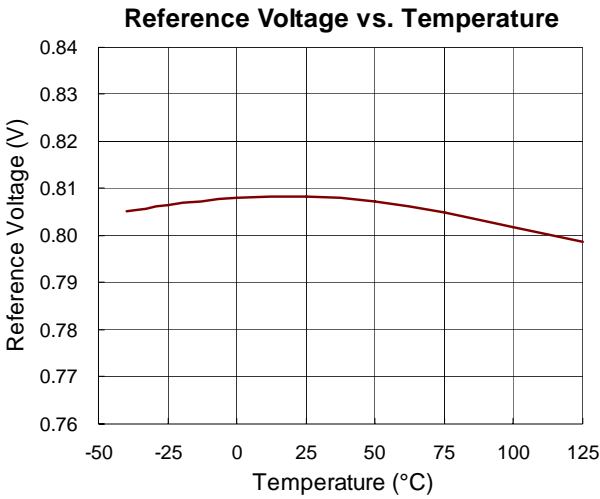
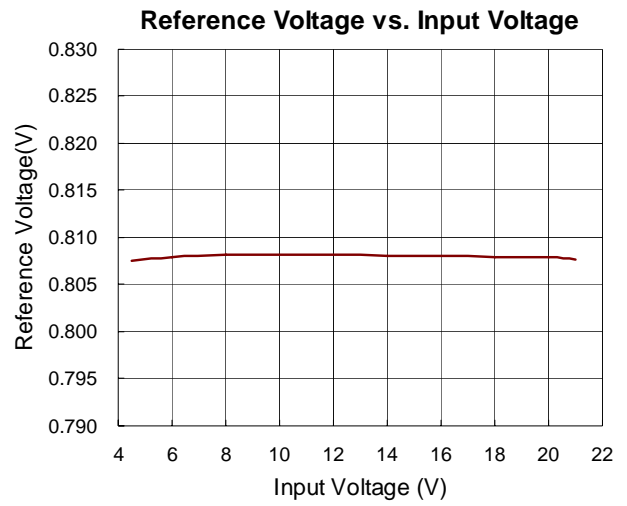
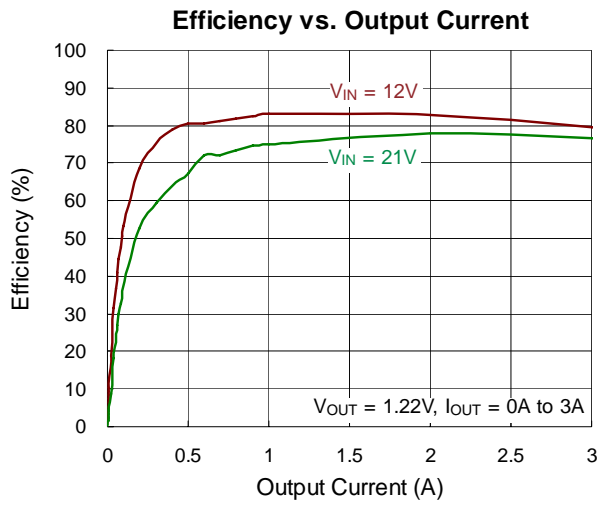
**Note 1.** Stresses listed as the above “Absolute Maximum Ratings” may cause permanent damage to the device. These are for stress ratings. Functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may remain possibility to affect device reliability.

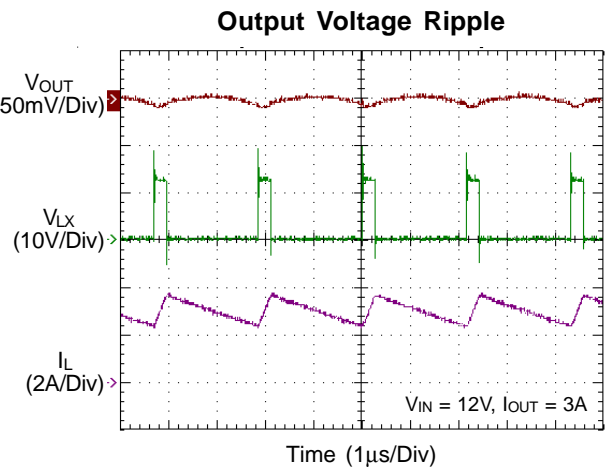
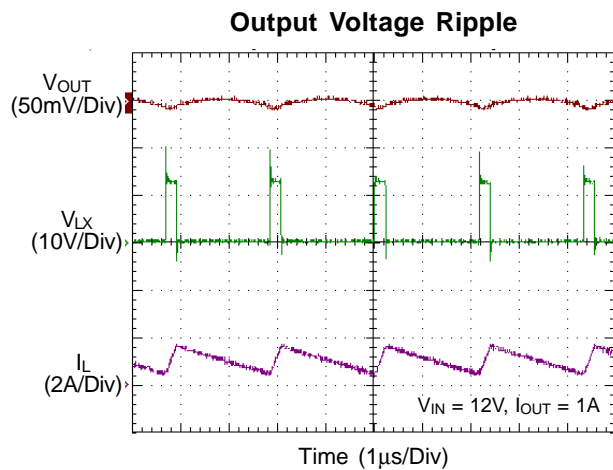
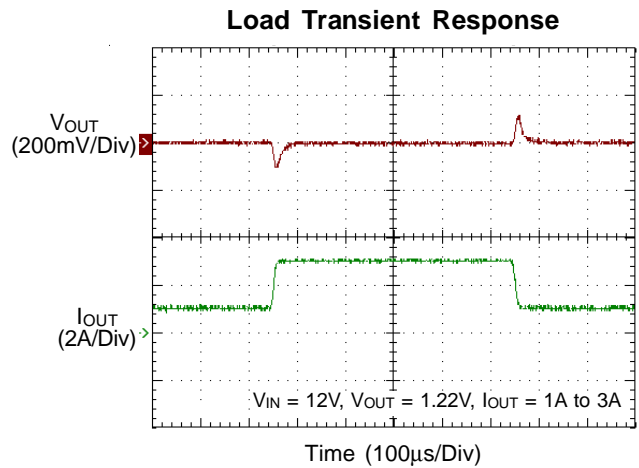
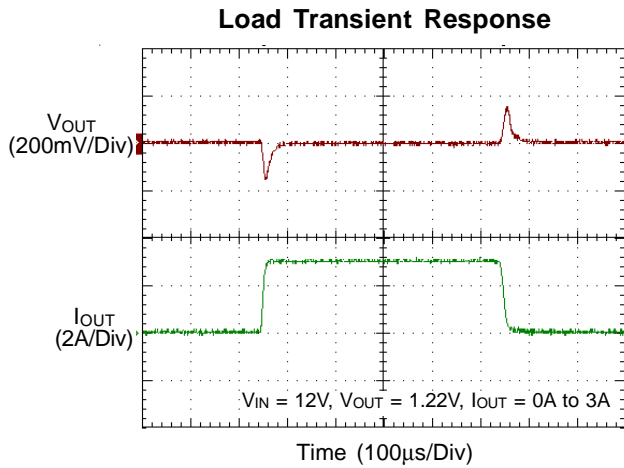
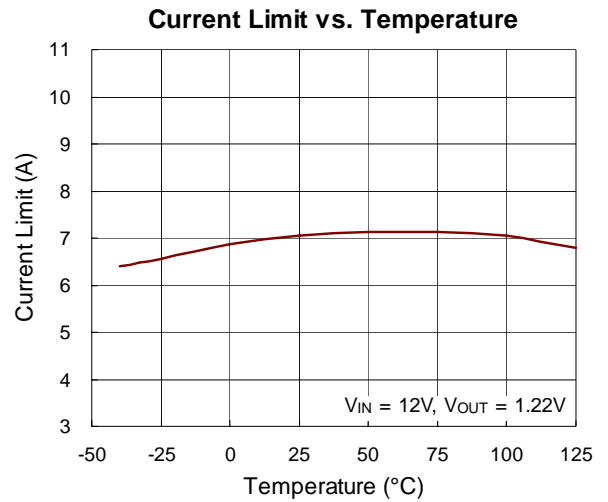
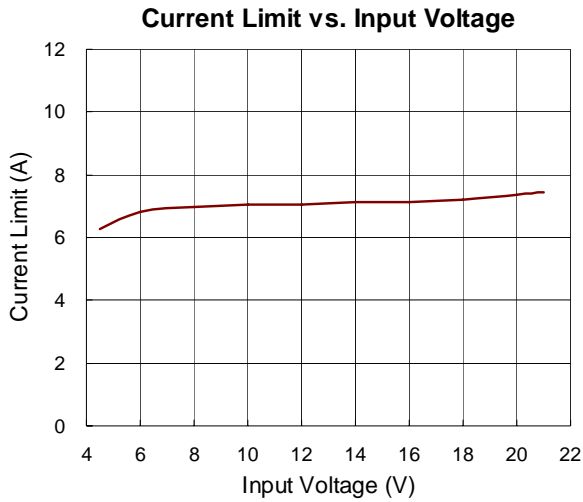
**Note 2.** θ<sub>JA</sub> is measured in natural convection at T<sub>A</sub> = 25°C on a high-effective thermal conductivity four-layer test board of JEDEC 51-7 thermal measurement standard. The measurement case position of θ<sub>JC</sub> is on the exposed pad of the package.

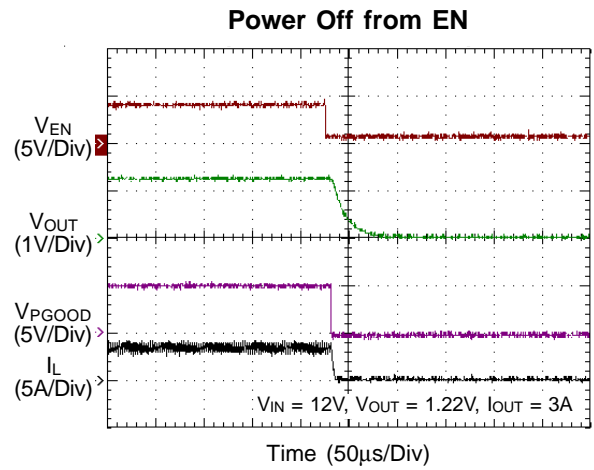
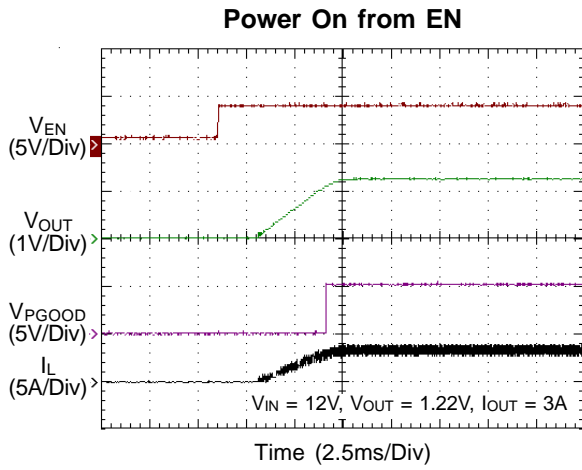
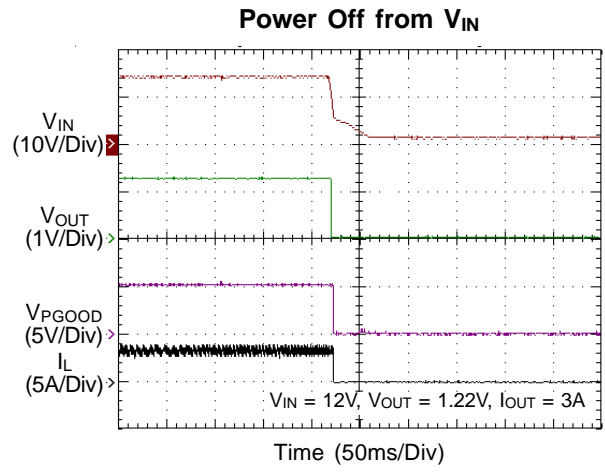
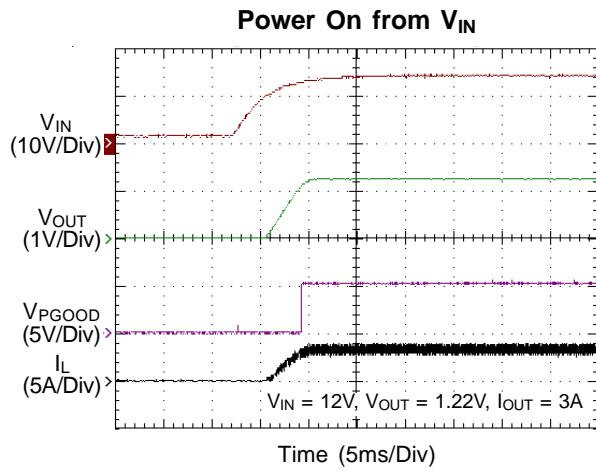
**Note 3.** Devices are ESD sensitive. Handling precaution is recommended.

**Note 4.** The device is not guaranteed to function outside its operating conditions.

Typical Operating Characteristics









### Application Information

The IC is a synchronous high voltage buck converter that can support the input voltage range from 4.5V to 21V and the output current can be up to 3A.

#### Output Voltage Setting

The output voltage is set by an external resistive divider according to the following equation :

$$V_{OUT} = V_{FB} \left( 1 + \frac{R1}{R2} \right)$$

where  $V_{FB}$  is the feedback reference voltage 0.808V (typ.).

The resistive divider allows the FB pin to sense a fraction of the output voltage as shown in Figure 1.

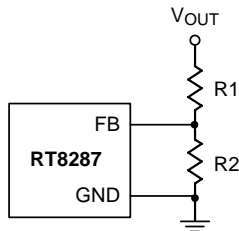


Figure 1. Output Voltage Setting

#### External Bootstrap Diode

Connect a 100nF low ESR ceramic capacitor between the BOOT pin and SW pin as shown in Figure 2. This capacitor provides the gate driver voltage for the high side MOSFET. It is recommended to add an external bootstrap diode between an external 5V and BOOT pin for efficiency improvement when input voltage is lower than 5.5V or duty ratio is higher than 65% .The bootstrap diode can be a low cost one such as IN4148 or BAT54. The external 5V can be a 5V fixed input from system or a 5V output of the IC. Note that the external boot voltage must be lower than 5.5V.

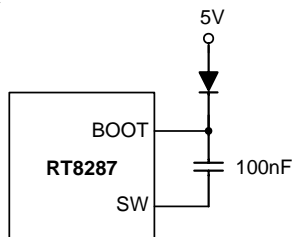


Figure 2. External Bootstrap Diode

#### Soft-Start

The IC contains an external soft-start clamp that gradually raises the output voltage. The soft-start timing is programmed by the external capacitor between SS pin and GND. The chip provides an internal 10µA charge current for the external capacitor. If 47nF capacitor is used to set the soft-start, the period will be 4.7ms (typ.).

#### Under Voltage Lockout Threshold

The IC includes an input Under Voltage Lockout Protection (UVLO). If the input voltage exceeds the UVLO rising threshold voltage (4.2V), the converter resets and prepares the PWM for operation. If the input voltage falls below the UVLO falling threshold voltage (3.8V) during normal operation, the device stops switching. The UVLO rising and falling threshold voltage includes a hysteresis to prevent noise caused reset.

#### Chip Enable Operation

The EN pin is the chip enable input. Pulling the EN pin low (<0.4V) will shut down the device. During shutdown mode, the IC quiescent current drops to lower than 1µA. Driving the EN pin high (>2V, < 5.5V) will turn on the device again. For external timing control (e.g.RC), the EN pin can also be externally pulled high by adding a  $R_{EN}^*$  resistor and  $C_{EN}^*$  capacitor from the VIN pin, as can be seen from the Figure 5.

An external MOSFET can be added to implement digital control on the EN pin when front age system voltage below 2.5V is available, as shown in Figure 3. In this case, a 100kΩ pull-up resistor,  $R_{EN}$ , is connected between  $V_{IN}$  and the EN pin. MOSFET Q1 will be under logic control to pull down the EN pin.

To prevent enabling circuit when  $V_{IN}$  is smaller than the  $V_{OUT}$  target value, a resistive voltage divider can be placed between the input voltage and ground and connected to the EN pin to adjust IC lockout threshold, as shown in Figure 4. For example, if an 8V output voltage is regulated from a 12V input voltage, the resistor  $R_{EN2}$  can be selected to set input lockout threshold larger than 8V.

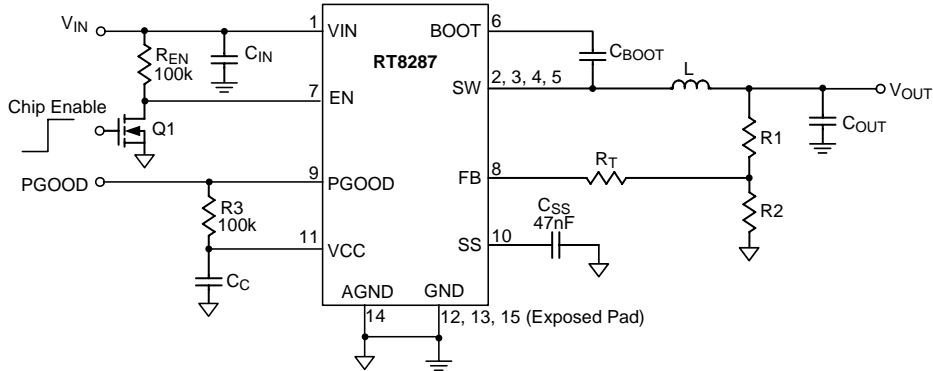


Figure 3. Enable Control Circuit for Logic Control with Low Voltage

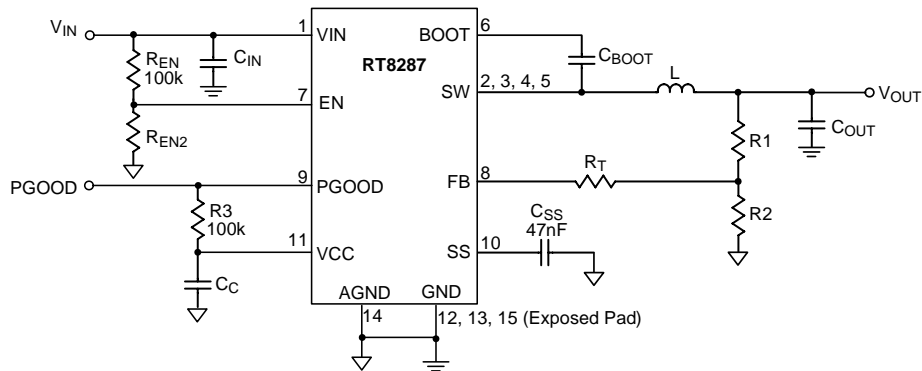


Figure 4. The Resistors can be Selected to Set IC Lockout Threshold

**Power Good Output**

The power good output is an open-drain output and requires a pull up resistor. When the output voltage is 70% below its set voltage, PGOOD will be pulled low. It is held low until the output voltage returns to within the allowed tolerances once more. During soft-start, PGOOD is actively held low and only allowed to transition high after soft-start is over and the output voltage has reached 90% of its set voltage.

**Under Output Voltage Protection-Hiccup Mode**

For the IC, Hiccup Mode of Under Voltage Protection (UVP) is provided. When the FB voltage drops below half of the feedback reference voltage,  $V_{FB}$ , the UVP function will be triggered and the IC will shut down for a period of time and then recover automatically. The Hiccup Mode of UVP can reduce input current in short-circuit conditions.

**Inductor Selection**

For a given input and output voltage, the inductor value and operating frequency determine the ripple current. The ripple current  $\Delta I_L$  increases with higher  $V_{IN}$  and decreases with higher inductance.

$$\Delta I_L = \left[ \frac{V_{OUT}}{f \times L} \right] \times \left[ 1 - \frac{V_{OUT}}{V_{IN}} \right]$$

Having a lower ripple current reduces not only the ESR losses in the output capacitors but also the output voltage ripple. Highest efficiency operation is achieved by reducing ripple current at low frequency, but it requires a large inductor to attain this goal.

For the ripple current selection, the value of  $\Delta I_L = 0.24(I_{MAX})$  will be a reasonable starting point. The largest ripple current occurs at the highest  $V_{IN}$ . To guarantee that the ripple current stays below a specified maximum, the inductor value should be chosen according to the following equation :

$$L = \left[ \frac{V_{OUT}}{f \times \Delta I_L(MAX)} \right] \times \left[ 1 - \frac{V_{OUT}}{V_{IN(MAX)}} \right]$$

The inductor's current rating (caused a 40°C temperature rising from 25°C ambient) should be greater than the maximum load current and its saturation current should be greater than the short circuit peak current limit. Please see Table 2 for the inductor selection reference and it is highly recommended to keep inductor value as close as possible to the recommended inductor values for each  $V_{OUT}$  as shown in Table 1.

**Table 2. Suggested Inductors for Typical Application Circuit**

Component Supplier	Series	Dimensions (mm)
<b>TDK</b>	VLF10045	10 x 9.7 x 4.5
<b>TDK</b>	SLF12565	12.5 x 12.5 x 6.5
<b>TAIYO YUDEN</b>	NR8040	8 x 8 x 4

**Input and Output Capacitors Selection**

The input capacitance,  $C_{IN}$ , is needed to filter the trapezoidal current at the source of the high side MOSFET. To prevent large ripple current, a low ESR input capacitor sized for the maximum RMS current should be used. The RMS current is given by :

$$I_{RMS} = I_{OUT(MAX)} \frac{V_{OUT}}{V_{IN}} \sqrt{\frac{V_{IN}}{V_{OUT}} - 1}$$

This formula has a maximum at  $V_{IN} = 2V_{OUT}$ , where  $I_{RMS} = I_{OUT} / 2$ . This simple worst case condition is commonly used for design because even significant deviations do not offer much relief.

Choose a capacitor rated at a higher temperature than required. Several capacitors may also be paralleled to meet size or height requirements in the design.

For the input capacitor, one 22µF low ESR ceramic capacitors are recommended. For the recommended capacitor, please refer to table 3 for more detail.

**Table 3. Suggested Capacitors for  $C_{IN}$  and  $C_{OUT}$**

Location	Component Supplier	Part No.	Capacitance (mF)	Case Size
<b><math>C_{IN}</math></b>	<b>MURATA</b>	GRM32ER71C226M	22	1210
<b><math>C_{IN}</math></b>	<b>TDK</b>	C3225X5R1C226M	22	1210
<b><math>C_{OUT}</math></b>	<b>MURATA</b>	GRM31CR60J476M	47	1206
<b><math>C_{OUT}</math></b>	<b>TDK</b>	C3225X5R0J476M	47	1210
<b><math>C_{OUT}</math></b>	<b>MURATA</b>	GRM32ER71C226M	22	1210
<b><math>C_{OUT}</math></b>	<b>TDK</b>	C3225X5R1C226M	22	1210

The selection of  $C_{OUT}$  is determined by the required ESR to minimize voltage ripple.

Moreover, the amount of bulk capacitance is also a key for  $C_{OUT}$  selection to ensure that the control loop is stable. Loop stability can be checked by viewing the load transient response.

The output ripple,  $\Delta V_{OUT}$ , is determined by :

$$\Delta V_{OUT} \leq \Delta L \left[ ESR + \frac{1}{8fC_{OUT}} \right]$$

Higher values, lower cost ceramic capacitors are now becoming available in smaller case sizes. Their high ripple current, high voltage rating and low ESR make them ideal for switching regulator applications. However, care must

be taken when these capacitors are used at input and output. When a ceramic capacitor is used at the input and the power is supplied by a wall adapter through long wires, a load step at the output can induce ringing at the input,  $V_{IN}$ . At best, this ringing can couple to the output and be mistaken as loop instability. At worst, a sudden inrush of current through the long wires can potentially cause a voltage spike at  $V_{IN}$  large enough to damage the part.

**EMI Consideration**

Since parasitic inductance and capacitance effects in PCB circuitry would cause a spike voltage on SW pin when high side MOSFET is turned-on/off, this spike voltage on

SW may impact on EMI performance in the system. In order to enhance EMI performance, there are two methods to suppress the spike voltage. One way is by placing an R-C snubber ( $R_S^*$ ,  $C_S^*$ ) between SW and GND and locating them as close as possible to the SW pin, as shown in Figure 5. Another method is by adding a resistor in series with the bootstrap capacitor,  $C_{BOOT}$ , but this method will

decrease the driving capability to the high side MOSFET. It is strongly recommended to reserve the R-C snubber during PCB layout for EMI improvement. Moreover, reducing the SW trace area and keeping the main power in a small loop will be helpful on EMI performance. For detailed PCB layout guide, please refer to the section Layout Considerations.

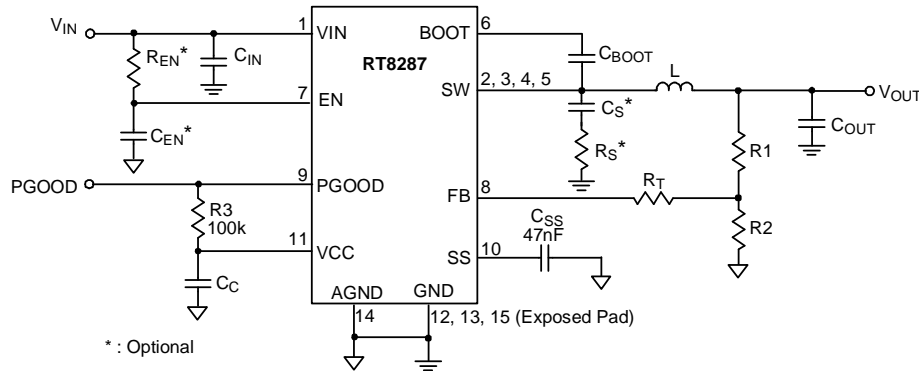


Figure 5. Reference Circuit with Snubber and Enable Timing Control

**Thermal Considerations**

For continuous operation, do not exceed absolute maximum junction temperature. The maximum power dissipation depends on the thermal resistance of the IC package, PCB layout, rate of surrounding airflow, and difference between junction and ambient temperature. The maximum power dissipation can be calculated by the following formula :

$$P_{D(MAX)} = (T_{J(MAX)} - T_A) / \theta_{JA}$$

where  $T_{J(MAX)}$  is the maximum junction temperature,  $T_A$  is the ambient temperature, and  $\theta_{JA}$  is the junction to ambient thermal resistance.

For recommended operating condition specifications of the RT8287, the maximum junction temperature is 125°C and  $T_A$  is the ambient temperature. The junction to ambient thermal resistance,  $\theta_{JA}$ , is layout dependent. For WDFN-14L 4x3 package, the thermal resistance,  $\theta_{JA}$ , is 60°C/W on a standard JEDEC 51-7 four-layer thermal test board. The maximum power dissipation at  $T_A = 25^\circ\text{C}$  can be calculated by the following formula :

$$P_{D(MAX)} = (125^\circ\text{C} - 25^\circ\text{C}) / (60^\circ\text{C/W}) = 1.667\text{W for WDFN-14L 4x3 package}$$

The maximum power dissipation depends on the operating ambient temperature for fixed  $T_{J(MAX)}$  and thermal resistance,  $\theta_{JA}$ . For the RT8287 package, the derating curve in Figure 6 allows the designer to see the effect of rising ambient temperature on the maximum power dissipation.

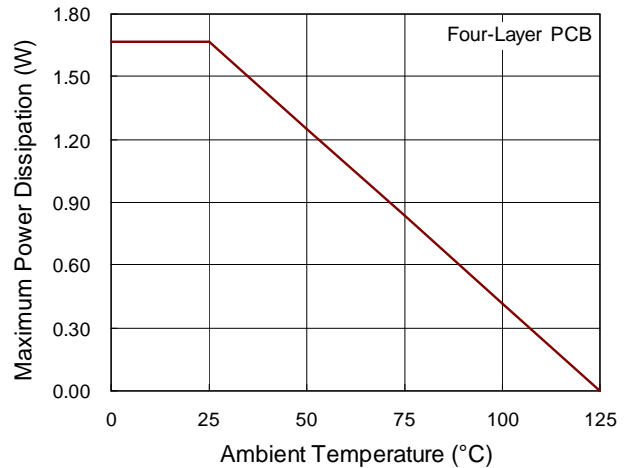


Figure 6. Derating Curve for RT8287 Package

**Layout Considerations**

Follow the PCB layout guidelines for optimal performance of the IC.

- } Keep the traces of the main current paths as short and wide as possible.
- } Put the input capacitor as close as possible to the device pins (VIN and GND).
- } SW node is with high frequency voltage swing and should be kept at small area. Keep analog components away from the SW node to prevent stray capacitive noise pickup.

- } Connect feedback network behind the output capacitors. Keep the loop area small. Place the feedback components near the IC.
- } Connect all analog grounds to a command node and then connect the command node to the power ground behind the output capacitors.
- } An example of PCB layout guide is shown in Figure 7 for reference.

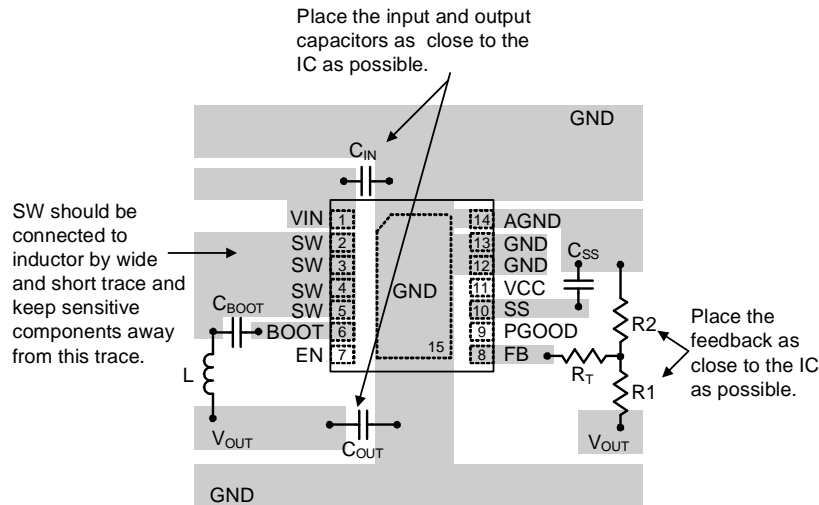
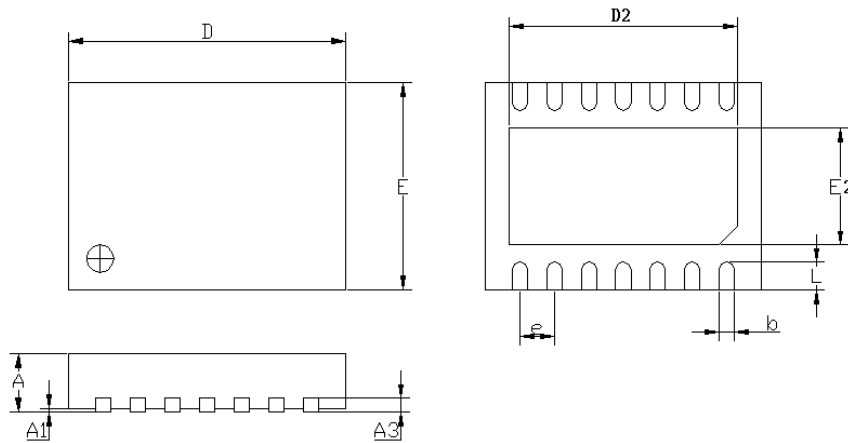


Figure 7. PCB Layout Guide

## Outline Dimension



Symbol	Dimensions In Millimeters		Dimensions In Inches	
	Min	Max	Min	Max
A	0.700	0.800	0.028	0.031
A1	0.000	0.050	0.000	0.002
A3	0.175	0.250	0.007	0.010
b	0.180	0.300	0.007	0.012
D	3.900	4.100	0.154	0.161
D2	3.250	3.350	0.128	0.132
E	2.900	3.100	0.114	0.122
E2	1.650	1.750	0.065	0.069
e	0.500		0.020	
L	0.350	0.450	0.014	0.018

**W-Type 14L DFN 4x3 Package**

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