

**LCD Panel Power Supplies with Low-Cost  
Linear-Regulator, Charge-Pumps and High-Current OP**

**Features**

- High-Performance Linear Regulator:
  - 1.6% Output Accuracy
  - Works with Small Ceramic Output Capacitors
  - Fast Transient Response
  - Foldback Current Limit
- High-Current Operational Amplifier:
  - 12V/μs Slew Rate
  - 12MHz, -3dB Bandwidth
  - Rail-to-Rail Inputs/Output
- 100mA Negative Charge Pump Regulator
- 50mA Positive Charge Pump Regulator with Adjustable Delay
- Built-In Power-Up Sequence
- Gate-on Pulse Modulator for Sequence & Discharge Control
- Thermal Protection
- Latched Fault Protection with Timer

**Applications**

- LCD Monitor Panel Modules
- LCD TV Panel Modules

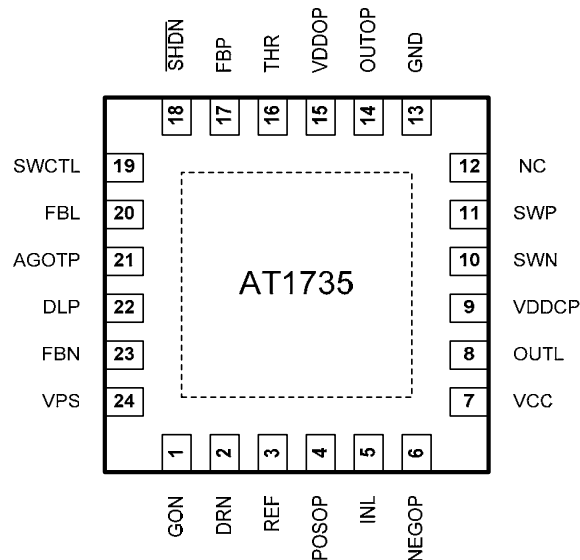
**General Description**

AT1735 provides a complete linear- regulator power supply solution for TFT LCD panels. AT1735 incorporates a high-performance linear regulator, two low-power charge-pump regulators, a high-current operational amplifier, and logic-controlled gate-on pulse modulator to control the positive charge-pump output sequence and waveform.

The linear regulator generates the source-driver supply voltage from the input voltage directly. The two charge-pump regulators generate the positive gate-on and negative gate-off supply voltages. The operational amplifier supplies the VCOM buffer with high output current, fast slew rate and wide bandwidth performances for driving capacitive loads. The gate-on pulse modulator control (SWCTL) is independent of the  $\overline{\text{SHDN}}$  chip enable control.

The AT1735 adopts a 24-pin thin QFN package which is 4mm x 4mm with a maximum thickness of 0.8mm for ultra-thin LCD panel application.

**Pin Configuration**

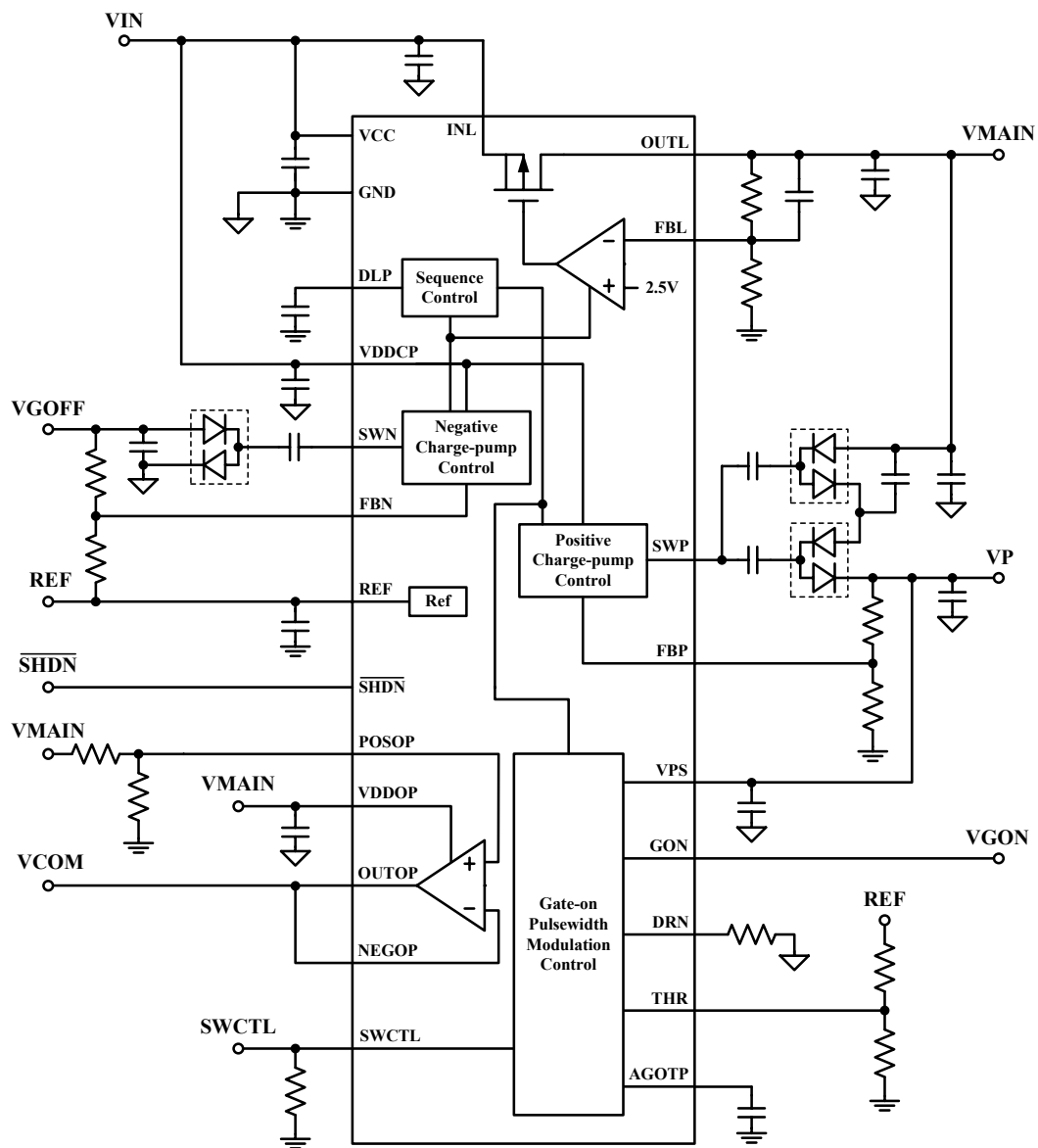


**Aimtron reserves the right without notice to change this circuitry and specifications.**

**Ordering Information**

Part number	Package	Marking
AT1735N_GRE	Thin QFN24, Green	AT1735N

**Block Diagram**



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**Pin Descriptions**

Pin No.	Pin Name	Function
1	GON	Internal High-Voltage MOSFET Switch Output Terminal for Gate-on Voltage Supply.
2	DRN	Discharge Switch Input. Connect a resistor to GND to discharge the $V_{GON}$ when SWCTL is low.
3	REF	Reference Output. Connect a 0.22 $\mu$ F capacitor from REF to GND. REF remains on in shutdown.
4	POSOP	Operational Amplifier Noninverting Input.
5	INL	Linear Regulator Input.
6	NEGOP	Operational Amplifier Inverting Input.
7	VCC	IC Supply Input. Connect VCC to GND with a 0.1 $\mu$ F bypass capacitor.
8	OUTL	Linear Regulator Output.
9	VDDCP	Supply Input for the Charge-Pump Regulators. Connect a 0.1 $\mu$ F bypass capacitor from VDDCP to GND.
10	SWN	Negative Charge-Pump Driver Output. Output high level is VDDCP, and output low level is GND. SWN is internally pulled to VDDCP in shutdown.
11	SWP	Positive Charge-Pump Driver Output. Output high level is VDDCP, and output low level is GND. SWP is internally pulled to GND in shutdown.
12	NC	No Connect.
13	GND	Ground.
14	OUTOP	Operational-Amplifier Output.
15	VDDOP	Operational-Amplifier Supply Input. Connect VDDOP to GND with a 0.1 $\mu$ F bypass capacitor.
16	THR	GON Voltage Low-Level Regulation Set-Point Input. Connect THR to the center of a resistive voltage-divider between REF and GND to set the low-level $V_{GON}$ regulation level. The threshold voltage is $10 \times V_{THR}$ .
17	FBP	Positive Charge-Pump Feedback Input. Place the voltage-divider to IC as close as possible.
18	$\overline{\text{SHDN}}$	Active-Low Shutdown Control Input. Pull $\overline{\text{SHDN}}$ low to turn off all sections of the device except REF. Pull $\overline{\text{SHDN}}$ high to enable the device. Cycle $\overline{\text{SHDN}}$ to reset the device after a fault.
19	SWCTL	Gate-on Pulse Modulator Timing Control Input.
20	FBL	Linear-Regulator Feedback Input. Place the voltage-divider to IC as close as possible.
21	AGOTP	Adjustable Gate-on Time Pulsewidth Modulator Input. AGOTP is high impedance when it is connected to REF. Connect a capacitor to GND to extend the Gate-on ON time.
22	DLP	Positive Charge-Pump Start-up Delay and Gate-on Pulse Modulator Delay Input. Connect a capacitor from DLP to GND to set the delay time. A 5 $\mu$ A current source charges $C_{DLP}$ .
23	FBN	Negative Charge-Pump Feedback Input. Place the voltage-divider to IC as close as possible.
24	VPS	Gate-on Pulse Modulator Voltage Supply Input. Source of the internal high-voltage P-channel MOSFET connected to GON.

**Absolute Maximum Ratings (Ta = 25 °C)**

Parameter	Rated Value		Unit
	Min.	Max.	
SWCTL, FBL, FBP, FBN, $\overline{\text{SHDN}}$ , REF, THR	-0.3	+6.0	V
AGOTP, DLP	-0.3	+6.0	V
VCC, INL, OUTL	-0.3	+18.0	V
VDDCP, VDDOP	-0.3	+18.0	V
POSOP, NEGOP, OUTOP	-0.3	+18.0	V
SWP, SWN	-0.3	+18.0	V
VPS, GON, DRN	-0.3	+30.0	V
DRN to GON	-30.0	+30.0	V
OUTOP Maximum Continuous Output Current	-40.0	+75.0	mA
Power Dissipation (Ta = 25 °C)	-	1349	mW
Operating Temperature	-35	+85	°C
Storage Temperature	-55	+150	°C
Lead Temperature (Soldering, 10s)	-	+300	°C
ESD Susceptibility (MM)	-200	200	V
ESD Susceptibility (HBM)	-2	2	KV

- Stresses beyond those listed under “Absolute Maximum Ratings” may cause permanent damage to the device. These are stress ratings only, and functional operations of the device at these or any other conditions beyond those indicated in the operational sections of the specifications are not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.
- Devices are ESD sensitive. Handling precaution recommended. The Human Body model is a 100pF capacitor discharged through a 1.5KΩ resistor into each pin.

**Recommended Operating Conditions**

Parameter	Symbol	Values			Unit
		Min.	Typ.	Max.	
Power Supply Voltage	V <sub>VCC</sub>	8	-	18	V
Operating Temperature*	T <sub>OP</sub>	-20	+25	+85	°C
Operating Junction Temperature	T <sub>J</sub>	-	-	+150	°C

\*Using X5R or X7R capacitors.

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**Electrical Characteristics**

(Test circuit is shown as Typical Application Circuit, unless otherwise noted.  $V_{CC} = V_{INL} = V_{VDDCP} = 12V$ ,  $V_{OUTL} = V_{VDDOP} = 10V$ ,  $V_{VPS} = 23V$ ,  $T_a = +25^\circ C$ .)

Parameter	Condition	Values			Unit
		Min.	Typ.	Max.	
VCC Operating Supply Range		8		18	V
VCC Quiescent Current	$\overline{SHDN} = GND$		0.7	0.9	mA
	$\overline{SHDN} = 3.3V$			2.5	
Duration to Trigger Fault Condition			44		ms
REF Output Voltage	$-10\mu A < I_{REF} < 1mA^*$ (excluding internal load)	4.9	5.0	5.1	V
VDDCP Input Supply Range		2.7		18	V
Charge-Pump Regulators Operating Frequency		1275	1500	1725	kHz
Thermal Shutdown	Rising temperature, 15 hysteresis		+160		
<b>Linear Regulator Section</b>					
INL Operation Supply Range	$V_{OUTL} < V_{INL}$	7		18	V
Dropout Voltage	$I_{OUTL} = 200mA$		200		mV
FBL Regulation Voltage	$I_{OUTL} = 50mA$	2.46	2.50	2.54	V
FBL Input Bias Current	$V_{FBL} = 2.5V$			50	nA
FBL Fault Trip Level (UVP)	Falling edge	1.85	2.00	2.15	V
FBL Line-Regulation Error	$V_{INL} = V_{CC} = 10.8V \sim 13.2V$ , $V_{OUTL} = 10V$ , $I_{OUTL} = 50mA$			15	mV
	$V_{INL} = V_{CC} = 11V \sim 20V$ , $V_{OUTL} = 10V$ , $I_{OUTL} = 50mA$		10		
Bandwidth	Guaranteed by design	1000			kHz
Maximum OUTL Current	$V_{FBL} = 2.4V$	500			mA
OUTL Soft-Start Period			2.73		ms
OUTL Load Regulation	$V_{CC} = 12V$ , $5mA < I_{OUTL} < 500mA$			2	%
<b>Operational Amplifier Section</b>					
VDDOP Supply Operating Range		4.5		16	V
VDDOP Supply Current	Buffer configuration, $V_{POSOP} = 4V$ , no load		1.0	1.5	mA
Input Offset Voltage	$(V_{NEGOP}, V_{POSOP}) = V_{VDDOP} / 2$ , $T_A = +25$	-16	0	16	mV
Input Bias Current	$(V_{NEGOP}, V_{POSOP}) = V_{VDDOP} / 2$	-50	+1	+50	nA
Common-Mode Input Range	$V_{NEGOP}, V_{POSOP}$	0		$V_{VDDOP}$	V

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Common-Mode Rejection Ratio	$0 \leq (V_{NEGOP}, V_{POSOP}) < V_{VDDOP}$	50	90		dB
Open-Loop Gain			125		dB
Output Voltage Swing High	$I_{OUTOP} = 100\mu A$	$V_{VDDOP} - 15$	$V_{VDDOP} - 8$		mV
	$I_{OUTOP} = 5mA$	$V_{VDDOP} - 150$	$V_{VDDOP} - 110$		
Output Voltage Swing Low	$I_{OUTOP} = -100\mu A$		20	35	mV
	$I_{OUTOP} = -5mA$		200	250	
Short-Circuit Current	Short to $V_{VDDOP} / 2$ , sourcing	50	125		mA
	Short to $V_{VDDOP} / 2$ , sinking	50	66		
Output Current	Buffer configuration, $V_{POSOP} = 4V$ , $V_{OUTOP\ error} < \pm 10mV$	-40		+80	mA
Power-Supply Rejection Ratio	$6V \leq V_{VDDOP} \leq 13.2V$ , DC ( $V_{NEGOP}, V_{POSOP}$ ) = $V_{VDDOP} / 2$	60	100		dB
Slew Rate			12		V/ $\mu s$
-3dB Bandwidth	Buffer configuration, $R_L = 10k\Omega$ , $C_L = 10pF$		12		MHz
Gain-Bandwidth Product	Buffer configuration, $R_L = 10k\Omega$ , $C_L = 10pF$		8		MHz
<b>Positive Charge-Pump Regulator Section</b>					
FBP Regulation Voltage	$I_{GON} = 10mA$	2.425	2.500	2.575	V
FBP Line-Regulation Error	$V_{OUTL} (V_{VDDCP}) = 10.8V \sim 13.2V$ , $V_{GON} = 23V$ , $I_{GON} = 20mA$			25	mV
FBP Input Bias Current	$V_{FBP} = 2.5V$	-50		+50	nA
SWP P-Channel On-Resistance			15	30	$\Omega$
SWP N-Channel On-Resistance	$V_{FBP} = 2.4V$		6	12	$\Omega$
	$V_{FBP} = 2.6V$	20			k $\Omega$
FBP Fault Trip Level (UVP)	Falling edge	1.85	2.00	2.15	V
Positive Charge-Pump Soft-Start Period			2.73		ms
<b>Negative Charge-Pump Regulator Section</b>					
FBN Regulation Voltage	$I_{GOFF} = -10mA$	200	250	300	mV
FBN Line-Regulation Error	$V_{OUTL} (V_{VDDCP}) = 10.8V \sim 13.2V$ , $V_{GOFF} = -6V$ , $I_{GOFF} = -50mA$			25	mV
FBN Input Bias Current	$V_{FBN} = 250mV$	-50		+50	nA
SWN P-Channel On-Resistance			3	6	$\Omega$
SWN N-Channel On-Resistance	$V_{FBN} = 350mV$		1.5	3	$\Omega$
	$V_{FBN} = 150mV$	20			k $\Omega$
FBN Fault Trip Level	Rising edge		700		mV
Negative Charge-Pump Soft-Start Period			2.73		ms
<b>Sequence Control Section</b>					

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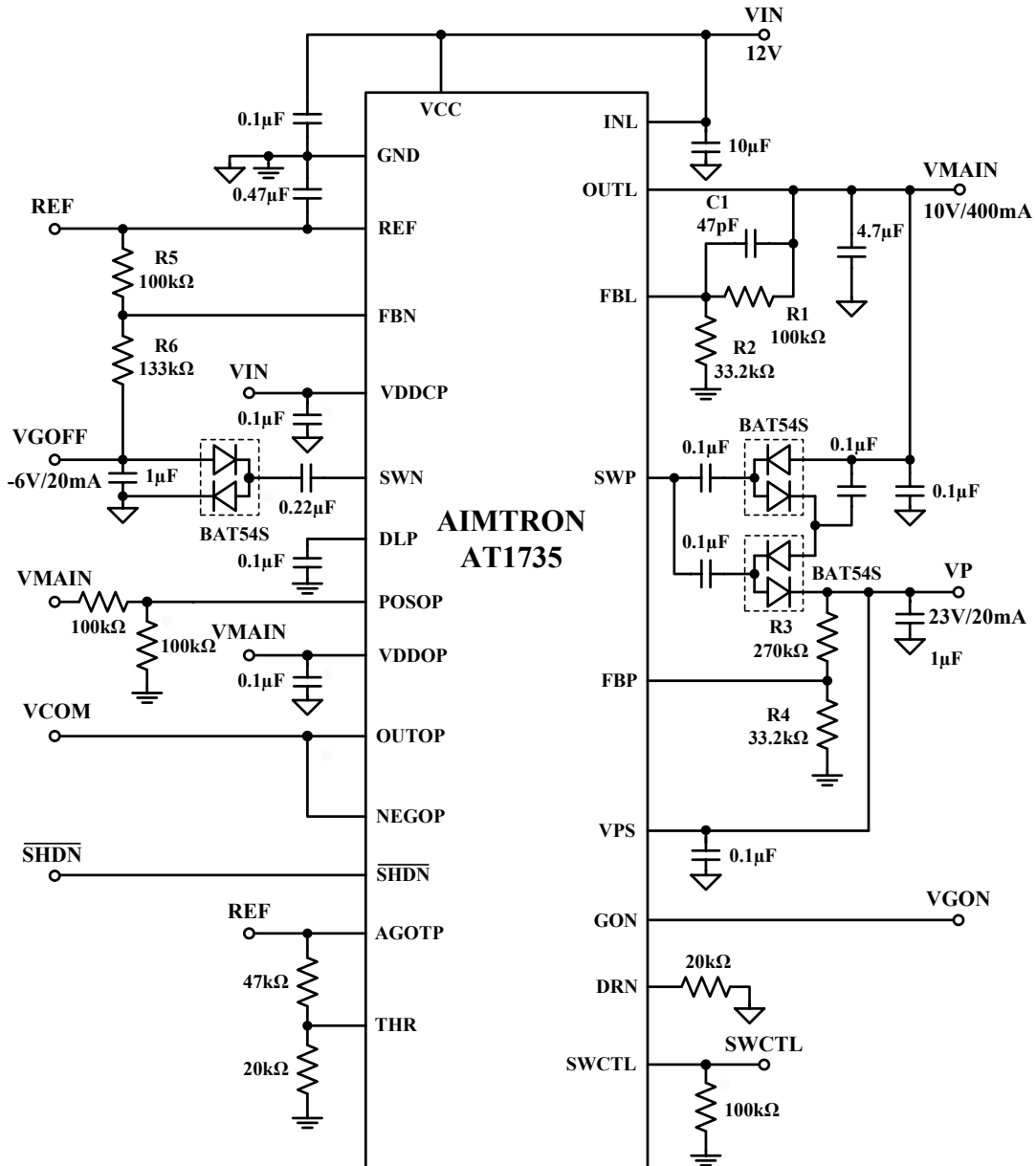
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SHDN Input Low Voltage				0.8	V
SHDN Input High Voltage		1.4			V
SHDN Input Current				2.5	μA
DLP Capacitor Charge Current	During startup, $V_{DLP} = 1.0V$	3.8	5	6.2	μA
DLP Turn-On Threshold		2.375	2.5	2.625	V
Pin Discharge Switch On-Resistance	SHDN = low or fault tripped; DLP, FBP, FBN to GND		60		Ω
	SHDN = low or fault tripped; OUTL, OUTOP to GND )		1.3		kΩ
	SWCTL=high, $V_{AGOPT} = V_{REF} / 2$ ; AGOTP to GND		1.3		kΩ
<b>Gate-on Pulse Modulator Section</b>					
SWCTL Input Low Voltage				1.0	V
SWCTL Input High Voltage		1.4			V
SWCTL Input Leakage Current		-1		+1	μA
SWCTL to GON Rising Propagation Delay	$V_{AGOPT} = V_{REF}$ , 1.5nF from GON to GND, $V_{SWCTL} = 0V$ to 3V step, no load on GON, measured from $V_{SWCTL} = 1.5V$ to GON = 20%		50		ns
SWCTL to GON Falling Propagation Delay	$V_{AGOPT} = V_{REF}$ , 1.5nF from GON to GND, $V_{SWCTL} = 3V$ to 0V step, DRN falling, no load on DRN and GON, measured from $V_{SWCTL} = 1.5V$ to GON = 80%		50		ns
VPS Input Voltage Range				30	V
VPS Input Current	$V_{AGOPT} = V_{REF}$ , $V_{DLP} = V_{REF}$ , SWCTL=high		80		μA
DRN Input Current	$V_{AGOPT} = V_{REF}$ , $V_{DRN} = 8V$ , $V_{DLP} = V_{REF}$ , SWCTL= low		80	120	μA
VPS to GON Switch On-Resistance	$V_{AGOPT} = V_{REF}$ , $V_{DLP} = V_{REF}$ , SWCTL=high		15	30	Ω
DRN to GON Switch On-Resistance	$V_{AGOPT} = V_{REF}$ , $V_{DLP} = V_{REF}$ , SWCTL =low		30		Ω
AGOTP Capacitor Charge-Current			50		μA
AGOTP Voltage Threshold for Enabling DRN Switch Control		2.3	2.5	2.7	V
AGOTP Current-Source Stop Voltage Threshold	$V_{AGOTP}$ rising edge	3.3	3.5	3.7	V
THR to GON Voltage Gain			10		V/V
GON Falling Slew Rate			13.5		V/μs

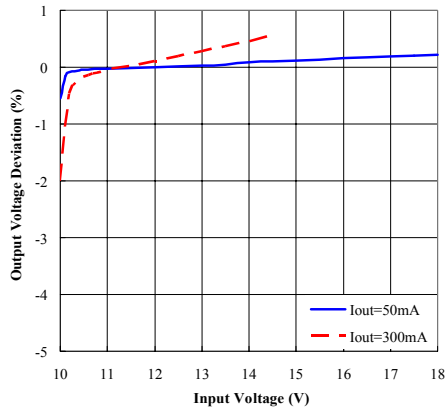
Typical Application Circuit



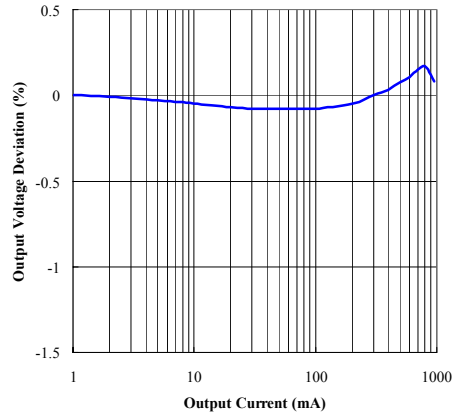


**Typical Characteristics**

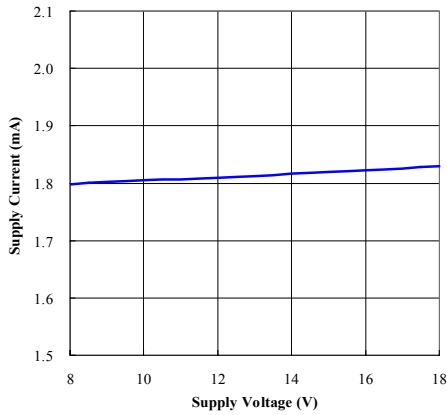
Linear Regulator Line Regulation



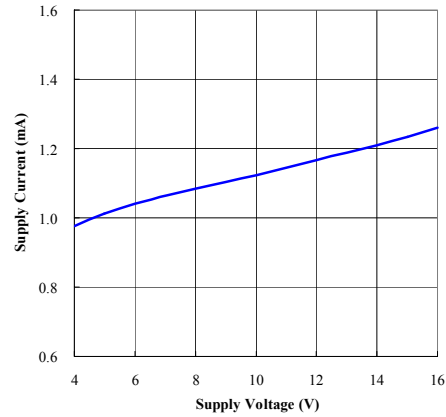
Linear Regulator Load Regulation



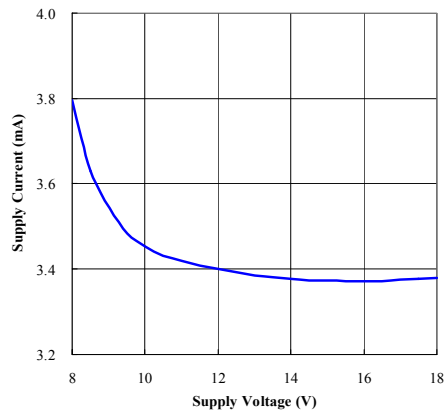
VCC No-load Supply Current vs. Supply Voltage



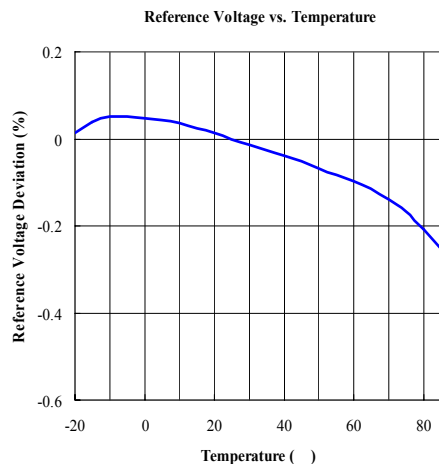
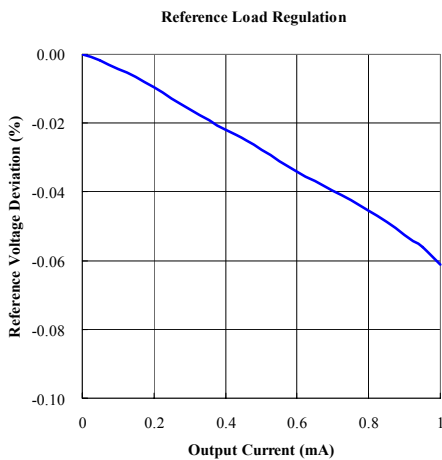
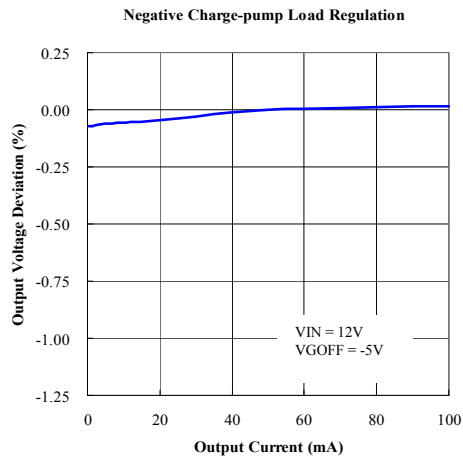
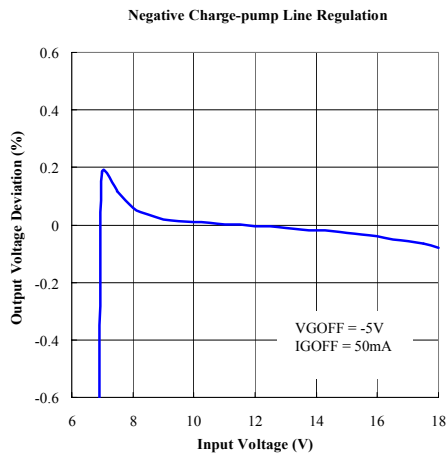
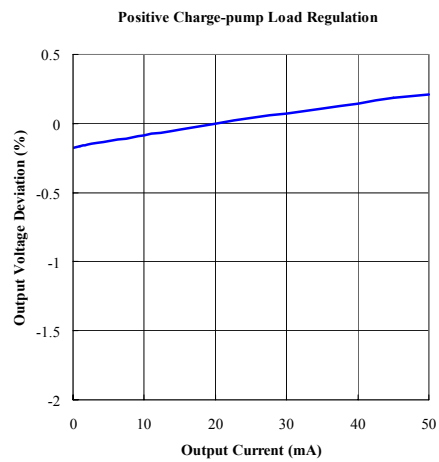
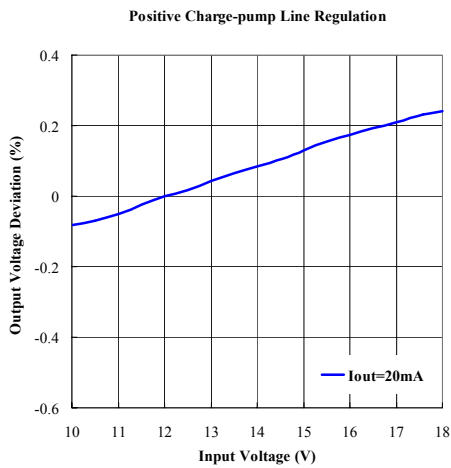
VDDOP No-load Supply Current vs. Supply Voltage



VDDCP No-load Supply Current vs. Supply Voltage



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(Test circuit is shown as Typical Application Circuit, unless otherwise noted.  $V_{CC} = V_{INL} = V_{VDDCP} =$

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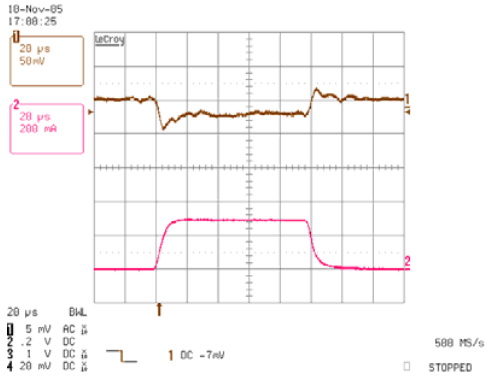
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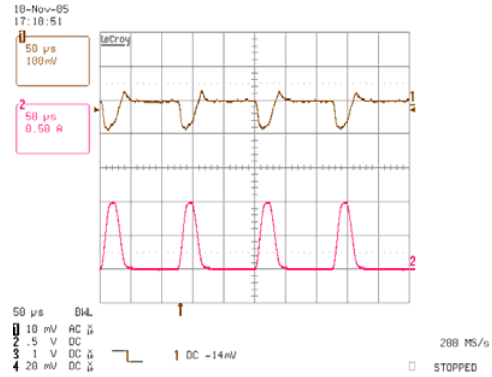
12V,  $V_{OUTL} = V_{VDDOP} = 10V$ ,  $V_{VPS} = 23V$ ,  $T_a = +25^\circ C$  .)

**Load Transient Response**



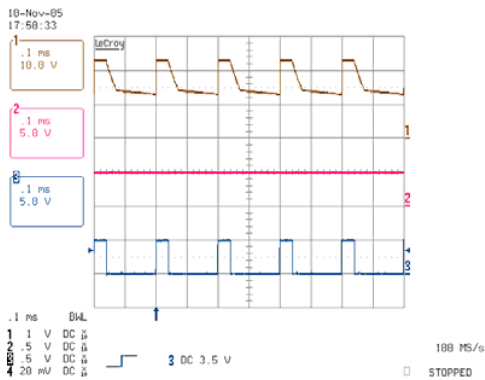
CH1:  $V_{OUTL}$   
CH2:  $I_{OUTL} = 0$  to 300mA

**Load Transient Response**



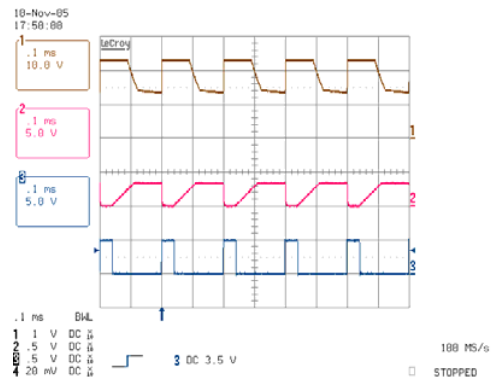
CH1:  $V_{OUTL}$   
CH2:  $I_{OUTL} = 0$  to 1A

**VGON Pulsewidth Modulation Control**



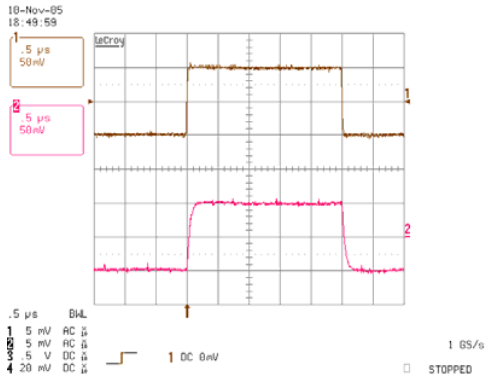
CH1: VGON  
CH2: AGOTP  
CH3: SWCTL

**VGON Pulsewidth Modulation Control**



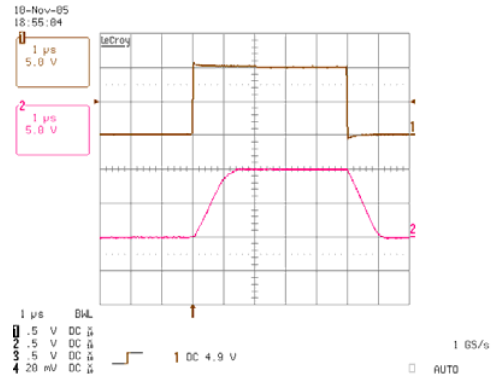
CH1: VGON  
CH2: AGOTP  
CH3: SWCTL

**OP Amp Small-signal Response**



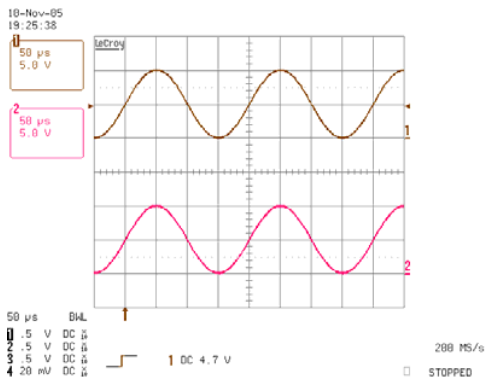
CH1:  $V_{POSOP}$   
 CH2:  $V_{OUTOP}$

**OP Amp Large-signal Response**



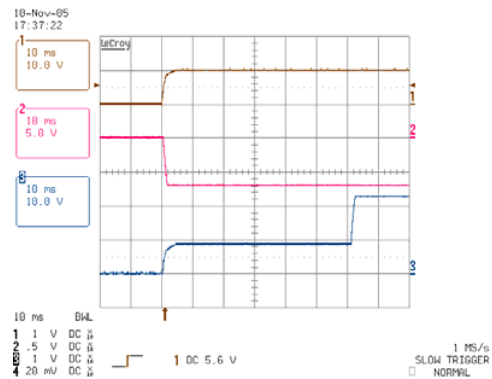
CH1:  $V_{POSOP}$   
 CH2:  $V_{OUTOP}$

**OP Amp Input & Output**



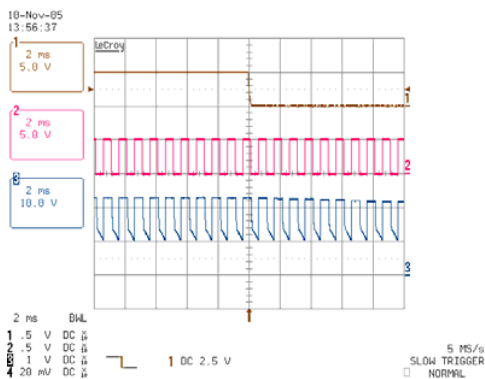
CH1:  $V_{POSOP}$   
 CH2:  $V_{OUTOP}$

**Power-up Sequence**



CH1:  $V_{MAIN}$  CH3:  $V_P$   
 CH2:  $V_{G OFF}$

**VGON Control**



CH1:  $\overline{SHDN}$  CH3:  $V_{GON}$   
 CH2:  $SWCTL$

### **Function Description**

The AT1735 consists of a high-performance linear regulator, two low-power charge-pump regulators, a high-current operational amplifier, and a gate-on pulse modulator to control the positive charge-pump output sequence and waveform.

The linear regulator generates the source-driver supply voltage from the input voltage directly. The two charge-pump regulators generate the positive gate-on and negative gate-off supply voltages. The operational amplifier supplies the VCOM buffer with high output current, fast slew rate and wide bandwidth performances for driving capacitive loads. The gate-on pulse modulator control, SWCTL, is independent of the  $\overline{\text{SHDN}}$  chip enable control in AT1735.

### **Linear Regulator**

The linear regulator of AT1735 uses an internal P-channel MOSFET to supply load currents up to 500mA. The internal reference voltage of linear regulator is 2.5V, connect an external resistive voltage-divider (R1 & R2 as the Typical Application Circuit shown) to set the output voltage as requirement. The linear regulator includes an OCP function to protect the internal transistor against over loads and short circuits. The operation input voltage range of the linear regulator is from 8V to 18V. The output voltage range of the linear regulator (OUTL) is up to 18V.

The linear regulator can driver at least 500mA output current continuously. The maximum application device power dissipation should not exceed the package-dissipation limit listed in the Absolute Maximum Ratings section.

After reference voltage reaches regulation and  $\overline{\text{SHDN}}$  is logic high, the linear regulator is enabled and starts to go through the soft-start procedure. The soft-start function is to ramp up its internal reference voltage from 0 to 2.5V in 128 steps. During the soft-start period, the output voltage fault protection function is disabled.

The internal current limit of linear-regulator is approximately 1.2A. The linear regulator output voltage starts to droop when the load current exceeds limit value.

### **Operational Amplifier**

The operational amplifier is with the excellent performances as high output current (150mA), fast slew rate (12V/ $\mu\text{s}$ ), and wide bandwidth (12MHz) to drive the distributed series capacitance and resistance of the TFT LCD backplane.

### Negative Charge-Pump Regulator

Negative charge-pump regulator contains internal P-channel and N-channel MOSFETs to perform the power transfer. The constant switching frequency of charge-pump regulator is 1.5MHz. The charge-pump inverts the supply voltage (VMAIN) and provides a regulated negative output voltage. Figure 1 shows charge-pump block diagram. During the first half-cycle, the P-channel MOSFET turns on and flying capacitor  $C_{CPN}$  charges to VMAIN minus a diode drop. During the second half-cycle, the P-channel MOSFET turns off, and the N-channel MOSFET turns on, level shifting  $C_{CPN}$ . This connects  $C_{CPN}$  in parallel with the reservoir capacitor  $C_{NEG}$ . The amount of charge transferred to the output is controlled by the variable N-channel on-resistance.

### Positive Charge-Pump Regulator

Positive charge-pump regulator also contains internal P-channel and N-channel MOSFETs to perform the power transfer. The internal MOSFETs switch at a constant 1.5MHz. The charge-pump inverts the doubles supply voltage (VMAIN) and provides a regulated positive output voltage. During the first half-cycle, the N-channel MOSFET turns on and flying capacitor  $C_{CPP}$  charges to VMAIN minus a diode drop. During the second half-cycle, the N-channel MOSFET turns off, and the P-channel MOSFET turns on, level shifting  $C_{CPP}$  by VMAIN volts. This connects  $C_{CPP}$  in parallel with the reservoir capacitor  $C_{POS}$ . The amount of charge transferred to the output is controlled by the variable N-channel on-resistance.

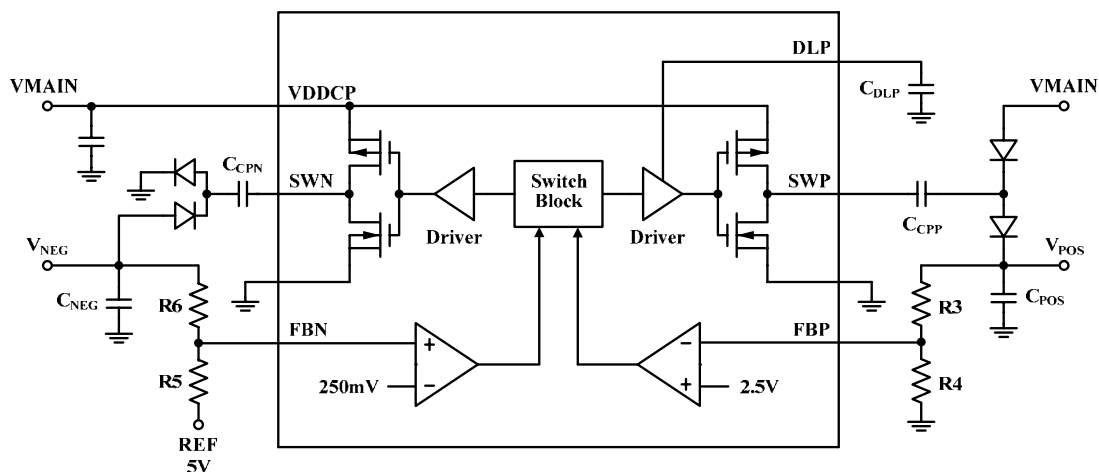


Figure 1. Charge-Pump Regulator Function Block

### **Output Voltage Fault Protection**

After soft-start period, if feedback voltage of the linear regulator or any of the charge-pump regulator outputs does not exceed its fault-detection threshold, the AT1735 enables the internal fault timer. If any fault condition exceeds the fault-timer duration (44ms typical), the AT1735 shuts down all the outputs except the reference. Once the fault condition is removed, toggle the  $\overline{\text{SHDN}}$  signal or cycle the input voltage to reactivate the chip.

### **Reference Voltage**

The reference output voltage is typical 5V and the source ability is up to 1mA. Connecting a 0.22 $\mu\text{F}$  bypass ceramic capacitor between REF and GND is recommended.

### **Gate-On Pulse Modulator**

The AT1735 includes a gate-on pulse modulator to control gate-on voltage waveform by SWCTL and AGOPT signals to reduce the flicker on TFT LCD panel.

There are two high voltage switches Q1 and Q2 connecting to GON. Another terminal of Q1 is connected to positive charge-pump output for the positive high voltage input, and Q2 is connected with a series resistor to ground for discharging the positive gate-on voltage. These two switches are controlled by DLP, SWCTL, AGOTP and THR. The switches start to be active after the  $V_{\text{DLP}}$  reaches  $V_{\text{REF}}/2$ . The operation that Q1 turns on and Q2 turns off is controlled by the condition SWCTL is logic high or  $V_{\text{AGOTP}}$  is lower than 2.5V. When  $V_{\text{AGOTP}}$  is higher than 2.5V, the Q1 turns off and the Q2 turns on. Once the  $V_{\text{GON}}/10$  is lower than the  $V_{\text{THR}}$ , both the two switches turn off. The control operations can be set to two difference modes as Fig 3 shown. Mode 1, connect AGOTP to REF. The high voltage period of VGON is identical to the SWCTL signal. Mode 2, connect a capacitor from AGOTP to ground. A constant current source (50 $\mu\text{A}$  typical) starts to charge this capacitor linearly when SWCTL is logic low. The VGON remains connecting to high input voltage VP as the  $V_{\text{AGOTP}}$  is lower than 2.5V.

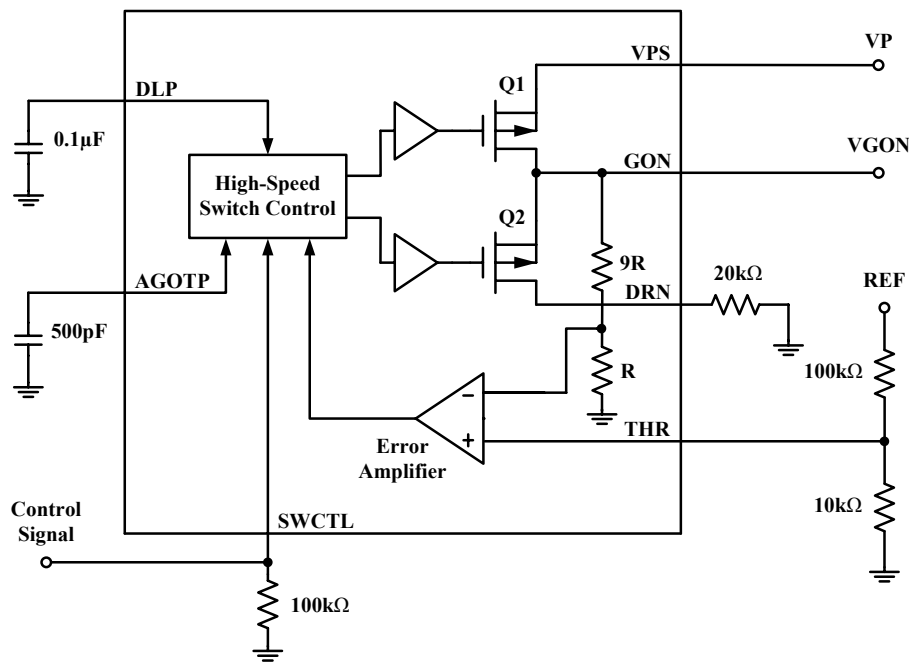


Figure 2. Gate-On Pulse Modulator Block Diagram

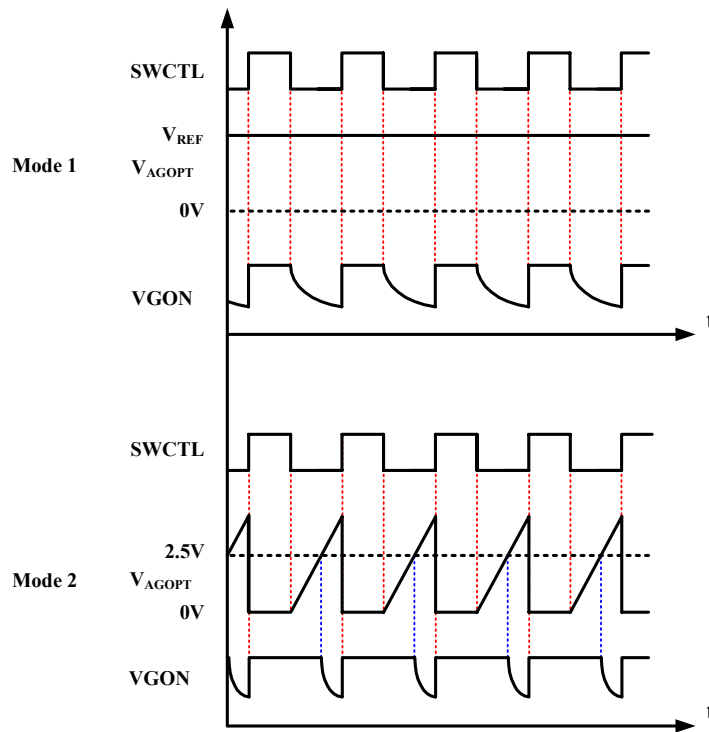


Figure 3. Gate-On Pulse Modulator Timing



**Power-Up Sequence**

When the AT1735 is powered up, the REF voltage rises with the input power. After the REF voltage is regulated and  $\overline{\text{SHDN}}$  is logic high, the linear regulator, OPA and the negative charge-pump regulator are enabled and enter the soft-start period.

A capacitor connecting from DLP pin to GND supplies positive charge-pump regulator start-up delay. When the REF is regulated and  $\overline{\text{SHDN}}$  is logic high, a 5.0uA current source charges  $C_{\text{DLP}}$ . When  $V_{\text{DLP}}$  goes above 2.5V, the positive charge pump regulator starts up and begins its soft-start period.

During the soft-start period, all the output voltage fault protection functions are disabled.

Select  $C_{\text{DLP}}$  using the following equation:

$$C_{\text{DLP}} = T_{\text{DELAY}} \times \frac{5.0\mu\text{A}}{V_{\text{REF}} / 2}$$

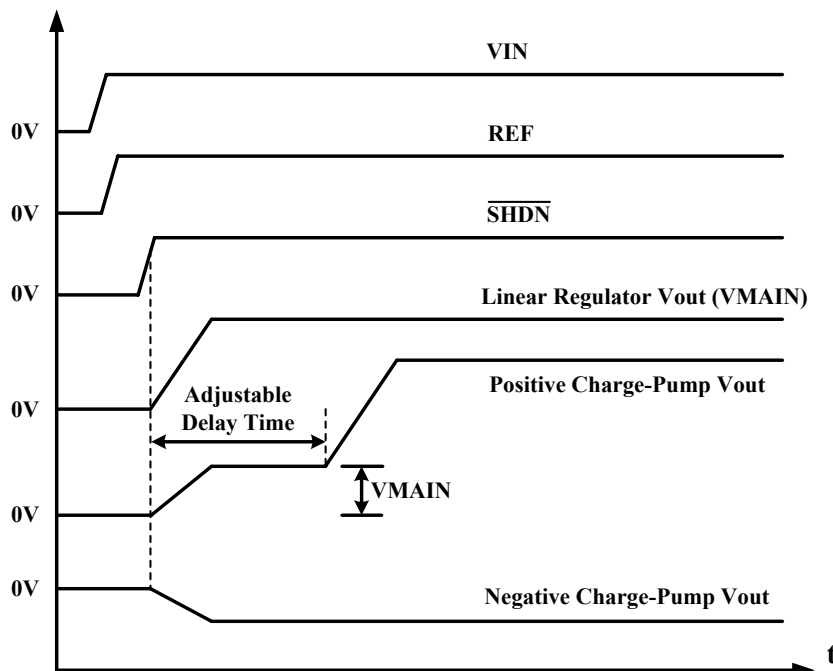


Figure 4. Power-Up Sequence

### Output Voltages Setting

The output voltages of linear regulator and charge-pump converters are set by each resistive voltage-divider as Typical Application Circuit shown. The AT1735 applies a 2.5V feedback reference voltage at FBL pin of linear regulator, and the output voltage setting is according to the following equation:

$$V_{VMAN} = 2.5 \times \left( 1 + \frac{R1}{R2} \right) \text{ (V)}$$

The feedback reference voltage of positive charge-pump  $V_{FBP}$  is typical 2.5V. The output voltage is set by the following equation:

$$V_{VP} = 2.5 \times \left( 1 + \frac{R3}{R4} \right) \text{ (V)}$$

The feedback reference voltage of negative charge-pump  $V_{FBN}$  is typical 250mV, and the reference voltage ( $V_{REF}$ ) is typical 5V. So the output voltage is set by the following equation:

$$V_{VGOFF} = 0.25 - \left( \frac{4.75 \times R6}{R5} \right) \text{ (V)}$$

### External Transistor for Higher Current

The linear regulator's power dissipation can be calculated in the following equation:

$$P_D = (V_{INL} - V_{OUTL}) \times I_{OUTL}$$

For some applications, the load current may be much higher than the regulator's guaranteed output current for the AT1735. It can be connect an external PNP transistor to solve this issue as shown in Figure 5.

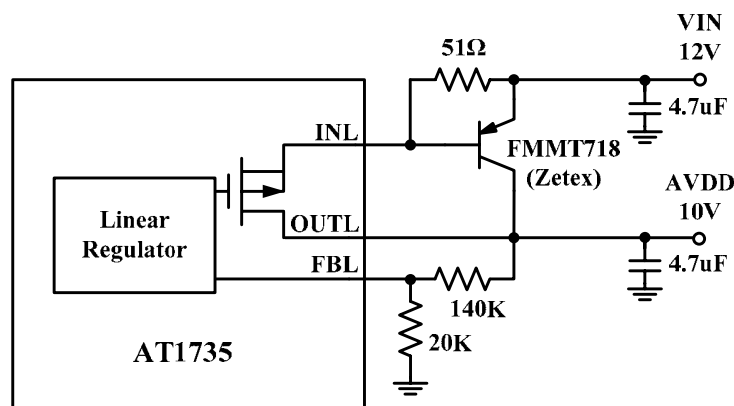
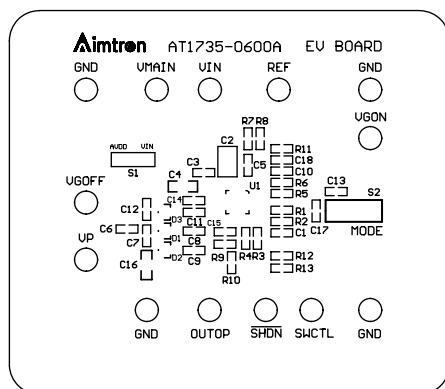


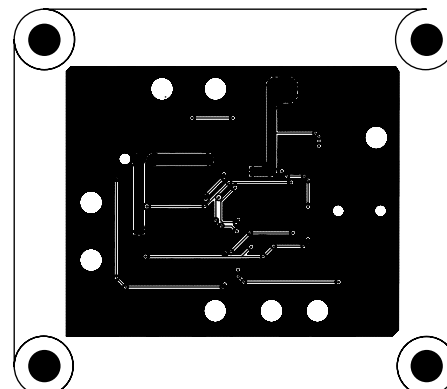
Figure 5. High-Current Linear Regulator

**PC Board Layout**

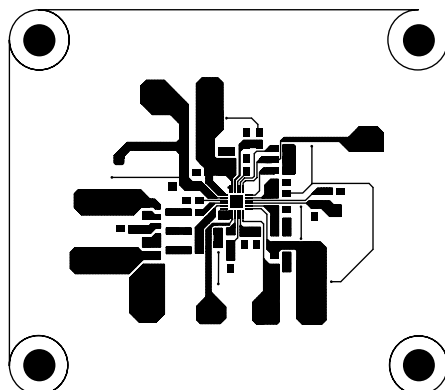
1. The most critical aspect of the layout is the placements of the input bypass capacitors of pin VCC, INL, VDDCP, VDDOP, VPS and REF. They must be placed as close as possible to the AT1735 to reduce the input ripple voltage and noise coupling.
2. Power loops on the input and output of the converters should be connected with the shortest and widest traces as possible. The long and narrow trace increases the ESR and ESL, and that will induce more effective noise at high frequency easily.
3. The feedback resistors should connect to FB pins as close as possible. And each route connected to output should be away from the switching noise source, such as charge-pump power loops.
4. Connecting all the ground-side of components at the backside ground-plane may effectively reduce the occurrence of unnecessary loop.



Component side

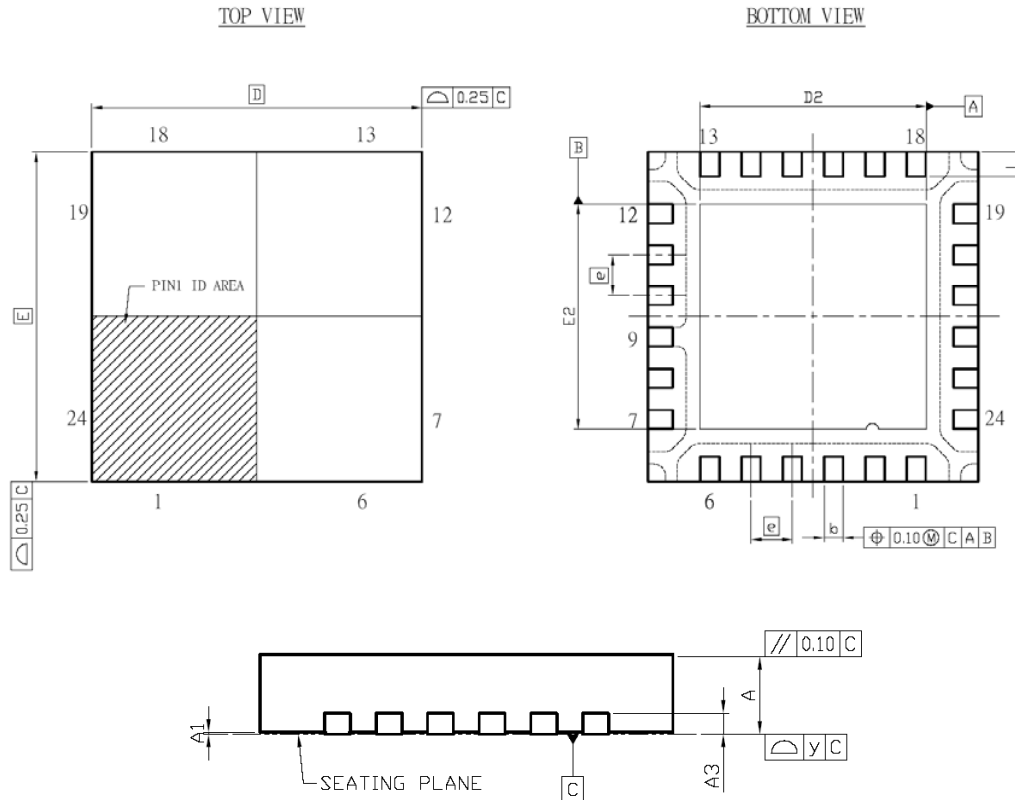


Bottom-layer



Top-layer

**Package Outline: Thin QFN-24**



SYMBOL	DIMENSION (MM)			DIMENSION (MIL)		
	MIN.	NOM.	MAX.	MIN.	NOM.	MAX.
A	0.70	0.75	0.80	27.6	29.5	31.5
A1	0	0.02	0.05	0	0.79	1.97
A3	0.203 REF			8 REF		
b	0.18	0.25	0.30	7.09	9.84	11.81
D	3.90	4.00	4.10	153.5	157.5	161.4
D2	2.66	2.74	2.82	104.7	107.9	111.0
E	3.90	4.00	4.10	153.5	157.5	161.4
E2	2.66	2.74	2.82	104.7	107.9	111.0
e	0.50 BSC			19.7 BSC		
L	0.22	0.30	0.38	8.8	11.8	14.8
y	0.08			3.15		
R	0.10 BSC			4.0 BSC		

7F, No.9,PARK AVENUE. II, Science-Based Industrial Park, Hsinchu 300,Taiwan, R.O.C.

Tel: 886-3-563-0878

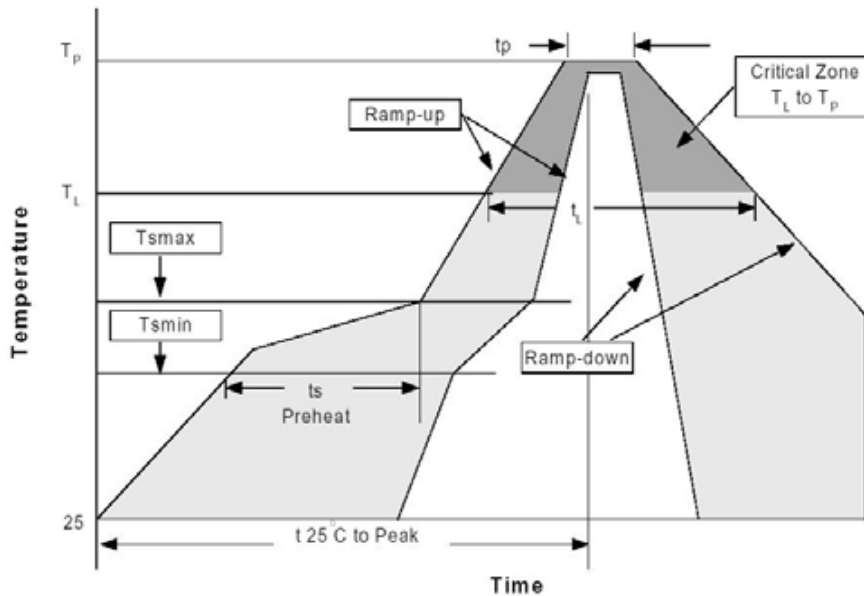
Fax: 886-3-563-0879

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3/20/2008 REV:1.1

Email: [service@aimtron.com.tw](mailto:service@aimtron.com.tw)

**Reflow Profiles**



Profile Feature	Sn-Pb Eutectic Assembly		Pb-Free Assembly	
	Large Body Pkg. thickness ≥2.5mm or Pkg. volume ≥350mm <sup>3</sup>	Small Body Pkg. thickness <2.5mm or Pkg. volume <350mm <sup>3</sup>	Large Body Pkg. thickness ≥2.5mm or Pkg. volume ≥350mm <sup>3</sup>	Small Body Pkg. thickness <2.5mm or Pkg. volume <350mm <sup>3</sup>
Average ramp-up rate (T <sub>L</sub> to T <sub>P</sub> )	3°C/second max.		3°C/second max.	
Preheat				
-Temperature Min(T <sub> Amin</sub> )	100°C		150°C	
-Temperature Max (T <sub> Tmax</sub> )	150°C		200°C	
-Time (min to max)(t <sub>s</sub> )	60-120 seconds		60-180 seconds	
T <sub> Tmax</sub> to T <sub> L</sub>				
-Ramp-up Rate			3°C/second max.	
Time maintained above:				
-Temperature (T <sub> L</sub> )	183°C		217°C	
-Time (t <sub> l</sub> )	60-150 seconds		60-150 seconds	
Peak Temperature(T <sub> P</sub> )	225+0/-5°C	240+0/-5°C	245+0/-5°C	250+0/-5°C
Time within 5°C of actual Peak Temperature (t <sub> p</sub> )	10-30 seconds	10-30 seconds	10-30 seconds	20-40 seconds
Ramp-down Rate	6°C/second max.		6°C/second max.	
Time 25°C to Peak Temperature	6 minutes max.		8 minutes max.	

\*All temperatures refer to topside of the package, measured on the package body surface.