# **UBA2211**

# Half-bridge power IC family for CFL lamps

Rev. 2.1 — 7 March 2011

Preliminary data sheet

## 1. General description

The UBA2211 family of integrated circuits are a range of high voltage monolithic ICs for driving Compact Fluorescent Lamps (CFL) in half-bridge configurations. The family is specifically designed to provide easy integration of lamp loads across a range of burner power and mains voltages.

Patented technologies and integrated protection types:

#### Preheat state:

- Preheat applications: Adjustable current controlled preheat mode technology enables the preheat time (t<sub>ph</sub>) and preheat current to be set. This mode is triggered during start up.
- Non-preheat applications: Glow-time control minimizes electrode damage just after ignition of the lamp.
- Saturation Current Protection (SCP): This protection is active during ignition ensuring the lamp inductor can operate at the saturation current limit without exceeding the current ratings of the integrated half-bridge power transistors.
- RMS current control: The IC internally calculates the RMS current and changes the
  frequency (f<sub>osc</sub>) to ensure the RMS current remains constant. RMS current control is
  active in the burn state ensuring a constant half-bridge burner current and IC
  dissipation. The nominal half-bridge burner current is set using the sense resistor
  (R<sub>SENSE</sub>).
- OverTemperature Protection (OTP) and Capacitive Mode Protection (CMP):
   Overtemperature and capacitive mode protection monitor the application ensuring, in non-standard conditions, correct system shutdown and a safe condition at the burner's end-of-life.

#### 2. Features and benefits

### 2.1 System integration

- Integrated half-bridge power transistors
  - ♦ UBA2211A: 220 V mains; 13.5 Ω; 0.9 A maximum ignition current
  - ♦ UBA2211B: 220 V mains; 9 Ω; 1.35 A maximum ignition current
  - ♦ UBA2211C: 220 V mains; 6.6 Ω; 1.85 A maximum ignition current
- Integrated bootstrap diode
- Integrated high voltage supply



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### 2.2 Burner lifetime

- Current controlled preheat with adjustable preheat time and preheat current
- Minimum glow time control to support cold start
- Lamp power independent from mains voltage variations
- Lamp inductor saturation protection during ignition

### 2.3 Safety

- Overtemperature protection
- Capacitive mode protection
- Overpower control
- System shutdown at burner end of life

#### 2.4 Ease of use

- Adjustable operating frequency for easy fit with various burners
- Each device in the family incorporates the same controller functionality ensuring easy power scaling and roll-out across a complete range of CFLs

# 3. Applications

■ Compact Fluorescent Lamps up to 25 W for indoor and outdoor applications

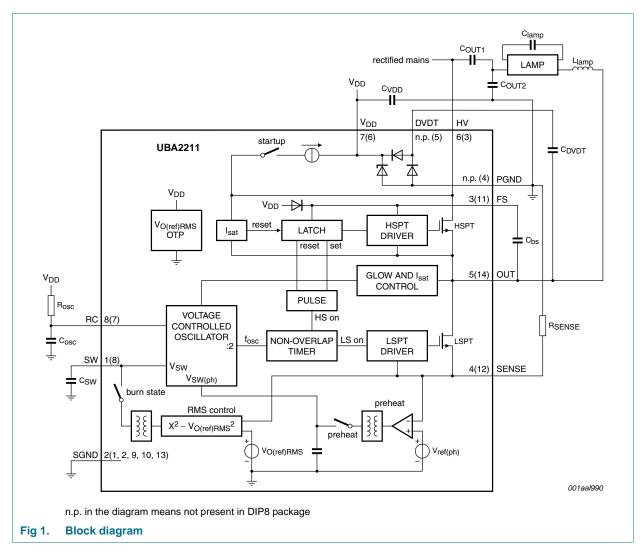
# 4. Ordering information

Table 1. Ordering information

Type number	Package					
	Name	Description	Version			
UBA2211AP/N1	DIP8	plastic dual in-line package; 8 leads (300 mil)	SOT97-1			
UBA2211BP/N1						
UBA2211CP/N1						
UBA2211AT/N1	SO14	plastic small outline package; 14 leads; body width 3.9 mm	SOT108-1			
UBA2211BT/N1						
UBA2211CT/N1						

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# 5. Block diagram



In the SO14 package, the two diodes which are required for the DVDT supply are integrated and connected between pins DVDT and PGND.

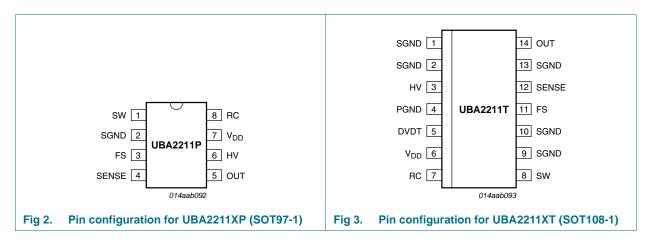
In the DIP8 package, these diodes are not bonded out and need to be placed externally.

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# 6. Pinning information

### 6.1 Pinning



### 6.2 Pin description

Table 2. Pin description

Symbol	Pin		Description
	UBA2211XP	UBA2211XT	
SW	1	8	sweep timing and VCO input
SGND	2	1, 2, 9, 10, 13	signal ground
FS	3	11	high-side floating supply output
SENSE	4	12	voltage sense for preheat and RMS control
OUT	5	14	half-bridge output
HV	6	3	high-voltage supply
$V_{DD}$	7	6	internal low-voltage supply output
RC	8	7	internal oscillator input
DVDT	n.p.	5	DVDT supply input
PGND	n.p.	4	DVDT supply ground

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## 7. Functional description

### 7.1 Supply voltage

The UBA2211 family is powered using the start-up current source and the  $V_{DD}$  supply. When the voltage on pin HV increases, the  $V_{DD}$  capacitor ( $C_{VDD}$ ) is charged using the internal Junction gate Field-Effect Transistor (JFET) current source. The voltage on pin  $V_{DD}$  rises until  $V_{DD}$  equals  $V_{DD(start)}$ . The start-up current source is then disabled. The half-bridge starts switching causing the charge pump activate and in turn supply  $V_{DD}$ .

The amount of current flowing towards  $V_{DD}$  equals  $V_{HV} \times C_{DVDT} \times f$  where f represents the momentary frequency. The charge pump consists of an external half-bridge capacitor ( $C_{DVDT}$ ). The SO14 package contains two internal diodes with an internal Zener diode. However, with the DIP8 package, these diodes must be mounted externally. The Zener diode ensures the  $V_{DD}$  voltage cannot rise above the maximum  $V_{DD}$  rating.

The DVDT supply has its own ground pin (PGND) to prevent large peak currents from flowing through the external small signal ground pin (SGND).

The start-up current source is enabled when the voltage on pin V<sub>DD</sub> is below V<sub>DD(stop)</sub>.

#### 7.2 Start-up state

When the supply voltage on pin  $V_{DD}$  increases, the IC enters the start-up state. In the start-up state the High-Side Power Transistor (HSPT) is switched off and the Low-Side Power Transistor (LSPT) is switched on. The circuit is reset and the capacitors on the bootstrap pin FS ( $C_{bs}$ ) and the low-voltage supply pin  $V_{DD}$  ( $C_{VDD}$ ) are charged. Pins RC and SW are switched to ground.

When pin  $V_{DD}$  is above  $V_{DD(start)}$ , the start-up state is exited and the preheat state is entered. If the voltage on pin  $V_{DD}$  falls below  $V_{DD(stop)}$ , the system returns to the start-up state.

**Remark:** If OTP is active, the IC remains in the start-up state for as long as this is the case. The  $V_{DD}$  voltage slowly oscillates between  $V_{DD} = V_{DD(stop)}$  and  $V_{DD} = V_{DD(start)}$ .

#### 7.3 Reset

A DC reset circuit is incorporated in the high-side driver. The high-side transistor is switched off when the voltage on pin FS is below the high-side lockout voltage.

#### 7.4 Oscillation control

The oscillation frequency is based on the 555-timer function. A self oscillating circuit is created comprising the external components: resistors  $R_{\text{osc}}$ ,  $R_{\text{SENSE}}$  and capacitor  $C_{\text{osc}}$ . The nominal oscillating frequency is determined by  $R_{\text{osc}}$  and  $C_{\text{osc}}$ .

An internal divider  $0.5 \times f_{osc(int)}$  is used to generate the accurate 50 % duty cycle. The divider sets the bridge frequency at half the oscillator frequency.

Signal  $V_{SW}$  is generated by the input on pin SW and it is used to determine the frequency in all states except preheat. Signal  $V_{SW(ph)}$  is an internally generated signal used to determine the frequency during the preheat state.

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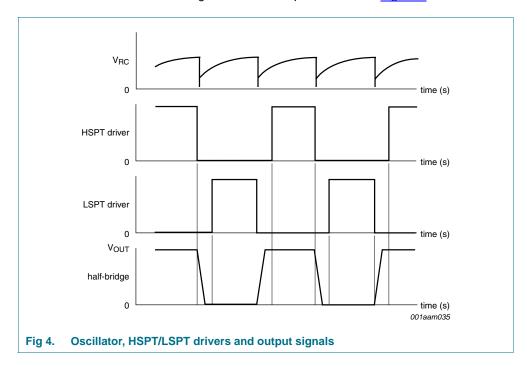
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The output voltage of the bridge changes with the falling edge of the signal on pin RC. The nominal half-bridge frequency is shown in <u>Equation 1</u>:

$$f_{osc(nom)} = \frac{1}{k_{osc} \times R_{osc} \times C_{osc}}$$
 (1)

The maximum frequency is  $2.5 \times f_{osc(nom)}$  and is set at  $V_{SW}$ . An overview of the oscillator, internal LSPT and HSPT drive signals and the output is shown in Figure 4.



#### 7.5 Preheat state

As described in Section 7.2, the IC enters the preheat state when the voltage on pin  $V_{DD}$  is above  $V_{DD(start)}$  and OTP is not active. The capacitor on pin SW ( $C_{SW}$ ) is charged by the sweep current ( $I_{SW}$ ). The preheat Operational Transconductance Amplifier (OTA) is enabled and the half-bridge circuit starts oscillating.

The preheat current is monitored using the external  $R_{SENSE}$  resistor. The OTA controls the frequency using output voltage  $V_{SW(ph)}$  so that the peak voltage across  $R_{SENSE}$  equals the internal reference voltage ( $V_{ref(ph)}$ ). The peak voltage is the voltage at the end of the LSPT conduction time. The preheat peak current through the lamp filament is calculated as shown in Equation 2:

$$I_{ph(peak)} = \frac{V_{ref(ph)}}{R_{SENSE}} \tag{2}$$

The preheat time is set by the external capacitor ( $C_{SW}$ ). The preheat state ends when the down-going  $C_{SW}$  voltage equals  $V_{SW(ph)}$ ; see Figure 4.

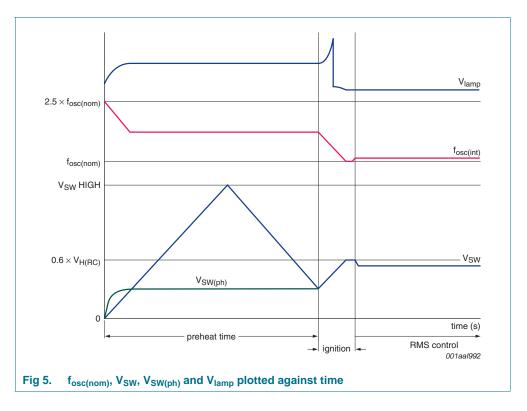
If during the preheat time, capacitive mode is sensed, the internal  $V_{SW}$  HIGH node is discharged and the frequency sweep restarts at  $f_{\text{max}}$ .

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### 7.6 Ignition state

The ignition state is entered after the preheat state has finished. The capacitor on pin SW ( $C_{SW}$ ) is charged by  $I_{SW}$  up to  $0.6 \times V_{H(RC)}$  which corresponds to the frequency  $f_{osc(nom)}$ .

During this frequency sweep, the resonance frequency is reached resulting in the ignition of the lamp (see <u>Figure 4</u>). The resonance frequency is set by the lamp inductor ( $L_{lamp}$ ) and lamp capacitor ( $C_{lamp}$ ). The ignition state ends when the voltage on pin SW ( $V_{SW}$ ) reaches  $0.6 \times V_{H(RC)}$ .

#### 7.7 Steady state

In the steady state, the RMS current control is active. This control sets the frequency so that the RMS voltage across the sense resistor ( $R_{SENSE}$ ) is equal to  $V_{O(ref)RMS}$ . This ensures the current through the power switches and through the lamp is constant. This results in constant IC dissipation and temperature at a fixed ambient temperature.

During one oscillator clock cycle, the voltage on pin SENSE (V<sub>SENSE</sub>) is squared and converted into a positive current. This discharge current is added to the capacitor C<sub>SW</sub>.

During the other oscillator clock cycle, the input of the squarer is connected to the internal reference voltage  $V_{O(ref)RMS}$ . This voltage is squared and converted into a negative current. This charge current is also added to capacitor  $C_{SW}$ . When both currents are equal, then Equation 3 is true:

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$$\frac{1}{T_{osc}} \times \int_{0}^{T_{osc}} V_{SENSE^{2}(t)DT} = \frac{1}{T_{osc}} \times \int_{0}^{T_{osc}} V_{O(ref)RMS^{2}DT}$$
(3)

Where Tosc equals the operating frequency fosc / 1.

Taking the square root of both sides results in Equation 4:

$$\sqrt{\frac{1}{T_{osc}} \times \int_{0}^{T_{osc}} V_{SENSE^{2}(t)DT}} = \sqrt{\frac{1}{T_{osc}} \times \int_{0}^{T_{osc}} V_{O(ref)RMS^{2}DT}}$$
(4)

or

$$RMS \ V_{SENSE} = V_{O(ref)RMS} = R_{SENSE} \times I_{LSPT} \tag{5}$$

A constant current flows through the power switches and the lamp which is defined by the internal reference voltage ( $V_{O(ref)RMS}$ ) and the external  $R_{SENSE}$  resistor.

The R<sub>SENSE</sub> resistor sets both the preheat current and the RMS half-bridge current. The ratio between them is fixed. However by adding a resistor in parallel to C<sub>sw</sub> (see <u>Figure 7</u>) this ratio can be adjusted. This is described in more detail in the *UBA2211 user manual*.

### 7.8 Non-overlap time

The non-overlap time is defined as the time when both MOSFETs are not conducting. The non-overlap time is fixed internally.

#### 7.9 OverTemperature Protection (OTP)

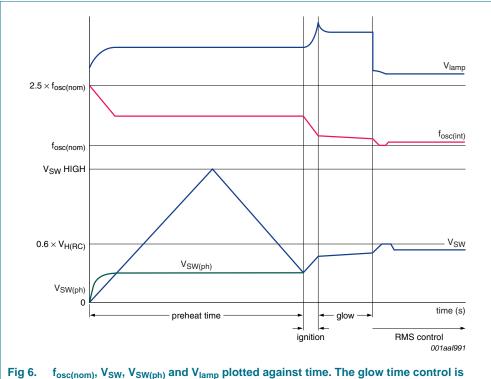
OTP is active in all states. When the die temperature reaches the OTP activation threshold ( $T_{th(act)otp}$ ), the oscillator is stopped and the power switches (LSPT/HSPT) are set to the startup state. When the oscillator is stopped, the DVDT supply no longer generates the supply current  $I_{DVDT}$ . Voltage  $V_{DD}$  gradually decreases and the start-up state is entered as described in <u>Section 7.2 on page 5</u>. OTP is reset when the temperature  $< T_{th(rel)otp}$ .

#### 7.10 Minimum glow time control

If the preheat time is set too short or omitted, the lamp electrodes do not have the correct temperature in the ignition state. This results in instant light but also in a reduced switching lifetime because when the electrode temperature is too low electrode sputtering and damage occur. The minimum glow time control minimizes electrode damage by ensuring maximum power use during the glow phase to heat the electrodes heat as quickly as possible (see Figure 6).

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 $f_{osc(nom)},\,V_{SW},\,V_{SW(ph)}$  and  $V_{lamp}$  plotted against time. The glow time control is active as t<sub>nh</sub> is too short to preheat the electrodes

### 7.11 Saturation Current Protection (SCP)

A critical parameter in the design of the lamp inductor is its saturation current. When the momentary inductor exceeds its saturation current, the inductance drops significantly. If this happens, the inductor current and the current flowing through the LSPT and HSPT power switches increases rapidly. This can cause the current to exceed the half-bridge power transistors maximum ratings.

Saturation of the lamp inductor is likely to occur in cost-effective and miniaturized CFLs. The UBA2211 family internally monitors the power transistor current. When this current exceeds the momentary rating of the internal half-bridge power transistors, the conduction time is reduced and the frequency is slowly increased (by discharging C<sub>SW</sub>). This causes the system to balance at the edge of the current rating of the power switches.

#### 7.12 Capacitive Mode Protection (CMP)

When capacitive mode is detected, capacitor C<sub>SW</sub> is discharged causing the frequency to increase. The system sets itself to the operating point where capacitive mode switching is minimized. CMP is active during the ignition state and in the steady state.

If capacitive mode is sensed during the preheat time, the oscillator restarts at f<sub>max</sub>. CMP could be triggered by an end of lamp life condition when a lamp electrode is broken.

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# 8. Limiting values

Table 3. Limiting values
In accordance with the Absolute Maximum Rating System (IEC 60134).

Symbol	Parameter	Conditions	Min	Max	Unit
$V_{HV}$	voltage on pin HV	operating	-	373	V
		mains transients: 10 minutes maximum over lifetime	-	550	V
$V_{FS}$	voltage on pin FS	with respect to pin OUT	0	14	V
$V_{DD}$	supply voltage	DC supply	0	15	V
$V_{SENSE}$	voltage on pin SENSE		-5	+5	V
$V_{RC}$	voltage on pin RC	I <sub>RC</sub> < 1 mA	0	$V_{DD}$	V
$V_{SW}$	voltage on pin SW	I <sub>SW</sub> < 1 mA	0	$V_{DD}$	V
I <sub>OUT</sub> current on pin OUT	current on pin OUT	T <sub>j</sub> < 125 °C	<u>[1]</u>		
		UBA2211AX	-0.9	+0.9	Α
		UBA2211BX	-1.35	+1.35	Α
		UBA2211CX	-1.65	+1.65	Α
I <sub>DVDT</sub>	current on pin DVDT	T <sub>j</sub> < 125 °C	-0.9	+0.9	Α
SR	slew rate	repetitive output on pin OUT	-4	+4	V/ns
Tj	junction temperature		-40	+150	°C
T <sub>stg</sub>	storage temperature		-55	+150	°C
V <sub>ESD</sub>	electrostatic discharge	HBM:	[2]		
	voltage	pins HV, FS, OUT	-	1000	V
		pins SW, RC, VDD, DVDT	-	2500	V
		MM:	[3]		
		all pins	-	250	V
		CDM:	[3]		
		all pins	-	500	V

<sup>[1]</sup> X where the last letter is P or T.

<sup>[2]</sup> In accordance with the Human Body Model (HBM): equivalent to discharging a 100 pF capacitor through a 1.5  $k\Omega$  series resistor.

<sup>[3]</sup> In accordance with the Machine Model (MM): equivalent to discharging a 200 pF capacitor through a 1.5 k $\Omega$  series resistor and a 0.75  $\mu$ H inductor.

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## 9. Thermal characteristics

Table 4. Thermal characteristics

Symbol	Parameter	Conditions	Тур	Unit
$R_{th(j-a)}$	thermal resistance from junction to ambient	in free air	<u>[1]</u> 95	K/W
R <sub>th(j-c)</sub>	thermal resistance from junction to case	in free air	<u>11</u> 16	K/W

<sup>[1]</sup> In accordance with IEC 60747-1

# 10. Characteristics

Table 5. Characteristics

 $T_j = 25$  °C; all voltages are measured with respect to SGND; positive currents flow into the IC.

Symbol	Parameter	Conditions	Min	Тур	Max	Unit
High-volta	ge supply					
$V_{HV}$	voltage on pin HV	t < 10 minutes; $I_{HV}$ < 30 $\mu$ A	0	-	550	V
$V_{FS}$	voltage on pin FS	t < 10 minutes; $I_{HV}$ < 30 $\mu$ A	0	-	564	V
Low-voltag	ge supply					
Start-up sta	ate					
$I_{HV}$	current on pin HV	V <sub>HV</sub> = 100 V	-	0.85	-	mΑ
V <sub>DD(start)</sub>	start supply voltage	oscillation start	10.7	11.7	12.7	V
$V_{DD(stop)}$	stop supply voltage	oscillation stop	8	8.5	9	V
V <sub>DD(hys)</sub>	hysteresis of supply voltage	start – stop	3	3.5	4	V
$V_{DD(reg)}$	regulation supply voltage		-	13.8	-	V
I <sub>sink</sub>	sink current	capability of VDD regulator	6	-	-	mΑ
Output stag	ge					
Ron	on-state resistance	high-side transistor:	[1]			
		UBA2211AX; $V_{HV} = 310 \text{ V}$ ; $I_D = 100 \text{ mA}$	-	13.5	-	Ω
		UBA2211BX; $V_{HV} = 310 \text{ V}$ ; $I_D = 100 \text{ mA}$	-	9.3	-	Ω
		UBA2211CX; $V_{HV} = 310 \text{ V}$ ; $I_D = 100 \text{ mA}$	-	6.6	-	Ω
		low-side transistor:	[1]			
		UBA2211AX; I <sub>D</sub> = 100 mA	-	13.5	-	Ω
		UBA2211BX; I <sub>D</sub> = 100 mA	-	8.2	-	Ω
		UBA2211CX; I <sub>D</sub> = 100 mA	-	6.6	-	Ω
R <sub>on(150)</sub> / R <sub>on(25)</sub>	on-state resistance ratio (150 °C to 25 °C)		-	1.7	-	
V <sub>F</sub>	forward voltage	HS; I <sub>F</sub> = 200 mA	-	-	2.0	V
		LS; I <sub>F</sub> = 200 mA	-	-	2.0	V
		bootstrap diode; I <sub>F</sub> = 1 mA	0.7	1.0	1.3	V
t <sub>no</sub>	non-overlap time		1.05	1.35	1.65	μS
V <sub>FS</sub>	voltage on pin FS	lockout voltage	3.6	4.2	4.8	V
I <sub>FS</sub>	current on pin FS	$V_{HV} = 310 \text{ V}; V_{FS} = 12 \text{ V}$	10	14	18	μΑ

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 Table 5.
 Characteristics ...continued

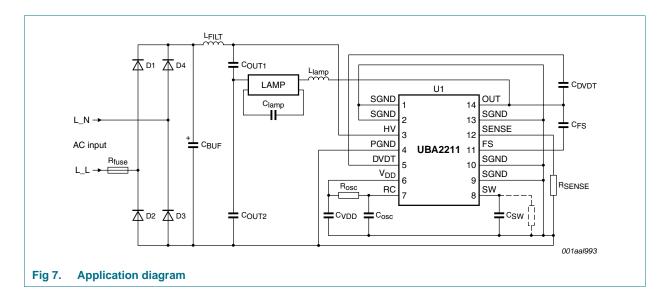
 $T_i = 25$  °C; all voltages are measured with respect to SGND; positive currents flow into the IC.

Symbol	Parameter	Conditions		Min	Тур	Max	Unit
I <sub>sat</sub>	saturation current	high-side transistor:	[1]				
		UBA2211AX; $V_{DS}$ = 30 V; $T_j \le$ 125 °C; $V_{HV}$ = 310 V		0.90	-	-	Α
		UBA2211BX; $V_{DS} = 30 \text{ V}; T_j \le 125 \text{ °C};$ $V_{HV} = 310 \text{ V}$		1.35	-	-	Α
		UBA2211CX; $V_{DS} = 30 \text{ V}; T_j \le 125 \text{ °C};$ $V_{HV} = 310 \text{ V}$		1.85	-	-	Α
		low-side transistor:	[1]				
		UBA2211AX; $V_{DS} = 30 \text{ V}$ ; $T_j \le 125 \text{ °C}$		0.90	-	-	Α
		UBA2211BX; $V_{DS} = 30 \text{ V}; T_j \le 125 ^{\circ}\text{C}$		1.35	-	-	Α
		UBA2211CX; $V_{DS}$ = 30 V; $T_j \le 125$ °C		1.85	-	-	Α
Internal osc	illator						
f <sub>osc(int)</sub>	internal oscillator frequency	$V_{SW} = V_{DD}$		-	-	60	kHz
f <sub>osc(nom)</sub>	nominal oscillator frequency	$R_{osc}$ = 100 k $\Omega$ ; $C_{osc}$ = 220 pF; $V_{SW}$ = $V_{DD}$		40.05	41.32	42.68	kHz
$\Delta f_{osc(nom)}/\Delta T$	nominal oscillator frequency variation with temperature	$R_{osc}$ = 100 k $\Omega$ ; $C_{osc}$ = 220 pF; $\Delta T$ = -20 to +150 °C		-	2	-	%
k <sub>H</sub>	high-level trip point factor			0.371	0.384	0.397	
k <sub>L</sub>	low-level trip point factor			0.028	0.032	0.036	
V <sub>H(RC)</sub>	HIGH-level voltage on pin RC	trip point; $V_{H(RC)} = k_H \times V_{DD}$		4.08	4.22	4.37	V
V <sub>L(RC)</sub>	LOW-level voltage on pin RC	trip point; $V_{L(RC)} = k_L \times V_{DD}$		0.308	0.352	0.396	V
K <sub>osc</sub>	oscillator constant	$R_{osc}$ = 100 k $\Omega$ ; $C_{osc}$ = 220 pF		1.065	1.1	1.135	
Preheat fund	ction						
V <sub>ref(ph)</sub>	preheat reference voltage			-	620	-	mV
t <sub>ph</sub>	preheat time	C <sub>SW</sub> = 100 nF		-	1.5	-	s
RMS curren	t control function						
V <sub>O(ref)RMS</sub>	RMS reference output voltage			262	285	308	mV
OTP functio	n						
T <sub>th(act)otp</sub>	overtemperature protection activation threshold temperature			155	175	-	°C
T <sub>th(rel)otp</sub>	overtemperature protection release threshold temperature			-	100	-	°C

<sup>[1]</sup> X where the last letter is P or T.

### Half-bridge power IC family for CFL lamps

# 11. Application information

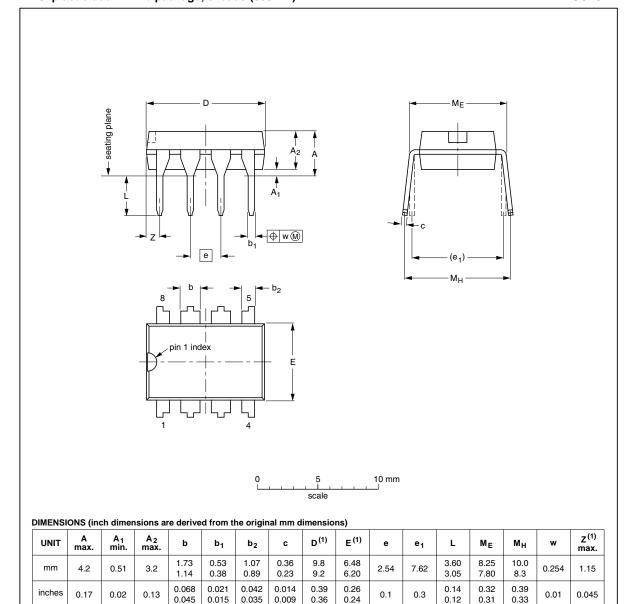


### Half-bridge power IC family for CFL lamps

# 12. Package outline

#### DIP8: plastic dual in-line package; 8 leads (300 mil)

SOT97-1



#### Note

1. Plastic or metal protrusions of 0.25 mm (0.01 inch) maximum per side are not included.

OUTLINE	E REFE		INE REFERENCES		EUROPEAN	ISSUE DATE	
VERSION	IEC	JEDEC	JEITA		PROJECTION	ISSUE DATE	
SOT97-1	050G01	MO-001	SC-504-8			<del>99-12-27</del> 03-02-13	

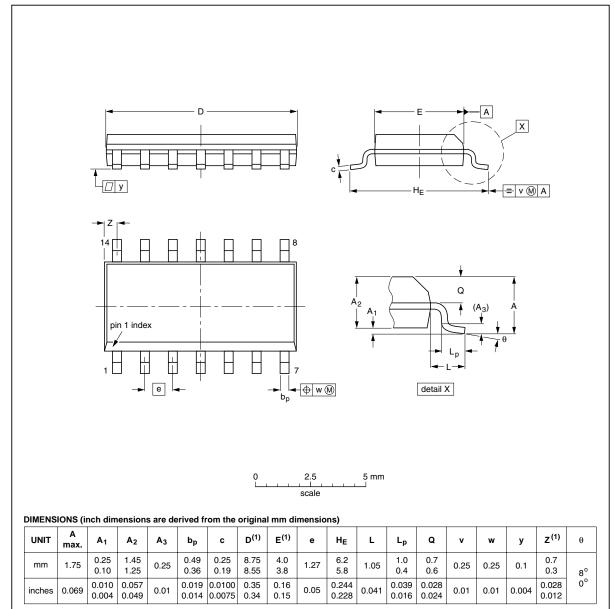
Fig 8. Package outline SOT97-1 (DIP8)

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#### Half-bridge power IC family for CFL lamps

### SO14: plastic small outline package; 14 leads; body width 3.9 mm

SOT108-1



#### Note

1. Plastic or metal protrusions of 0.15 mm (0.006 inch) maximum per side are not included.

OUTLINE	REFERENCES			EUROPEAN	ISSUE DATE	
VERSION	IEC	JEDEC	JEITA		PROJECTION	ISSUE DATE
SOT108-1	076E06	MS-012				<del>99-12-27</del> 03-02-19

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Fig 9. Package outline SOT108-1 (SO14)

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# 13. Revision history

### Table 6. Revision history

Document ID	Release date	Data sheet status	Change notice	Supersedes
UBA2211 v.2.1	20110307	Preliminary data sheet	-	UBA2211 v.2
Modifications:	<ul> <li>Data sheet s</li> </ul>	tatus change from objective da	ata sheet to prelimina	ary data sheet.
UBA2211 v.2	20110103	Objective data sheet	-	UBA2211 v.1
UBA2211 v.1	20100628	Objective data sheet	-	-

#### Half-bridge power IC family for CFL lamps

# 14. Legal information

#### 14.1 Data sheet status

Document status[1][2]	Product status[3]	Definition
Objective [short] data sheet	Development	This document contains data from the objective specification for product development.
Preliminary [short] data sheet	Qualification	This document contains data from the preliminary specification.
Product [short] data sheet	Production	This document contains the product specification.

- [1] Please consult the most recently issued document before initiating or completing a design.
- [2] The term 'short data sheet' is explained in section "Definitions"
- [3] The product status of device(s) described in this document may have changed since this document was published and may differ in case of multiple devices. The latest product status information is available on the Internet at URL http://www.nxp.com.

#### 14.2 Definitions

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### Half-bridge power IC family for CFL lamps

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### Half-bridge power IC family for CFL lamps

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Date of release: 7 March 2011 Document identifier: UBA2211