December 8, 2010

LM6172QML

Dual High Speed, Low Power, Low Distortion, Voltage Feedback Amplifiers

General Description

The LM6172 is a dual high speed voltage feedback amplifier. It is unity-gain stable and provides excellent DC and AC performance. With 100MHz unity-gain bandwidth, 3000V/µs slew rate and 50mA of output current per channel, the LM6172 offers high performance in dual amplifiers; yet it only consumes 2.3mA of supply current each channel.

The LM6172 operates on ±15V power supply for systems requiring large voltage swings, such as ADSL, scanners and ultrasound equipment. It is also specified at ±5V power supply for low voltage applications such as portable video systems.

The LM6172 is built with National's advanced VIP® III (Vertically Integrated PNP) complementary bipolar process.

Features

- Available with radiation guaranteed 300 krad(Si)

(Typical Unless Otherwise Noted)

- Easy to Use Voltage Feedback Topology
- High Slew Rate 3000V/µs
- Wide Unity-Gain Bandwidth 100MHz
- Low Supply Current 2.3mA / Amplifier
- High Output Current 50mA / Amplifier
- Specified for ±15V and ±5V operation

Applications

- Scanner I- to -V Converters
- ADSL/HDSL Drivers
- Multimedia Broadcast Systems
- Video Amplifiers
- NTSC, PAL® and SECAM Systems
- ADC/DAC Buffers
- Pulse Amplifiers and Peak Detectors

Ordering Information

NS Part Number	SMD Part Number	NS Package Number	Package Description
LM6172AMJ-QML	5962-9560401QPA	J08A	8LD Ceramic Dip
LM6172AMJFQML	5962F9560401QPA 300 krad(Si)	J08A	8LD Ceramic Dip
LM6172AMJFQMLV	5962F9560401VPA 300 krad(Si)	J08A	8LD Ceramic Dip
LM6172AMWG-QML	5962-9560401QXA	WG16A	10LD Ceramic SOIC
LM6172AMWGFQMLV	5962F9560401VXA 300 krad(Si)	WG16A	10LD Ceramic SOIC
LM6172 MDR		(*Note 1*)	Bare Die

Note 1: FOR ADDITIONAL DIE INFORMATION, PLEASE VISIT THE HI REL WEB SITE AT: www.national.com/analog/space/level_die

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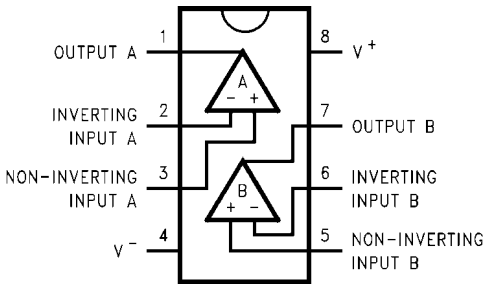
Connection Diagrams

8-Pin DIP



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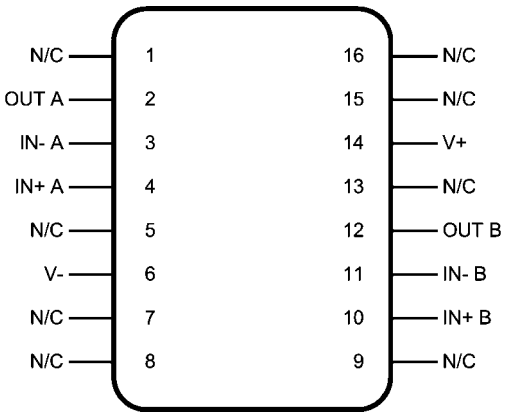
Top View

16LD Ceramic SOIC



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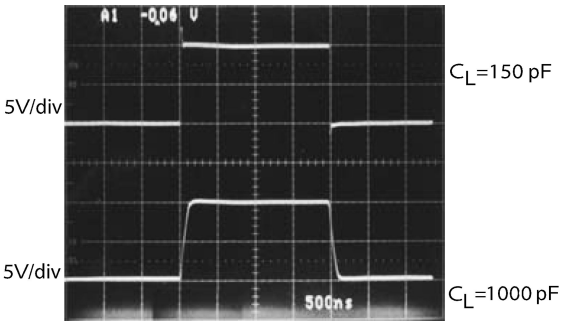
Top View

LM6172 Driving Capacitive Load



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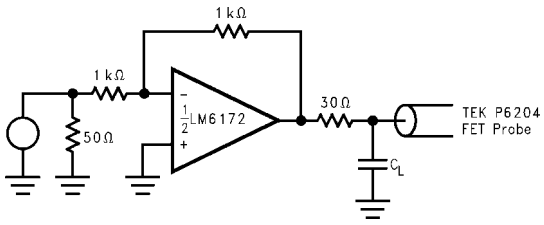

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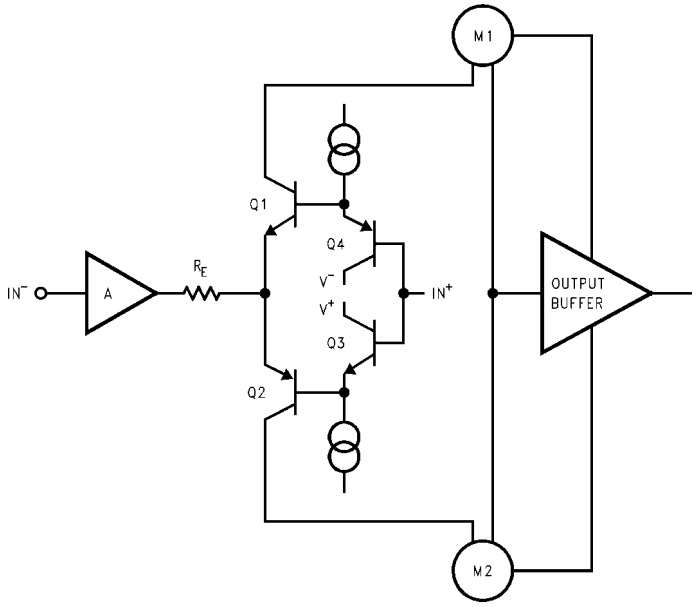
LM6172 Simplified Schematic (Each Amplifier)



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Absolute Maximum Ratings (*Note 2*)

Supply Voltage ($V^+ - V^-$)	36V
Differential Input Voltage (*Note 7*)	±10V
Maximum Junction Temperature	150°C
Power Dissipation (*Note 3*), (*Note 4*)	1.03W
Output Short Circuit to Ground (*Note 6*)	Continuous
Storage Temperature Range	$-65°C \leq T_A \leq +150°C$
Common Mode Voltage Range	$V^+ +0.3V$ to $V^- -0.3V$
Input Current	±10mA
Thermal Resistance (*Note 8*)	
θ_{JA}	
8LD Ceramic Dip (Still Air)	100°C/W
8LD Ceramic Dip (500LF/Min Air Flow)	46°C/W
16LD Ceramic SOIC (Still Air)	124°C/W
16LD Ceramic SOIC (500LF/Min Air Flow)	74°C/W
θ_{JC} (*Note 4*)	
8LD Ceramic Dip	2°C/W
16LD Ceramic SOIC	6°C/W
Package Weight	
8LD Ceramic Dip	980mg
16LD Ceramic SOIC	365mg
ESD Tolerance (*Note 5*)	4KV

Recommended Operating Conditions (*Note 2*)

Supply Voltage	$5.5V \leq V_S \leq 36V$
Operating Temperature Range	$-55°C \leq T_A \leq +125°C$

Quality Conformance Inspection

Mil-Std-883, Method 5005 - Group A

Subgroup	Description	Temp (°C)
1	Static tests at	+25
2	Static tests at	+125
3	Static tests at	-55
4	Dynamic tests at	+25
5	Dynamic tests at	+125
6	Dynamic tests at	-55
7	Functional tests at	+25
8A	Functional tests at	+125
8B	Functional tests at	-55
9	Switching tests at	+25
10	Switching tests at	+125
11	Switching tests at	-55
12	Settling time at	+25
13	Settling time at	+125
14	Settling time at	-55

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LM6172 (±5V) Electrical Characteristics (*Note 14*)

DC Parameters

The following conditions apply, unless otherwise specified. T_J = 25°C, V^+ = +5V, V^- = −5V, V_{CM} = 0V & R_L > 1MΩ

Symbol	Parameter	Conditions	Notes	Min	Max	Units	Sub-groups
V_{IO}	Input Offset Voltage				1.0	mV	1
					3.0	mV	2, 3
I_{IB}	Input Bias Current				2.5	µA	1
					3.5	µA	2, 3
I_{IO}	Input Offset Current				1.5	µA	1
					2.2	µA	2, 3
CMRR	Common Mode Rejection Ratio	V_{CM} = ±2.5V		70		dB	1
				65		dB	2, 3
PSRR	Power Supply Rejection Ratio	V_S = ±15V to ±5V		75		dB	1
				70		dB	2, 3
A_V	Large Signal Voltage Gain	R_L = 1KΩ	(*Note 9*)	70		dB	1
			(*Note 9*)	65		dB	2, 3
		R_L = 100Ω	(*Note 9*)	65		dB	1
			(*Note 9*)	60		dB	2, 3
V_O	Output Swing	R_L = 1KΩ		3.1	-3.1	V	1
				3.0	-3.0	V	2, 3
		R_L = 100Ω		2.5	-2.4	V	1
				2.4	-2.3	V	2, 3
I_L	Output Current (Open Loop)	Sourcing R_L = 100Ω	(*Note 13*)	25		mA	1
			(*Note 13*)	24		mA	2, 3
		Sinking R_L = 100Ω	(*Note 13*)		-24	mA	1
			(*Note 13*)		-23	mA	2, 3
I_S	Supply Current	Both Amplifiers			6.0	mA	1
					7.0	mA	2, 3

DC Drift Parameters (*Note 14*)

The following conditions apply, unless otherwise specified. T_J = 25°C, V^+ = +5V, V^- = −5V, V_{CM} = 0V & R_L > 1MΩ

Delta calculations performed on QMLV devices at group B , subgroup 5.

Symbol	Parameter	Conditions	Notes	Min	Max	Units	Sub-groups
V_{IO}	Input Offset Voltage			-0.25	0.25	mV	1
I_{IB}	Input Bias Current			-0.50	0.50	µA	1
I_{IO}	Input Ofset Current			-0.25	0.25	µA	1

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LM6172 (±15V) Electrical Characteristics

DC Parameters (*Note 14*)

The following conditions apply, unless otherwise specified. T_J = 25°C, V^+ = +15V, V^- = −15V, V_{CM} = 0V, & R_L = 1MΩ

Symbol	Parameter	Conditions	Notes	Min	Max	Units	Sub-groups
V_{IO}	Input Offset Voltage				1.5	mV	1
					3.5	mV	2, 3
I_{IB}	Input Bias Current				3.0	µA	1
					4.0	µA	2, 3
I_{IO}	Input Offset Current				2.0	µA	1
					3.0	µA	2, 3
CMRR	Common Mode Rejection Ratio	V_{CM} = ±10V		70		dB	1
				65		dB	2, 3
PSRR	Power Supply Rejection Ratio	V_S = ±15V to ±5V		75		dB	1
				70		dB	2, 3
A_V	Large Signal Voltage Gain	R_L = 1KΩ	(*Note 9*)	75		dB	1
			(*Note 9*)	70		dB	2, 3
		R_L = 100Ω	(*Note 9*)	65		dB	1
			(*Note 9*)	60		dB	2, 3
V_O	Output Swing	R_L = 1KΩ		12.5	-12.5	V	1
				12	-12	V	2, 3
		R_L = 100Ω		6.0	-6.0	V	1
				5.0	-5.0	V	2, 3
I_L	Output Current (Open Loop)	Sourcing R_L = 100Ω	(*Note 13*)	60		mA	1
			(*Note 13*)	50		mA	2, 3
		Sinking R_L = 100Ω	(*Note 13*)		-60	mA	1
			(*Note 13*)		-50	mA	2, 3
I_S	Supply Current	Both Amplifiers			8.0	mA	1
					9.0	mA	2, 3

AC Parameters (*Note 14*)

The following conditions apply, unless otherwise specified. T_J = 25°C, V^+ = +15V, V^- = −15V, V_{CM} = 0V

Symbol	Parameter	Conditions	Notes	Min	Max	Units	Sub-groups
SR	Slew Rate	A_V = 2, V_I = ±2.5V 3nS Rise & Fall time	(*Note 10*), (*Note 11*)	1700		V/µS	4
GBW	Unity-Gain Bandwidth		(*Note 12*)	80		MHz	4

DC Drift Parameters (*Note 14*)

The following conditions apply, unless otherwise specified. T_J = 25°C, V^+ = +15V, V^- = −15V, V_{CM} = 0V

Delta calculations performed on QMLV devices at group B , subgroup 5.

Symbol	Parameter	Conditions	Notes	Min	Max	Units	Sub-groups
V_{IO}	Input Offset Voltage			-0.25	0.25	mV	1
I_{IB}	Input Bias Current			-0.50	0.50	µA	1
I_{IO}	Input Offset Current			-0.25	0.25	µA	1

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Note 2: Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is functional, but do not guarantee specific performance limits. For guaranteed specifications and test conditions, see the Electrical Characteristics. The guaranteed specifications apply only for the test conditions listed. Some performance characteristics may degrade when the device is not operated under the listed test conditions.

Note 3: The maximum power dissipation must be derated at elevated temperatures and is dictated by T_{Jmax} (maximum junction temperature), θ_{JA} (package junction to ambient thermal resistance), and T_A (ambient temperature). The maximum allowable power dissipation at any temperature is $P_{Dmax} = (T_{Jmax} - T_A)/\theta_{JA}$ or the number given in the Absolute Maximum Ratings, whichever is lower.

Note 4: The package material for these devices allows much improved heat transfer over our standard ceramic packages. In order to take full advantage of this improved heat transfer, heat sinking must be provided between the package base (directly beneath the die), and either metal traces on, or thermal vias through, the printed circuit board. Without this additional heat sinking, device power dissipation must be calculated using θ_{JA}, rather than θ_{JC}, thermal resistance. It must not be assumed that the device leads will provide substantial heat transfer out the package, since the thermal resistance of the leadframe material is very poor, relative to the material of the package base. The stated θ_{JC} thermal resistance is for the package material only, and does not account for the additional thermal resistance between the package base and the printed circuit board. The user must determine the value of the additional thermal resistance and must combine this with the stated value for the package, to calculate the total allowed power dissipation for the device.

Note 5: Human body model, 1.5 kΩ in series with 100 pF.

Note 6: Continuous short circuit operation can result in exceeding the maximum allowed junction temperature of 150°C

Note 7: Differential Input Voltage is measured at $V_S = \pm 15V$.

Note 8: All numbers apply for packages soldered directly into a PC board.

Note 9: Large signal voltage gain is the total output swing divided by the input signal required to produce that swing. For $V_S = \pm 15V$, $V_{OUT} = \pm 5V$. For $V_S = \pm 5V$, $V_{OUT} = \pm 1V$.

Note 10: See AN0009 for SR test circuit.

Note 11: Slew Rate measured between ±4V.

Note 12: See AN0009 for GBW test circuit.

Note 13: The open loop output current is guaranteed by measurement of the open loop output voltage swing using 100Ω output load.

Note 14: Pre and post irradiation limits are identical to those listed under AC and DC electrical characteristics except as listed in the Post Radiation Limits Table. These parts may be dose rate sensitive in a space environment and demonstrate enhanced low dose rate effect. Radiation end point limits for the noted parameters are guaranteed only for the conditions as specified in Mil-Std-883, Method 1019.5, Condition A.

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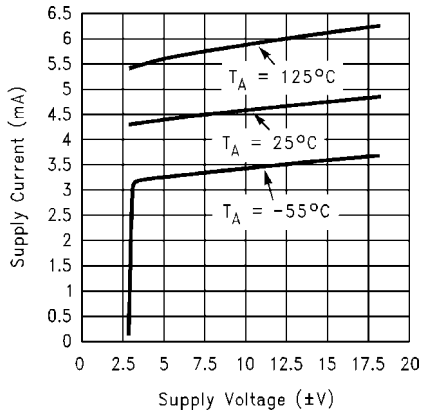
Typical Performance Characteristics

Unless otherwise noted, T_A = 25°C

Supply Voltage vs. Supply Current



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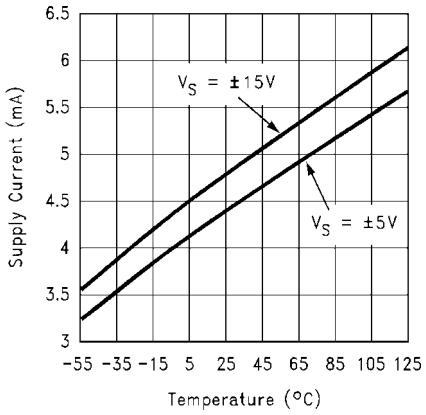
Supply Current vs. Temperature



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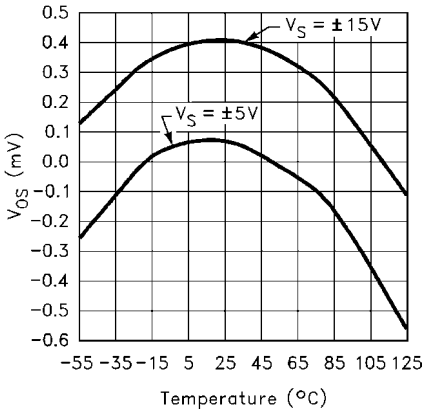
Input Offset Voltage vs. Temperature



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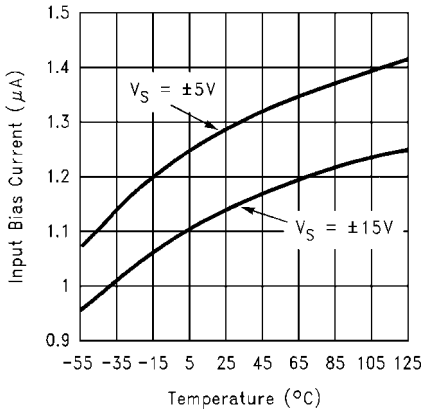
Input Bias Current vs. Temperature



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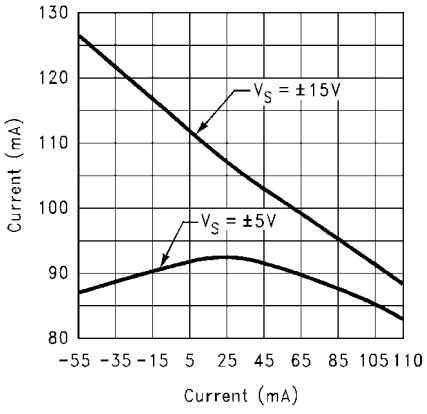
Short Circuit Current vs. Temperature (Sourcing)



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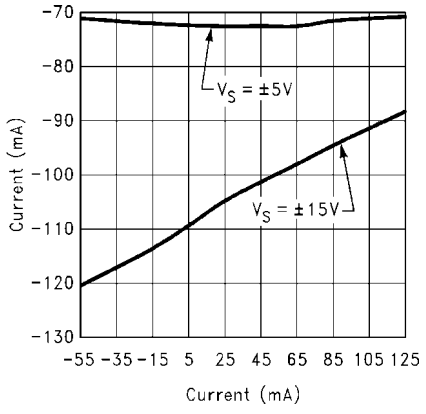
Short Circuit Current vs. Temperature (Sinking)



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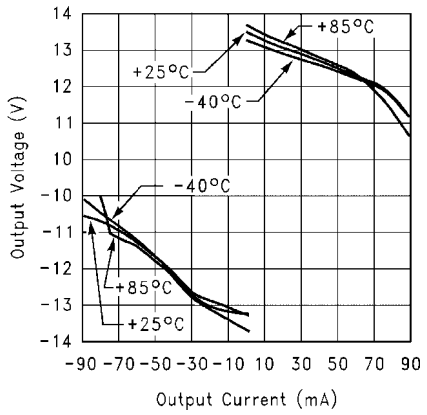
Output Voltage vs. Output Current (V_S = ±15V)



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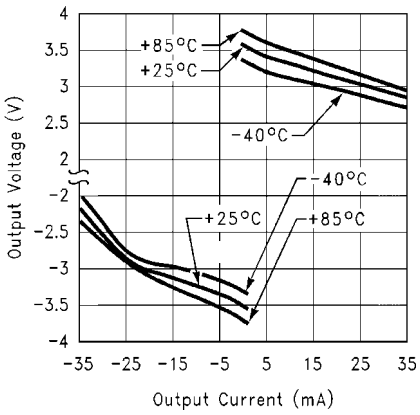
Output Voltage vs. Output Current (V_S = ±5V)



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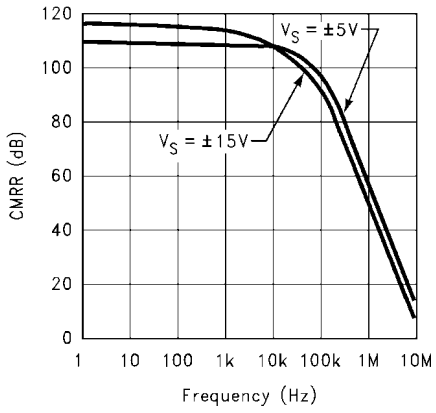
CMRR vs. Frequency



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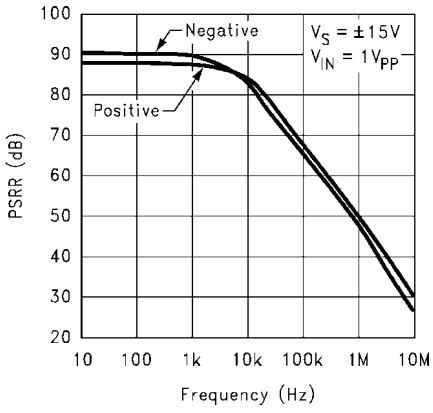
PSRR vs. Frequency



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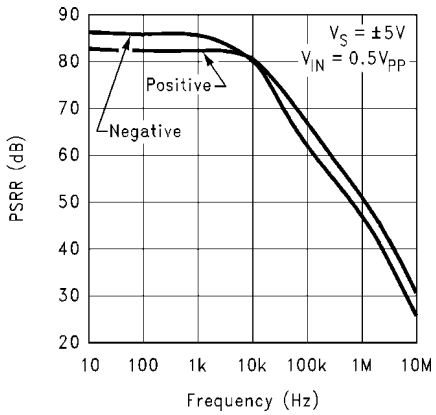
PSRR vs. Frequency



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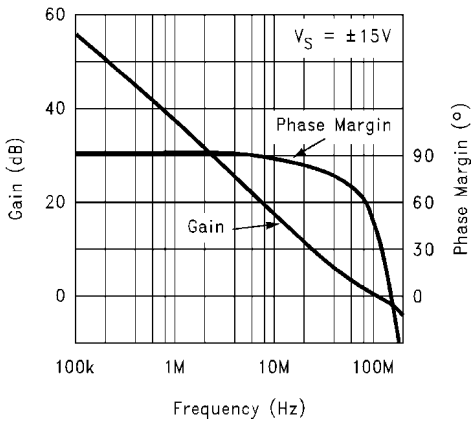
Open-Loop Frequency Response



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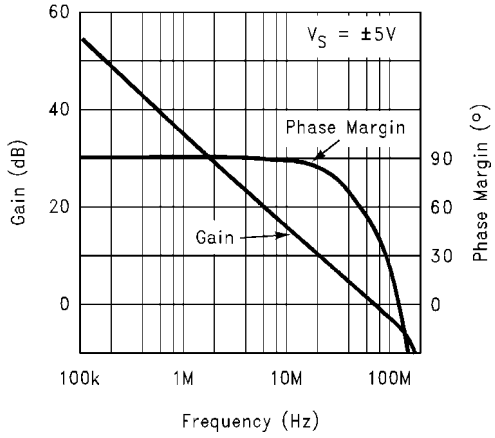
Open-Loop Frequency Response



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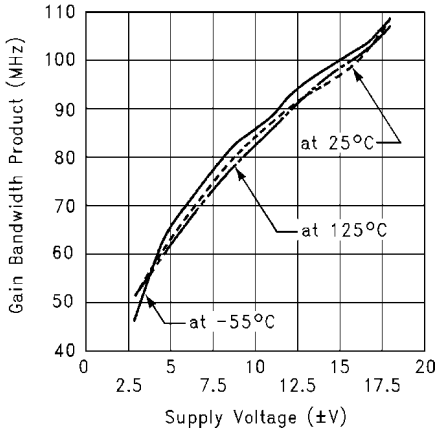
Gain-Bandwidth Product vs. Supply Voltage at Different Temperature



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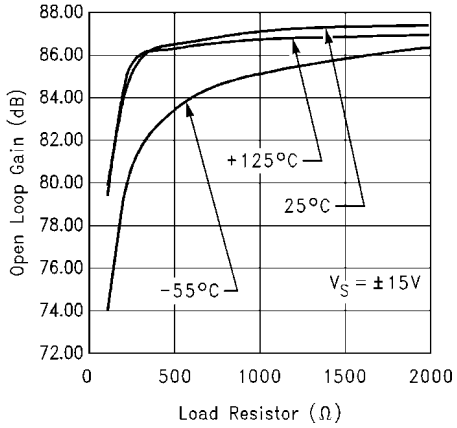
Large Signal Voltage Gain vs. Load



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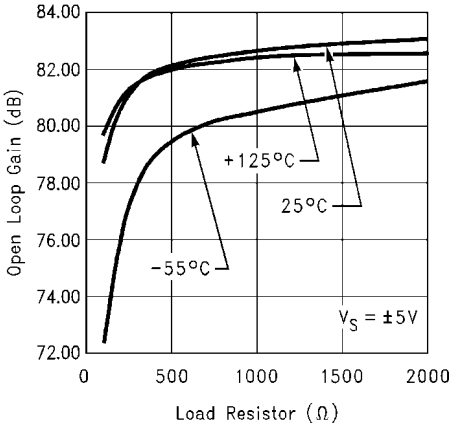
Large Signal Voltage Gain vs. Load



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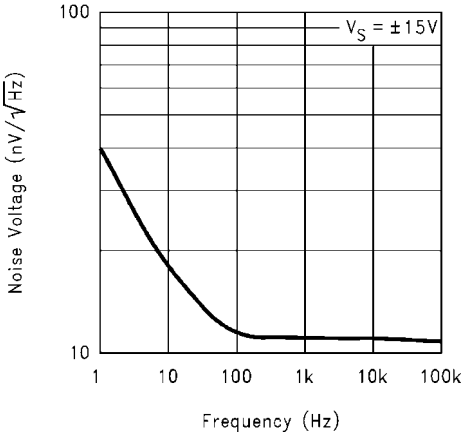
Input Voltage Noise vs. Frequency



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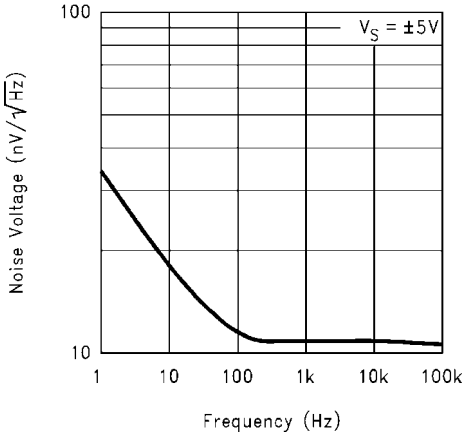
Input Voltage Noise vs. Frequency



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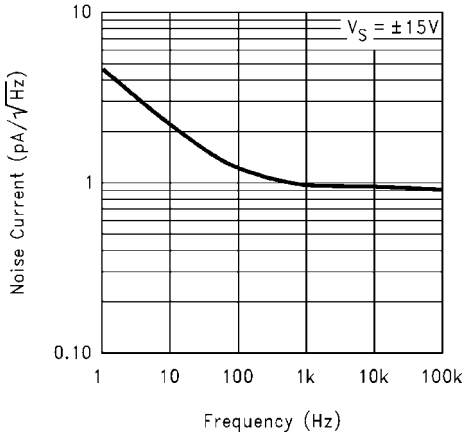
Input Current Noise vs. Frequency



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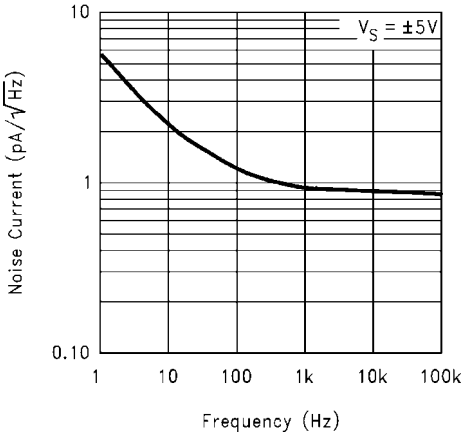
Input Current Noise vs. Frequency



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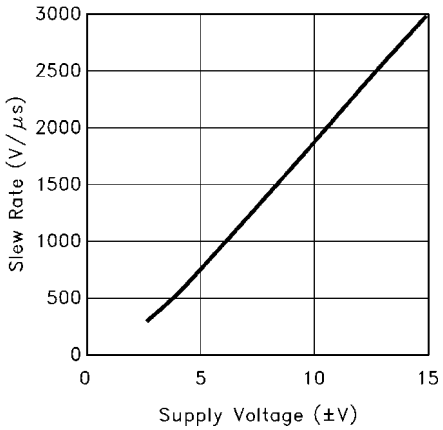
Slew Rate vs. Supply Voltage



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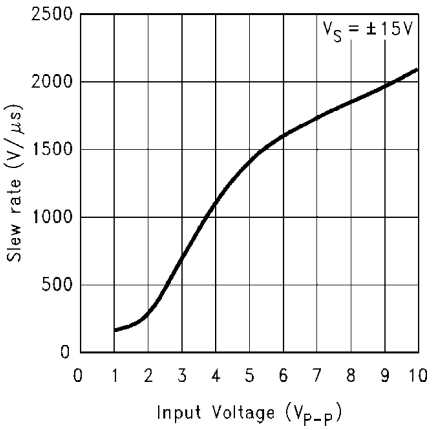
Slew Rate vs. Input Voltage



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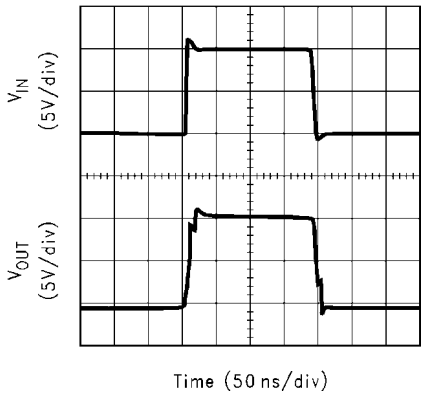
Large Signal Pulse Response
A_V = +1, V_S = ±15V



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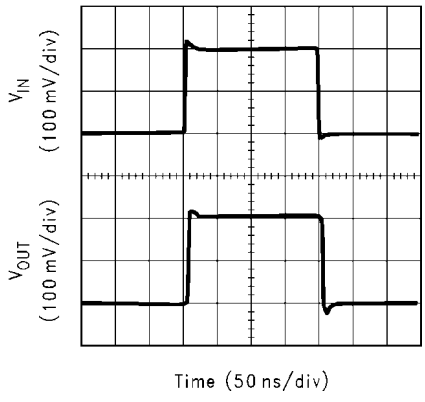
Small Signal Pulse Response
A_V = +1, V_S = ±15V



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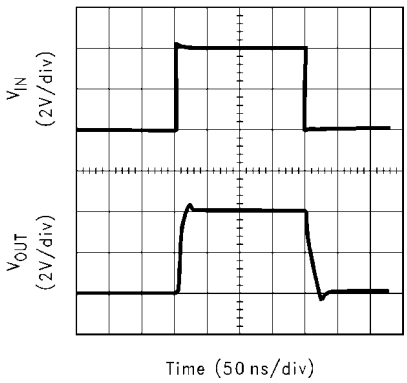
Large Signal Pulse Response
A_V = +1, V_S = ±5V



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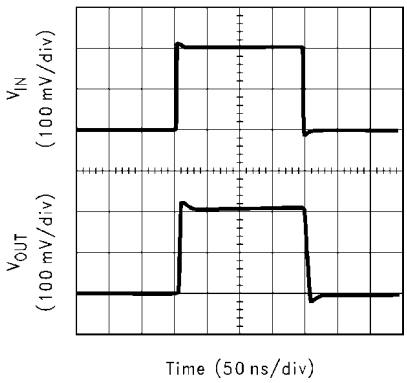
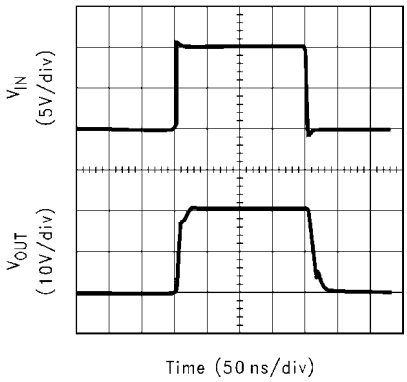
Small Signal Pulse Response
A_V = +1, V_S = ±5V



20159405

Large Signal Pulse Response
A_V = +2, V_S = ±15V



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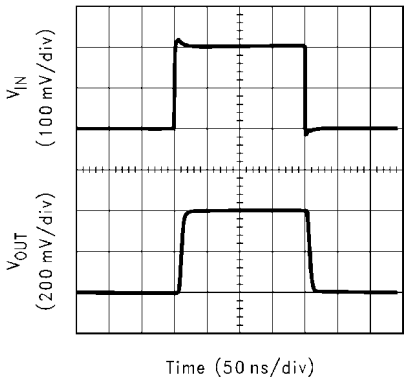
Small Signal Pulse Response
A_V = +2, V_S = ±15V



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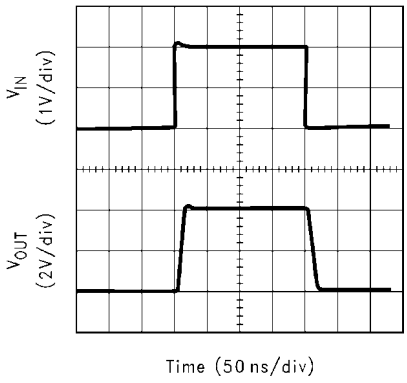
Large Signal Pulse Response
A_V = +2, V_S = ±5V



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Small Signal Pulse Response
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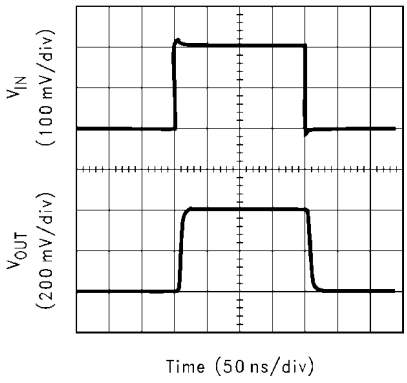

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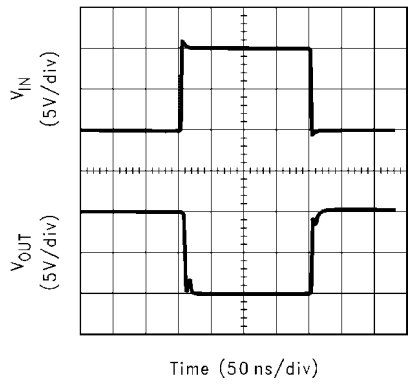
Large Signal Pulse Response
$A_V = -1$, $V_S = \pm 15V$



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Small Signal Pulse Response
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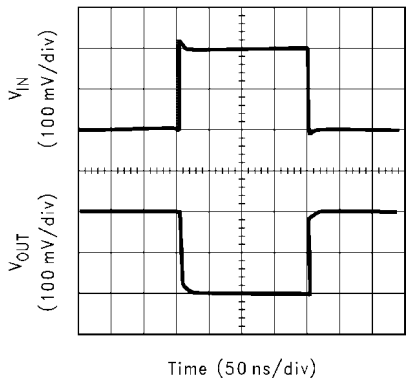

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Large Signal Pulse Response
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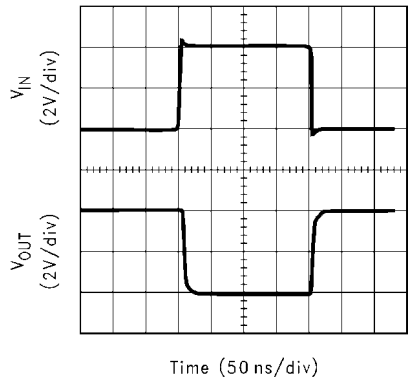

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Small Signal Pulse Response
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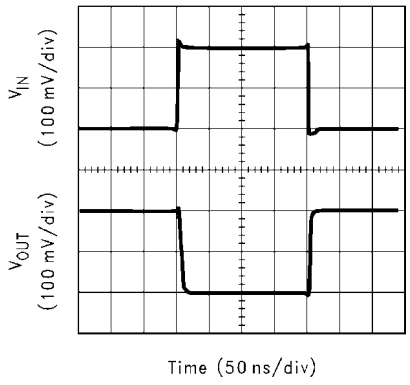
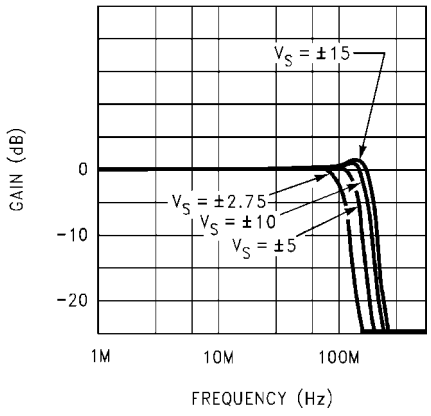


20159413

Closed Loop Frequency Response vs. Supply Voltage
($A_V = +1$)



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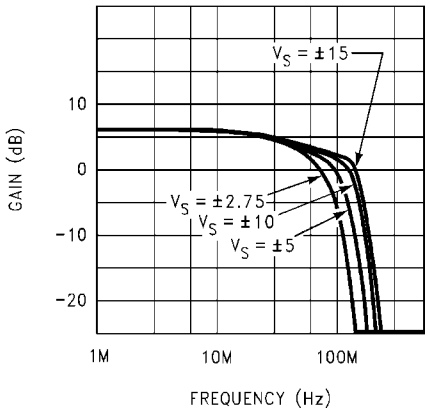
Closed Loop Frequency Response vs. Supply Voltage
($A_V = +2$)



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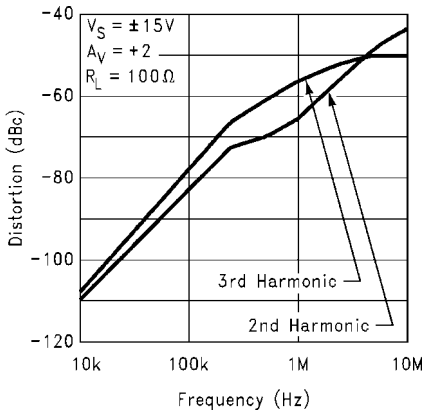
Harmonic Distortion vs. Frequency (V_S = ±15V)



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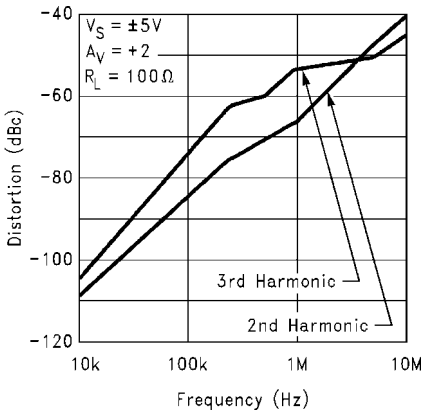
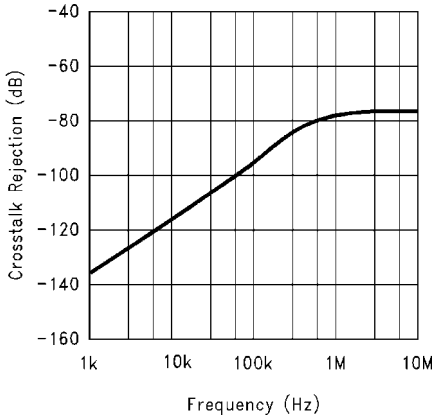
Harmonic Distortion vs. Frequency (V_S = ±5V)



20159434

Crosstalk Rejection vs. Frequency



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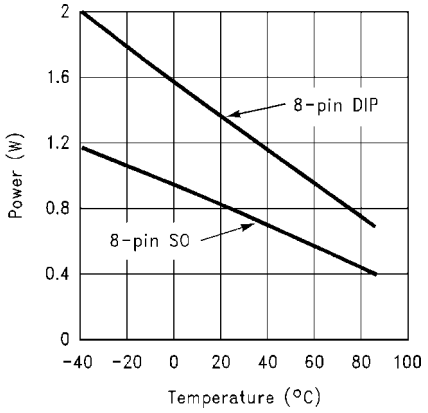
Maximum Power Dissipation vs. Ambient Temperature



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Application Notes

LM6172 PERFORMANCE DISCUSSION

The LM6172 is a dual high-speed, low power, voltage feedback amplifier. It is unity-gain stable and offers outstanding performance with only 2.3mA of supply current per channel. The combination of 100MHz unity-gain bandwidth, 3000V/µs slew rate, 50mA per channel output current and other attractive features makes it easy to implement the LM6172 in various applications. Quiescent power of the LM6172 is 138mW operating at ±15V supply and 46mW at ±5V supply.

LM6172 CIRCUIT OPERATION

The class AB input stage in LM6172 is fully symmetrical and has a similar slewing characteristic to the current feedback amplifiers. In the LM6172 Simplified Schematic (Page 2), Q1 through Q4 form the equivalent of the current feedback input buffer, R_E the equivalent of the feedback resistor, and stage A buffers the inverting input. The triple-buffered output stage isolates the gain stage from the load to provide low output impedance.

LM6172 SLEW RATE CHARACTERISTIC

The slew rate of LM6172 is determined by the current available to charge and discharge an internal high impedance node capacitor. This current is the differential input voltage divided by the total degeneration resistor R_E. Therefore, the slew rate is proportional to the input voltage level, and the higher slew rates are achievable in the lower gain configurations.

When a very fast large signal pulse is applied to the input of an amplifier, some overshoot or undershoot occurs. By placing an external series resistor such as 1kΩ to the input of LM6172, the slew rate is reduced to help lower the overshoot, which reduces settling time.

REDUCING SETTLING TIME

The LM6172 has a very fast slew rate that causes overshoot and undershoot. To reduce settling time on LM6172, a 1kΩ resistor can be placed in series with the input signal to decrease slew rate. A feedback capacitor can also be used to reduce overshoot and undershoot. This feedback capacitor serves as a zero to increase the stability of the amplifier circuit. A 2pF feedback capacitor is recommended for initial evaluation. When the LM6172 is configured as a buffer, a feedback resistor of 1kΩ must be added in parallel to the feedback capacitor.

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Another possible source of overshoot and undershoot comes from capacitive load at the output. Please see the section "Driving Capacitive Loads" for more detail.

DRIVING CAPACITIVE LOADS

Amplifiers driving capacitive loads can oscillate or have ringing at the output. To eliminate oscillation or reduce ringing, an isolation resistor can be placed as shown in *Figure 1*. The combination of the isolation resistor and the load capacitor forms a pole to increase stability by adding more phase margin to the overall system. The desired performance depends upon the value of the isolation resistor; the bigger the isolation resistor, the more damped (slow) the pulse response becomes. For LM6172, a 50Ω isolation resistor is recommended for initial evaluation.

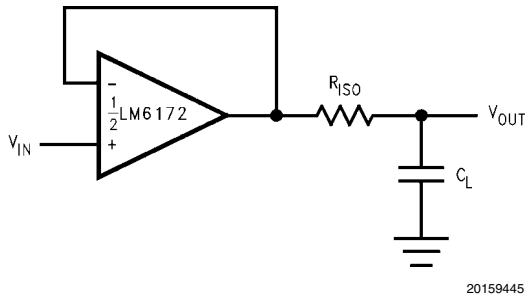

FIGURE 1. Isolation Resistor Used to Drive Capacitive Load

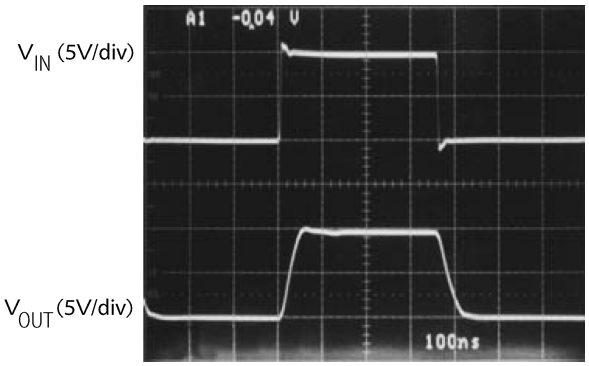

FIGURE 2. The LM6172 Driving a 510pF Load with a 30Ω Isolation Resistor

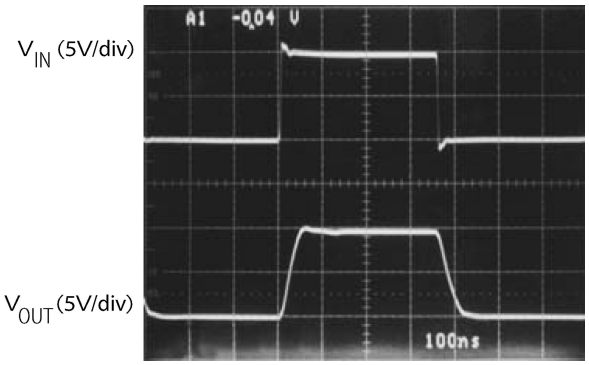

FIGURE 3. The LM6172 Driving a 220 pF Load with a 50Ω Isolation Resistor

LAYOUT CONSIDERATION

Printed Circuit Boards And High Speed Op Amps

There are many things to consider when designing PC boards for high speed op amps. Without proper caution, it is very easy to have excessive ringing, oscillation and other degraded AC performance in high speed circuits. As a rule, the signal traces should be short and wide to provide low inductance and low impedance paths. Any unused board space needs to be grounded to reduce stray signal pickup. Critical components should also be grounded at a common point to eliminate voltage drop. Sockets add capacitance to the board and can affect frequency performance. It is better to solder the amplifier directly into the PC board without using any socket.

Using Probes

Active (FET) probes are ideal for taking high frequency measurements because they have wide bandwidth, high input impedance and low input capacitance. However, the probe ground leads provide a long ground loop that will produce errors in measurement. Instead, the probes can be grounded directly by removing the ground leads and probe jackets and using scope probe jacks.

Components Selection And Feedback Resistor

It is important in high speed applications to keep all component leads short because wires are inductive at high frequency. For discrete components, choose carbon composition-type resistors and mica-type capacitors. Surface mount components are preferred over discrete components for minimum inductive effect.

Large values of feedback resistors can couple with parasitic capacitance and cause undesirable effects such as ringing or oscillation in high speed amplifiers. For LM6172, a feedback resistor less than 1kΩ gives optimal performance.

COMPENSATION FOR INPUT CAPACITANCE

The combination of an amplifier's input capacitance with the gain setting resistors adds a pole that can cause peaking or oscillation. To solve this problem, a feedback capacitor with a value

$$C_F > (R_G \times C_{IN})/R_F$$

can be used to cancel that pole. For LM6172, a feedback capacitor of 2pF is recommended. *Figure 4* illustrates the compensation circuit.

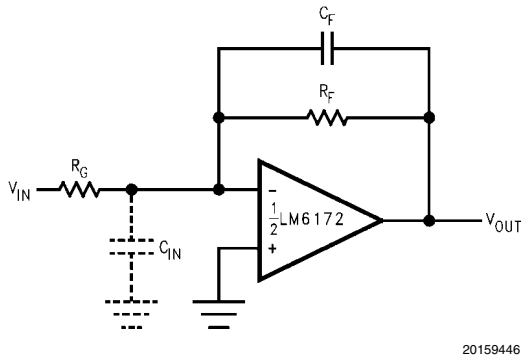

FIGURE 4. Compensating for Input Capacitance

POWER SUPPLY BYPASSING

Bypassing the power supply is necessary to maintain low power supply impedance across frequency. Both positive and negative power supplies should be bypassed individually by

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placing 0.01µF ceramic capacitors directly to power supply pins and 2.2µF tantalum capacitors close to the power supply pins.

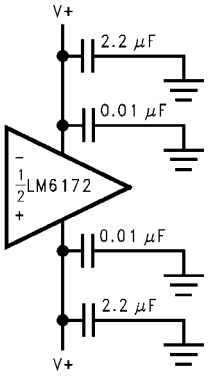

FIGURE 5. Power Supply Bypassing

TERMINATION

In high frequency applications, reflections occur if signals are not properly terminated. *Figure 6* shows a properly terminated signal while *Figure 7* shows an improperly terminated signal.

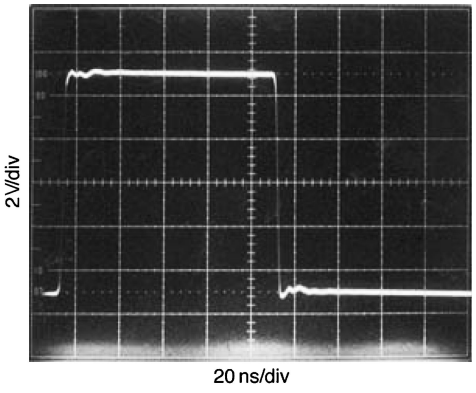

FIGURE 6. Properly Terminated Signal

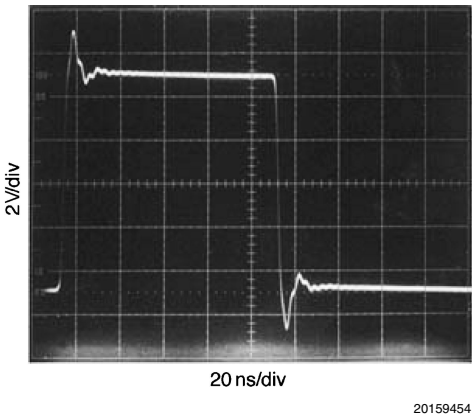

FIGURE 7. Improperly Terminated Signal

To minimize reflection, coaxial cable with matching characteristic impedance to the signal source should be used. The other end of the cable should be terminated with the same value terminator or resistor. For the commonly used cables, RG59 has 75Ω characteristic impedance, and RG58 has 50Ω characteristic impedance.

POWER DISSIPATION

The maximum power allowed to dissipate in a device is defined as:

$$P_D = (T_{J(max)} - T_A)/\theta_{JA}$$

Where P_D is the power dissipation in a device

$T_{J(max)}$ is the maximum junction temperature

T_A is the ambient temperature

θ_{JA} is the thermal resistance of a particular package

For example, for the LM6172 in a SO-16 package, the maximum power dissipation at 25°C ambient temperature is 1000mW.

Thermal resistance, θ_{JA}, depends on parameters such as die size, package size and package material. The smaller the die size and package, the higher θ_{JA} becomes. The 8-pin DIP package has a lower thermal resistance (95°C/W) than that of 8-pin SO (160°C/W). Therefore, for higher dissipation capability, use an 8-pin DIP package.

The total power dissipated in a device can be calculated as:

$$P_D = P_Q + P_L$$

P_Q is the quiescent power dissipated in a device with no load connected at the output. P_L is the power dissipated in the device with a load connected at the output; it is not the power dissipated by the load.

Furthermore,

P_Q: = supply current x total supply voltage with no load

P_L: = output current x (voltage difference between supply voltage and output voltage of the same supply)

For example, the total power dissipated by the LM6172 with $V_S = \pm 15V$ and both channels swinging output voltage of 10V into 1kΩ is

P_D: = $P_Q + P_L$

: = 2[(2.3mA)(30V)] + 2[(10mA)(15V − 10V)]

: = 138mW + 100mW

: = 238mW

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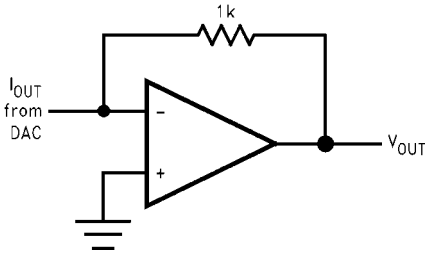
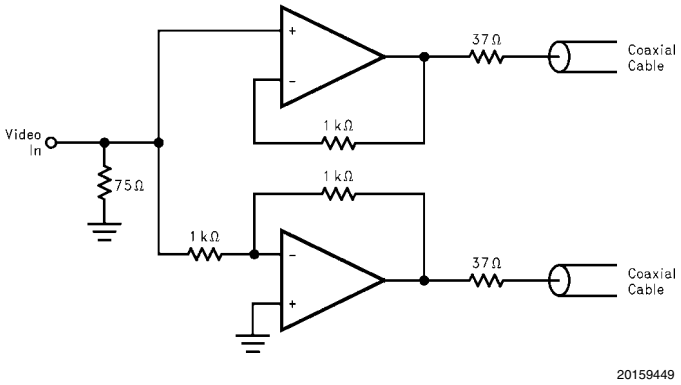
Application Circuits

I- to -V Converters



Differential Line Driver



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Revision History

Released	Revision	Section	Changes
12/08/2010	A	New Release, Corporate format	1 MDS data sheet converted into one Corp. data sheet format. MNLM6172AM-X-RH Rev 0A0 will be archived.

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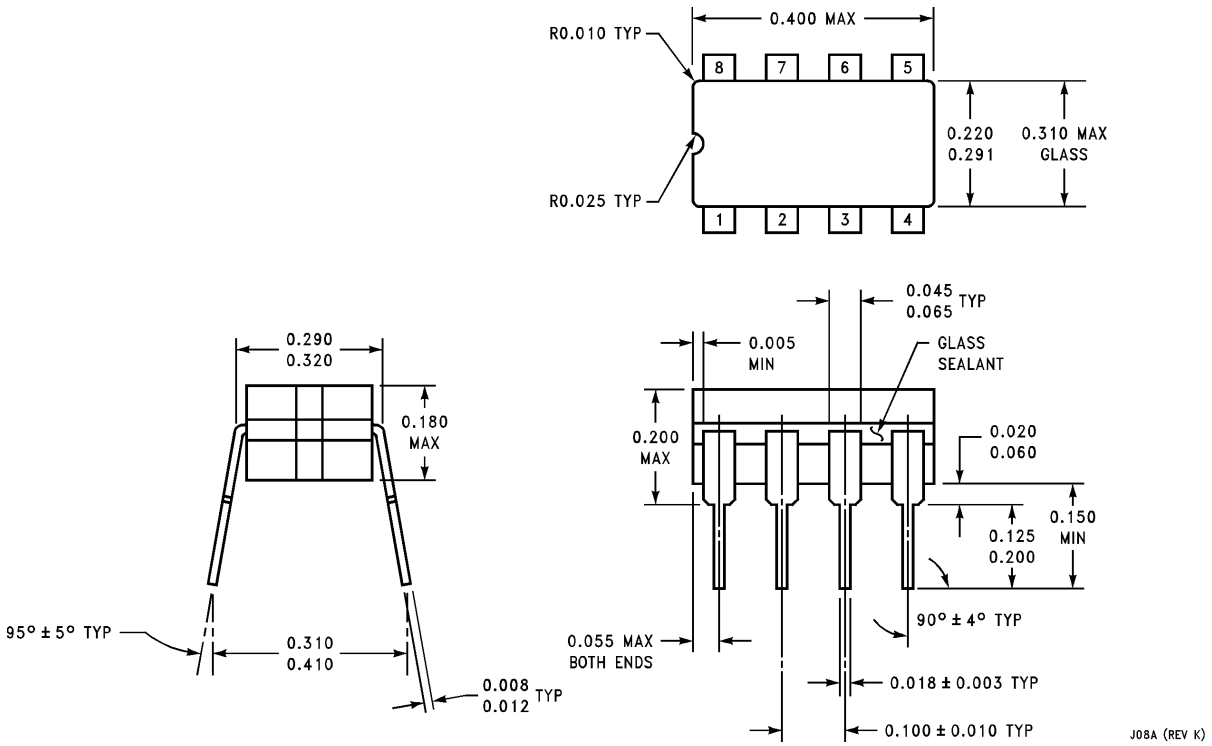
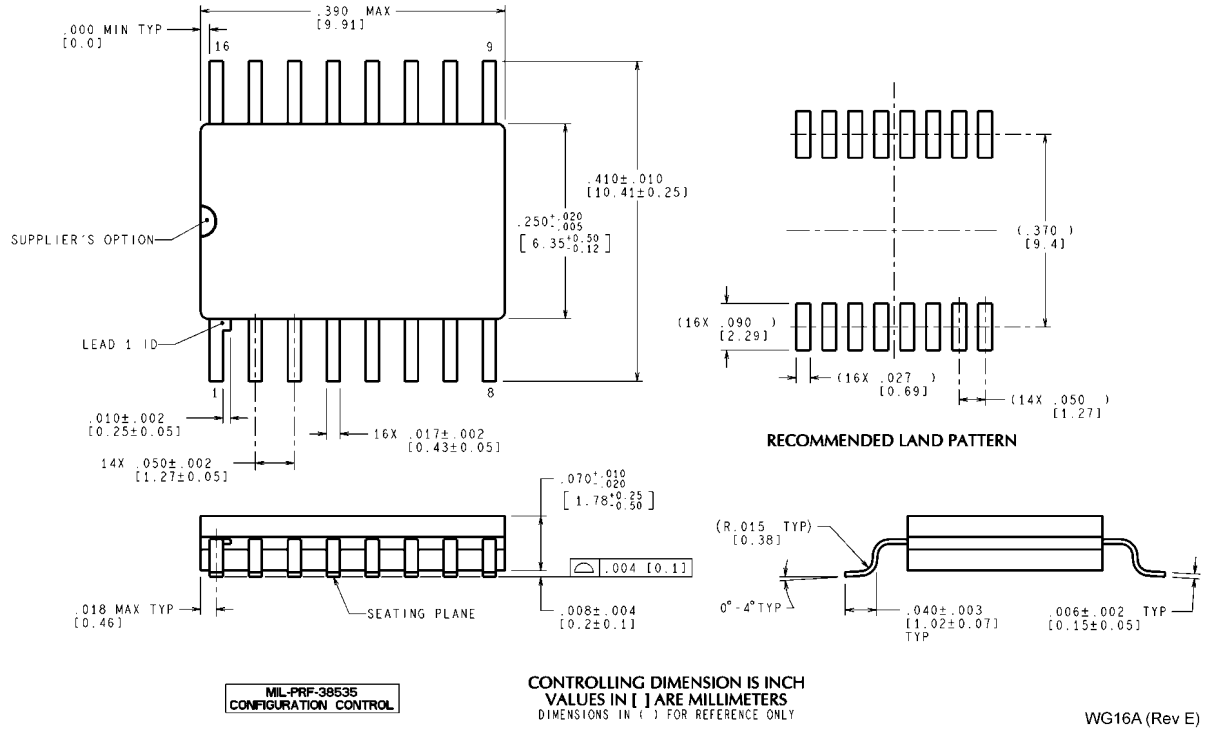
Physical Dimensions inches (millimeters) unless otherwise noted



8-Lead Ceramic Dual-In-Line Package
ONS Package Number J08A



16-Lead Ceramic SOIC Package
NS Package Number WG16A

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Notes

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Notes

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