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The S-8423 Series is a CMOS IC designed for use in the switching circuits of main and backup power supplies of 3-V or 5-V operation microcomputers. It consists of two voltage regulators, three voltage detectors, a switchover circuit, and a control circuit. In addition to being able to switch from primary to backup power supplies, the S-8423 Series has three types of voltage detection output signal corresponding to the power supply voltage. The special sequence for switch control prevents unnecessary exhaustion of the backup power supply; this feature is suitable for structuring backup systems.

### ■ Features

- Low power consumption  
Normal operation: 43  $\mu\text{A}$  max. ( $V_{\text{IN}} = 6 \text{ V}$ )  
Backup: 2.1  $\mu\text{A}$  max.
- Voltage regulator  
Small input/output voltage differences :  
0.35 V max. ( $I_{\text{OUT}} = 50\text{mA}$ )  
Output voltage tolerance :  $\pm 2\%$
- Three built-in voltage detectors ( $\overline{\text{CS}}$ ,  $\overline{\text{PREEND}}$ ,  $\overline{\text{RESET}}$ )  
Detection voltage tolerance:  $\pm 2\%$
- Special sequence  
Backup voltage is not output, if the primary power supply voltage does not reach the  $\overline{\text{RESET}}$  voltage that activates a CPU.

### ■ Applications

- Video camera recorder
- Still video camera
- Memory card
- SRAM backup equipment

### ■ Selection Guide

( $T_a = 25^\circ\text{C}$ )

Model No.	Output voltage*(V)			CS detection voltage(V)			CS release voltage(V)			$\overline{\text{RESET}}$ detection voltage(V)		
	Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.
S-8423AFS	3.23	3.30	3.37	3.919	4.000	4.081	4.003	4.100	4.197	2.253	2.300	2.347
S-8423NFS	3.135	3.200	3.265	3.234	3.300	3.366	3.315	3.400	3.485	2.351	2.400	2.449
S-8423LFS	4.90	5.00	5.10	4.507	4.600	4.693	4.609	4.719	4.828	2.253	2.300	2.347

\*  $V_{\text{RO}} = V_{\text{OUT}}$

■ **Block Diagram**

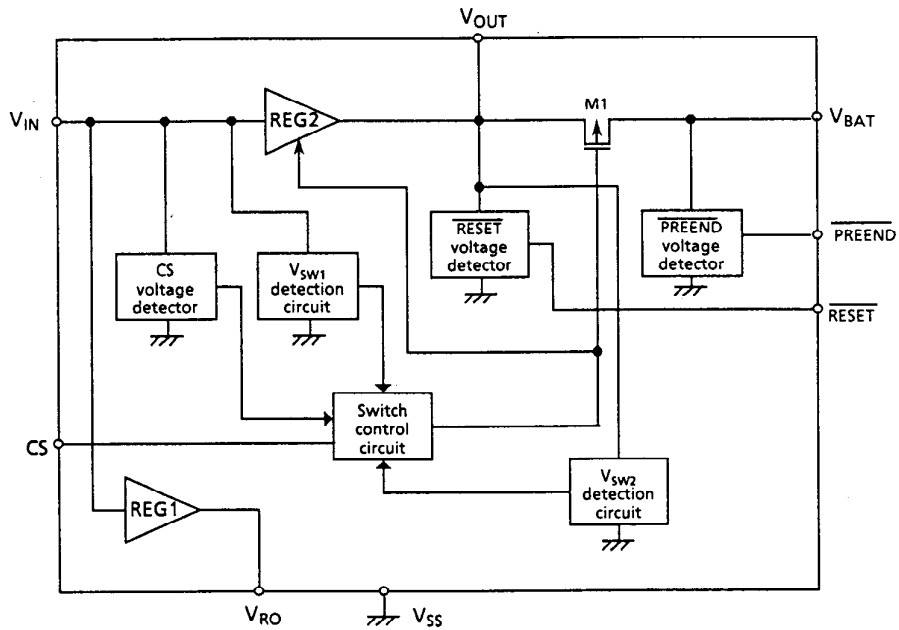
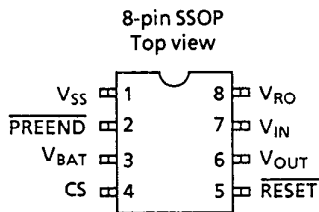


Figure 1

■ **Pin Assignment**



Pin name	Functions
CS	Output pin of CS voltage detector
RESET	Output pin of RESET voltage detector
PREEND	Output pin of PREEND voltage detector
V <sub>IN</sub> *	Primary power supply input pin
V <sub>BAT</sub> *	Backup power supply input pin
V <sub>OUT</sub> *	Output pin of voltage regulator 2
V <sub>RO</sub> *	Output pin of voltage regulator 1
V <sub>SS</sub>	Ground

\* Mount capacitors between V<sub>SS</sub> (GND) and the V<sub>IN</sub>, V<sub>BAT</sub>, V<sub>OUT</sub>, and V<sub>RO</sub> pins. (See "Standard Circuit")

Figure 2

■ **Absolute Maximum Ratings**

Table 1

T <sub>a</sub> = 25°C				
Parameter	Symbol	Ratings	Unit	
Primary power supply input voltage	V <sub>IN</sub>	V <sub>SS</sub> -0.3 to 17	V	
Backup power supply input voltage	V <sub>BAT</sub>	V <sub>SS</sub> -0.3 to 17	V	
Output voltage of voltage regulator	V <sub>RO</sub> , V <sub>OUT</sub>	V <sub>SS</sub> -0.3 to V <sub>IN</sub> + 0.3	V	
Output voltage of	$\left\{ \begin{array}{l} \overline{\text{CS}} \\ \overline{\text{RESET}} \\ \overline{\text{PREEND}} \end{array} \right.$	$\left\{ \begin{array}{l} V_{\text{CS}} \\ V_{\text{RESET}} \\ V_{\text{PRE}} \end{array} \right.$	V <sub>SS</sub> -0.3 to 17	V
Power dissipation	P <sub>D</sub>	300	mW	
Operating temperature	T <sub>opr</sub>	-40 to +85	°C	
Storage temperature	T <sub>stg</sub>	-40 to +125	°C	

■ Electrical Characteristics

1. S-8423AFS

Table 2

(Unless otherwise specified : Ta = 25°C)

Parameter	Symbol	Conditions	Min.	Typ.	Max.	Unit	Test cir.	
Voltage regulator	Output voltage 1	$V_{RO}$	$V_{IN} = 6V, I_{RO} = 30mA$	3.23	3.30	3.37	V	1
	I/O voltage difference 1	$V_{dif1}$	$I_{RO} = 30mA$	—	0.2	0.35	V	
	Load regulation 1	$\Delta V_{RO1}$	$V_{IN} = 6V$ $I_{RO} = 100\mu A \text{ to } 40mA$	—	40	100	mV	
	Line regulation 1	$\Delta V_{RO2}$	$V_{IN} = 6 \text{ to } 16V$ $I_{RO} = 30mA$	—	38	100	mV	
	Temperature coefficient of $V_{RO}$	$\frac{\Delta V_{RO}}{\Delta Ta}$	$Ta = -40^\circ C \text{ to } 85^\circ C$	—	$\pm 0.47$	—	mV/°C	
	Output voltage 2	$V_{OUT}$	$V_{IN} = 6V, I_{OUT} = 50mA$	3.23	3.30	3.37	V	
	I/O voltage difference 2	$V_{dif2}$	$I_{OUT} = 50mA$	—	0.2	0.35	V	
	Load regulation 2	$\Delta V_{OUT1}$	$V_{IN} = 6V$ $I_{OUT} = 100\mu A \text{ to } 60mA$	—	50	110	mV	
	Line regulation 2	$\Delta V_{OUT2}$	$V_{IN} = 6 \text{ to } 16V$ $I_{OUT} = 50mA$	—	50	110	mV	
	Temperature coefficient of $V_{OUT}$	$\frac{\Delta V_{OUT}}{\Delta Ta}$	$Ta = -40^\circ C \text{ to } 85^\circ C$	—	$\pm 0.47$	—	mV/°C	
Input voltage of primary power supply	$V_{IN}$		—	—	16	V		
Voltage detector	CS detection voltage	$-V_{DET1}$	Detects $V_{IN}$	3.919	4.000	4.081	V	2
	CS release voltage	$+V_{DET1}$		4.003	4.100	4.197	V	
	RESET detection voltage	$-V_{DET2}$	Detects $V_{OUT}$	2.253	2.300	2.347	V	
	RESET release voltage	$+V_{DET2}$		2.351	2.420	2.489	V	
	PREEND detection voltage	$-V_{DET3}$	Detects $V_{BAT}$	$-V_{DET2} + 0.15$	$-V_{DET2} + 0.20$	$-V_{DET2} + 0.25$	V	
	PREEND release voltage	$+V_{DET3}$		$-V_{DET3} + 0.11$	$-V_{DET3} + 0.14$	$-V_{DET3} + 0.17$	V	
	Operating voltage	$V_{opr}$	$V_{IN}$ or $V_{BAT}$	2.0	—	16	V	
	Temperature coefficient of detection voltage	$\frac{\Delta -V_{DET1}}{\Delta Ta}$	$Ta = -40^\circ C \text{ to } 85^\circ C$	—	$\pm 0.57$	—	mV/°C	
		$\frac{\Delta -V_{DET2}}{\Delta Ta}$	$Ta = -40^\circ C \text{ to } 85^\circ C$	—	$\pm 0.33$	—	mV/°C	
		$\frac{\Delta -V_{DET3}}{\Delta Ta}$	$Ta = -40^\circ C \text{ to } 85^\circ C$	—	$\pm 0.36$	—	mV/°C	
Sink current	$I_{SINK}$	$V_{DS} = 0.5V,$ $V_{IN} = V_{BAT} = 2.0V$	RESET	1.50	2.30	—	mA	
			PREEND	1.50	2.30	—	mA	
			CS	1.50	2.30	—	mA	
Leakage current	$I_{LEAK}$	$V_{DS} = 16V, V_{IN} = 16V$	—	—	0.1	$\mu A$		
Switch	Switchover voltage	$V_{SW1}$	$V_{BAT} = 2.8V$ Detects $V_{IN}$	$+V_{DET1} \times 0.75$	$+V_{DET1} \times 0.77$	$+V_{DET1} \times 0.79$	V	4
	CS output inhibit voltage	$V_{SW2}$	$V_{BAT} = 3V$ Detects $V_{OUT}$	$V_{OUT} \times 0.93$	$V_{OUT} \times 0.95$	$V_{OUT} \times 0.97$	V	5
	M1 switch leakage current	$I_{LEK}$	$V_{IN} = 6V$ $V_{BAT} = 0V$	—	—	1	$\mu A$	6
	M1 switch resistance value	$R_{SW}$	$V_{IN} = \text{open}, V_{BAT} = 3V$ $I_{OUT} = 10 \text{ to } 500\mu A$	—	—	100	$\Omega$	7
	Temperature coefficient of $V_{SW1}$	$\frac{\Delta V_{SW1}}{\Delta Ta}$	$Ta = -40^\circ C \text{ to } 85^\circ C$	—	$\pm 0.45$	—	mV/°C	4
	Temperature coefficient of $V_{SW2}$	$\frac{\Delta V_{SW2}}{\Delta Ta}$	$Ta = -40^\circ C \text{ to } 85^\circ C$	—	$\pm 0.45$	—	mV/°C	5
Current consumption	$I_{SS1}$ $I_{BAT1}$ $I_{BAT2}$	$V_{IN} = 6V, \text{ Unloaded}$ $V_{BAT} = 3V$	—	28	43	$\mu A$	8	
			—	0.26	0.50	$\mu A$		
		$V_{IN} = \text{open}$ $V_{BAT} = 3V, \text{ Unloaded}$	$Ta = 25^\circ C$	—	1.0	2.1		$\mu A$
		$Ta = 85^\circ C$	—	—	3.5	$\mu A$		
Input voltage of backup power supply	$V_{BAT}$		2.0	—	4.0	V	7	

# BATTERY BACKUP IC S-8423 Series

2. S-8423NFS

Table 3

(Unless otherwise specified : Ta = 25°C)

Parameter	Symbol	Conditions	Min.	Typ.	Max.	Unit	Test cir.	
Voltage regulator	Output voltage1	V <sub>RO</sub>	V <sub>IN</sub> = 3.6 V, I <sub>RO</sub> = 15 mA	3.135	3.200	3.265	V	1
	I/O voltage difference 1	V <sub>dif1</sub>	I <sub>RO</sub> = 15 mA	—	60	180	mV	
	Load regulation 1	ΔV <sub>RO1</sub>	V <sub>IN</sub> = 3.6 V I <sub>RO</sub> = 100 μA to 20 mA	—	40	100	mV	
	Line regulation 1	ΔV <sub>RO2</sub>	V <sub>IN</sub> = 3.6 to 16 V I <sub>RO</sub> = 15 mA	—	38	100	mV	
	Temperature coefficient of V <sub>RO</sub>	$\frac{\Delta V_{RO}}{\Delta T_a}$	Ta = -40°C to 85°C	—	± 0.46	—	mV/°C	
	Output voltage 2	V <sub>OUT</sub>	V <sub>IN</sub> = 3.6 V, I <sub>OUT</sub> = 15 mA	3.135	3.200	3.265	V	
	I/O voltage difference 1	V <sub>dif2</sub>	I <sub>OUT</sub> = 15 mA	—	20	60	mV	
	Load regulation 2	ΔV <sub>OUT1</sub>	V <sub>IN</sub> = 3.6 V I <sub>OUT</sub> = 100 μA to 20 mA	—	50	110	mV	
	Line regulation 2	ΔV <sub>OUT2</sub>	V <sub>IN</sub> = 3.6 to 16 V I <sub>OUT</sub> = 15 mA	—	50	110	mV	
	Temperature coefficient of V <sub>OUT</sub>	$\frac{\Delta V_{OUT}}{\Delta T_a}$	Ta = -40°C to 85°C	—	± 0.46	—	mV/°C	
	Input voltage of primary power supply	V <sub>IN</sub>		—	—	16	V	
	Voltage detector	CS detection voltage	-V <sub>DET1</sub>	Detects V <sub>IN</sub>	3.234	3.300	3.366	
CS release voltage		+V <sub>DET1</sub>		3.315	3.400	3.485	V	
RESET detection voltage		-V <sub>DET2</sub>	Detects V <sub>OUT</sub>	2.351	2.400	2.449	V	
RESET release voltage		+V <sub>DET2</sub>		2.457	2.528	2.599	V	
PREEND detection voltage		-V <sub>DET3</sub>	Detects V <sub>BAT</sub>	-V <sub>DET2</sub> + 0.15	-V <sub>DET2</sub> + 0.20	-V <sub>DET2</sub> + 0.25	V	
PREEND release voltage		+V <sub>DET3</sub>		-V <sub>DET3</sub> + 0.11	-V <sub>DET3</sub> + 0.14	-V <sub>DET3</sub> + 0.17	V	
Operating voltage		V <sub>opr</sub>	V <sub>IN</sub> or V <sub>BAT</sub>	2.0	—	16	V	
Temperature coefficient of detection voltage		$\frac{\Delta -V_{DET1}}{\Delta T_a}$	Ta = -40°C to 85°C	—	± 0.47	—	mV/°C	
		$\frac{\Delta -V_{DET2}}{\Delta T_a}$	Ta = -40°C to 85°C	—	± 0.34	—	mV/°C	
		$\frac{\Delta -V_{DET3}}{\Delta T_a}$	Ta = -40°C to 85°C	—	± 0.37	—	mV/°C	
Sink current	I <sub>SINK</sub>	V <sub>DS</sub> = 0.5 V, V <sub>IN</sub> = V <sub>BAT</sub> = 2.0 V	RESET	1.50	2.30	—	mA	
			PREEND	1.50	2.30	—	mA	
			CS	1.50	2.30	—	mA	
Leakage current	I <sub>LEAK</sub>	V <sub>DS</sub> = 16 V, V <sub>IN</sub> = 16 V	—	—	0.1	μA		
Switch	Switchover voltage	V <sub>SW1</sub>	V <sub>BAT</sub> = 2.8 V Detects V <sub>IN</sub>	+V <sub>DET1</sub> × 0.83	+V <sub>DET1</sub> × 0.85	+V <sub>DET1</sub> × 0.87	V	4
	CS output inhibit voltage	V <sub>SW2</sub>	V <sub>BAT</sub> = 3 V Detects V <sub>OUT</sub>	V <sub>OUT</sub> × 0.93	V <sub>OUT</sub> × 0.95	V <sub>OUT</sub> × 0.97	V	5
	M1 switch leakage current	I <sub>LEK</sub>	V <sub>IN</sub> = 3.6 V V <sub>BAT</sub> = 0 V	—	—	1	μA	6
	M1 switch resistance value	R <sub>SW</sub>	V <sub>IN</sub> = open, V <sub>BAT</sub> = 3 V	—	—	100	Ω	7
	Temperature coefficient of V <sub>SW1</sub>	$\frac{\Delta V_{SW1}}{\Delta T_a}$	Ta = -40°C to 85°C	—	± 0.41	—	mV/°C	4
	Temperature coefficient of V <sub>SW2</sub>	$\frac{\Delta V_{SW2}}{\Delta T_a}$	Ta = -40°C to 85°C	—	± 0.43	—	mV/°C	5
	Current consumption	I <sub>SS1</sub>	V <sub>IN</sub> = 3.6 V, Unloaded	—	28	43	μA	8
I <sub>BAT1</sub>		V <sub>BAT</sub> = 3 V	—	0.26	0.50	μA		
I <sub>BAT2</sub>		V <sub>IN</sub> = open V <sub>BAT</sub> = 3 V, Unloaded	Ta = 25°C	—	1.0	2.1	μA	
			Ta = 85°C	—	—	3.5	μA	
Input voltage of backup power supply	V <sub>BAT</sub>		2.0	—	4.0	V	7	

3. S-8423LFS

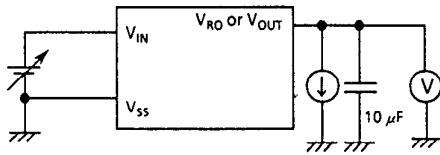
Table 4

(Unless otherwise specified : Ta = 25°C)

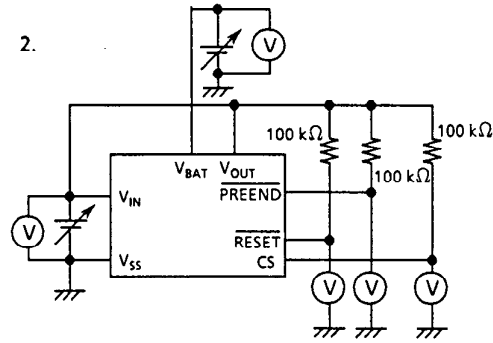
Parameter	Symbol	Conditions	Min.	Typ.	Max.	Unit	Test cir.	
Voltage regulator	Output voltage 1	$V_{RO}$	$V_{IN} = 6V, I_{RO} = 30mA$	4.90	5.00	5.10	V	1
	I/O voltage difference 1	$V_{dif1}$	$I_{RO} = 30mA$	—	0.2	0.35	V	
	Load regulation 1	$\Delta V_{RO1}$	$V_{IN} = 6V$ $I_{RO} = 100\mu A \text{ to } 40mA$	—	50	110	mV	
	Line regulation 1	$\Delta V_{RO2}$	$V_{IN} = 6 \text{ to } 16V$ $I_{RO} = 30mA$	—	50	110	mV	
	Temperature coefficient of $V_{RO}$	$\frac{\Delta V_{RO}}{\Delta Ta}$	$Ta = -40^\circ C \text{ to } 85^\circ C$	—	$\pm 0.71$	—	mV/°C	
	Output voltage 2	$V_{OUT}$	$V_{IN} = 6V, I_{OUT} = 50mA$	4.90	5.00	5.10	V	
	I/O voltage difference 1	$V_{dif2}$	$I_{OUT} = 50mA$	—	0.2	0.35	V	
	Load regulation 2	$\Delta V_{OUT1}$	$V_{IN} = 6V$ $I_{OUT} = 100\mu A \text{ to } 60mA$	—	50	110	mV	
	Line regulation 2	$\Delta V_{OUT2}$	$V_{IN} = 6 \text{ to } 16V$ $I_{OUT} = 50mA$	—	50	110	mV	
	Temperature coefficient of $V_{OUT}$	$\frac{\Delta V_{OUT}}{\Delta Ta}$	$Ta = -40^\circ C \text{ to } 85^\circ C$	—	$\pm 0.71$	—	mV/°C	
	Input voltage of primary power supply	$V_{IN}$		—	—	16	V	
	Voltage detector	CS detection voltage	$-V_{DET1}$	Detects $V_{IN}$	4.507	4.600	4.693	
CS release voltage		$+V_{DET1}$		4.609	4.719	4.828	V	
RESET detection voltage		$-V_{DET2}$	Detects $V_{OUT}$	2.253	2.300	2.347	V	
RESET release voltage		$+V_{DET2}$		2.351	2.420	2.489	V	
PREEND detection voltage		$-V_{DET3}$	Detects $V_{BAT}$	$-V_{DET2} + 0.15$	$-V_{DET2} + 0.20$	$-V_{DET2} + 0.25$	V	
PREEND release voltage		$+V_{DET3}$		$-V_{DET3} + 0.11$	$-V_{DET3} + 0.14$	$-V_{DET3} + 0.17$	V	
Operating voltage		$V_{opr}$	$V_{IN}$ or $V_{BAT}$	2.0	—	16	V	
Temperature coefficient of detection voltage		$\frac{\Delta -V_{DET1}}{\Delta Ta}$	$Ta = -40^\circ C \text{ to } 85^\circ C$	—	$\pm 0.66$	—	mV/°C	
		$\frac{\Delta -V_{DET2}}{\Delta Ta}$	$Ta = -40^\circ C \text{ to } 85^\circ C$	—	$\pm 0.33$	—	mV/°C	
		$\frac{\Delta -V_{DET3}}{\Delta Ta}$	$Ta = -40^\circ C \text{ to } 85^\circ C$	—	$\pm 0.36$	—	mV/°C	
Sink current	$I_{SINK}$	$V_{DS} = 0.5V, V_{IN} = V_{BAT} = 2.0V$	RESET	1.50	2.30	—	mA	
		PREEND	1.50	2.30	—	mA		
		CS	1.50	2.30	—	mA		
Leakage current	$I_{LEAK}$	$V_{DS} = 16V, V_{IN} = 16V$	—	—	0.1	$\mu A$		
Switch	Switchover voltage	$V_{SW1}$	$V_{BAT} = 2.8V$ Detects $V_{IN}$	$+V_{DET1} \times 0.75$	$+V_{DET1} \times 0.77$	$+V_{DET1} \times 0.79$	V	4
	CS output inhibit voltage	$V_{SW2}$	$V_{BAT} = 3V$ Detects $V_{OUT}$	$V_{OUT} \times 0.93$	$V_{OUT} \times 0.95$	$V_{OUT} \times 0.97$	V	5
	M1 switch leakage current	$I_{LEK}$	$V_{IN} = 6V$ $V_{BAT} = 0V$	—	—	1	$\mu A$	6
	M1 switch resistance value	$R_{SW}$	$V_{IN} = \text{open}, V_{BAT} = 3V, I_{OUT} = 10 \text{ to } 500\mu A$	—	—	100	$\Omega$	7
	Temperature coefficient of $V_{SW1}$	$\frac{\Delta V_{SW1}}{\Delta Ta}$	$Ta = -40^\circ C \text{ to } 85^\circ C$	—	$\pm 0.51$	—	mV/°C	4
	Temperature coefficient of $V_{SW2}$	$\frac{\Delta V_{SW2}}{\Delta Ta}$	$Ta = -40^\circ C \text{ to } 85^\circ C$	—	$\pm 0.68$	—	mV/°C	5
	Current consumption	$I_{SS1}$	$V_{IN} = 6V, \text{ Unloaded}$	—	29	45	$\mu A$	8
$I_{BAT1}$		$V_{BAT} = 3V$	—	0.26	0.50	$\mu A$		
$I_{BAT2}$		$V_{IN} = \text{open}, V_{BAT} = 3V, \text{ Unloaded}$	$Ta = 25^\circ C$	—	1.0	2.1	$\mu A$	
			$Ta = 85^\circ C$	—	—	3.5	$\mu A$	
Input voltage of backup power supply	$V_{BAT}$		2.0	—	4.0	V	7	

■ **Test Circuit**

1.

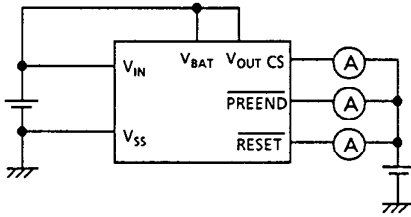


2.

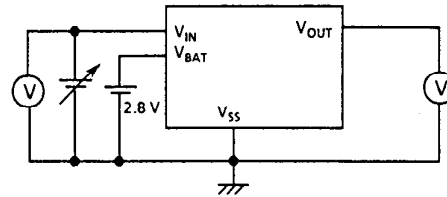


When measuring  $V_{DET3}$ , apply 6 V to  $V_{IN}$

3.

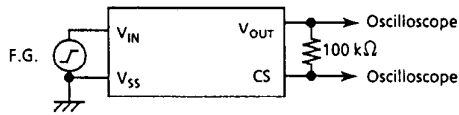


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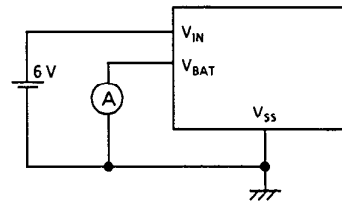


Measure the value after applying 5 V or more to  $V_{IN}$

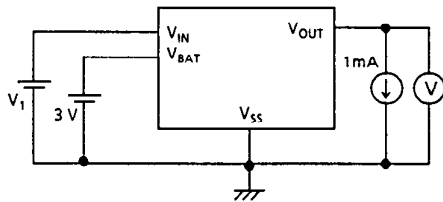
5.



6.

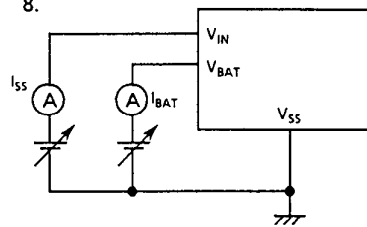


7.



Open and measure the value after applying 6 V to  $V_1$

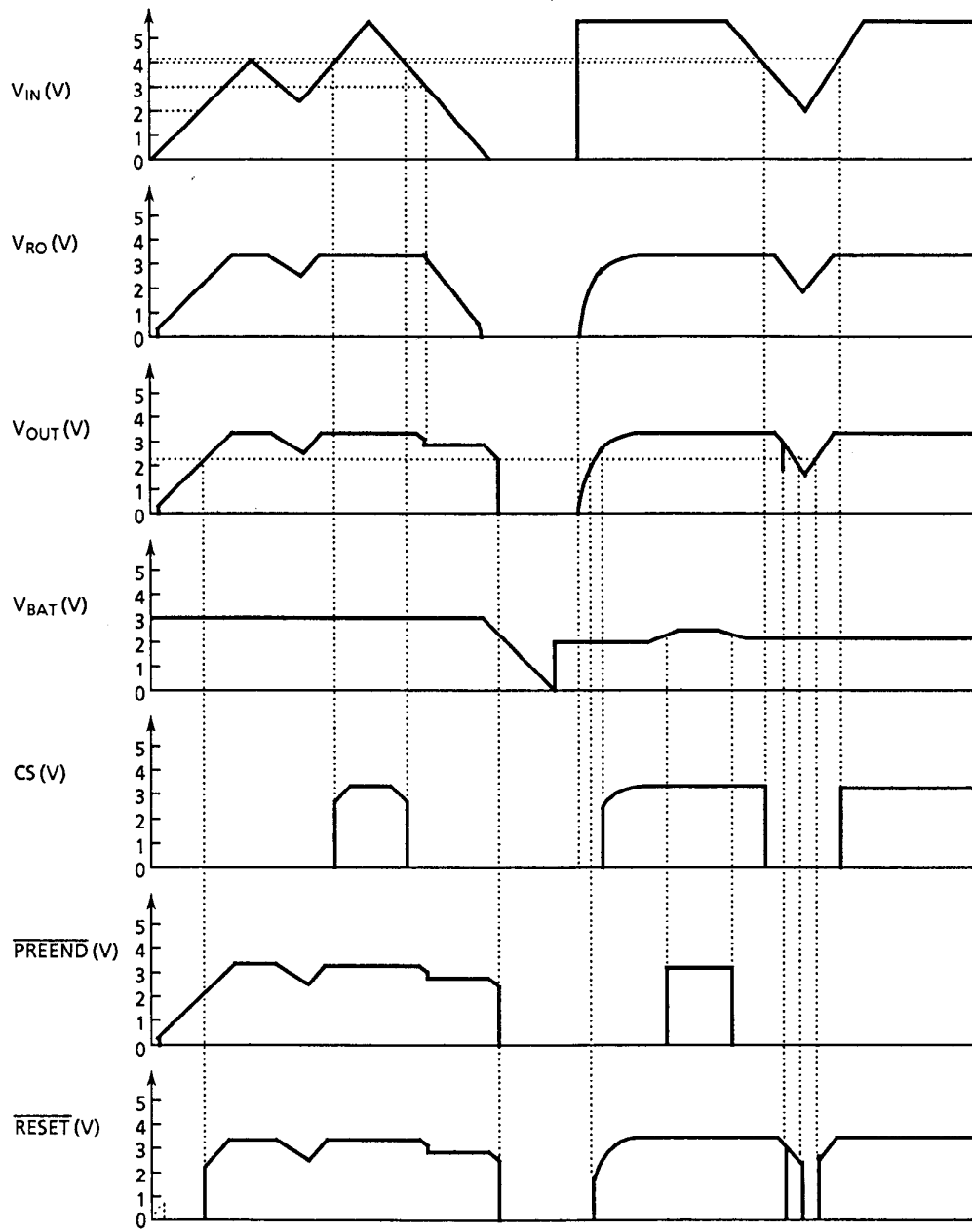
8.



To measure  $I_{BAT2}$ , first apply 3 V to  $V_{BAT}$  and 6 V or more to  $V_{IN}$ . Then open  $V_{IN}$  and measure the current when  $V_{BAT}$  is 3 V.

**Figure 3**

■ Operation Timing Chart (S-8423AFS)



CS, and  $\overline{\text{PREEND}}$  and  $\overline{\text{RESET}}$  are pulled up to V<sub>OUT</sub>.

Figure 4



■ **Operation**

The S-8423 Series consists of two voltage regulators, and three voltage detectors. The voltage regulator 1 regulates input voltage  $V_{IN}$  and outputs to  $V_{RO}$ . The voltage regulator 2 outputs to  $V_{OUT}$ . This section describes the functions and operations of each part.

1. Voltage regulators 1 and 2

The built-in regulators have very small I/O voltage difference ( $V_{dif1} = 0.2\text{ V typ. at } I_{RO} = 30\text{ mA}$ ). The output voltage of  $V_{RO}$  and  $V_{OUT}$  can be selected independently between 2.8 and 3.8 V by 0.1 V step.

I/O voltage difference  $V_{dif1}$  or  $V_{dif2}$

Assume that the  $V_{RO}$  voltage when  $V_{IN}$  is 6 V and  $I_{RO}$  is 30 mA is  $V_{initial}$ . When the amount voltage of I/O voltage difference  $V_{dif1}$  or  $V_{dif2}$  and  $V_{initial}$  is applied to the  $V_{IN}$  pin, 95% of the  $V_{initial}$  voltage is output at the  $V_{RO}$  pin.

2. Switch

The switch consists of the switch control circuit,  $V_{SW1}$  and  $V_{SW2}$  detection circuits, voltage regulator 2 and switch transistor M1.

2.1  $V_{SW1}$  detection circuit

The  $V_{SW1}$  detection circuit monitors the  $V_{IN}$  voltage and sends the results of detection to the switch control circuit. In the S-8423AFS (CS detection voltage ranges from 4.0 to 5.0 V), detection voltage ( $V_{SW1}$ ) is set to  $77 \pm 2\%$  of CS release voltage +  $V_{DET1}$ ; in the S-8423NFS (CS detection voltage ranges from 3.0 to 4.0 V) is set to  $85 \pm 2\%$  of CS release voltage +  $V_{DET1}$ .

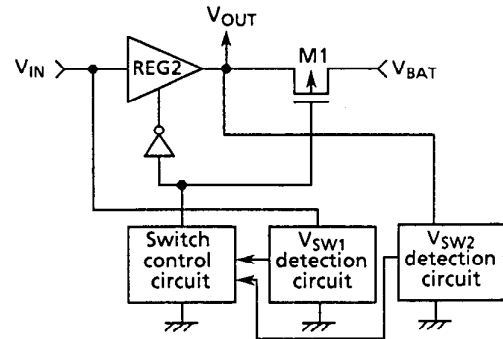


Figure 5 Switch

2.2  $V_{SW2}$  detection circuit

$V_{SW2}$  voltage detector monitors  $V_{OUT}$  terminal voltage and keeps CS release voltage output low until  $V_{OUT}$  terminal voltage rises to  $V_{SW2}$ . Then CS output changes from low to high if  $V_{IN}$  terminal voltage is more than  $+V_{DET1}$  (CS release voltage), when  $V_{OUT}$  terminal voltage rises to 95% of  $V_{OUT2}$  (output voltage of voltage regulator 2). CS output changes from high to low regardless of  $V_{SW2}$ , if  $V_{IN}$  terminal voltage falls down to less than  $-V_{DET1}$  (CS detection voltage). CS output holds high if  $V_{IN}$  terminal voltage keeps higher than  $-V_{DET1}$ , when  $V_{OUT}$  terminal voltage falls down to less than  $V_{SW2}$  because of undershoot.

2.3 Switch control circuit

The switch control circuit receives the signal from the  $V_{SW1}$  detection circuit and controls M1 and voltage regulator 2. The switch control circuit operates in two statuses: the special and normal sequences. In the special sequence status, the circuit does not receive nor control signals according to the  $V_{IN}$  (or  $V_{BAT}$ ) voltage sequence. In the normal sequence status, the circuit receives and controls signals. Initially, the circuit is kept in the special sequence status. When  $V_{IN}$  increases until CS signal goes high, the circuit enters the normal sequence status.

(1) Special sequence status

When the  $V_{IN}$  (or  $V_{BAT}$ ) voltage rises, the switch control circuit is kept in the special sequence status until CS signal goes high.

At that time, the switch control circuit turns voltage regulator 2 on and turns M1 off regardless of the status of the  $V_{SW1}$  detection circuit. The voltage regulator 2 has a switchover function.

(2) Normal sequence status

When  $V_{IN}$  voltage increases until CS signal, which monitors  $V_{OUT}$  terminal, goes high, the switch control circuit enters the normal sequence.

Once the circuit enters the normal sequence, it turns voltage regulator 2 and M1 on and off according to the  $V_{IN}$  voltage as shown in Table 5. It takes hundreds  $\mu s$  in the worst case until voltage regulator 2 goes ON from OFF. During this period, as both voltage regulator 2 and M1 are OFF,  $V_{OUT}$  voltage may drop. To protect this drop, do not fail to add 10  $\mu F$  or more of capacitor to  $V_{OUT}$  terminal.

The circuit returns to the special sequence status, when  $\overline{RESET}$  signal goes low.

Table 5

$V_{IN}$ voltage	Voltage regulator 2	M1	$V_{OUT}$
$V_{IN} > V_{SW1}$	ON	OFF	$V_{OUT2}$
$V_{IN} < V_{SW1}$	OFF	ON	$V_{BAT} - V_{dif3}$

2.4 Switch transistor M1

Voltage regulator 2 is also used for switch from  $V_{IN}$  to  $V_{OUT}$ . Therefore, no reverse current flows from  $V_{OUT}$  to  $V_{IN}$ , when voltage regulator 2 is off.

The output voltage of voltage regulator 2 can be selected between 2.8 V and 3.8 V by 0.1 V step.

The ON resistance of M1 is 100  $\Omega$  or less when  $I_{OUT}$  is between 10 and 500  $\mu A$ .

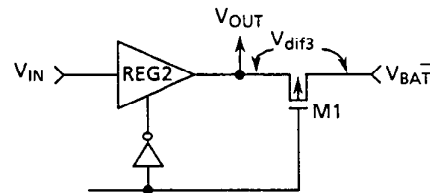


Figure 6 Definitions of  $V_{dif3}$

Therefore, when M1 is turned on to connect  $V_{OUT}$  to  $V_{BAT}$ , the maximum voltage drop  $V_{dif3}$  due to M1 is  $100 \times I_{OUT}$  (output current). The minimum output at the  $V_{OUT}$  pin is  $V_{BAT} - V_{dif3}$  (max.).

When voltage regulator 2 is on and M1 is off, the leakage current of M1 is kept below 1  $\mu A$  ( $V_{IN} = 6 V$ ,  $T_a = 25^\circ C$ ) with the  $V_{BAT}$  pin connected to the ground ( $V_{SS}$ ).

3. Voltage detector

The S-8423 Series has three voltage detectors and  $V_{SW2}$  voltage detector. Three detectors feature high precision and low power consumption with hysteresis characteristics. And  $V_{SW2}$  voltage detector inhibit CS release output. The power of CS voltage detector is supplied from the  $V_{IN}$  and  $V_{BAT}$  pins. Therefore, the output is stable as long as the primary or backup power supplies are within the operating voltage range (2 to 16 V). All outputs are Nch open-drains, and need about 100 k $\Omega$  of pull-up resistors.

(1) CS voltage detector

CS monitors  $V_{IN}$  terminal voltage. The detection voltage can be selected between 3.0 and 5.0 V by 0.1 V step. The result of detection is output at the CS pin: "L" for lower voltages than the detection level and "H" for higher voltages than the release level.

(2)  $\overline{\text{PREEND}}$  voltage detector

$\overline{\text{PREEND}}$  monitors the  $V_{\text{BAT}}$  pin. The detection voltage can be selected between 2.2 V and 2.7 V by 0.1 V step, and also higher than  $\overline{\text{RESET}}$  voltage with any difference voltage, indicating that the backup power supply is running out. The result of detection is output at the  $\overline{\text{PREEND}}$  pin: "L" for lower voltages than the detection level and "H" for higher voltages than the release level. The power of this detector is supplied from  $V_{\text{IN}}$  terminal. The output is valid only when voltage is supplied from  $V_{\text{IN}}$  terminal to  $V_{\text{OUT}}$  terminal ( $V_{\text{IN}} \geq V_{\text{SW1}}$ ) and the output when voltage is supplied from  $V_{\text{BAT}}$  terminal to  $V_{\text{OUT}}$  terminal ( $V_{\text{IN}} < V_{\text{SW1}}$ ) is "L."

(3)  $\overline{\text{RESET}}$  voltage detector

$\overline{\text{RESET}}$  monitors the  $V_{\text{OUT}}$  pin. The detection voltage can be selected between 2.0 V and 2.7 V by 0.1 V step. The result of detection is output at the  $\overline{\text{RESET}}$  pin: "L" for lower voltages than the detection level and "H" for higher voltages than the release level.  $\overline{\text{RESET}}$  outputs normal logic when  $V_{\text{OUT}}$  terminal voltage is 1.0 V or more terminal

**NOTE**  $\overline{\text{PREEND}}$  and  $\overline{\text{RESET}}$  are detected at different pins. In practice, current is taken from the  $V_{\text{BAT}}$  side, so consider the I/O voltage difference ( $V_{\text{dif3}}$ ) of M1 when M1 is turned on.

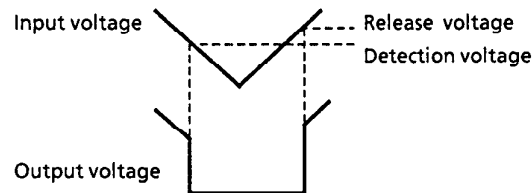


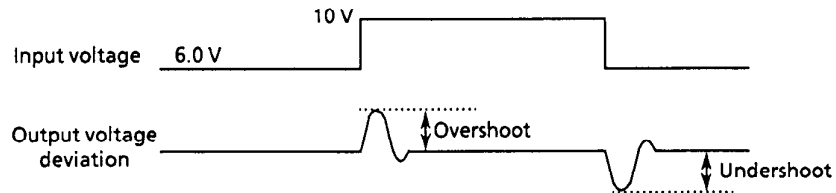
Figure 7 Detection potentials of voltage detectors

## ■ Transient Response

### 1. Line transient response against input voltage fluctuation

Input voltage fluctuation differs with the types of the signal applied: type I (square wave between 6.0 V and 10 V) and type II (square wave from 0 V to 10 V) (see Figure 8). This section describes the ringing waveforms and parameter dependency of each type. For reference, Figure 9 describes the measuring circuit.

#### Type I : Square wave between 6.0 V and 10 V



#### Type II : Square wave from 0 V to 10 V

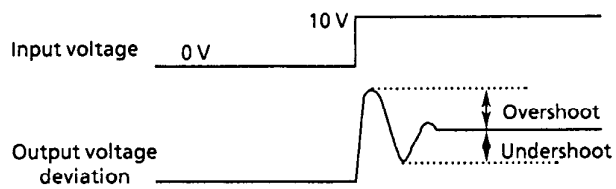


Figure 8

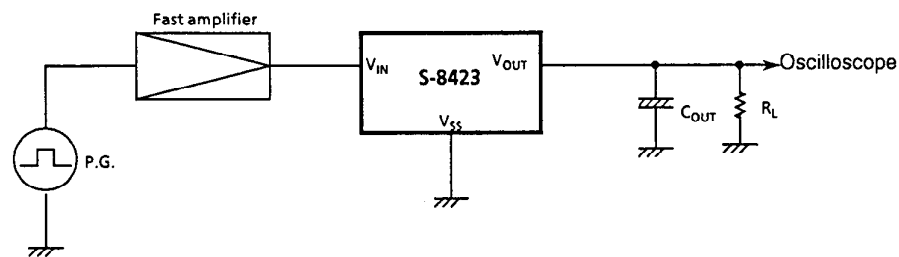


Figure 9 Measuring circuit

Type I

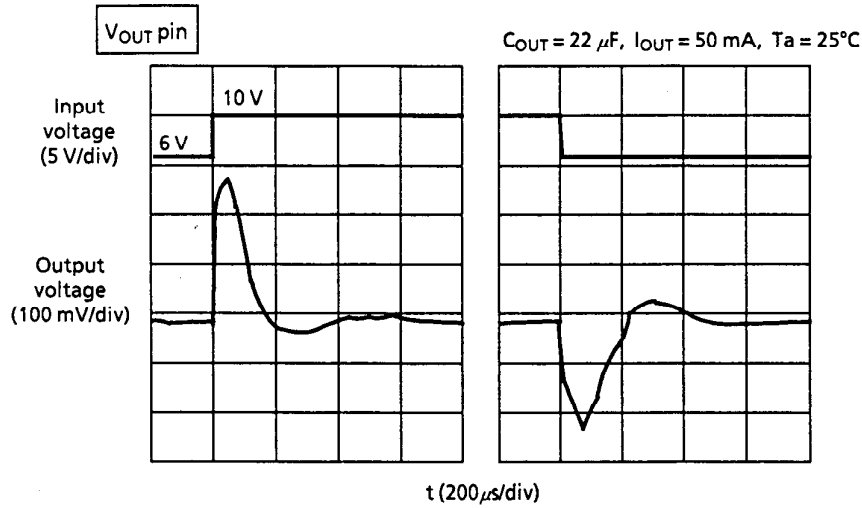


Figure 10 Type I ringing waveform (V<sub>OUT</sub> pin)

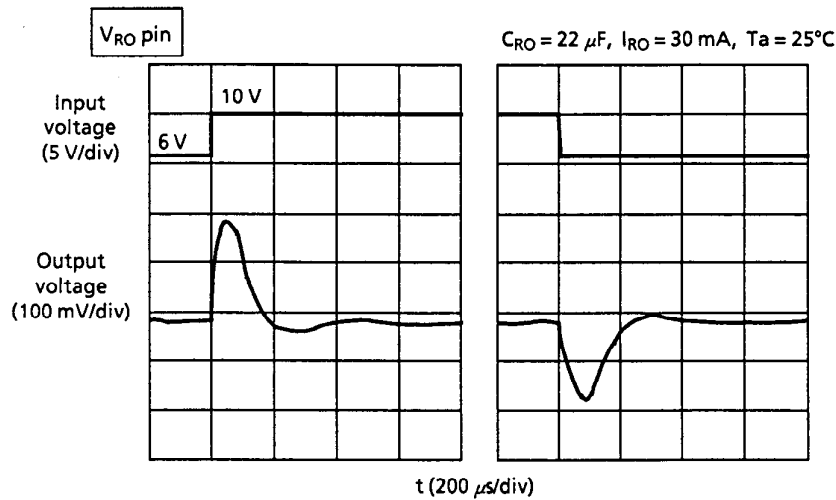


Figure 11 Type I ringing waveform (V<sub>RO</sub> pin)

Table 6 Type I parameter dependency

Parameter	Conditions	Method to decrease overshoot	Method to decrease undershoot
Output current $I_{OUT}$	5 to 60 mA	Decrease	Decrease
Load capacitance $C_{RO}$	5 to 47 $\mu F$	Increase	Increase
Input fluctuation $\Delta V_{IN}$	1 to 4 V	Decrease	Decrease
Temperature $T_a$	-40°C to +85°C	Low temperature	Low temperature

Type II

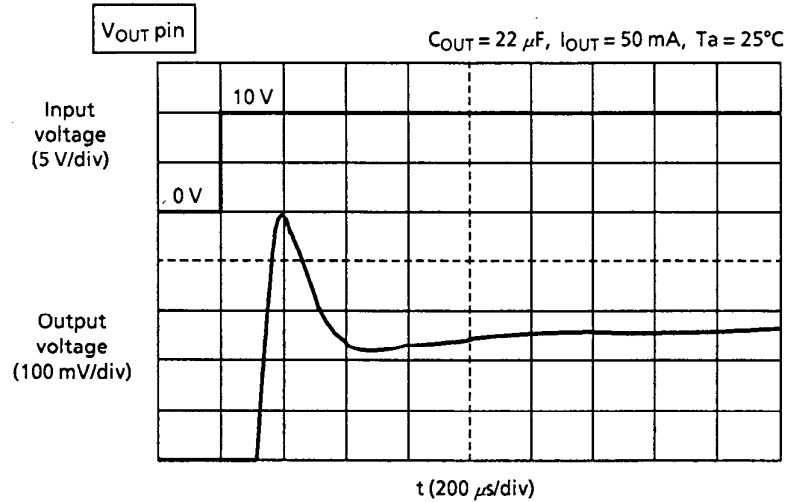


Figure 12 Type II ringing waveform (V<sub>OUT</sub> pin)

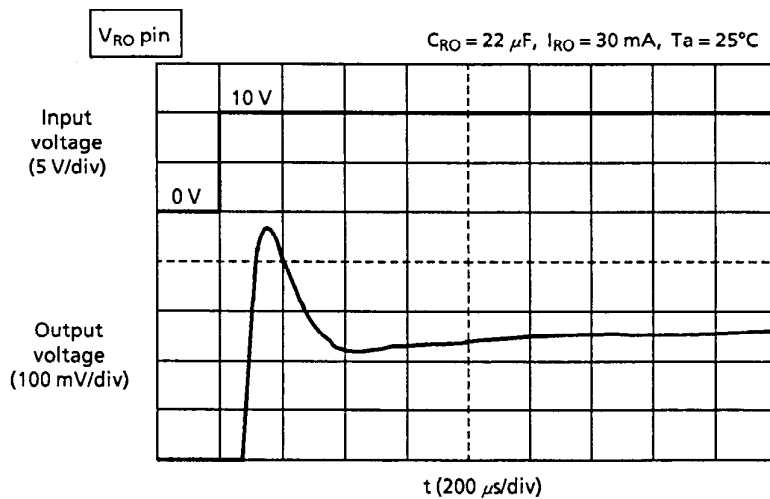


Figure 13 Type II ringing waveform (V<sub>RO</sub> pin)

Table 7 Type II parameter dependency

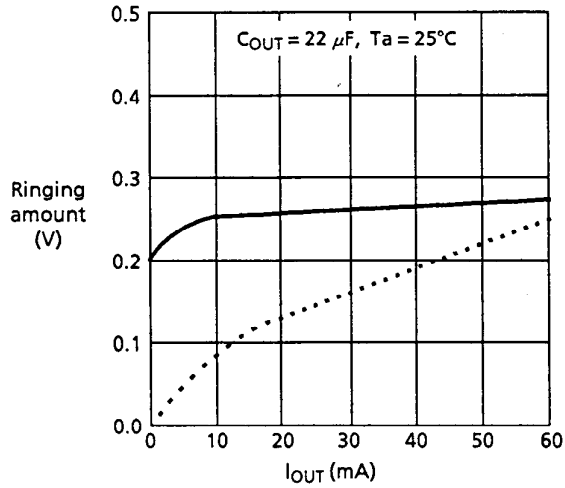
Parameter	Conditions	Method to decrease overshoot	Method to decrease undershoot
Output current I <sub>OUT</sub>	5 to 60 mA	—	—
Load capacitance C <sub>OUT</sub>	5 to 22 μF	Decrease	Decrease
Load capacitance C <sub>OUT</sub>	22 to 47 μF	Increase	Increase
Temperature T <sub>a</sub>	-40°C to +85°C	Low temperature	Low temperature

For reference, the following pages describe the results of measuring the ringing amounts at the V<sub>OUT</sub> and V<sub>RO</sub> pins using the output current (I<sub>OUT</sub>), load capacitance (C<sub>RO</sub>), input fluctuation width (ΔV<sub>IN</sub>), and temperature as parameters.

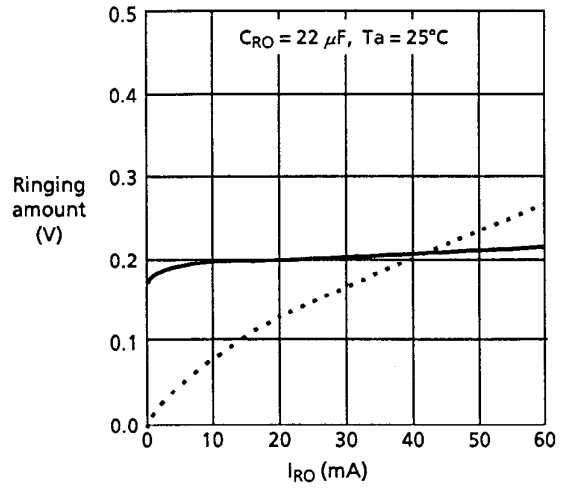
Reference data: Type I

1.  $I_{OUT}$  dependency

1.1  $V_{OUT}$  pin

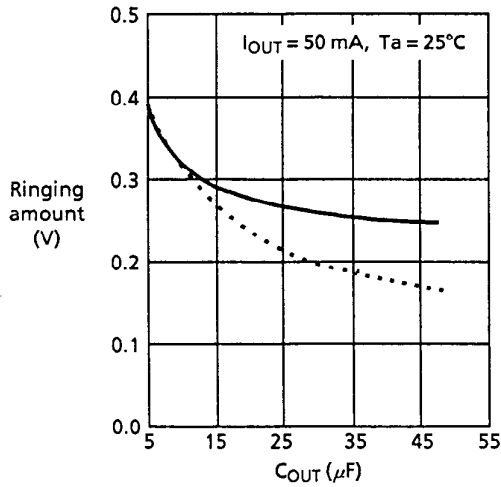


1.2  $V_{RO}$  pin

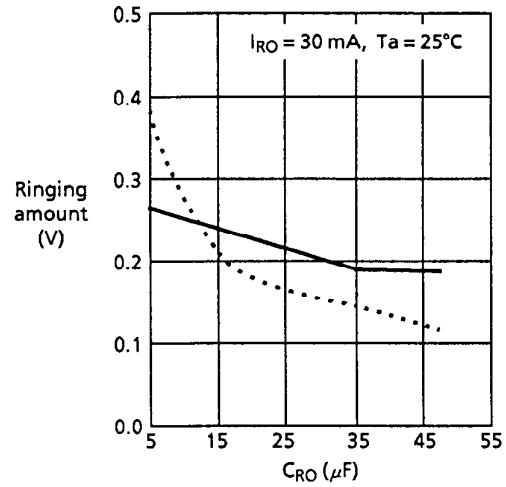


2.  $C_{RO}$  dependency

2.1  $V_{OUT}$  pin



2.2  $V_{RO}$  pin

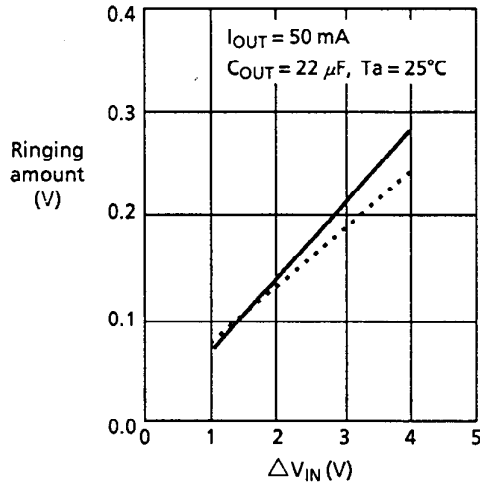


— Overshoot  
 ..... Undershoot

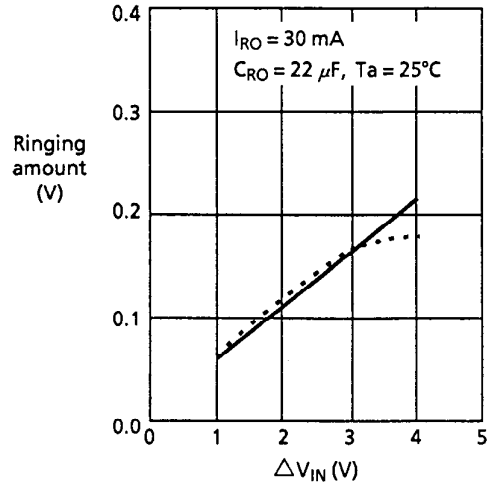
3.  $\Delta V_{IN}$  dependency

$\Delta V_{IN}$  shows the difference between the low voltage fixed to 6 V and the high voltage. For example,  $\Delta V_{IN} = 2$  V means the difference between 6 V and 8 V.

3.1  $V_{OUT}$  pin

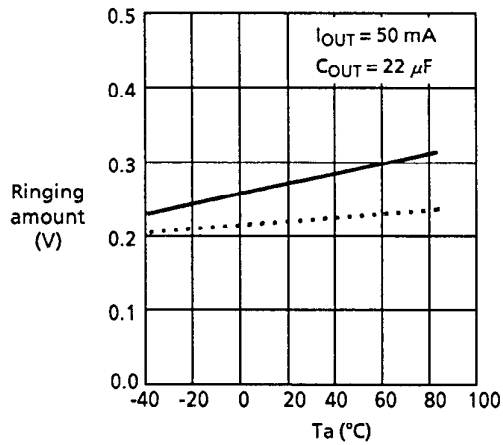


3.2  $V_{RO}$  pin

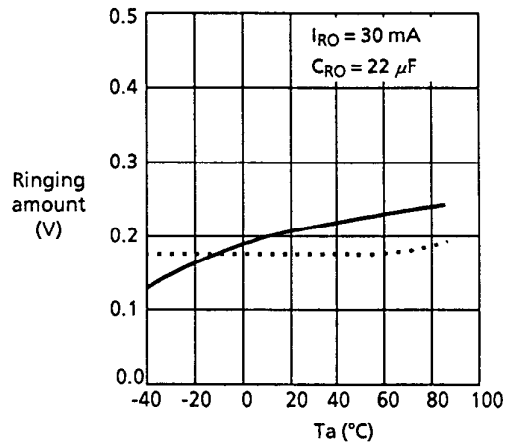


4. Temperature dependency

4.1  $V_{OUT}$  pin



4.2  $V_{RO}$  pin



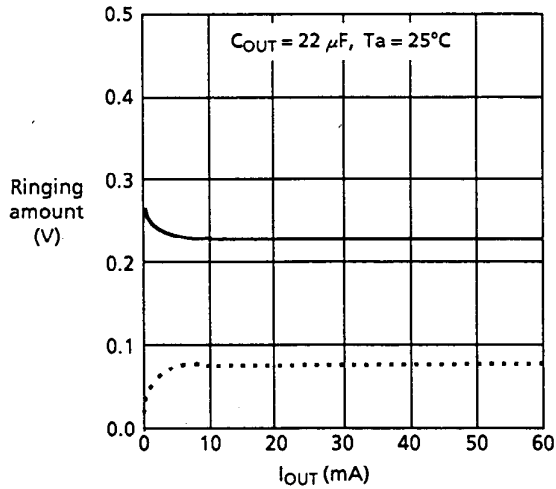
— Overshoot  
..... Undershoot



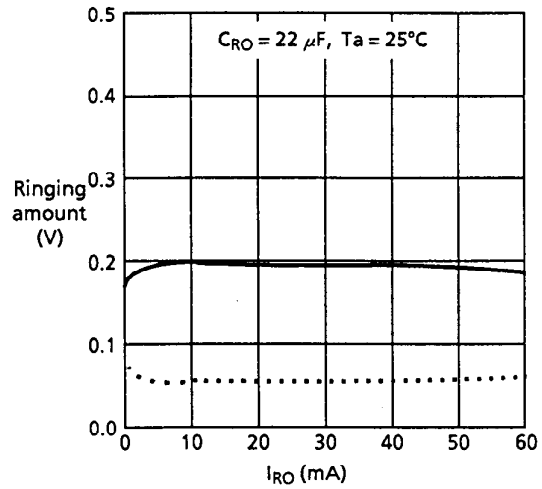
Reference data: Type II

1.  $I_{OUT}$  dependency

1.1  $V_{OUT}$  pin

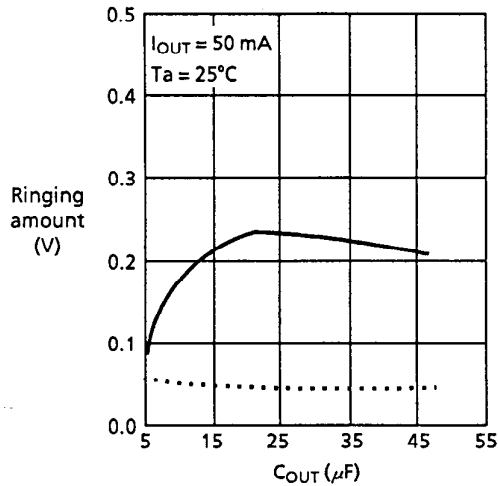


1.2  $V_{RO}$  pin

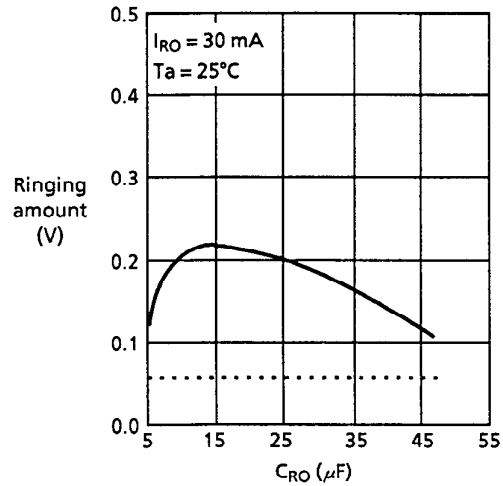


2.  $C_{RO}$  dependency

2.1  $V_{OUT}$  pin

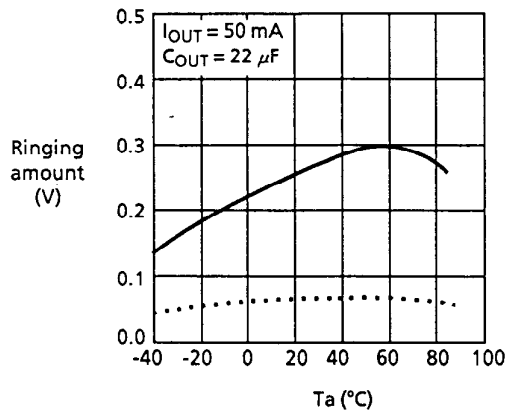


2.2  $V_{RO}$  pin

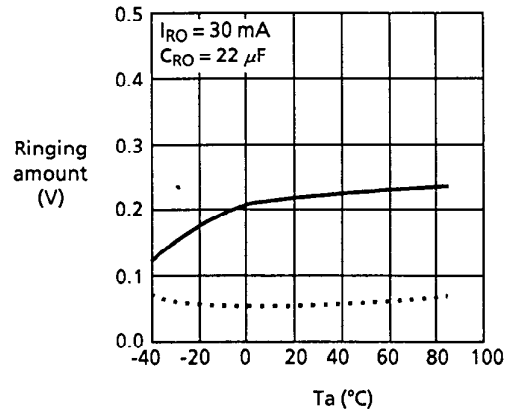


3. Temperature dependency

3.1  $V_{OUT}$  pin



3.2  $V_{RO}$  pin



— Overshoot  
 ..... Undershoot

2. Load transient response based on output current fluctuation

The overshoot and undershoot are caused in the output voltage if the output current fluctuates between 10  $\mu\text{A}$  and 50 mA (between 10  $\mu\text{A}$  and 30 mA at the  $V_{RO}$  pin) while the input voltage is constant. Figure 14 shows the output voltage fluctuation due to change of output current. Figure 15 shows the measuring circuit for reference. The latter half of this section describes ringing waveform and parameter dependency.

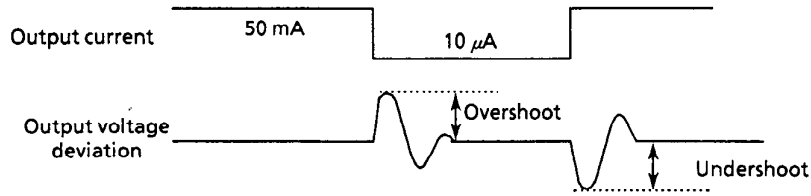


Figure 14

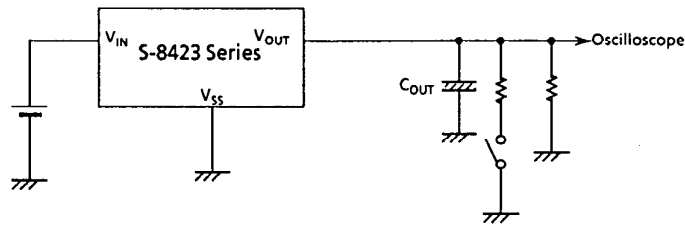


Figure 15 Measuring circuit

Output current fluctuation causes ringing. Figure 18 shows the ringing waveform at the  $V_{OUT}$  pin and Figure 19 shows that waveform at the  $V_{RO}$  pin.

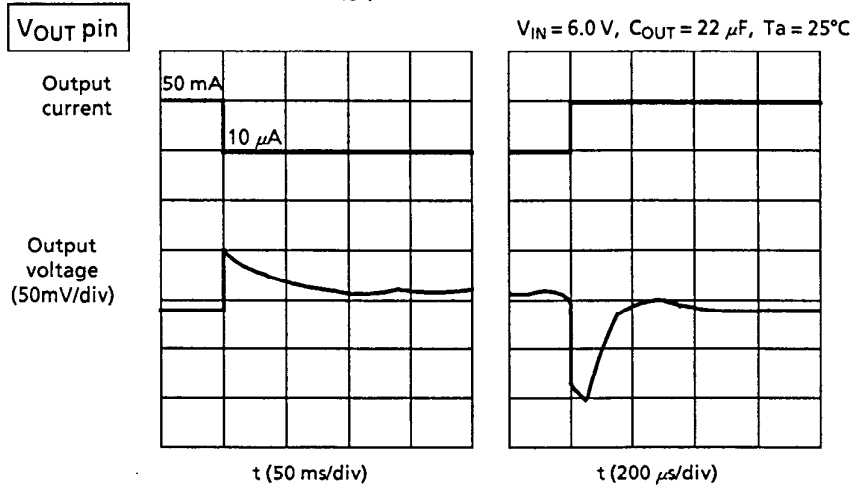


Figure 16 Ringing waveform due to output current fluctuation ( $V_{OUT}$  pin)

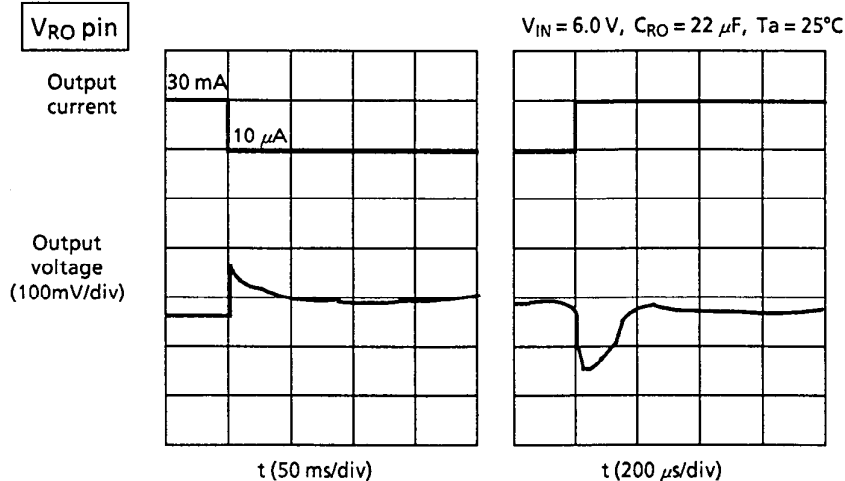


Figure 17 Ringing waveform due to output current fluctuation ( $V_{RO}$  pin)

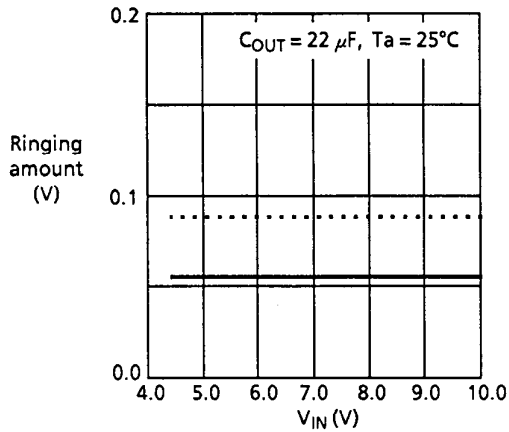
**Table 8 Parameter dependency due to output current fluctuation**

Parameter	Method to decrease overshoot	Method to decrease undershoot
Input voltage $V_{IN}$	—	—
Load capacitance $C_{RO}$	Increase	Increase
Output fluctuation $\Delta I_{OUT}$	Decrease	Decrease
Temperature $T_a$	Low temperature	Low temperature

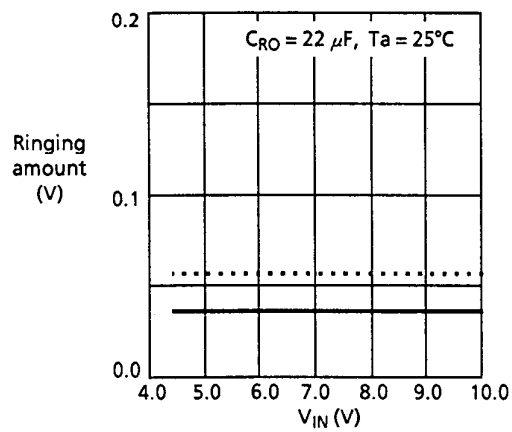
**Reference data**

1.  $V_{IN}$  dependency

1.1  $V_{OUT}$  pin

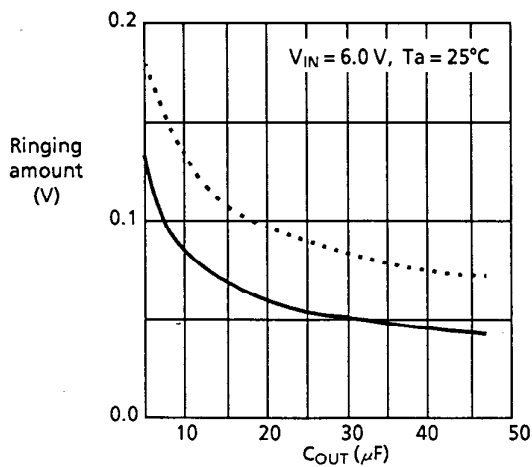


1.2  $V_{RO}$  pin

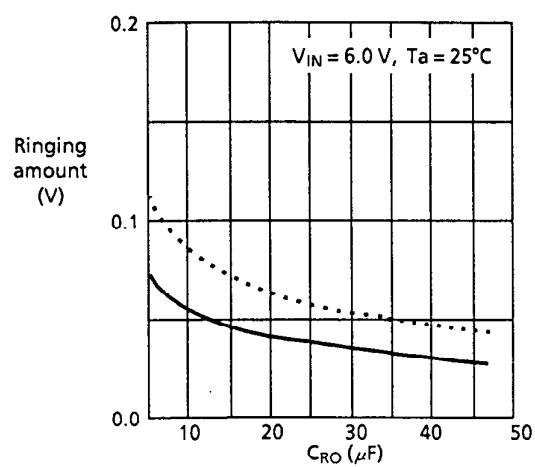


2.  $C_{OUT}$  dependency

2.1  $V_{OUT}$  pin



2.2  $V_{RO}$  pin

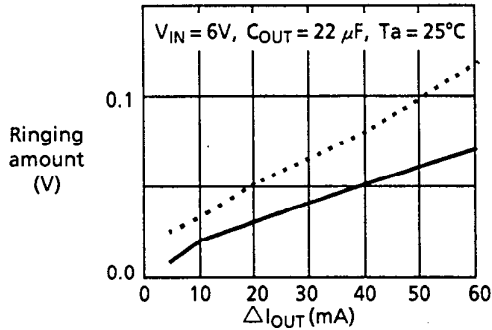


— Overshoot  
 ..... Undershoot

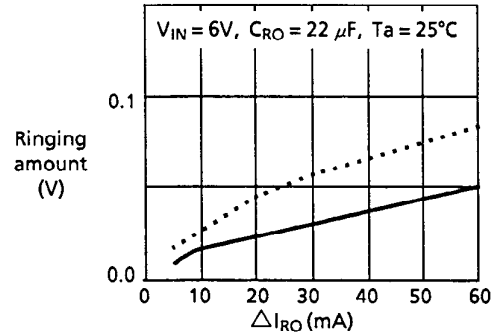
3.  $\Delta I_{OUT}$  Dependency

$\Delta I_{OUT}$  or  $\Delta I_{RO}$  shows the fluctuation between the low current stabilized at 10  $\mu A$  and the high current. For example,  $\Delta I_{OUT} = 10$  mA means the fluctuation between 10  $\mu A$  and 10 mA.

3.1  $V_{OUT}$  pin

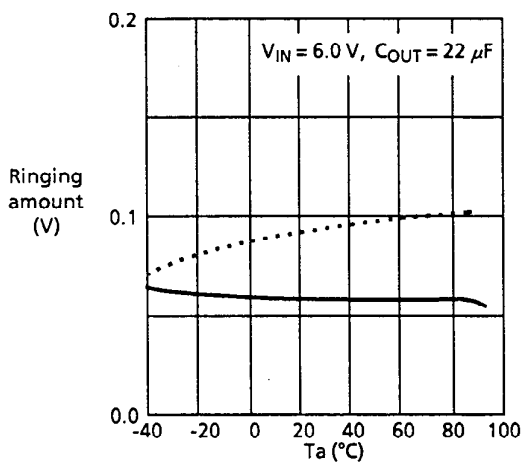


3.2  $V_{RO}$  pin

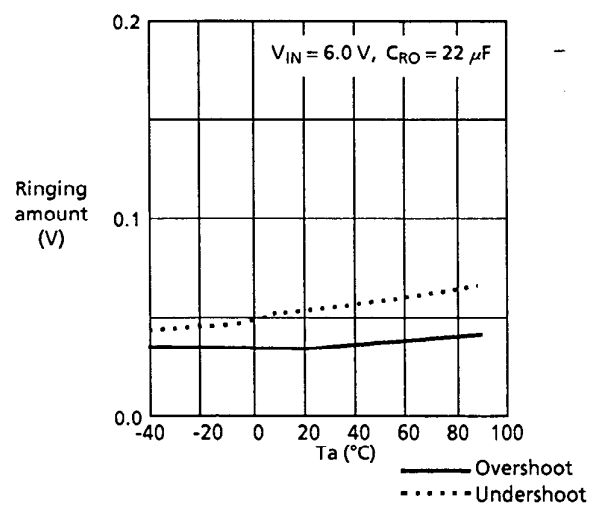


4. Temperature dependency

4.1  $V_{OUT}$  pin



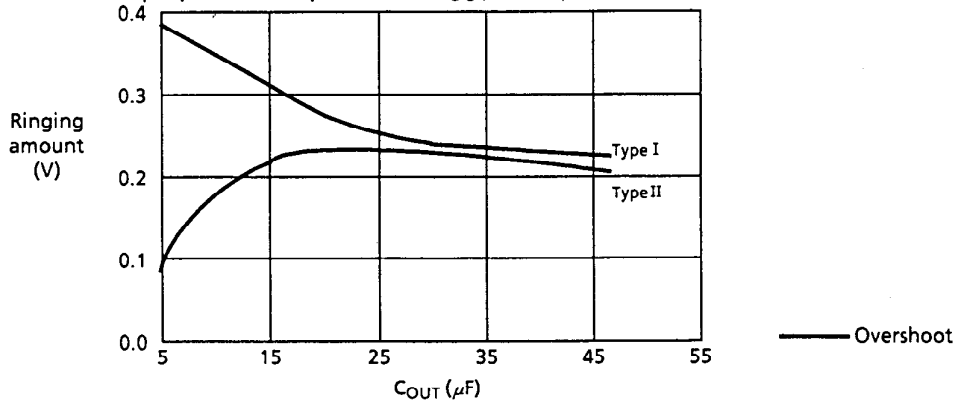
4.2  $V_{RO}$  pin



**3. Selecting Load Capacitance**

The results in 1 and 2 show that the parameter dependency due to the input voltage fluctuation of type II is the opposite of type I, and the output current fluctuation (the amount of ringing is small). Comparing types I and II with respect to the input voltage fluctuation allows the proper load capacitance to be determined.

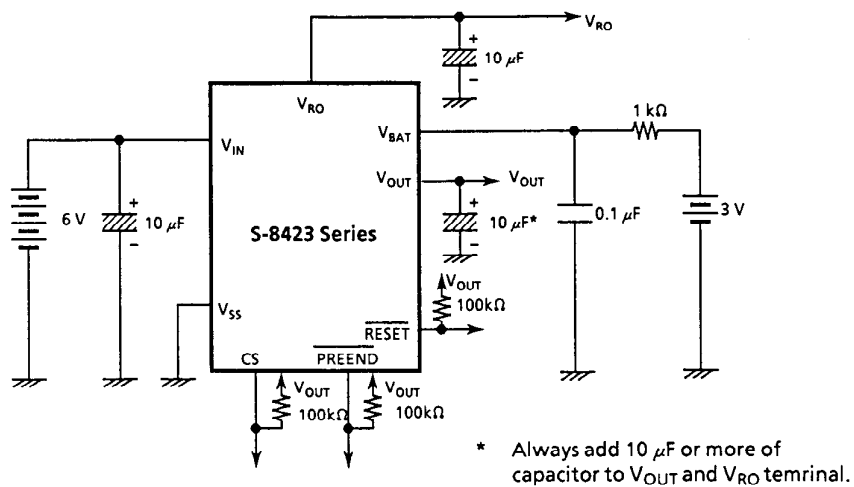
For example, Figure 18 shows the  $C_{OUT}$  dependency of types I and II at  $V_{OUT}$  pin, respectively. This shows that the proper load capacitance  $C_{OUT}$  is 22  $\mu F$  or more.



**Figure 18**

When IC chips or capacitors connected to the  $V_{RO}$  and  $V_{OUT}$  pins have sufficient room for overshoot and little room for undershoot ( $V_{OUT}$  output voltage is close to the detection voltage of the  $\overline{RESET}$  voltage detector), use of a capacitor of 22  $\mu F$  or more is recommended. In both cases, check the temperature characteristics.

**Standard Circuit**



**Figure 19**

## ■ Application Circuits

### 1. Merits in designing

- (1) A switching circuit for primary and backup power supplies is usually configured with discrete components. The S-8423 Series enables you to configure the circuit with a single chip. Some microcomputers can enter standby mode (or low clock mode) from normal mode (or high clock mode) only, and need about 3 V each time they are used. If a low voltage (such as the backup voltage) is applied to these microcomputers initially, they may run away and vast current consumption may flow. The S-8423 Series is designed to have a *special sequence* that stops the backup voltage until the primary power supply voltage reaches the initial voltage that trips the switch.
- (2) Systems can be structured easily. Three types of built-in voltage detectors ( $\overline{\text{CS}}$ ,  $\overline{\text{PREEND}}$ , and  $\overline{\text{RESET}}$ ) send three types of voltage detection signal to microcomputers.
- (3) Battery service life are prolonged.
  - The I/O voltage difference of the voltage regulator 2 switch is very small, and allows the primary power supply to be used until just before they are completely discharged.
  - The current consumption during backup operation is very small (2.1  $\mu\text{A}$  max.), and allows the backup power supply to have a long service life.

### 2. Design considerations

- In applications with small  $I_{\text{RO}}$  or  $I_{\text{OUT}}$ , output voltages ( $V_{\text{RO}}$  and  $V_{\text{OUT}}$ ) may rise to cause the load stability to violate standards. Set  $I_{\text{RO}}$  and  $I_{\text{OUT}}$  to 10  $\mu\text{A}$  or more.
- Attach the proper capacitor to the  $V_{\text{OUT}}$  pin to prevent the  $\overline{\text{RESET}}$  voltage detector (which monitors the  $V_{\text{OUT}}$  pin) from being active due to undershoot.
- Watch for overshoot and ensure it does not exceed the ratings of the IC chips and/or capacitors attached to the  $V_{\text{RO}}$  and  $V_{\text{OUT}}$  pins.
- Power dissipation of SSOP8 package is shown as Figure 20.
- To prevent improper oscillation of the IC, attach a capacitor of 0.01  $\mu\text{F}$  or more to the  $V_{\text{RO}}$  pin.
- When the  $V_{\text{IN}}$  starts to rise from voltage that is more than  $V_{\text{SW1}}$ , a low pulse of less than 4 ms flows through the  $\overline{\text{PREEND}}$  pin even when  $V_{\text{BAT}}$  is more than the  $\overline{\text{PREEND}}$  release voltage. Thus when monitoring the  $\overline{\text{PREEND}}$  pin, always make sure it is more than 4 ms after the rising of  $V_{\text{IN}}$ .
- When  $V_{\text{IN}}$  falls to 0 V, design peripheral circuits so that  $V_{\text{IN}}$  falls at the falling edge of 10 ms or more ( $C_{\text{OUT}} = 10\mu\text{F}$ ,  $C_{\text{RO}} = 10\mu\text{F}$ ). In the case of a falling edge of 10 ms or less, the  $\overline{\text{RESET}}$  pin goes "L."

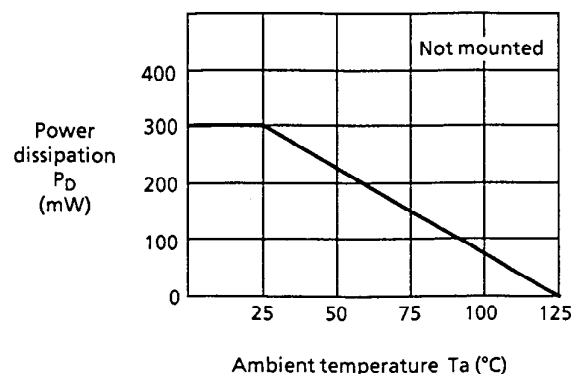


Figure 20 Power dissipation

3. Application examples

(1) When using a timer microcomputer for backup and displaying  $\overline{\text{PREEND}}$  on the main CPU

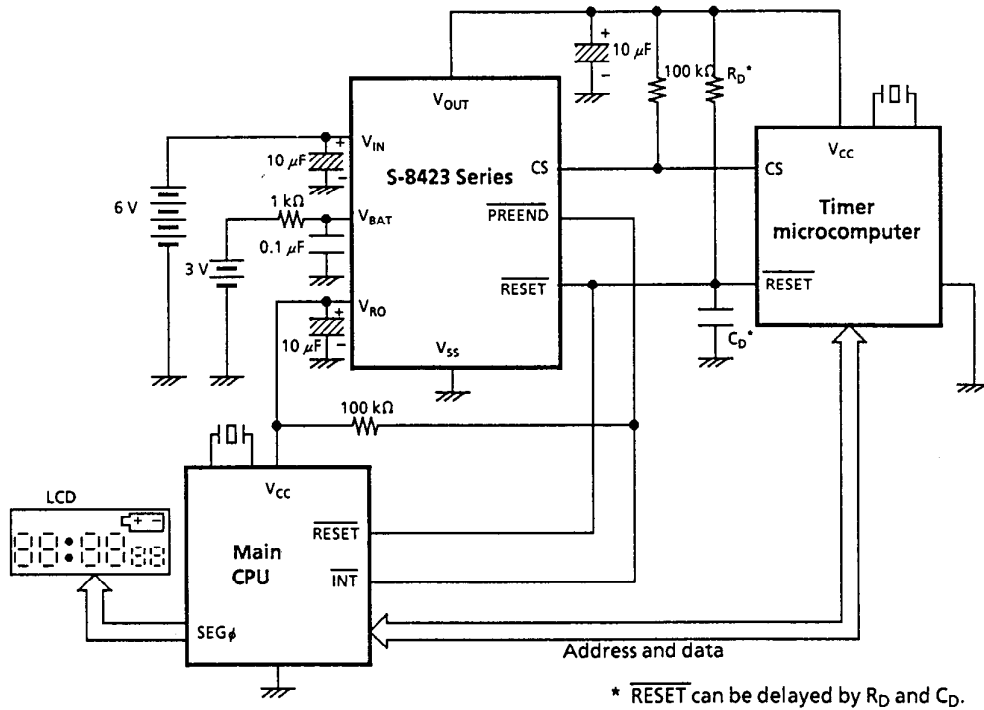
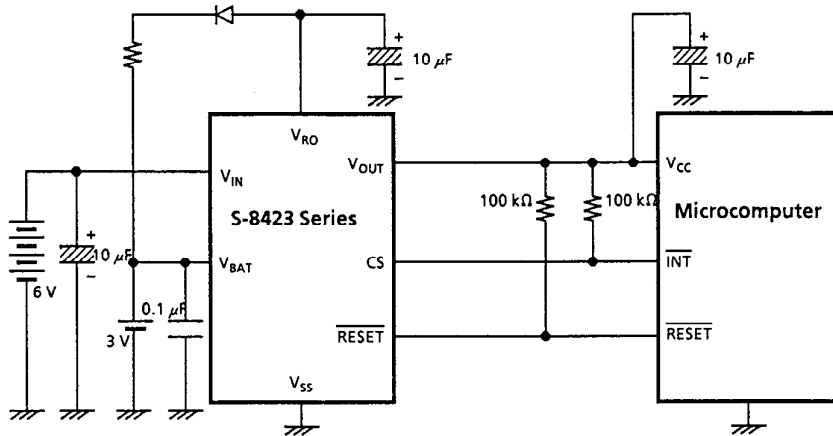


Figure 21

(2) When using rechargeable battery as a backup battery



Backup battery can be floating-recharged by using voltage regulator1

Figure 22

(3) Memory card

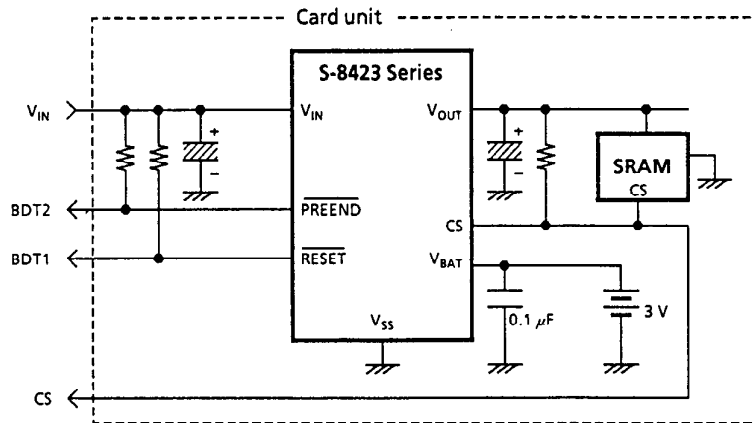


Figure 23

■ Dimensions

8-pin SSOP

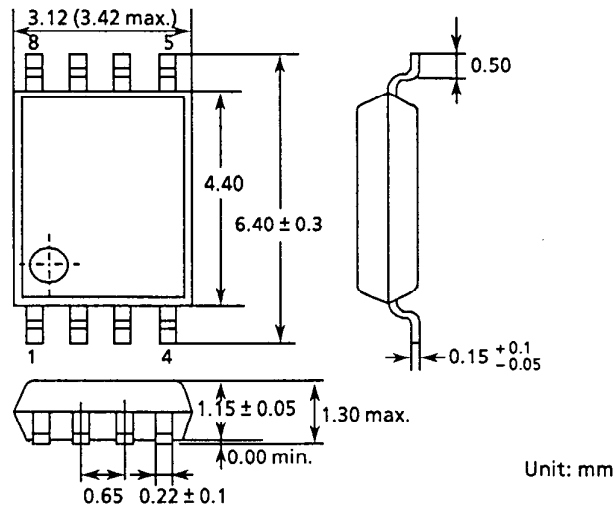
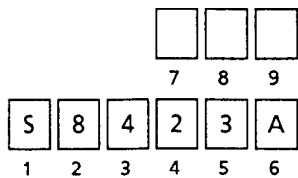


Figure 24

■ Markings



- 1 to 6 : Product name
- 7 : Assembly code
- 8 : Year of assembly (last digit)
- 9 : Month of assembly; Jan. = 1, Feb. = 2, Mar. = 3, Apr. = 4, May = 5, June = 6, July = 7, Aug. = 8, Sept. = 9, Oct. = X, Nov. = Y, Dec. = Z

Figure 25



**BATTERY BACKUP IC**  
**S-8423 Series**

■ **Taping**

1. Tape specifications

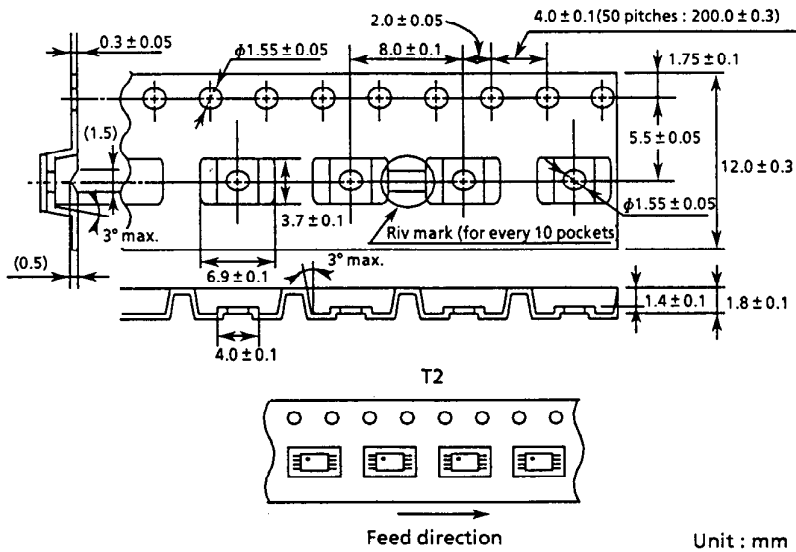


Figure 26

2. Reel specifications

1 reel holds 2000 ICs.

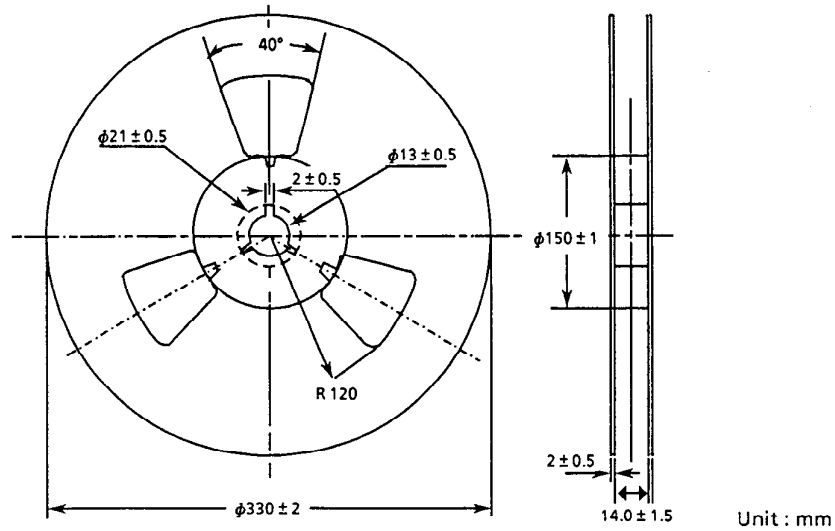


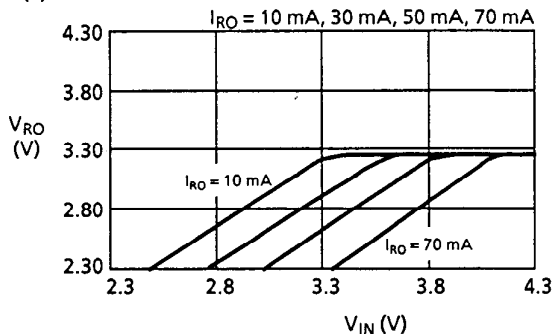
Figure 27

■ Characteristics

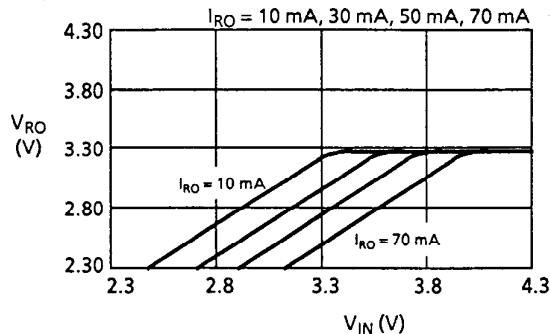
1. Voltage regulator (S-8423AFS)

1.1 Input voltage ( $V_{IN}$ ) – Output voltage ( $V_{RO}$ ) (REG1)

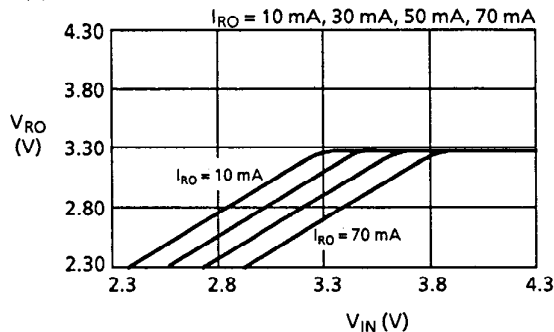
(1)  $T_a = 85^\circ\text{C}$



(2)  $T_a = 25^\circ\text{C}$

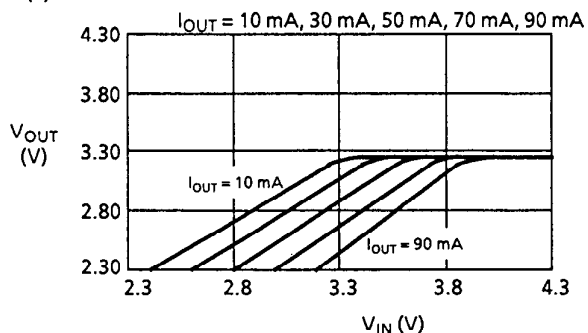


(3)  $T_a = -40^\circ\text{C}$

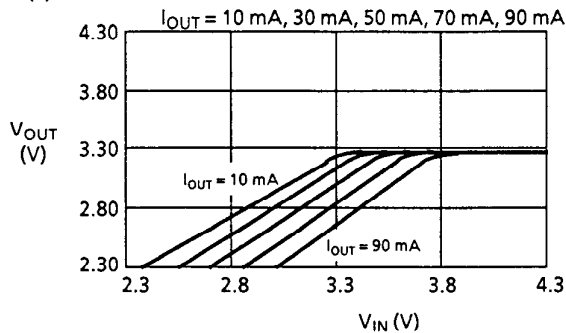


1.2 Input voltage ( $V_{IN}$ ) – Output voltage ( $V_{OUT}$ ) (REG2)

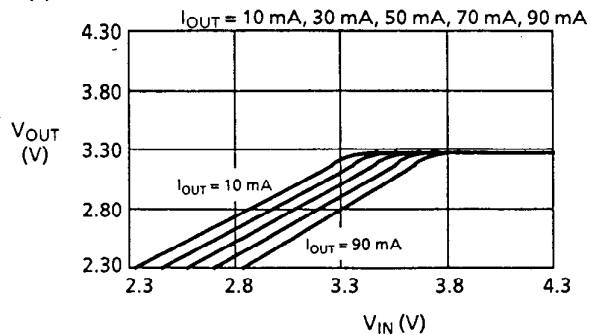
(1)  $T_a = 85^\circ\text{C}$



(2)  $T_a = 25^\circ\text{C}$

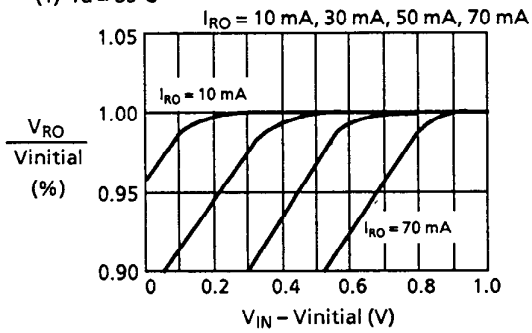


(3)  $T_a = -40^\circ\text{C}$

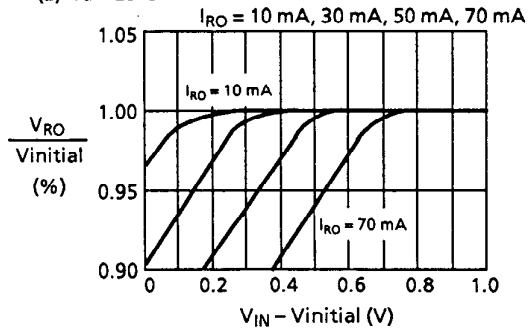


1.3 I/O voltage difference ( $V_{dif1}$ ) – Output voltage (REG1)

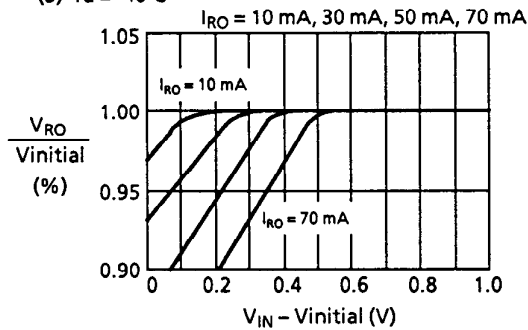
(1)  $T_a = 85^\circ\text{C}$



(2)  $T_a = 25^\circ\text{C}$



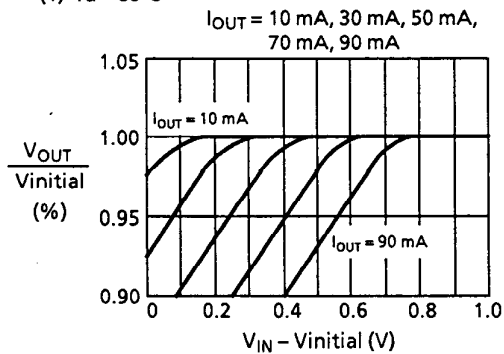
(3)  $T_a = -40^\circ\text{C}$



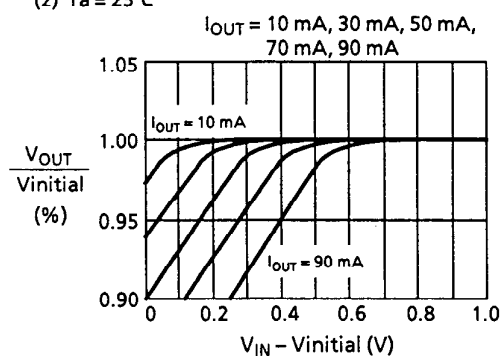
Vinitial :  $V_{RO}$  value when input voltage is 6 V.

1.4 I/O voltage difference ( $V_{dif2}$ ) – Output voltage (REG2)

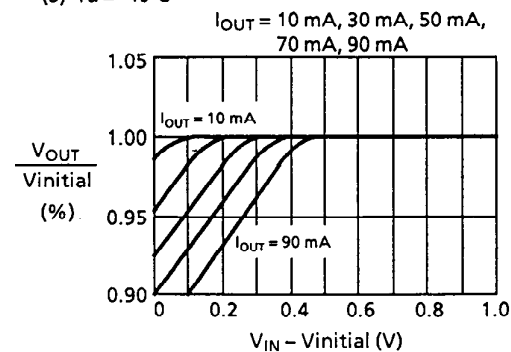
(1)  $T_a = 85^\circ\text{C}$



(2)  $T_a = 25^\circ\text{C}$

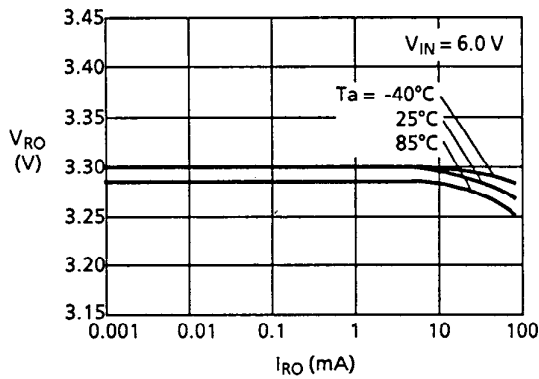


(3)  $T_a = -40^\circ\text{C}$

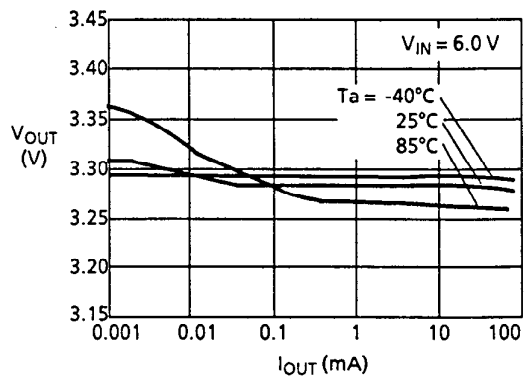


Vinitial :  $V_{OUT}$  value when input voltage is 6 V.

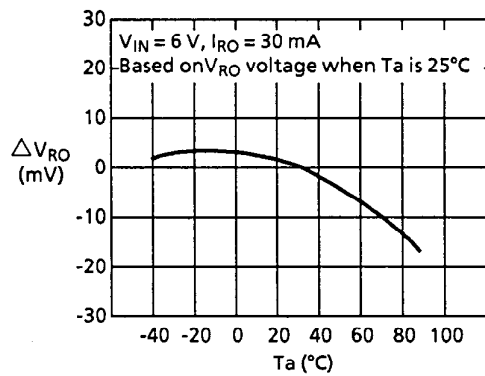
1.5 Output current ( $I_{RO}$ ) - Output voltage ( $V_{RO}$ )



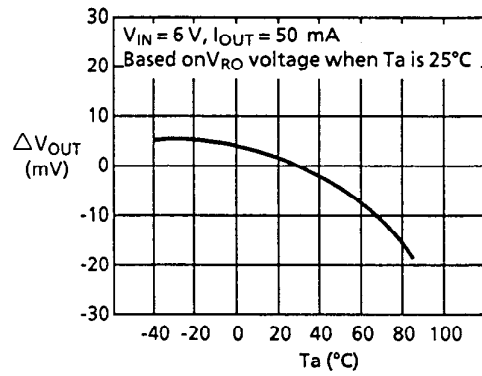
1.6 Output current ( $I_{OUT}$ ) - Output voltage ( $V_{OUT}$ )



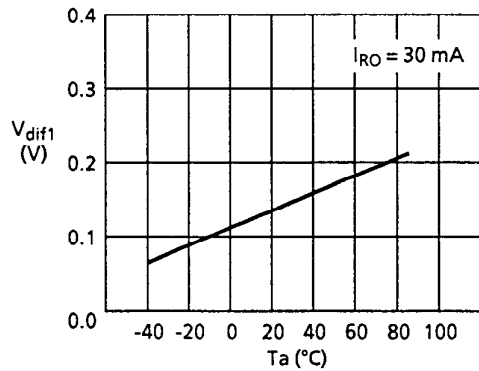
1.7 Output voltage ( $V_{RO}$ ) - Temperature



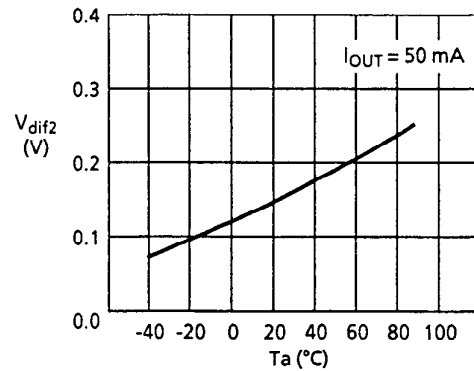
1.8 Output voltage ( $V_{OUT}$ ) - Temperature



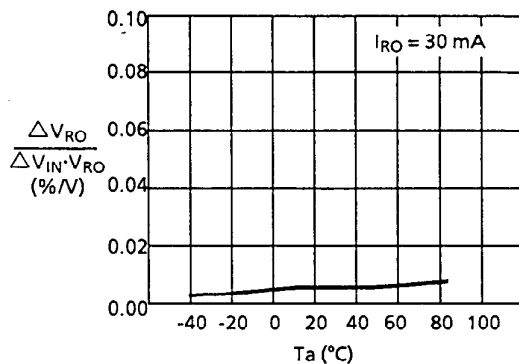
1.9 I/O voltage difference ( $V_{dif1}$ ) - Temperature



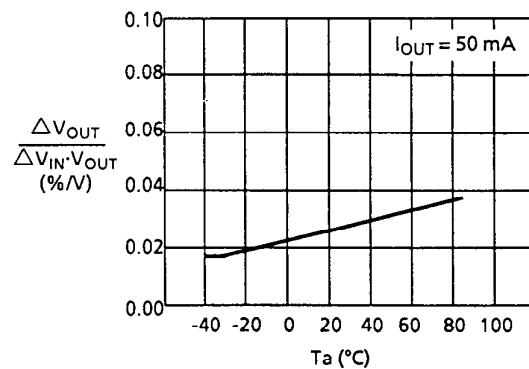
1.10 I/O voltage difference ( $V_{dif2}$ ) - Temperature



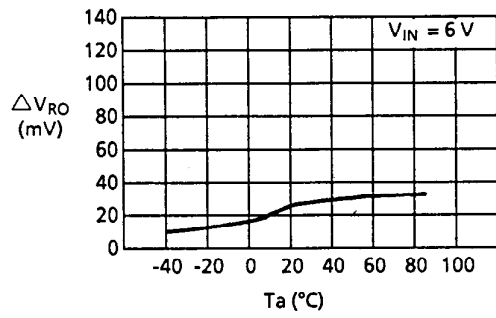
1.11 Input stability ( $V_{RO}$ ) - Temperature



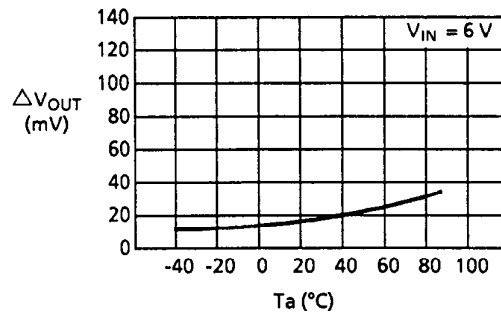
1.12 Input stability ( $V_{OUT}$ ) - Temperature



1.13 Load stability ( $V_{RO}$ ) – Temperature



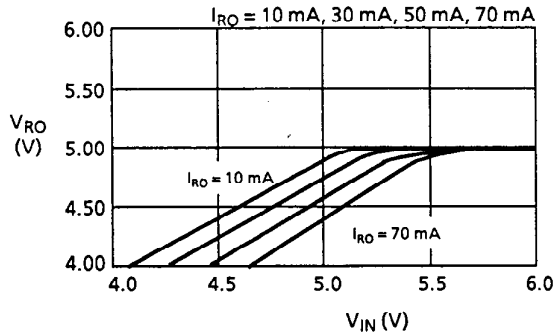
1.14 Load stability ( $V_{OUT}$ ) – Temperature



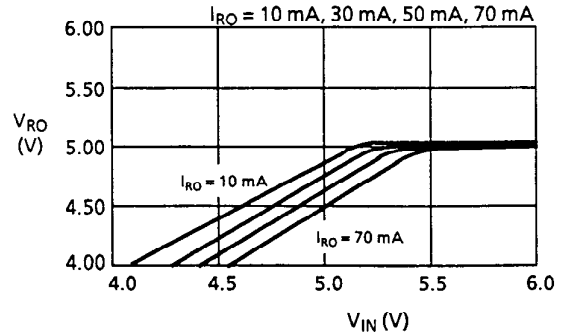
- 2. Voltage regulator (S-8423LFS)

2.1 Input voltage ( $V_{IN}$ ) – Output voltage ( $V_{RO}$ ) (REG1)

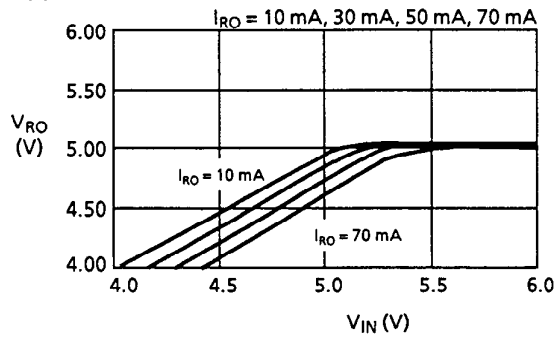
(1)  $T_a = 85^\circ\text{C}$



(2)  $T_a = 25^\circ\text{C}$

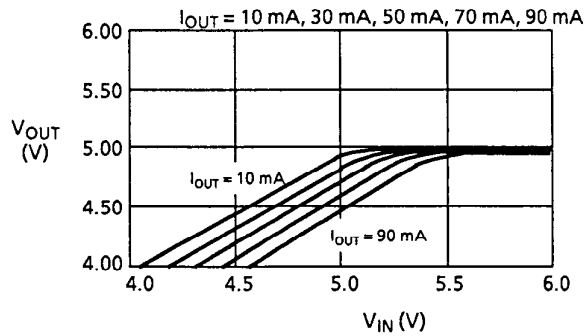


(3)  $T_a = -40^\circ\text{C}$

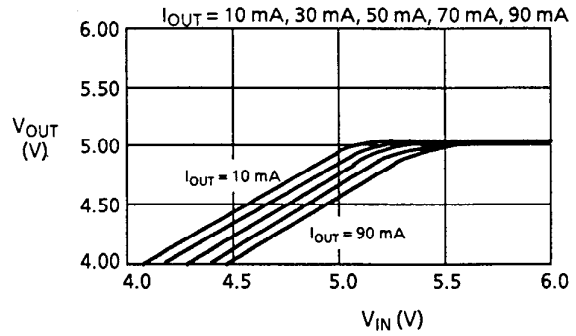


2.2 Input voltage ( $V_{IN}$ ) – Output voltage ( $V_{OUT}$ ) (REG2)

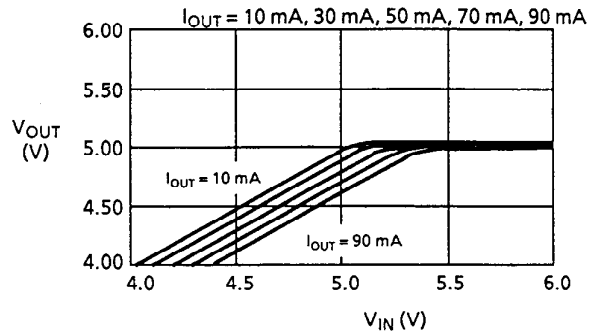
(1)  $T_a = 85^\circ\text{C}$



(2)  $T_a = 25^\circ\text{C}$

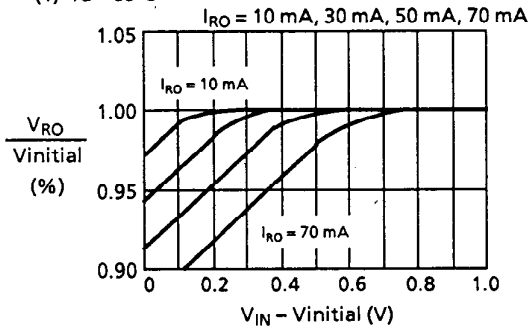


(3)  $T_a = -40^\circ\text{C}$

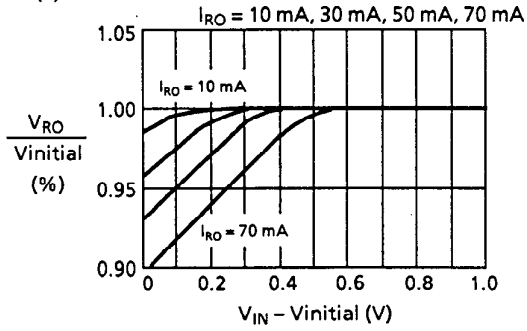


2.3 I/O voltage difference ( $V_{dif1}$ ) – Output voltage (REG1)

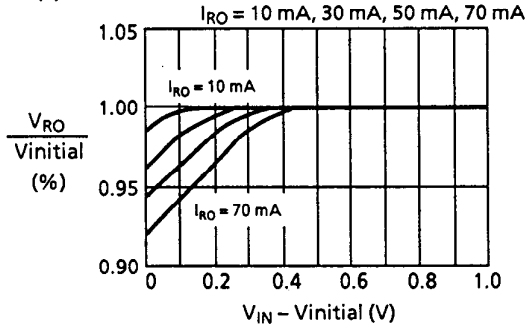
(1)  $T_a = 85^\circ\text{C}$



(2)  $T_a = 25^\circ\text{C}$



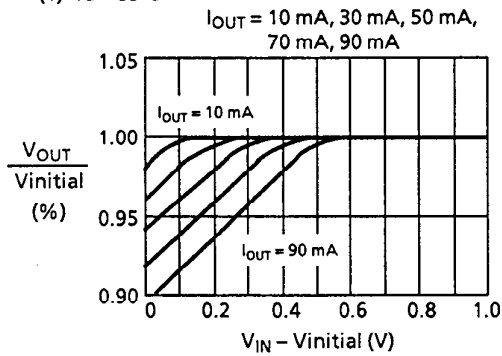
(3)  $T_a = -40^\circ\text{C}$



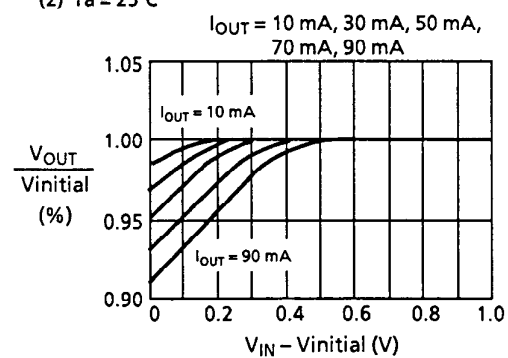
Vinitial :  $V_{RO}$  value when input voltage is 6 V.

2.4 I/O voltage difference ( $V_{dif2}$ ) – Output voltage (REG2)

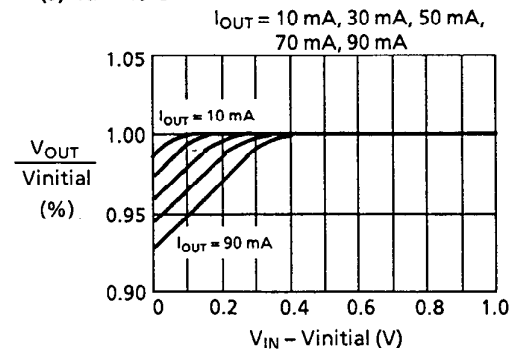
(1)  $T_a = 85^\circ\text{C}$



(2)  $T_a = 25^\circ\text{C}$

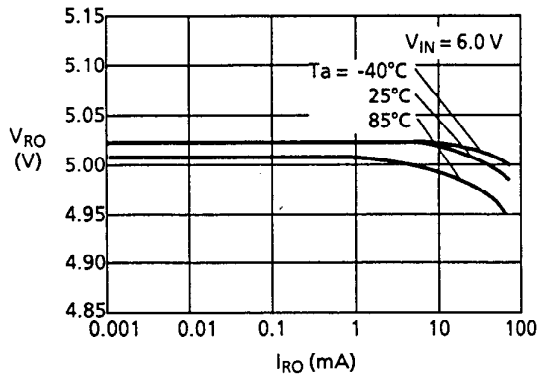


(3)  $T_a = -40^\circ\text{C}$

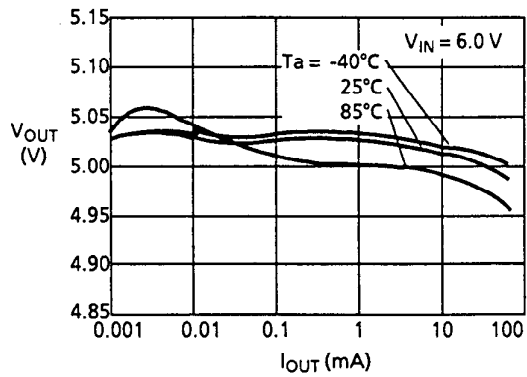


Vinitial :  $V_{OUT}$  value when input voltage is 6 V.

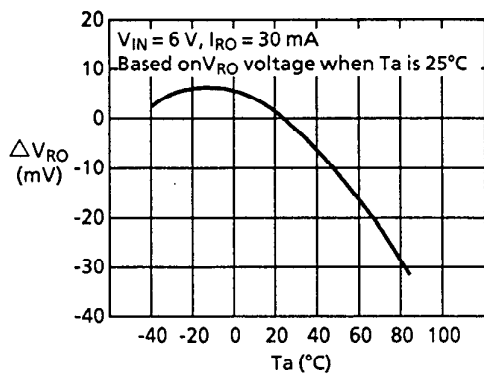
2.5 Output current ( $I_{RO}$ ) – Output voltage ( $V_{RO}$ )



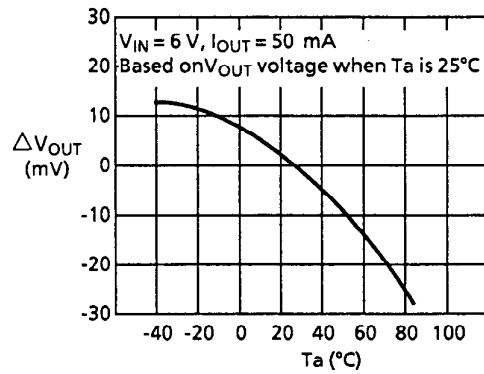
2.6 Output current ( $I_{OUT}$ ) – Output voltage ( $V_{OUT}$ )



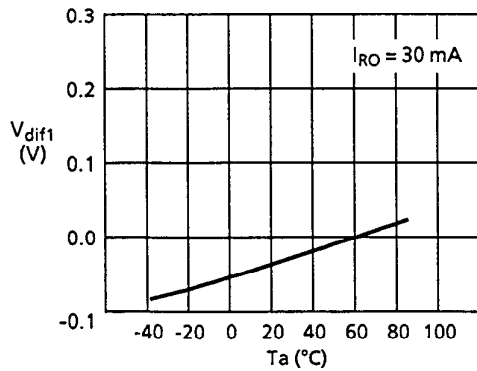
2.7 Output voltage ( $V_{RO}$ ) – Temperature



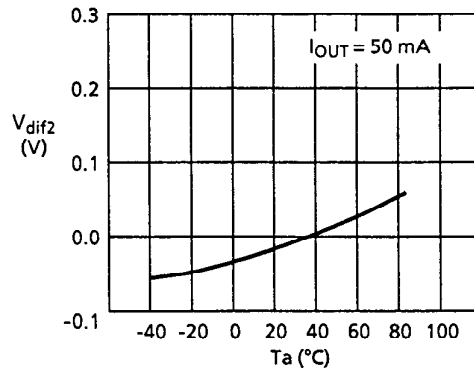
2.8 Output voltage ( $V_{OUT}$ ) – Temperature



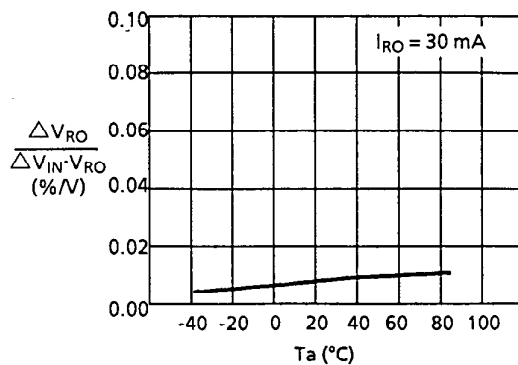
2.9 I/O voltage difference ( $V_{dif1}$ ) – Temperature



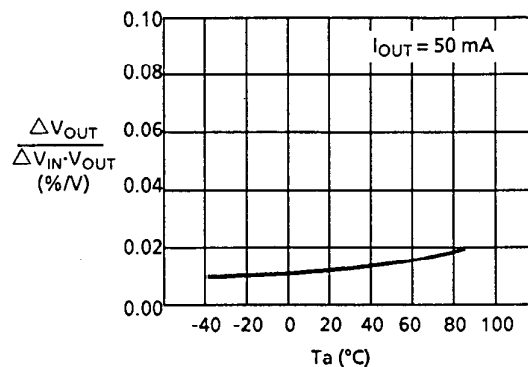
2.10 I/O voltage difference ( $V_{dif2}$ ) – Temperature



2.11 Input stability ( $V_{RO}$ ) – Temperature

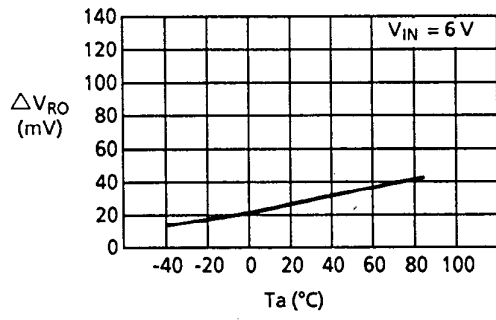


2.12 Input stability ( $V_{OUT}$ ) – Temperature

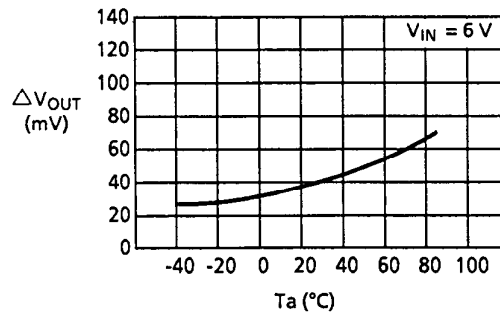




2.13 Load stability ( $V_{RO}$ ) – Temperature

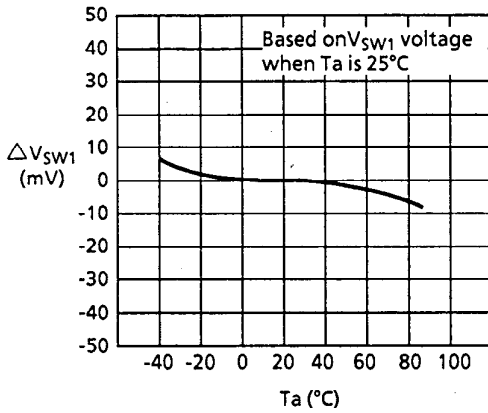


2.14 Load stability ( $V_{OUT}$ ) – Temperature

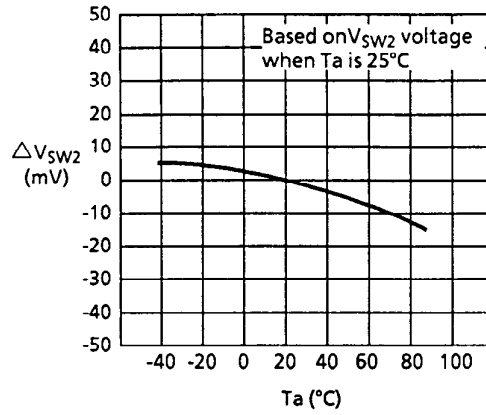


3. Switch

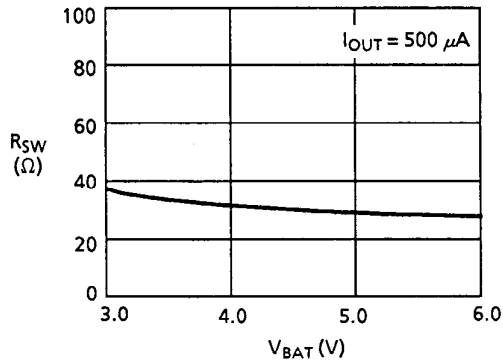
3.1 Switch voltage ( $V_{SW1}$ ) – Temperature



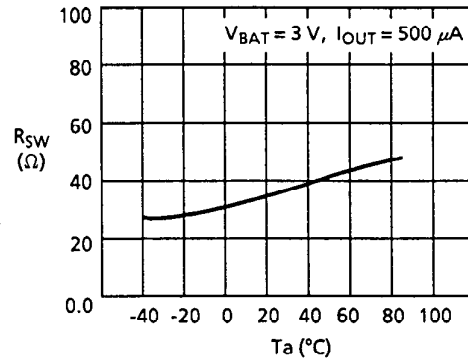
3.2 CS output prohibition voltage ( $V_{SW2}$ ) – Temperature



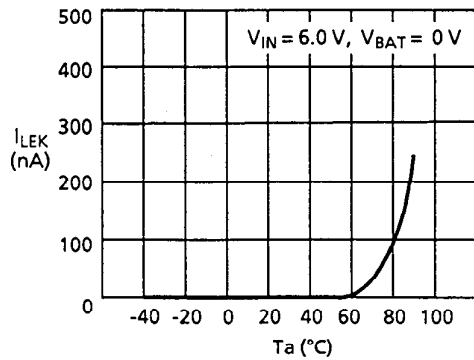
3.3 Input voltage ( $V_{BAT}$ ) –  $V_{BAT}$  switch resistance



3.4  $V_{BAT}$  switch resistance – Temperature



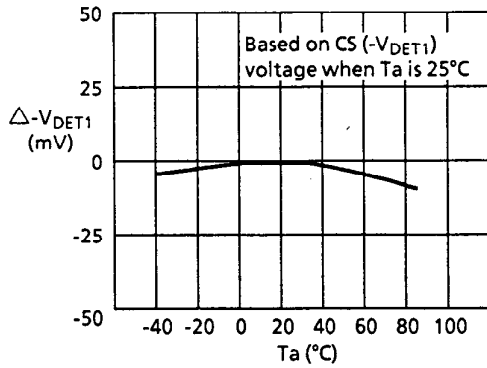
3.5  $V_{BAT}$  switch leak current ( $I_{LEK}$ ) – Temperature



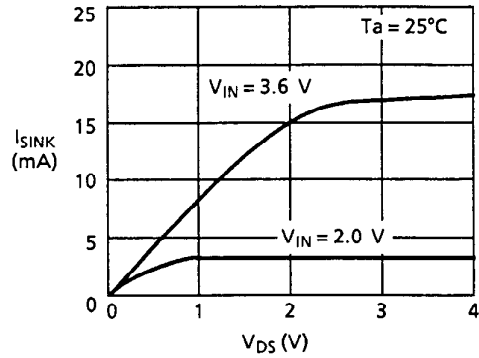
4. Voltage detectors

4.1 CS voltage detector

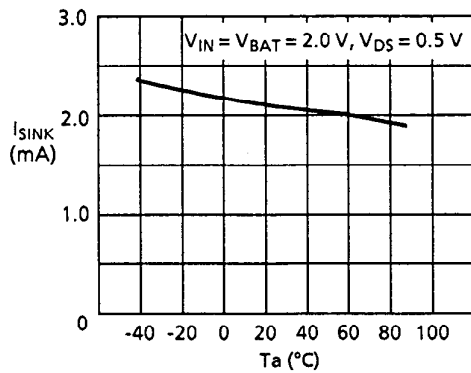
(1) Detection voltage ( $-V_{DET1}$ ) - Temperature



(2) Output current ( $I_{SINK}$ )

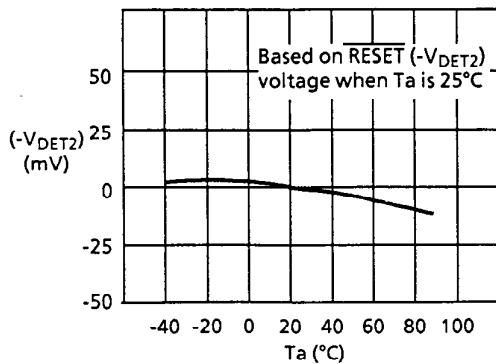


(3) Output current ( $I_{SINK}$ ) - Temperature

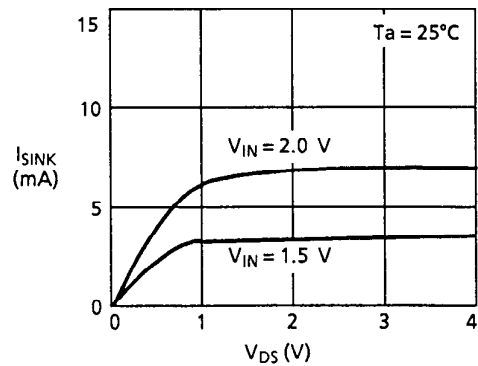


4.2 RESET voltage detector

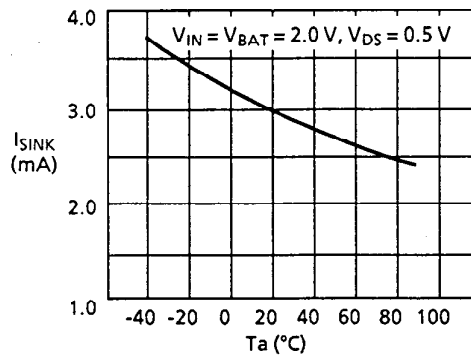
(1) Detection voltage ( $-V_{DET2}$ ) - Temperature



(2) Output current ( $I_{SINK}$ )

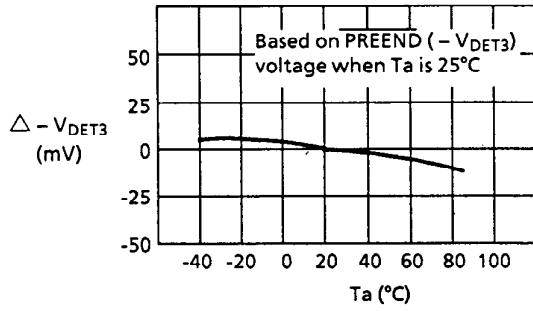


(3) Output current ( $I_{SINK}$ ) - Temperature

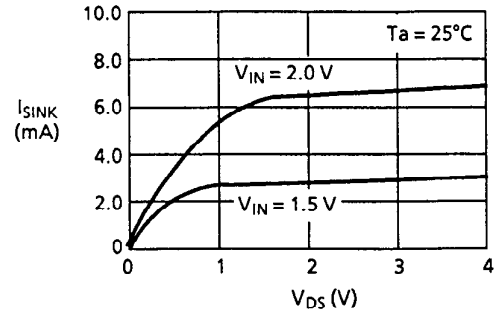


4.3  $\overline{\text{PREEND}}$  voltage detector

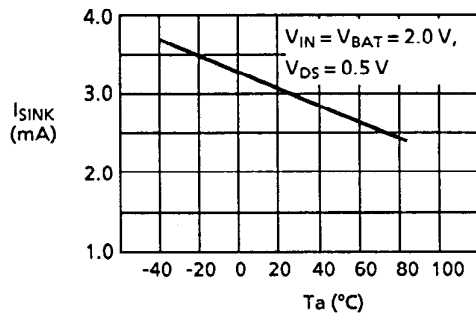
(1) Detection voltage ( $-V_{\text{DET3}}$ ) – Temperature



(2) Output current ( $I_{\text{SINK}}$ )

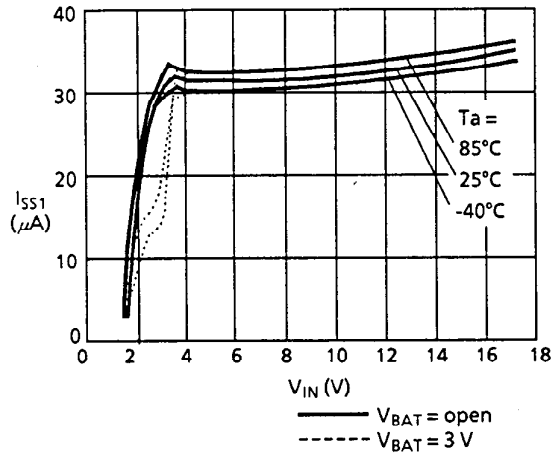


(3) Output current ( $I_{\text{SINK}}$ ) – Temperature

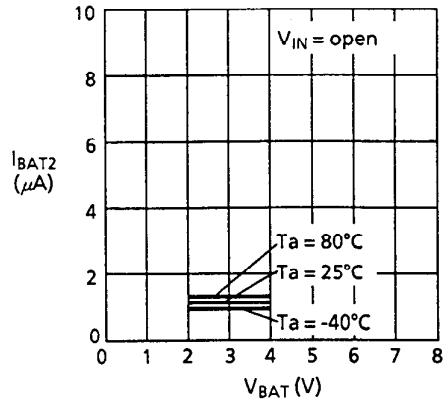


5. Current consumption

5.1  $V_{IN} - V_{IN}$  current consumption ( $I_{SS1}$ )

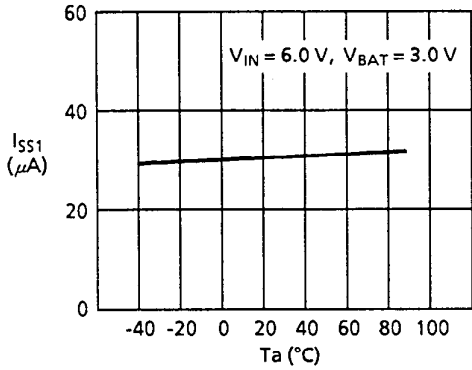


5.2  $V_{BAT} - V_{BAT2}$  current consumption ( $I_{BAT2}$ )

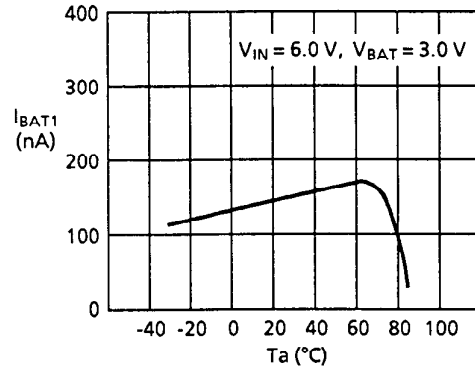


5.3 Temperature

(1)  $I_{SS1}$



(2)  $I_{BAT1}$



(3)  $I_{BAT2}$

