## Features

- MOSFET Input Stage
- Very High Input Impedance ( $\mathrm{Z}_{\mathrm{IN}}$ ) . . . . . . . . 1.7T $\Omega$ (Typ)
- Very Low Input Current at $\mathrm{V}_{+}=5 \mathrm{~V}$. . . . . . . 3.5pA (Typ)
- Wide Common Mode Input Voltage Range (VICR) Can Be Swung 1.5V (Typ) Below Negative Supply Voltage Rail
- Virtually Eliminates Errors Due to Flow of Input Currents
- Output Voltage Compatible with TTL, DTL, ECL, MOS, and CMOS Logic Systems in Most Applications


## Applications

- High Source Impedance Voltage Comparators
- Long Time Delay Circuits
- Square Wave Generators
- A/D Converters
- Window Comparators


## Part Number Information

| PART <br> NUMBER | TEMP <br> RANGE $\left({ }^{\circ} \mathbf{C}\right)$ | PACKAGE | PKG. NO. |
| :--- | :---: | :--- | :--- |
| CA3290AE | -55 to 125 | 8 Ld PDIP | E8.3 |
| CA3290E | -55 to 125 | 8 Ld PDIP | E8.3 |

## Schematic Diagram

## (ONLY ONE IS SHOWN)



## Absolute Maximum Ratings

Supply Voltage
Single Supply . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . +36 V
Dual Supply. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . $\pm 18 \mathrm{~V}$
Differential Input Voltage . . . . . . . . . . . . . . . . 36V or [(V+- V-) +5 V ] (whichever is less)
DC Input Voltage $\qquad$ . $\mathrm{V}++5 \mathrm{~V}$ to $\mathrm{V}--5 \mathrm{~V}$ Output to V- Short Circuit Duration (Note 1) . . . . . . . . . . . Continuous Input Current
$\qquad$

## Operating Conditions

Temperature Range. $\qquad$ -55 to $125^{\circ} \mathrm{C}$
CAUTION: Stresses above those listed in "Absolute Maximum Ratings" may cause permanent damage to the device. This is a stress only rating and operation of the device at these or any other conditions above those indicated in the operational sections of this specification is not implied.

NOTES:

1. Short circuits from the output to $V+$ can cause excessive heating and eventual destruction of the device.
2. $\theta_{\mathrm{JA}}$ is measured with the component mounted on an evaluation PC board in free air.

## Electrical Specifications $\quad \mathrm{V}-=0 \mathrm{~V}$, Unless Otherwise Specified

| PARAMETER | SYMBOL | TEST CONDITIONS | $\begin{gathered} \text { TEMP } \\ \left({ }^{\circ} \mathrm{C}\right) \end{gathered}$ | CA3290A |  |  | CA3290 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\mathrm{V}_{\mathrm{IO}}$ | $\mathrm{V}_{\mathrm{CM}}=\mathrm{V}_{\mathrm{O}}=1.4 \mathrm{~V}, \mathrm{~V}+=5 \mathrm{~V}$ | Full | - | 4.5 | - | - | 8.5 | - | mV |
|  |  | $\begin{aligned} & \mathrm{V}_{\mathrm{CM}}=\mathrm{V}_{\mathrm{O}}=0 \mathrm{~V}, \mathrm{~V}_{+}=+15 \mathrm{~V}, \\ & \mathrm{~V}-=-15 \mathrm{~V} \end{aligned}$ | Full | - | 8.5 | - | - | 8.5 | - | mV |
|  |  | $\mathrm{V}_{\mathrm{CM}}=\mathrm{V}_{\mathrm{O}}=1.4 \mathrm{~V}, \mathrm{~V}_{+}=5 \mathrm{~V}$ | 25 | - | 4.0 | 10 | - | 7.5 | 20 | mV |
|  |  | $\begin{aligned} & \mathrm{V}_{\mathrm{CM}}=\mathrm{V}_{\mathrm{O}}=0 \mathrm{~V}, \mathrm{~V}_{+}=+15 \mathrm{~V}, \\ & \mathrm{~V}-=-15 \mathrm{~V} \end{aligned}$ | 25 | - | 4.0 | 10 | - | 7.5 | 20 | mV |
| Temperature Coefficient of Input Offset Voltage | $\Delta \mathrm{V}_{1 \mathrm{O}} / \Delta \mathrm{T}$ |  |  | - | 8 | - | - | 8 | - | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Input Offset Current | 10 | $\mathrm{V}_{\mathrm{CM}}=1.4 \mathrm{~V}, \mathrm{~V}+=5 \mathrm{~V}$ | Full | - | 2 | 28 | - | 2 | 32 | nA |
|  |  | $\begin{aligned} & \mathrm{V}_{\mathrm{CM}}=0 \mathrm{~V}, \mathrm{~V}_{+}=+15 \mathrm{~V}, \mathrm{~V}-=- \\ & 15 \mathrm{~V} \end{aligned}$ | Full | - | 7 | 28 | - | 7 | 32 | nA |
|  |  | $\mathrm{V}_{\mathrm{CM}}=1.4 \mathrm{~V}, \mathrm{~V}+=5 \mathrm{~V}$ | 25 | - | 2 | 25 | - | 2 | 30 | pA |
|  |  | $\begin{aligned} & \mathrm{V}_{\mathrm{CM}}=0 \mathrm{~V}, \\ & \mathrm{~V}_{+}=+15 \mathrm{~V}, \mathrm{~V}-=-15 \mathrm{~V} \end{aligned}$ | 25 | - | 7 | 25 | - | 7 | 30 | pA |
| Input Current | 1 | $\mathrm{V}_{\mathrm{CM}}=1.4 \mathrm{~V}, \mathrm{~V}+=5 \mathrm{~V}$ | 125 | - | 2.8 | 45 | - | 2.8 | 55 | nA |
|  |  | $\begin{aligned} & \mathrm{V}_{\mathrm{CM}}=0 \mathrm{~V}, \mathrm{~V}_{+}=+15 \mathrm{~V}, \mathrm{~V}-=- \\ & 15 \mathrm{~V} \end{aligned}$ | 125 | - | 13 | 45 | - | 13 | 55 | nA |
|  |  | $\mathrm{V}_{\mathrm{CM}}=1.4 \mathrm{~V}, \mathrm{~V}+=5 \mathrm{~V}$ | 25 | - | 3.5 | 40 | - | 3.5 | 50 | pA |
|  |  | $\begin{aligned} & \mathrm{V}_{\mathrm{CM}}=0 \mathrm{~V}, \mathrm{~V}_{+}=+15 \mathrm{~V}, \mathrm{~V}-=- \\ & 15 \mathrm{~V} \end{aligned}$ | 25 | - | 12 | 40 | - | 12 | 50 | pA |
| Supply Current | I+ | $\mathrm{R}_{\mathrm{L}}=\infty, \mathrm{V}+=5 \mathrm{~V}$ | -55 | - | 0.85 | 1.0 | - | 0.85 | 1.6 | mA |
|  |  | $\mathrm{R}_{\mathrm{L}}=\infty, \mathrm{V}+=30 \mathrm{~V}$ | -55 | - | 1.62 | 3.0 | - | 1.62 | 3.5 | mA |
|  |  | $\mathrm{R}_{\mathrm{L}}=\infty, \mathrm{V}+=5 \mathrm{~V}$ | 25 | - | 0.8 | 1.4 | - | 0.8 | 1.4 | mA |
|  |  | $\mathrm{R}_{\mathrm{L}}=\infty, \mathrm{V}+=30 \mathrm{~V}$ | 25 | - | 1.35 | 3.0 | - | 1.35 | 3.0 | mA |
| Voltage Gain | AOL | $\begin{aligned} & R_{\mathrm{L}}=15 \mathrm{k} \Omega, \mathrm{~V}+=+15 \mathrm{~V}, \\ & \mathrm{~V}-=-15 \mathrm{~V} \end{aligned}$ | Full | - | 150 | - | - | 150 | - | $\mathrm{V} / \mathrm{mV}$ |
|  |  |  |  | - | 103 | - | - | 103 | - | dB |
|  |  | $\begin{aligned} & R_{\mathrm{L}}=15 \mathrm{k} \Omega, \mathrm{~V}_{+}=+15 \mathrm{~V}, \\ & \mathrm{~V}-=-15 \mathrm{~V} \end{aligned}$ | 25 | 25 | 800 | - | 25 | 800 | - | V/mV |
|  |  |  |  | 88 | 118 | - | 88 | 118 | - | dB |

## Electrical Specifications $\quad \mathrm{V}-=0 \mathrm{~V}$, Unless Otherwise Specified (Continued)

| PARAMETER | SYMBOL | TEST CONDITIONS | $\begin{aligned} & \text { TEMP } \\ & \left({ }^{\circ} \mathrm{C}\right) \end{aligned}$ | CA3290A |  |  | CA3290 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Saturation Voltage | $\mathrm{V}_{\text {SAT }}$ | $\begin{aligned} & \operatorname{ISINK}=4 \mathrm{~mA}, \mathrm{~V}+=5 \mathrm{~V}, \\ & +\mathrm{V}_{\mathrm{I}}=0 \mathrm{~V},-\mathrm{V}_{\mathrm{I}}=1 \mathrm{~V} \end{aligned}$ | 125 | - | 0.22 | 0.7 | - | 0.22 | 0.7 | V |
|  |  | $\begin{aligned} & \text { ISINK }=4 \mathrm{~mA}, \mathrm{~V}+=5 \mathrm{~V}, \\ & +\mathrm{V}_{\mathrm{I}}=0 \mathrm{~V},-\mathrm{V}_{\mathrm{I}}=1 \mathrm{~V} \end{aligned}$ | -55 | - | 0.1 | - | - | 0.1 | - | V |
|  |  | $\begin{aligned} & \text { ISINK }=4 \mathrm{~mA}, \mathrm{~V}+=5 \mathrm{~V}, \\ & +\mathrm{V}_{\mathrm{I}}=0 \mathrm{~V},-\mathrm{V}_{\mathrm{I}}=1 \mathrm{~V} \end{aligned}$ | 25 | - | 0.12 | 0.4 | - | 0.12 | 0.4 | V |
| Output Leakage Current | ${ }^{\text {IOL }}$ | $\mathrm{V}+=15 \mathrm{~V}$ | Full | - | 65 | - | - | 65 | - | nA |
|  |  | $\mathrm{V}+=36 \mathrm{~V}$ | Full | - | 130 | 1k | - | 130 | 1k | nA |
|  |  | $\mathrm{V}+=15 \mathrm{~V}$ | 25 | - | 100 | - | - | 100 | - | pA |
|  |  | $\mathrm{V}+=36 \mathrm{~V}$ | 25 | - | 500 | - | - | 500 | - | pA |
| Common Mode Input Voltage Range | VICR | $\mathrm{V}_{\mathrm{O}}=1.4 \mathrm{~V}, \mathrm{~V}_{+}=5 \mathrm{~V}$ | 25 | $\begin{gathered} \mathrm{V}+-3.5 \\ \mathrm{~V}- \end{gathered}$ | $\begin{aligned} & \hline V+-3.1 \\ & V--1.5 \end{aligned}$ | - | $\begin{gathered} V+-3.5 \\ V- \end{gathered}$ | $\begin{aligned} & V+-3.1 \\ & V-1.5 \end{aligned}$ | - | V |
|  |  | $\mathrm{V}_{\mathrm{O}}=0 \mathrm{~V}, \mathrm{~V}_{+}=+15 \mathrm{~V}, \mathrm{~V}-=-15 \mathrm{~V}$ | 25 | $\begin{gathered} \mathrm{V}+-3.8 \\ \mathrm{~V}- \end{gathered}$ | $\begin{aligned} & \hline \mathrm{V}+-3.4 \\ & \mathrm{~V}--1.6 \end{aligned}$ | - | $\begin{gathered} \mathrm{V}+-3.8 \\ \mathrm{~V}- \end{gathered}$ | $\begin{aligned} & \hline V+-3.4 \\ & V--1.6 \end{aligned}$ | - | V |
| Common Mode Rejection Ratio | CMRR | $\mathrm{V}+=+15 \mathrm{~V}, \mathrm{~V}-=-15 \mathrm{~V}$ | 25 | - | 44 | 562 | - | 44 | 562 | $\mu \mathrm{V} / \mathrm{V}$ |
|  |  | $\mathrm{V}+=5 \mathrm{~V}$ | 25 | - | 100 | 562 | - | 100 | 562 | $\mu \mathrm{V} / \mathrm{V}$ |
| Power Supply Rejection Ratio | PSRR | $\mathrm{V}+=+15 \mathrm{~V}, \mathrm{~V}-=-15 \mathrm{~V}$ | 25 | - | 15 | 316 | - | 15 | 316 | $\mu \mathrm{V} / \mathrm{V}$ |
| Output Sink Current |  | $\mathrm{V}_{\mathrm{O}}=1.4 \mathrm{~V}, \mathrm{~V}_{+}=5 \mathrm{~V}$ | 25 | 6 | 30 | - | 6 | 30 | - | mA |
| Response Time Rising Edge | $t_{r}$ | $\mathrm{R}_{\mathrm{L}}=5.1 \mathrm{k} \Omega, \mathrm{V}+=15 \mathrm{~V}$ | 25 | - | 1.2 | - | - | 1.2 | - | $\mu \mathrm{s}$ |
| Response Time Falling Edge | $t_{f}$ | $\mathrm{R}_{\mathrm{L}}=5.1 \mathrm{k} \Omega, \mathrm{V}+=15 \mathrm{~V}$ | 25 | - | 200 | - | - | 200 | - | ns |
| Large Signal Response Time |  | $\mathrm{R}_{\mathrm{L}}=5.1 \mathrm{k} \Omega, \mathrm{V}+=15 \mathrm{~V}$ | 25 | - | 500 | - | - | 500 | - | ns |
|  |  | $\mathrm{R}_{\mathrm{L}}=5.1 \mathrm{k} \Omega, \mathrm{V}+=5 \mathrm{~V}$ | 25 | - | 400 | - | - | 400 | - | ns |

## Test Circuits and Waveforms




WITH $\mathrm{C}_{\mathrm{C}}$
Top Trace $\approx 4.5 \mathrm{mV} /$ Div. $=\mathrm{V}_{\mathrm{IN}}$ Bottom Trace $=10 \mathrm{~V} /$ Div. $=\mathrm{V}_{\text {OUT }}$ Time Scale $=5 \mu \mathrm{~s} /$ Div.


WITHOUT $\mathrm{C}_{\mathrm{C}}$
Top Trace $\approx 4.5 \mathrm{mV} /$ Div. Bottom Trace $=10 \mathrm{~V} /$ Div.
Time Scale $=5 \mu \mathrm{~s} /$ Div.

FIGURE 1. PARASITIC OSCILLATIONS TEST CIRCUIT AND WAVEFORMS

## Test Circuits and Waveforms



FIGURE 2. NON-INVERTING COMPARATOR RESPONSE TIME TEST CIRCUIT AND WAVEFORMS


FIGURE 3. INVERTING COMPARATOR RESPONSE TIME TEST CIRCUIT AND WAVEFORMS

## Circuit Description

## The Basic Comparator

Figure 4 shows the basic circuit diagram for one of the two comparators in the CA3290. It is generically similar to the industry type "139" comparators, with PMOS transistors replacing PNP transistors as input stage elements. Transistors $Q_{1}$ through $Q_{4}$ comprise the differential input stage, with $Q_{5}$ and $Q_{6}$ serving as a mirror connected active load and differential-to-single-ended converter. The differential input at $Q_{1}$ and $Q_{4}$ is amplified so as to toggle $Q_{6}$ in accordance with the input signal polarity. For example, if $+\mathrm{V}_{\mathrm{IN}}$ is greater than $-\mathrm{V}_{\mathrm{IN}}, \mathrm{Q}_{1}, \mathrm{Q}_{2}$, and current mirror transistors $Q_{5}$ and $Q_{6}$ will be turned off; Transistors $Q_{3}, Q_{4}$, and $Q_{7}$ will be turned on, causing $Q_{8}$ to be turned off. The output is pulled positive when a load resistor is connected between the output and $\mathrm{V}+$.

In essence, $Q_{1}$ and $Q_{4}$ function as source followers to drive $Q_{2}$ and $Q_{3}$, respectively, with zener diodes $D_{1}$ through $D_{4}$ providing gate oxide protection against input voltage
transients (e.g., static electricity). The current flow in $Q_{1}$ and $Q_{4}$ is established at approximately $50 \mu \mathrm{~A}$ by constant current sources $I_{1}$ and $I_{3}$, respectively. Since $Q_{1}$ and $Q_{4}$ are operated with a constant current load, their gate-to-source voltage drops will be effectively constant as long as the input voltages are within the common-mode range.

As a result, the input offset voltage $\left(V_{G S}(\mathrm{Q} 1)+\mathrm{V}_{\mathrm{BE}(\mathrm{Q} 2)}\right.$ -
$V_{B E(Q 3)}-V_{G S(Q 4)}$ will not be degraded when a large differential DC voltage is applied to the device for extended periods of time at high temperatures.

Additional voltage gain following the first stage is provided by transistors $Q_{7}$ and $Q_{8}$. The collector of $Q_{8}$ is open, offering the user a wide variety of options in applications. An additional discrete transistor can be added if it becomes necessary to boost the output sink current capability.

The detailed schematic diagram for one comparator and the common current source biasing is shown on the front page. PMOS transistors $Q_{9}$ through $Q_{12}$ are the current source
elements identified in Figure 4 as $I_{1}$ through $I_{4}$, respectively. Their gate source potentials $\left(\mathrm{V}_{\mathrm{GS}}\right)$ are supplied by a common bus from the biasing circuit shown in the right hand portion of the Schematic Diagram. The currents supplied by $Q_{10}$ and $Q_{12}$ are twice those supplied by $Q_{9}$ and $Q_{11}$. The transistor geometries are appropriately scaled to provide the requisite currents with common $\mathrm{V}_{\mathrm{GS}}$ applied to $\mathrm{Q}_{9}$ through $\mathrm{Q}_{12}$.


FIGURE 4. BASIC CIRCUIT DIAGRAM FOR ONE OF THE TWO COMPARATORS

## Operating Considerations

## Input Circuit

The use of MOS transistors in the input stage of the CA3290 series circuits provides the user with the following features for comparator applications:

1. Ultra high input impedance ( $(\underline{\underline{1} .7 \mathrm{~T} \Omega \text { ); }}$
2. The availability of common mode rejection for input signals at potentials below that of the negative power supply rail;
3. Retention of the in phase relationship of the input and output signals for input signals below the negative rail.
Although the CA3290 employs rugged bipolar (zener) diodes for protection of the input circuit, the input terminal currents should not exceed 1 mA . Appropriate series connected limiting resistors should be used in circuits where greater current flows might exist, allowing the signal input voltage to be greater than the supply voltage without damaging the circuit.

## Output Circuit

The output of the CA3290 is the open collector of an n-p-n transistor, a feature providing flexibility in a broad range of comparator applications. An output ORing function can be implemented by parallel connection of the open collectors. An output pull-up resistor can be connected to a power supply having a voltage range within the rating of the particular CA3290 in use; the magnitude of this voltage may be set at a value which is independent of that applied to the $\mathrm{V}+$ terminal of the CA3290.

## Parasitic Oscillations

The ideal comparator has, among other features, ultra high input impedance, high gain, and wide bandwidth. These desirable characteristics may, however, produce parasitic
oscillations unless certain precautions are observed to minimize the stray capacitive coupling between the input and output terminals. Parasitic oscillations manifest themselves during the output voltage transition intervals as the comparator switches states. For high source impedances, stray capacitance can induce parasitic oscillations. The addition of a small amount ( 1 mV to 10 mV ) of positive feedback (hysteresis) produces a faster transition, thereby reducing the likelihood of parasitic oscillations. Furthermore, if the input signal is a pulse waveform, with relatively rapid rise and fall times, parasitic tendencies are reduced.

When dual comparators, like the CA3290, are packaged in an 8 lead configuration, the output terminal of each comparator is adjacent to an input terminal. The lead-to-lead capacitance is approximately 1 pF , which may be sufficient to cause undesirable feedback effects in certain applications. Circuit factors such as impedance levels, supply voltage, switching rate, etc., may increase the possibility of parasitic oscillations. To minimize this potential oscillatory condition, it is recommended that for source impedances greater than $1 \mathrm{k} \Omega$ a capacitor $(\geq 1 \mathrm{pF}-2 \mathrm{pF})$ be connected between the appropriate input terminal and the output terminal. (See Figure 1.)

If either comparator is unused, its input terminals should also be tied to either the V + or V - supply rail.

## Typical Applications

## Light Controlled One-Shot Timer

In Figure 5 one comparator $\left(\mathrm{A}_{1}\right)$ of the CA3290 is used to sense a change in photo diode current. The other comparator $\left(\mathrm{A}_{2}\right)$ is configured as a one-shot timer and is triggered by the output of $\mathrm{A}_{1}$. The output of the circuit will switch to a low state for approximately 60 seconds after the light source to the photo diode has been interrupted. The circuit operates at normal room lighting levels. The sensitivity of the circuit may be adjusted by changing the values of $R_{1}$ and $R_{2}$. The ratio of $R_{1}$ to $R_{2}$ should be
constant to insure constant reverse voltage bias on the photo diode.


FIGURE 5. LIGHT CONTROLLED ONE-SHOT TIMER

## Low-Frequency Multivibrator

In this application, one half of the CA3290 is used as a conventional multivibrator circuit. Because of the extremely high input impedance of this device, large values of timing resistor $\left(\mathrm{R}_{1}\right)$ may be used for long time delays with relatively small leakage timing capacitors. The second half of the CA3290 is used as an output buffer to insure that the multivibrator frequency will not be affected by output loading. $R_{P}$ is the parallel combination of the two $1 \mathrm{M} \Omega$ resistors connected between +15 V and GND.


FIGURE 6. LOW FREQUENCY MULTIVIBRATOR

## Window Comparator

Both halves of the CA3290 can be used in a high input impedance window comparator as shown in Figure 7. The LED will be turned "on" whenever the input signal is above
the lower limit $\left(\mathrm{V}_{\mathrm{L}}\right)$ but below the upper limit $\left(\mathrm{V}_{\mathrm{U}}\right)$, as determined by the $R_{1} / R_{2} / R_{3}$ resistor divider.


FIGURE 7. WINDOW COMPARATOR

## Typical Performance Curves



FIGURE 8. SUPPLY CURRENT vs SUPPLY VOLTAGE (BOTH AMPLIFIERS)


FIGURE 10. INPUT CURRENT vs INPUT COMMON MODE VOLTAGE


FIGURE 9. INPUT CURRENT vs INPUT COMMON MODE VOLTAGE


FIGURE 11. POSITIVE COMMON MODE INPUT VOLTAGE RANGE vs SUPPLY VOLTAGE

## Typical Performance Curves (Continued)



FIGURE 12. NEGATIVE COMMON MODE INPUT VOLTAGE RANGE vs SUPPLY VOLTAGE


FIGURE 13. INPUT CURRENT vs TEMPERATURE


FIGURE 14. OUTPUT SATURATION VOLTAGE vs OUTPUT SINK CURRENT

## Metallization Mask Layout



The photographs and dimensions of each chip represent a chip when it is part of the wafer. When the wafer is cut into chips, the cleavage angles are $57^{\circ}$ instead of $90^{\circ}$ with respect to the face of the chip. Therefore, the isolated chip is actually $7 \mathrm{mils}(0.17 \mathrm{~mm})$ larger in both dimensions.

Dimensions in parentheses are in millimeters and are derived from the basic inch dimensions as indicated. Grid graduations are in mils ( $10^{-3}$ inch)

NOTE: Numbers in pads are for 8 lead DIP and TO-5 Can and numbers outside of chip are for 14 lead DIP.

## Dual-In-Line Plastic Packages (PDIP)


-B-


NOTES:

1. Controlling Dimensions: $\operatorname{INCH}$. In case of conflict between English and Metric dimensions, the inch dimensions control.
2. Dimensioning and tolerancing per ANSI Y14.5M-1982.
3. Symbols are defined in the "MO Series Symbol List" in Section 2.2 of Publication No. 95.
4. Dimensions $A, A 1$ and $L$ are measured with the package seated in JEDEC seating plane gauge GS-3.
5. D, D1, and E1 dimensions do not include mold flash or protrusions. Mold flash or protrusions shall not exceed 0.010 inch ( 0.25 mm ).
6. $E$ and $e_{A}$ are measured with the leads constrained to be perpendicular to datum $-\mathrm{C}-$.
7. $e_{B}$ and $e_{C}$ are measured at the lead tips with the leads unconstrained. $e_{C}$ must be zero or greater.
8. B1 maximum dimensions do not include dambar protrusions. Dambar protrusions shall not exceed 0.010 inch ( 0.25 mm ).
9. $N$ is the maximum number of terminal positions.
10. Corner leads ( $1, \mathrm{~N}, \mathrm{~N} / 2$ and $\mathrm{N} / 2+1$ ) for E8.3, E16.3, E18.3, E28.3, E42.6 will have a B1 dimension of $0.030-0.045$ inch (0.76-1.14mm).

E8.3 (JEDEC MS-001-BA ISSUE D) 8 LEAD DUAL-IN-LINE PLASTIC PACKAGE

| SYMBOL | INCHES |  | MILLIMETERS |  | NOTES |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | MIN | MAX | MIN | MAX |  |
| A | - | 0.210 | - | 5.33 | 4 |
| A1 | 0.015 | - | 0.39 | - | 4 |
| A2 | 0.115 | 0.195 | 2.93 | 4.95 | - |
| B | 0.014 | 0.022 | 0.356 | 0.558 | - |
| B1 | 0.045 | 0.070 | 1.15 | 1.77 | 8,10 |
| C | 0.008 | 0.014 | 0.204 | 0.355 | - |
| D | 0.355 | 0.400 | 9.01 | 10.16 | 5 |
| D1 | 0.005 | - | 0.13 | - | 5 |
| E | 0.300 | 0.325 | 7.62 | 8.25 | 6 |
| E1 | 0.240 | 0.280 | 6.10 | 7.11 | 5 |
| e | 0.10 | SC | 2.5 | BSC | - |
| $\mathrm{e}_{\mathrm{A}}$ | 0.30 | SC | 7.6 | BSC | 6 |
| $\mathrm{e}_{\mathrm{B}}$ | - | 0.430 | - | 10.92 | 7 |
| L | 0.115 | 0.150 | 2.93 | 3.81 | 4 |
| N | 8 |  | 8 |  | 9 |

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