# MOTOROLA SEMICONDUCTOR TECHNICAL DATA

# MC3367

# LOW VOLTAGE FM NARROWBAND RECEIVER

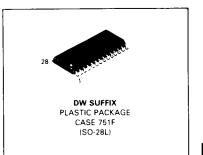
... with single conversion circuitry including oscillator, mixer, IF amplifiers, limiting IF circuitry, and quadrature discriminator. The MC3367 is perfect for narrowband audio and data applications up to 75 MHz which require extremely low power consumption. Battery powered applications down to  $V_{\rm CC}=1.1$  V are possible. The MC3367 also includes an on-board voltage regulator, low battery detection circuitry, a receiver enable allowing a power down "sleep mode," two undedicated buffer amplifiers to allow simultaneous audio and data reception, and a comparator for enhancing FSK (Frequency Shift Keyed) data reception to 1200 baud.

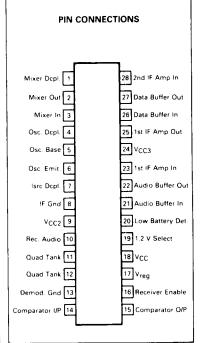
- Low Supply Voltage: VCC = 1.1 to 3.0 Vdc
- Low Power Consumption: PD = 1.5 to 5.0 mW
- Input Bandwidth 75 MHz
- Excellent Sensitivity: Input Limiting Voltage for 12 dB Sinad = 0.5 μVrms from Conjugated Matched Source
- Voltage Regulator Available (Source Capability 3.0 mA)
- Receiver Enable to Allow Active/Standby Operation
- Low Battery Detection Circuitry
- Self Biasing Audio Buffer with Nominal Gain Ay = 4.0
- Data Buffer with Nominal Gain Ay = 3.2
- FSK Data Shaping Comparator Included
- Standard 28-Lead Surface Mount (SOIC) Package

# FIGURE 1 — BLOCK DIAGRAM FIGURE 1 — BLOCK DIAGRAM Output Amp Output Pass Filter Voltage Regulator Reserver Enable Reference Data Buffer Audio Battery Demodulator Reference Regulator 10 Audio Battery Detector 19

# LOW VOLTAGE SINGLE CONVERSION FM RECEIVER

SILICON MONOLITHIC INTEGRATED CIRCUIT





MOTOROLA LINEAR/INTERFACE ICs DEVICE DATA

MAXIMUM RATINGS (Voltages with respect to Pins 8 and 13; T<sub>A</sub> = 25°C)

Rating	Pin	Value	Unit	
Supply Voltage	18	5.0	Vdc	
RF Input Signal	3	1.0	Vrms	
Audio Buffer Input	21	1.0	Vrms	
Data Buffer Input	26	1.0	Vrms	
Comparator Input	14	1.0	Vrms	
Junction Temperature		150	°C	
Storage Temperature		-65 to +150	°C	

Devices should not be operated at or outside these values. The "Recommended Operating Limits" provide for actual device operation.

# RECOMMENDED OPERATING CONDITIONS

Parameter	Pin	Value	Unit	
Supply Voltage	18	1.1 to 3.0	Vdc	
Receiver Enable Voltage	16	0 or VCC	Vdc	
1.2 V Select Voltage	19	Open or VCC	Vdc	
RF Input Signal Level	3	0.001 to 100	mVrms	
RF Input Frequency	3	0 to 75	MHz	
Intermediate Frequency (IF)	_	455	kHz	
Audio Buffer Input	21	0 to 75	mVrms	
Data Buffer Input	26	0 to 75	. mVrms	
Comparator Input	14	10 to 300	mVrms	
Ambient Temperature		0 to 70	°C	

**ELECTRICAL CHARACTERISTICS** ( $V_{CC}=1.3~V, f_0=10.7~MHz, f_{mod}=1.0~kHz, Deviation=3.0~kHz, T_A=25°C, Test Circuit of Figure 2 unless otherwise noted)$ 

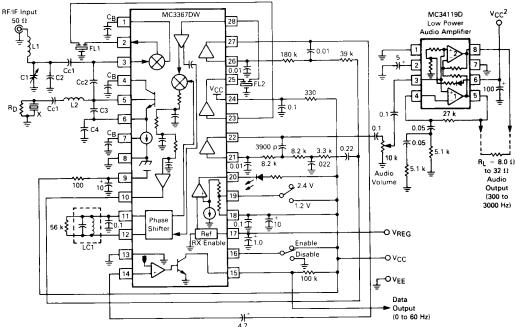
Characteristic	Pin	Min	Тур	Max	Units
OVERALL MC3367 PERFORMANCE			•		
Drain Current — Pin 15 = V <sub>CC</sub>	T		1.4	3.0	mA
— Pin 15 = 0 Vdc			0.5	l. –	μΑ
Recovered Audio (RF Input = 10 mV)	10	_	13	_	mVrms
Noise Output (RF Input = 0 mV)	10		4.5	_	mVrms
Input for -3.0 dB Limiting	3	_	0.2	_	μVrms
MIXER			+	•	
Mixer Input Resistance (Rp)	3	_	3.0	_	kΩ
Mixer Input Capacitance (Cp)	3	_	9.0	_	pF
FIRST IF AMPLIFIER		<u> </u>	•		
First IF Amp Voltage Gain	T -		25	T _	dB
AUDIO BUFFER				·	
Voltage Gain	<del>-</del>	_	4.0		V/V
Input Resistance	21	_	125	_	kΩ
Maximum Input for Undistorted Output	21	-	70	_	mVrms
Maximum Output Swing	22		800		mVpp
Output Resistance	22		680		Ω
DATA BUFFER			•		
Voltage Gain		T =	3.2	_	V/V
Input Resistance	26	_	8.0,		MΩ
Maximum Input for Undistorted Output (< 3% THD)	26	_	70	<u> </u>	mVrms
Maximum Output Swing	27	_	600	_	mVpp
Output Resistance	27	† · · · -	1.5	_	kΩ

(continued)

**ELECTRICAL CHARACTERISTICS** — continued ( $V_{CC}=1.3\ V$ ,  $f_0=10.7\ MHz$ ,  $f_{mod}=1.0\ kHz$ , Deviation = 3.0 kHz,  $T_{A}=25^{\circ}C$ , Test Circuit of Figure 2 unless otherwise noted)

Characteristic	Pin	Min	Тур	Max	Units
OMPARATOR					
Minimum Input for Triggering	14	_	7.0		mVrms
Maximum Input Frequency (R <sub>L</sub> = 100 kΩ)	14		25		kHZ
Rise Time (10–90%; $R_L = 100 \text{ k}\Omega$ )	15	_	5.0		μs
Fall Time (90–10%; $R_L = 100 \text{ k}\Omega$ )	15	_	0.4		μs
OW BATTERY DETECTOR		_			
Low Battery Trip Point	18	_	1.09		Vdc
Low Battery Output — V <sub>CC</sub> = 0.9 V — V <sub>CC</sub> = 1.3 V	20 20		0.2 VCC		Vdc Vdc
OLTAGE REGULATOR					
Regulated Output (see Figure 6)	17		0.95		Vdc
Source Capability	17	_	_	3.0	mA

# FIGURE 2 — EVALUATION CIRCUIT



- NO IES:

  1. FL1 and FL2 are 455 kHz ceramic bandpass filters, which should have input and output impedances of 1.5 kΩ to 2.0 kΩ. Suggested part numbers are muRata CFU455X or CFW455X the "X" suffix denotes
- numbers are muRata CFU45SX or CFW45SX the "X" suffix denotes bandwidth.

  2. LC1 is a 455 kHz resonator. Recommended part number are Toko America 7M8128Z. The evaluation board layout shown provides for use of either resonator. Ceramic discriminator elements cannot be used with the MC3367 due to their low input Impedance. The damping resistor value can be raised to increase the recovered audio or lowered to increase the quadrature detector's bandwidth and timesrity—practical limits are proroximately 27 Kg to 75 KZ. Typically linearity — practical limits are approximately 27 k $\Omega$  to 75 k $\Omega$ . Typically the quadrature detector's bandwidth should match the low IF filter's
- the quadrature elected is provided by a substantial that a corner frequency of approximately 200 Hz. The audio buffer is a bandpass filter with corner frequencies of 300 Hz and 3.0 kHz. The audio amplifier provides bass suppression.
- 4. Cc1 and Cc3 are RF coupling capacitors and should have  $\leq 20~\Omega$  impedance at the desired input and oscillator frequencies. 5. Cc2 provides "light coupling" of the oscillator signal into the mixer, and should have a  $\simeq 3.0~k\Omega$  to  $5.0~k\Omega$  impedance at the desired local
- and should have a  $\approx 3.0 \, \mathrm{k}\Omega$  to  $5.0 \, \mathrm{k}\Omega$  impedance at the desired local oscillator frequency. 6. Capacitors labelled CB are bypass capacitors and should have  $\leqslant 20 \, \Omega$  impedance at the desired RF and local oscillator frequencies. 7. The network of L1, C1 and C2 provides impedance matching of the mixer input (nominally  $3.0 \, \mathrm{k}\Omega$  shunted by  $9.0 \, \mathrm{pF}$ ) to  $50 \, \Omega$  at the desired RFIF input frequency. This will allow for bench testing of the receiver from typical RF signal generators or radio service monitors, but additional or different matching will be required to maximize receiver sensitivity when used in conjunction with an antenna, RF preamplifier or mixer.

# FIGURE 3 — RECOVERED AUDIO versus SUPPLY

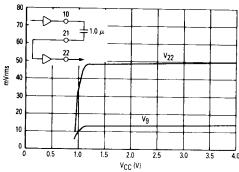


FIGURE 4 — DRAIN versus SUPPLY

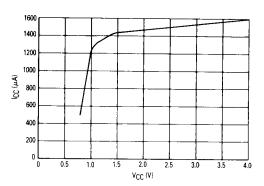


FIGURE 5 — S+N, N versus INPUT

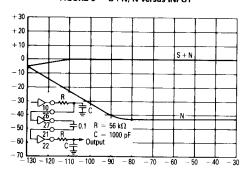


FIGURE 6 — VREG versus SUPPLY

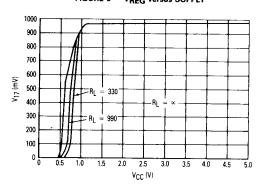


FIGURE 7 — REGULATED OUTPUT AND RECOVERED AUDIO

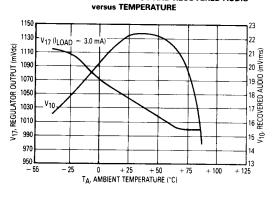
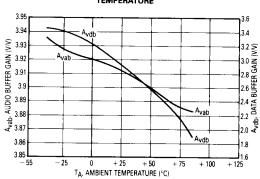


FIGURE 8 — BUFFER AMPLIFIER GAINS versus TEMPERATURE



MOTOROLA LINEAR/INTERFACE ICs DEVICE DATA

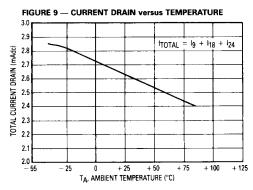
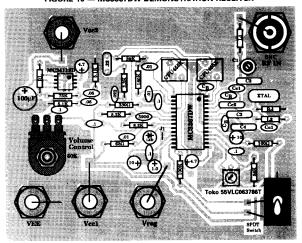


FIGURE 10 — MC3367DW DEMONSTRATION RECEIVER



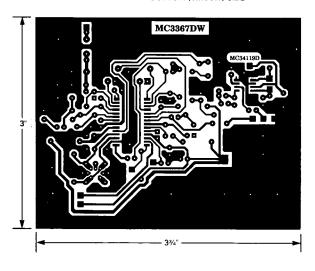


Alternate input circuit for 72 MHz receiver.

In. Freq.	L1	L2	C1	C2	СЗ	C4	Cc1	Cc2	CB	RD
10.7 MHz	6.8 µH	Short	2-82 pF	10 pF	120 pF	50 pF	1.0 k pF	5.0 pF	0.1 μF	Open
45 MHz	0.68 μH	1.2 μH	5-25 pF	Open	30 pF	5.0 pF	1.0 k pF	1.0 pF	1.0 k pF	1.0 k
72 MHz	0.22 μΗ	0.22 μΗ	5-25 pF	Open	18 pF	3.0 pF	470 pF	1.0 pF	470 pF	1.0 k

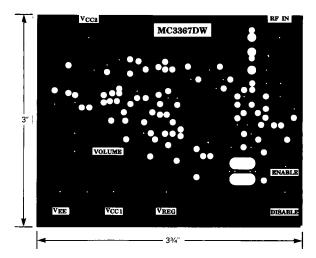
Volume Control: CRL B12503SL
VCC1: 1.1 V to 3.0 V
VCc2: 2.0 V to 16 V
Speaker: 8.0 IX to 32 IX
J1: Jumper — install for 1.2 V operation. Leave open for 2.4 V operation.
ICs mount on circuit side (back) of PC board.
C3, C4 must be 5% silver mica

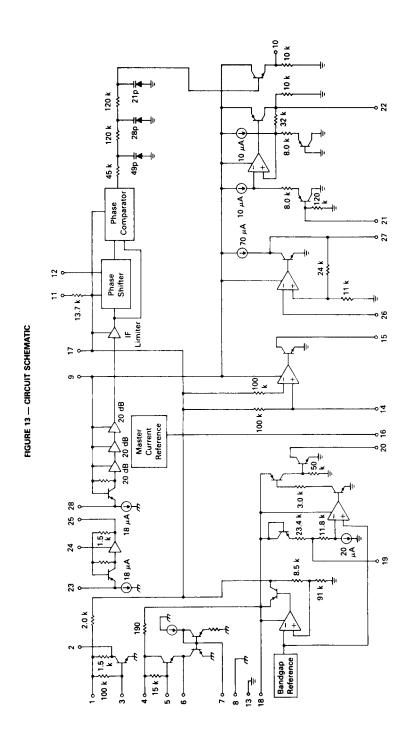
FIGURE 11 - BOTTOM (CIRCUIT) SIDE



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FIGURE 12 --- TOP (COMPONENT/GROUND PLANE) SIDE





## CIRCUIT DESCRIPTION

The MC3367 is an FM narrowband receiver capable of operation to 75 MHz. The low voltage design yields low power drain and excellent sensitivity in narrowband voice and data link applications. In the typical application the mixer amplifies the incoming RF or IF signal and converts this frequency to 455 kHz. The signal is then filtered by a 455 kHz ceramic filter and applied to the first intermediate frequency (IF) amplifier input, before passing through a second ceramic filter. The modulated IF signal is then applied to the limiting IF amplifier and detector circuitry. Modulation is recovered by a conventional quadrature detector. The typical modulation bandwidth available is 3.0 to 5.0 kHz.

Features available include buffers for audio/data amplification and active filtering, on board voltage regulator, low battery detection circuitry with programmable level, and receiver disable circuitry. The MC3367 is an FM utility receiver to be used for voice and/or narrowband data reception. It is especially suitable where extremely low power consumption and high design flexibility are required.

# **APPLICATION**

The MC3367 can be used as a high performance FM IF for use in low power dual conversion receivers. Because of the MC3367's extremely good sensitivity (0.6  $\mu V$  for 20 dB (S+N)/N, see Figure 5), it can also be used as a stand alone single conversion narrow-band receiver to 75 MHz for applications not sensitive to image frequency interference. An RF preamplifier will likely be needed to overcome preselector losses.

The oscillator is a Colpitts type which must be run under crystal control. For fundamental mode crystals choose resonators, parallel resonant, for a 32 pF load. For higher frequencies, use a 3rd overtone series mode type. The coil (L2) and RD resistor are needed to ensure proper operation.

The best adjacent channel and sensitivity response occur when two 455 kHz ceramic filters are used, as shown in Figure 2. Either can be replaced by a 0.1  $\mu$ F coupling capacitor to reduce cost, but some degradation in sensitivity and/or stability is suspected

The detector is a quadrature type, with the connection from the limiter output to the detector input provided internally as with the MC3359 and the MC3361. A 455 kHz LC tank circuit must be provided externally. One of the tank pins (Pin 11) must be decoupled using a 0.1  $\mu F$  capacitor. The 56 k $\Omega$  damping resistor (see Figure 2), determines the peak separation of the detector (and thus its bandwidth). Smaller values will increase the separation and bandwidth but decrease recovered audio and sensitivity.

The data buffer is a noninverting amplifier with a nominal voltage gain of 3.2 V/V. This buffer needs its dc bias (approx. 250 mV) provided externally or else debiasing will occur. A single-pole RC filter, as shown in Figure 5, connecting the recovered audio output to the data buffer input provides the necessary dc bias and some post detection filtering. The buffer can also be used as an active filter.

The audio buffer is a noninverting amplifier with a nominal voltage gain of 4.0 V/V. This buffer is self-biasing so its input should be ac coupled. The two buffers, when applied as active filters, can be used together to allow simultaneous audio and very low speed data reception. Another possible configuration is to receive audio only and include a noise-triggered squelch.

The comparator is a noninverting type with an open collector output. Typically, the pull-up resistor used between Pin 15 and VCC is 100 k $\Omega$ . With R $_L=100~k\Omega$  the comparator is capable of operation up to 25 kHz. This circuit is self-biasing, so its input should be ac coupled.

The regulator is a 0.95 V reference capable of sourcing 3.0 mA. This pin (Pin 17) needs to be decoupled using a 1.0–10  $\mu$ F capacitor to maintain stability of the MC3367

All three V<sub>CCs</sub> on the MC3367 (V<sub>CC</sub>, V<sub>CC2</sub>, V<sub>CC3</sub>) run on the same supply voltage. V<sub>CC</sub> is typically decoupled using capacitors only. V<sub>CC2</sub> and V<sub>CC3</sub> should be bypassed using the RC bypasses shown in Figure 2. Eliminating the resistors on the V<sub>CC2</sub> and V<sub>CC3</sub> bypasses may be possible in some applications, but a reduction in sensitivity and quieting will likely occur.

The low battery detection circuit gives an NPN open collector output at Pin 20 which drops low when the MC3367 supply voltage drops below 1.1 V. Typically it would be pulled up via a 100 k $\Omega$  resistor to supply.

The 1.2 V Select pin, when connected to the MC3367 supply, programs the low battery detector to trip at V<sub>CC</sub> < 1.1 V. Leaving this pin open raises the trip voltage on the low battery detector.

Pin 16 is a receiver enable which is connected to VCC for normal operation. Connecting this pin to ground shuts off receiver and reduces current drain to ICC  $\leq$  0.5  $\mu A_{\odot}$ 

# **APPENDIX**

Design of 2nd Order Sallen-Key Low Pass Filters

The audio and data buffers can easily be configured as active low pass filters using the circuit configuration shown above. The circuit has a center frequency ( $f_0$ ) and quality factor (Q) given by the following:

$$G_{0} = \frac{1}{2\pi \sqrt{R1R2C1C2}}$$
 
$$Q = \frac{1}{\sqrt{\frac{R2C2}{R1C1} + \sqrt{\frac{R1C2}{R2C1} + (1 - K)} \sqrt{\frac{R1C1}{R2C2}}}$$

If possible, let R1 = R2 or C1 = C2 to simplify the above equations. Be sure to avoid a negative Q value to prevent instability. Setting Q =  $1/\sqrt{2}$  = 0.707 yields a maximally flat filter response.

Data Buffer Design

$$f_0 = 200 \text{ Hz}$$
  
C1 = C2 = 0.01  $\mu$ F

The data buffer is designed as follows:  $f_0 = 200 \text{ Hz}$   $C1 = C2 = 0.01 \ \mu\text{F}$  Q = 0.707 (target) K = 3.2 (data buffer open loop voltage gain)

Setting C1 = C2 yields:

$$f_{O} = \frac{1}{2\pi C1\sqrt{R1R2}}$$

$$Q = \frac{1}{\sqrt{\frac{R2}{R1} + (2 - K)} \sqrt{\frac{R1}{R2}}}$$

Iteration yields R2 = 4.2 (R1) to make Q = 0.707. Substitution into the equation for fo yields:

$$R2 = 4.2 (R1) = 180 kg$$

$$C1 = C2 = 0.01 \mu F$$

Audio Buffer Design

The audio buffer is designed as follows:

$$R1 = R2 = 8.2 \text{ k}\Omega$$

$$Q = 0.707 \text{ (target)}$$

 $\begin{array}{c} f_0 = 3000 \text{ Hz} \\ \text{R1} = \text{R2} = 8.2 \text{ k}\Omega \\ \text{Q} = 0.707 \text{ (target)} \\ \text{K} = 4.0 \text{ (audio buffer open loop voltage gain)} \end{array}$ 

Setting R1 = R2 yields:

$$f_O = \frac{1}{2\pi R1\sqrt{C1C2}}$$

Setting HY = H2 yields.  

$$f_{O} = \frac{1}{2\pi R1\sqrt{C1C2}}$$

$$O = \frac{1}{2\sqrt{\frac{C2}{C1}} + (1 - K)\sqrt{\frac{C1}{C2}}}$$

Iteration yields C2 = 2.65 (C1) to make Q = 0.707. Substitution into the equation for  $f_0$  yields: C1 = 3900 pF C2 = 2.65 (C1) = 0.01  $\mu$ F R1 = R2 = 8.2 k $\Omega$ 

$$C1 = 3900 \text{ pF}$$
  
 $C2 = 2.65 (C1) = 0.01 \mu$ 

$$C2 = 2.65 (C1) = 0.01 \mu$$

$$R1 = R2 = 8.2 \text{ k}\Omega$$