LT1995

## feATURES

- Internal Gain Setting Resistors
- Pin Configurable as a Difference Amplifier, Inverting and Noninverting Amplifier
- Difference Amplifier:

Gain Range 1 to 7
CMRR > 65dB

- Noninverting Amplifier: Gain Range 1 to 8
- Inverting Amplifier:

Gain Range -1 to -7

- Gain Error: <0.2\%
- Slew Rate: $1000 \mathrm{~V} / \mathrm{\mu s}$
- Bandwidth: 32 MHz (Gain = 1)
- Op Amp Input Offset Voltage: 2.5mV Max
- Quiescent Current: 9mA Max
- Wide Supply Range: $\pm 2.5 \mathrm{~V}$ to $\pm 15 \mathrm{~V}$
- Available in 10-Lead MSOP and 10-Lead ( $3 \mathrm{~mm} \times 3 \mathrm{~mm}$ ) DFN Packages


## APPLICATIONS

- Instrumentation Amplifier
- Current Sense Amplifier
- Video Difference Amplifier
- Automatic Test Equipment


## DESCRIPTIOn

The $\mathrm{LT}^{\circledR} 1995$ is a high speed, high slew rate, gain selectable amplifier with excellent DC performance. Gains from -7 to 8 with a gain accuracy of $0.2 \%$ can be achieved using no external components. The device is particularly well suited for use as a difference amplifier, where the excellent resistor matching results in a typical common mode rejection ratio of 79 dB .
The amplifier is a single gain stage design similar to the LT1363 and features superb slewing and settling characteristics. Input offset of the internal operational amplifier is less than 2.5 mV and the slew rate is $1000 \mathrm{~V} / \mathrm{\mu s}$. The output can drive a $150 \Omega$ load to $\pm 2.5 \mathrm{~V}$ on $\pm 5 \mathrm{~V}$ supplies, making it useful in cable driver applications.

The resistors have excellent matching, $0.2 \%$ maximum at room temperature and $0.3 \%$ from $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$. The temperature coefficient of the resistors is typically $-30 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$. The resistors are extremely linear with voltage, resulting in a gain nonlinearity of 10ppm.

The LT1995 is fully specified at $\pm 2.5 \mathrm{~V}, \pm 5 \mathrm{~V}$ and $\pm 15 \mathrm{~V}$ supplies and from $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$. The device is available in space saving 10-lead MSOP and 10-Lead ( $3 \mathrm{~mm} \times 3 \mathrm{~mm}$ ) DFN packages. For a micropower precision amplifier with precision resistors, see the LT1991 and LT1996.

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## TYPICAL APPLICATION

High Slew Rate Differential Gain of 1


Large-Signal Transient ( $G=1$ )


## ABSOLUTE MAXIMUM RATINGS <br> (Note 1)


Storage Temperature Range
MS Package
DD Package ................................... $-65^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$
Maximum Junction Temperature...... $65^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$
MS Package ............................................. $150^{\circ} \mathrm{C}$
DD Package e................................ $125^{\circ} \mathrm{C}$
Lead Temperature (Soldering, 10 sec).............. $300^{\circ} \mathrm{C}$

PACKAGE/ORDER INFORMATION

| DD PACKAGE <br> 10-LEAD $(3 \mathrm{~mm} \times 3 \mathrm{~mm})$ PLASTIC DFN <br> $\mathrm{T}_{\mathrm{JMAX}}=125^{\circ} \mathrm{C}, \theta_{\mathrm{JA}}=160^{\circ} \mathrm{C} / \mathrm{W}$ (NOTE 6) EXPOSED PAD INTERNALLY CONNECTED TO V $_{s}{ }^{-}$ PCB CONNECTION OPTIONAL | ORDER PART NUMBER |  | ORDER PART NUMBER |
| :---: | :---: | :---: | :---: |
|  | LT1995CDD |  | LT1995CMS |
|  | LT1995IDD |  | LT1995IMS |
|  | DD PART MARKING* |  | MS PART MARKING* |
|  | $\begin{aligned} & \text { LBJF } \\ & \text { LBJF } \end{aligned}$ |  | $\begin{aligned} & \text { LTBJD } \\ & \text { LTBJD } \end{aligned}$ |

Order Options Tape and Reel: Add \#TR
Lead Free: Add \#PBF Lead Free Tape and Reel: Add \#TRPBF
Lead Free Part Marking: http://www.linear.com/leadfree/
Consult LTC Marketing for parts specified with wider operating temperature ranges. *The temperature grades are identified by a label on the shipping container.

## eLeCTRICAL CHARACTERISTICS

Difference Amplifier Configuration. $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{REF}}=\mathrm{V}_{\mathrm{CM}}=\mathrm{OV}$ and unused gain pins are unconnected, unless otherwise noted.

| SYMBOL | PARAMETER | CONDITIONS | $V_{\text {SUPPLY }}$ | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| GE | Gain Error | $\mathrm{V}_{\text {OUT }}= \pm 12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=1 \mathrm{k}, \mathrm{G}=1$ | $\pm 15 \mathrm{~V}$ |  | 0.05 | 0.2 | \% |
|  |  | $\mathrm{V}_{\text {OUT }}= \pm 12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=1 \mathrm{k}, \mathrm{G}=2$ | $\pm 15 \mathrm{~V}$ |  | 0.05 | 0.2 | \% |
|  |  | $V_{\text {OUT }}= \pm 12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=1 \mathrm{k}, \mathrm{G}=4$ | $\pm 15 \mathrm{~V}$ |  | 0.05 | 0.2 | \% |
|  |  | $V_{\text {OUT }}= \pm 5 V, R_{L}=150 \Omega, G=1$ | $\pm 15 \mathrm{~V}$ |  | 0.05 | 0.25 | \% |
|  |  | $V_{\text {OUT }}= \pm 2.5 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=500 \Omega, \mathrm{G}=1$ | $\pm 5 \mathrm{~V}$ |  | 0.05 | 0.2 | \% |
|  |  | $V_{\text {OUT }}= \pm 2.5 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=150 \Omega, \mathrm{G}=1$ | $\pm 5 \mathrm{~V}$ |  | 0.05 | 0.25 | \% |
| GNL | Gain Nonlinearity | $\mathrm{V}_{\text {OUT }}= \pm 12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=1 \mathrm{k}, \mathrm{G}=1$ | $\pm 15 \mathrm{~V}$ |  | 10 |  | ppm |
| $\mathrm{V}_{\text {OS }}$ | Input Offset Voltage Referred to Input (Note 7) | $\mathrm{G}=1$ (MS10) | $\pm 15 \mathrm{~V}$ |  | 1 | 5 | mV |
|  |  | $G=1$ (DD10) | $\pm 15 \mathrm{~V}$ |  | 1.5 | 9 | mV |
|  |  | $\mathrm{G}=2$ (MS10) | $\pm 15 \mathrm{~V}$ |  | 0.7 | 4 | mV |
|  |  | $G=2($ D10 $)$ | $\pm 15 \mathrm{~V}$ |  | 1.2 | 6.8 | mV |
|  |  | $\mathrm{G}=4$ (MS10) | $\pm 15 \mathrm{~V}$ |  | 0.6 | 3.75 | mV |
|  |  | $\mathrm{G}=4$ (DD10) | $\pm 15 \mathrm{~V}$ |  | 0.9 | 5.6 | mV |
|  |  | $G=1(\mathrm{MS10})$ | $\pm 5 \mathrm{~V}$ |  | 1 | 5 | mV |
|  |  | $G=1$ (DD10) | $\pm 5 \mathrm{~V}$ |  | 1.4 | 9 | mV |
|  |  | $G=1 \text { (MS10) }$ | $\pm 2.5 \mathrm{~V}$ |  | $1$ | 5 | mV |
|  |  | $\mathrm{G}=1$ (DD10) | $\pm 2.5 \mathrm{~V}$ |  | 1.3 | 9 | mV |
|  |  |  |  |  |  |  | 1995fb |
| $?$ |  |  |  |  |  |  | AD |

## ELECTRICAL CHARACTERISTICS

Difference Amplifier Configuration. $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{REF}}=\mathrm{V}_{\mathrm{CM}}=\mathrm{OV}$ and unused gain pins are unconnected, unless otherwise noted.

| SYMBOL | PARAMETER | CONDITIONS | V SUPPLY | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V OS_OA | Op Amp Input Offset Voltage (Note 10) | $\begin{aligned} & G=1 \text { (MS10) } \\ & G=1 \text { (DD10) } \end{aligned}$ | $\begin{aligned} & \pm 2.5 \mathrm{~V}, \pm 5 \mathrm{~V}, \pm 15 \mathrm{~V} \\ & \pm 2.5 \mathrm{~V}, \pm 5 \mathrm{~V}, \pm 15 \mathrm{~V} \end{aligned}$ |  | $\begin{gathered} \hline 0.5 \\ 0.75 \end{gathered}$ | $\begin{aligned} & 2.5 \\ & 4.5 \end{aligned}$ | $\begin{aligned} & \mathrm{mV} \\ & \mathrm{mV} \end{aligned}$ |
| $\mathrm{e}_{\mathrm{n}}$ | Input Noise Voltage | $\begin{aligned} & G=1, f=10 \mathrm{kHz} \\ & G=2, f=10 \mathrm{kHz} \\ & G=4, f=10 \mathrm{kHz} \end{aligned}$ | $\begin{aligned} & \pm 2.5 \mathrm{~V} \text { to } \pm 15 \mathrm{~V} \\ & \pm 2.5 \mathrm{~V} \text { to } \pm 15 \mathrm{~V} \\ & \pm 2.5 \mathrm{~V} \text { to } \pm 15 \mathrm{~V} \end{aligned}$ |  | $\begin{aligned} & 27 \\ & 18 \\ & 14 \end{aligned}$ |  | $\mathrm{nV} / \sqrt{\mathrm{Hz}}$ $\mathrm{nV} / \sqrt{\mathrm{Hz}}$ $\mathrm{nV} / \sqrt{\mathrm{Hz}}$ |
| $\underline{\text { R }}$ N | Common Mode Input Resistance | $V_{C M}= \pm 15 \mathrm{~V}, \mathrm{G}=1$ | $\pm 15 \mathrm{~V}$ |  | 4 |  | $\mathrm{k} \Omega$ |
| $\mathrm{C}_{\text {IN }}$ | Input Capacitance |  | $\pm 15 \mathrm{~V}$ |  | 2.5 |  | pF |
|  | Input Voltage Range | $G=1$ | $\begin{aligned} & \pm 15 \mathrm{~V} \\ & \pm 5 \mathrm{~V} \\ & \pm 2.5 \mathrm{~V} \end{aligned}$ | $\begin{gathered} \pm 15 \\ \pm 5 \\ \pm 1 \end{gathered}$ | $\begin{gathered} \pm 15.5 \\ \pm 5.5 \\ \pm 1.5 \end{gathered}$ |  | V V V |
| CMRR | Common Mode Rejection Ratio Referred to Input | $\begin{aligned} & \mathrm{G}=1, \mathrm{~V}_{\mathrm{CM}}= \pm 15 \mathrm{~V} \\ & \mathrm{G}=2, \mathrm{~V}_{\mathrm{CM}}= \pm 15 \mathrm{~V} \\ & \mathrm{G}=4, \mathrm{~V}_{\mathrm{CM}}= \pm 15 \mathrm{~V} \\ & \mathrm{G}=1, \mathrm{~V}_{\mathrm{CM}}= \pm 5 \mathrm{~V} \\ & \mathrm{G}=1, \mathrm{~V}_{\mathrm{CM}}= \pm 1 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & \pm 15 \mathrm{~V} \\ & \pm 15 \mathrm{~V} \\ & \pm 15 \mathrm{~V} \\ & \pm 5 \mathrm{~V} \\ & \pm 2.5 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 65 \\ & 71 \\ & 75 \\ & 65 \\ & 61 \end{aligned}$ | $\begin{aligned} & 79 \\ & 84 \\ & 87 \\ & 73 \\ & 68 \end{aligned}$ |  | dB dB dB dB dB |
| PSRR | Power Supply Rejection Ratio | $\mathrm{P} 1=\mathrm{M} 1=0 \mathrm{~V}, \mathrm{G}=1, \mathrm{~V}_{S}= \pm 2.5 \mathrm{~V}$ to $\pm 15 \mathrm{~V}$ |  | 78 | 87 |  | dB |
| V OUT | Output Voltage Swing | $\begin{aligned} & \mathrm{R}_{\mathrm{L}}=1 \mathrm{k} \\ & \mathrm{R}_{\mathrm{L}}=500 \Omega \\ & \mathrm{R}_{\mathrm{L}}=500 \Omega \\ & \mathrm{R}_{\mathrm{L}}=500 \Omega \end{aligned}$ | $\begin{aligned} & \pm 15 \mathrm{~V} \\ & \pm 15 \mathrm{~V} \\ & \pm 5 \mathrm{~V} \\ & \pm 2.5 \mathrm{~V} \end{aligned}$ | $\begin{gathered} \pm 13.5 \\ \pm 13 \\ \pm 3.5 \\ \pm 1.3 \end{gathered}$ | $\begin{gathered} \pm 14 \\ \pm 13.5 \\ \pm 4 \\ \pm 2 \end{gathered}$ |  | V V V V |
| ISC | Short-Circuit Current | $\mathrm{G}=1$ | $\pm 15 \mathrm{~V}$ | $\pm 70$ | $\pm 120$ |  | mA |
| SR | Slew Rate | $\begin{aligned} & \mathrm{G}=-2, \mathrm{~V}_{\text {OUT }}= \pm 12 \mathrm{~V}, \mathrm{P} 2=0 \mathrm{~V} \\ & \text { Measured at } \mathrm{V}_{\text {OUT }}= \pm 10 \mathrm{~V} \\ & \mathrm{G}=-2, \mathrm{~V}_{\text {OUT }}= \pm 3.5 \mathrm{~V}, \mathrm{P} 2=0 \mathrm{~V} \\ & \text { Measured at } \mathrm{V}_{\text {OUT }}= \pm 2 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & \pm 15 \mathrm{~V} \\ & \pm 5 \mathrm{~V} \end{aligned}$ | $750$ | $\begin{aligned} & 1000 \\ & 450 \end{aligned}$ |  | V/ $\mu \mathrm{S}$ <br> $\mathrm{V} / \mathrm{\mu s}$ |
| FPBW | Full Power Bandwidth | 10V Peak, G = -2 (Note 8) 3V Peak, G = -2 (Note 8) | $\begin{aligned} & \pm 15 \mathrm{~V} \\ & \pm 5 \mathrm{~V} \end{aligned}$ |  | $\begin{aligned} & 16 \\ & 24 \end{aligned}$ |  | $\begin{aligned} & \mathrm{MHz} \\ & \mathrm{MHz} \end{aligned}$ |
| HD | Total Harmonic Distortion | $G=1, f=1 \mathrm{MHz}, \mathrm{R}_{\mathrm{L}}=1 \mathrm{k}, \mathrm{V}_{\text {OUT }}=2 \mathrm{~V}_{\text {P-P }}$ | $\pm 15 \mathrm{~V}$ |  | -81 |  | dB |
|  | -3dB Bandwidth | $\mathrm{G}=1$ | $\begin{aligned} & \pm 15 \mathrm{~V} \\ & \pm 5 \mathrm{~V} \\ & \pm 2.5 \mathrm{~V} \end{aligned}$ |  | $\begin{aligned} & 32 \\ & 25 \\ & 21 \end{aligned}$ |  | MHz <br> MHz <br> MHz |
| $\mathrm{tr}_{\mathrm{r}}, \mathrm{t}_{\mathrm{f}}$ | Rise Time, Fall Time | $10 \%$ to $90 \%, 0.1 \mathrm{~V}, \mathrm{G}=1$ | $\begin{array}{\|l} \hline \pm 15 \mathrm{~V} \\ \pm 5 \mathrm{~V} \\ \hline \end{array}$ |  | $\begin{aligned} & 10 \\ & 15 \\ & \hline \end{aligned}$ |  | ns ns |
| OS | Overshoot | $0.1 \mathrm{~V}, \mathrm{G}=1, \mathrm{C}_{L}=10 \mathrm{pF}$ | $\begin{aligned} & \pm 15 \mathrm{~V} \\ & \pm 5 \mathrm{~V} \end{aligned}$ |  | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ |  | \% |
| $t_{\text {pd }}$ | Propagation Delay | $50 \% \mathrm{~V}_{\text {IN }}$ to $50 \% \mathrm{~V}_{\text {OUT }}, 0.1 \mathrm{~V}, \mathrm{G}=1$ | $\begin{array}{\|l} \hline \pm 15 \mathrm{~V} \\ \pm 5 \mathrm{~V} \\ \hline \end{array}$ |  | $\begin{gathered} \hline 9 \\ 11 \\ \hline \end{gathered}$ |  | ns ns |
| $\mathrm{t}_{\text {s }}$ | Settling Time | 10 V Step, $0.1 \%, \mathrm{G}=1$ <br> 5V Step, $0.1 \%$, G = 1 | $\begin{aligned} & \pm 15 \mathrm{~V} \\ & \pm 5 \mathrm{~V} \end{aligned}$ |  | $\begin{aligned} & 100 \\ & 110 \end{aligned}$ |  | ns |
| $\Delta \mathrm{G}$ | Differential Gain | $\mathrm{G}=2, \mathrm{R}_{\mathrm{L}}=150 \Omega$ | $\pm 15 \mathrm{~V}$ |  | 0.06 |  | \% |
| $\Delta \theta$ | Differential Phase | $G=2, R_{L}=150 \Omega$ | $\pm 15 \mathrm{~V}$ |  | 0.15 |  | Deg |
| R OUT | Output Resistance | $f=1 \mathrm{MHz}, \mathrm{G}=1$ | $\pm 15 \mathrm{~V}$ |  | 1.5 |  | $\Omega$ |
| IS | Supply Current | $\mathrm{G}=1$ | $\begin{aligned} & \pm 15 \mathrm{~V} \\ & \pm 5 \mathrm{~V} \end{aligned}$ |  | $\begin{aligned} & 7.1 \\ & 6.7 \end{aligned}$ | $\begin{aligned} & 9.0 \\ & 8.5 \end{aligned}$ | mA |

ELECRRCRL CHARFCTERASTCS The o denotes the specifications which apply over the $0^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq 70^{\circ} \mathrm{C}$. Difference Amplifier Configuration. $\mathrm{V}_{\mathrm{REF}}=\mathrm{V}_{\mathrm{CM}}=\mathrm{OV}$ and unused gain pins are unconnected, unless otherwise noted.

| SYMBOL | PARAMETER | CONDITIONS | V SUPPLY |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| GE | Gain Error | $\begin{aligned} & V_{\text {OUT }}= \pm 12 \mathrm{~V}, R_{L}=1 \mathrm{k}, \mathrm{G}=1 \\ & \mathrm{~V}_{\text {OUT }}= \pm 12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=1 \mathrm{k}, \mathrm{G}=2 \\ & \mathrm{~V}_{\text {OUT }}= \pm 12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=1 \mathrm{k}, \mathrm{G}=4 \\ & \mathrm{~V}_{\text {OUT }}= \pm 2.5 \mathrm{~V}, R_{\mathrm{L}}=500 \Omega, G=1 \\ & \mathrm{~V}_{\text {OUT }}= \pm 2.5 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=150 \Omega, G=1 \\ & \hline \end{aligned}$ | $\begin{array}{\|l}  \pm 15 \mathrm{~V} \\ \pm 15 \mathrm{~V} \\ \pm 15 \mathrm{~V} \\ \pm 5 \mathrm{~V} \\ \pm 5 \mathrm{~V} \\ \hline \end{array}$ | $\stackrel{\bullet}{\bullet}$ |  | $\begin{aligned} & 0.05 \\ & 0.05 \\ & 0.05 \\ & 0.05 \\ & 0.05 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.25 \\ & 0.25 \\ & 0.25 \\ & 0.25 \\ & 0.35 \\ & \hline \end{aligned}$ | $\begin{aligned} & \% \\ & \% \\ & \% \\ & \% \\ & \% \\ & \% \\ & \hline \end{aligned}$ |
| $\mathrm{V}_{0 S}$ | Input Offset Voltage Referred to Input (Note 7) | $\begin{aligned} & G=1(\text { MS10 }) \\ & G=1(\text { DD10 }) \\ & G=2(\text { MS10 }) \\ & G=2(\text { DD10 }) \\ & G=4(\text { MS10 }) \\ & G=4(\text { DD10 }) \\ & G=1(\text { MS10 }) \\ & G=1(\text { DD10 }) \\ & G=1(\text { MS10 }) \\ & G=1(\text { DD10 }) \end{aligned}$ | $\begin{aligned} & \pm 15 \mathrm{~V} \\ & \pm 15 \mathrm{~V} \\ & \pm 15 \mathrm{~V} \\ & \pm 15 \mathrm{~V} \\ & \pm 15 \mathrm{~V} \\ & \pm 15 \mathrm{~V} \\ & \pm 5 \mathrm{~V} \\ & \pm 5 \mathrm{~V} \\ & \pm 2.5 \mathrm{~V} \\ & \pm 2.5 \mathrm{~V} \end{aligned}$ | $\square$ |  | $\begin{gathered} \hline 1.1 \\ 1.5 \\ 0.8 \\ 1.2 \\ 0.7 \\ 0.9 \\ 1 \\ 1.4 \\ 1 \\ 1.3 \end{gathered}$ | $\begin{gathered} \hline 6.5 \\ 11.5 \\ 5.5 \\ 9 \\ 5 \\ 7.5 \\ 6.5 \\ 11.5 \\ 6.5 \\ 11.5 \end{gathered}$ | mV <br> mV <br> mV <br> mV <br> mV <br> mV <br> mV <br> mV <br> mV <br> mV |
| $\mathrm{V}_{\text {OS }}$ TC | Input Offset Voltage Drift Referred to Input (Note 9) | $\begin{aligned} & G=1 \text { (MS10) } \\ & G=1 \text { (DD10) } \end{aligned}$ | $\begin{aligned} & \pm 15 \mathrm{~V} \\ & \pm 15 \mathrm{~V} \end{aligned}$ | $\bullet$ |  | $\begin{aligned} & 10 \\ & 10 \end{aligned}$ | $\begin{aligned} & 26 \\ & 35 \end{aligned}$ | $\begin{aligned} & \mu \mathrm{V} /{ }^{\circ} \mathrm{C} \\ & \mu \mathrm{~V} /{ }^{\circ} \mathrm{C} \end{aligned}$ |
| V ${ }_{\text {S__OA }}$ | Op Amp Input Offset Voltage (Note 10) | $\begin{aligned} & G=1 \text { (MS10) } \\ & G=1 \text { (DD10) } \\ & \hline \end{aligned}$ | $\begin{aligned} & \pm 2.5 \mathrm{~V}, \pm 5 \mathrm{~V}, \pm 15 \mathrm{~V} \\ & \pm 2.5 \mathrm{~V}, \pm 5 \mathrm{~V}, \pm 15 \mathrm{~V} \end{aligned}$ | $\bullet$ |  | $\begin{aligned} & 0.55 \\ & 0.75 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.25 \\ & 5.75 \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{mV} \\ & \mathrm{mV} \end{aligned}$ |
|  | Input Voltage Range | $\mathrm{G}=1$ | $\begin{aligned} & \pm 15 \mathrm{~V} \\ & \pm 5 \mathrm{~V} \\ & \pm 2.5 \mathrm{~V} \end{aligned}$ | $\bullet$ | $\begin{aligned} & \pm 15 \\ & \pm 5 \\ & \pm 1 \\ & \hline \end{aligned}$ | $\begin{gathered} \pm 15.5 \\ \pm 5.5 \\ \pm 1.5 \\ \hline \end{gathered}$ |  | V |
| CMRR | Common Mode Rejection Ratio Referred to Input | $\begin{aligned} & V_{C M}= \pm 15 \mathrm{~V}, \mathrm{G}=1 \\ & V_{\mathrm{CM}}= \pm 15 \mathrm{~V}, \mathrm{G}=2 \\ & \mathrm{~V}_{\mathrm{CM}}= \pm 15 \mathrm{~V}, \mathrm{G}=4 \\ & \mathrm{~V}_{\mathrm{CM}}= \pm 5 \mathrm{~V}, \mathrm{G}=1 \\ & \mathrm{~V}_{\mathrm{CM}}= \pm 1 \mathrm{~V}, \mathrm{G}=1 \end{aligned}$ | $\begin{aligned} & \pm 15 \mathrm{~V} \\ & \pm 15 \mathrm{~V} \\ & \pm 15 \mathrm{~V} \\ & \pm 5 \mathrm{~V} \\ & \pm 2.5 \mathrm{~V} \end{aligned}$ | $\bullet \bullet$ | $\begin{aligned} & 63 \\ & 69 \\ & 73 \\ & 62 \\ & 59 \end{aligned}$ | $\begin{aligned} & 77 \\ & 83 \\ & 86 \\ & 72 \\ & 66 \end{aligned}$ |  | $\begin{aligned} & \mathrm{dB} \\ & \mathrm{~dB} \\ & \mathrm{~dB} \\ & \mathrm{~dB} \\ & \mathrm{~dB} \end{aligned}$ |
| PSRR | Power Supply Rejection Ratio | $\mathrm{P} 1=\mathrm{M} 1=0 \mathrm{~V}, \mathrm{G}=1, \mathrm{~V}_{S}= \pm 2.5 \mathrm{~V}$ to $\pm 15 \mathrm{~V}$ |  | $\bullet$ | 76 | 86 |  | dB |
| $\mathrm{V}_{\text {OUT }}$ | Output Voltage Swing | $\begin{aligned} & \hline \mathrm{R}_{\mathrm{L}}=1 \mathrm{k} \\ & \mathrm{R}_{\mathrm{L}}=500 \Omega \\ & \mathrm{R}_{\mathrm{L}}=500 \Omega \\ & \mathrm{R}_{\mathrm{L}}=500 \Omega \\ & \hline \end{aligned}$ | $\begin{aligned} & \pm 15 \mathrm{~V} \\ & \pm 15 \mathrm{~V} \\ & \pm 5 \mathrm{~V} \\ & \pm 2.5 \mathrm{~V} \end{aligned}$ | $\bullet \cdot$ | $\begin{gathered} \pm 13.1 \\ \pm 12.6 \\ \pm 3.4 \\ \pm 1.2 \end{gathered}$ | $\begin{gathered} \pm 14 \\ \pm 13.5 \\ \pm 4 \\ \pm 2 \end{gathered}$ |  | $\begin{aligned} & \text { V } \\ & \text { V } \\ & \text { V } \end{aligned}$ |
| $\mathrm{ISC}_{\text {S }}$ | Short-Circuit Current | $\mathrm{G}=1$ | $\pm 15 \mathrm{~V}$ | $\bullet$ | $\pm 55$ | $\pm 115$ |  | mA |
| SR | Slew Rate | $\begin{aligned} & \mathrm{G}=-2, \mathrm{~V}_{\text {OUT }}= \pm 12 \mathrm{~V}, \mathrm{P} 2=0 \mathrm{~V} \\ & \text { Measured at } \mathrm{V}_{\text {OUT }}= \pm 10 \mathrm{~V} \end{aligned}$ | $\pm 15 \mathrm{~V}$ | $\bullet$ | 600 | 900 |  | V/ $/ \mathrm{S}$ |
| $I_{S}$ | Supply Current | $\mathrm{G}=1$ | $\begin{aligned} & \pm 15 \mathrm{~V} \\ & \pm 5 \mathrm{~V} \end{aligned}$ | $\bullet$ |  | $\begin{aligned} & 7.9 \\ & 7.4 \end{aligned}$ | $\begin{gathered} 10.5 \\ 9.9 \end{gathered}$ | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \end{aligned}$ |

The $\bullet$ denotes the specifications which apply over the $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq 85^{\circ} \mathrm{C}$.
Difference Amplifier Configuration. $\mathrm{V}_{\mathrm{REF}}=\mathrm{V}_{\mathrm{CM}}=\mathrm{OV}$ and unused gain pins are unconnected, unless otherwise noted.

| SYMBOL | PARAMETER | CONDITIONS | $V_{\text {SUPPLY }}$ | MIN | TYP | MAX | UNITS |
| :--- | :--- | :--- | :--- | :--- | :--- | ---: | ---: |
| GE | Gain Error | $V_{\text {OUT }}= \pm 12 \mathrm{~V}, R_{L}=1 \mathrm{k}, \mathrm{G}=1$ | $\pm 15 \mathrm{~V}$ | $\bullet$ | 0.05 | 0.3 | $\%$ |
|  |  | $V_{\text {OUT }}= \pm 12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=1 \mathrm{k}, \mathrm{G}=2$ | $\pm 15 \mathrm{~V}$ | $\bullet$ | 0.05 | 0.35 | $\%$ |
|  |  | $\mathrm{~V}_{\text {OUT }}= \pm 12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=1 \mathrm{k}, \mathrm{G}=4$ | $\pm 15 \mathrm{~V}$ | $\bullet$ | 0.05 | 0.35 | $\%$ |
|  |  | $\mathrm{~V}_{\text {OUT }}= \pm 2.5 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=500 \Omega, \mathrm{G}=1$ | $\pm 5 \mathrm{~V}$ | $\bullet$ | 0.05 | 0.3 | $\%$ |
|  |  | $\mathrm{~V}_{\text {OUT }}= \pm 2.5 \mathrm{~V} R_{L}=150 \Omega, \mathrm{G}=1$ | $\pm 5 \mathrm{~V}$ | $\bullet$ | 0.05 | 0.5 | $\%$ |

ELECTRICRL CHARFCRERSTICS The o denotes the specifications which apply over the $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq 85^{\circ} \mathrm{C}$. Difference Amplifier Configuration. $V_{\text {REF }}=V_{C M}=0 V$ and unused gain pins are unconnected, unless otherwise noted.

| SYMBOL | PARAMETER | CONDITIONS | $V_{\text {SUPPLY }}$ |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{0 S}$ | Input Offset Voltage Referred to Input (Note 7) | $\begin{aligned} & G=1(\text { MS10 }) \\ & G=1(\text { DD10 }) \\ & G=2(\text { MS10 }) \\ & G=2(\text { DD10 }) \\ & G=4(\text { MS10 }) \\ & G=4(\text { DD10 }) \\ & G=1(\text { MS10 }) \\ & G=1(\text { DD10 }) \\ & G=1(\text { MS10 }) \\ & G=1(\text { DD10 }) \end{aligned}$ | $\begin{aligned} & \pm 15 \mathrm{~V} \\ & \pm 15 \mathrm{~V} \\ & \pm 15 \mathrm{~V} \\ & \pm 15 \mathrm{~V} \\ & \pm 15 \mathrm{~V} \\ & \pm 15 \mathrm{~V} \\ & \pm 5 \mathrm{~V} \\ & \pm 5 \mathrm{~V} \\ & \pm 2.5 \mathrm{~V} \\ & \pm 2.5 \mathrm{~V} \end{aligned}$ | $\square$ |  | $\begin{aligned} & 1.2 \\ & 1.6 \\ & 0.9 \\ & 1.2 \\ & 0.7 \\ & 0.9 \\ & 1.1 \\ & 1.4 \\ & 1.1 \\ & 1.5 \end{aligned}$ | $\begin{gathered} 7.5 \\ 13 \\ 6 \\ 10 \\ 5.5 \\ 8.5 \\ 7.5 \\ 13 \\ 7.5 \\ 13 \end{gathered}$ | mV <br> mV <br> mV <br> mV <br> mV <br> mV <br> mV <br> mV <br> mV <br> mV |
| $\mathrm{V}_{\text {OS }}$ TC | Input Offset Voltage Drift Referred to Input (Note 9) | $\begin{aligned} & G=1(\text { MS10 }) \\ & G=1 \text { (DD10) } \end{aligned}$ | $\begin{aligned} & \pm 15 \mathrm{~V} \\ & \pm 15 \mathrm{~V} \end{aligned}$ |  |  | $\begin{aligned} & 10 \\ & 10 \end{aligned}$ | $\begin{aligned} & 26 \\ & 35 \end{aligned}$ | $\begin{aligned} & \mu \mathrm{V} /{ }^{\circ} \mathrm{C} \\ & \mu \mathrm{~V} /{ }^{\circ} \mathrm{C} \end{aligned}$ |
| Vos_OA | Op Amp Input Offset Voltage (Note 10) | $\begin{aligned} & G=1(\text { MS10 }) \\ & G=1 \text { (DD10) } \\ & \hline \end{aligned}$ | $\begin{aligned} & \pm 2.5 \mathrm{~V}, \pm 5 \mathrm{~V}, \pm 15 \mathrm{~V} \\ & \pm 2.5 \mathrm{~V}, \pm 5 \mathrm{~V}, \pm 15 \mathrm{~V} \\ & \hline \end{aligned}$ | $\bullet$ |  | $\begin{aligned} & 0.6 \\ & 0.8 \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 3.75 \\ 6.5 \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{mV} \\ & \mathrm{mV} \end{aligned}$ |
|  | Input Voltage Range | $\mathrm{G}=1$ | $\begin{aligned} & \pm 15 \mathrm{~V} \\ & \pm 5 \mathrm{~V} \\ & \pm 2.5 \mathrm{~V} \end{aligned}$ | $\bullet$ | $\begin{gathered} \pm 15 \\ \pm 5 \\ \pm 1 \end{gathered}$ | $\begin{gathered} \pm 15.5 \\ \pm 5.5 \\ \pm 1.5 \end{gathered}$ |  | V |
| CMRR | Common Mode Rejection Ratio Referred to Input | $\begin{aligned} & V_{C M}= \pm 15 \mathrm{~V}, \mathrm{G}=1 \\ & V_{C M}= \pm 15 \mathrm{~V}, \mathrm{G}=2 \\ & V_{\mathrm{CM}}= \pm 15 \mathrm{~V}, \mathrm{G}=4 \\ & V_{\mathrm{CM}}= \pm 5 \mathrm{~V}, \mathrm{G}=1 \\ & V_{\mathrm{CM}}= \pm 1 \mathrm{~V}, \mathrm{G}=1 \end{aligned}$ | $\begin{aligned} & \pm 15 \mathrm{~V} \\ & \pm 15 \mathrm{~V} \\ & \pm 15 \mathrm{~V} \\ & \pm 5 \mathrm{~V} \\ & \pm 2.5 \mathrm{~V} \end{aligned}$ | $\stackrel{\bullet}{\bullet}$ | $\begin{aligned} & 62 \\ & 68 \\ & 72 \\ & 61 \\ & 57 \end{aligned}$ | $\begin{aligned} & 77 \\ & 83 \\ & 86 \\ & 72 \\ & 66 \end{aligned}$ |  | $\begin{aligned} & \mathrm{dB} \\ & \mathrm{~dB} \\ & \mathrm{~dB} \\ & \mathrm{~dB} \\ & \mathrm{~dB} \end{aligned}$ |
| PSRR | Power Supply Rejection Ratio | $\mathrm{P} 1=\mathrm{M} 1=0 \mathrm{~V}, \mathrm{G}=1, \mathrm{~V}_{S}= \pm 2.5 \mathrm{~V}$ to $\pm 15 \mathrm{~V}$ |  | $\bullet$ | 74 | 86 |  | dB |
| V OUT | Output Voltage Swing | $\begin{aligned} & \mathrm{R}_{\mathrm{L}}=1 \mathrm{k} \\ & \mathrm{R}_{\mathrm{L}}=500 \Omega \\ & \mathrm{R}_{\mathrm{L}}=500 \Omega \\ & \mathrm{R}_{\mathrm{L}}=500 \Omega \\ & \hline \end{aligned}$ | $\begin{aligned} & \pm 15 \mathrm{~V} \\ & \pm 15 \mathrm{~V} \\ & \pm 5 \mathrm{~V} \\ & \pm 2.5 \mathrm{~V} \end{aligned}$ | $\stackrel{\bullet}{\bullet}$ | $\begin{gathered} \pm 13 \\ \pm 12.5 \\ \pm 3.3 \\ \pm 1.1 \end{gathered}$ | $\begin{gathered} \pm 14 \\ \pm 13.5 \\ \pm 4 \\ \pm 2 \end{gathered}$ |  | $\begin{aligned} & \text { V } \\ & \text { V } \\ & \text { V } \end{aligned}$ |
| ISC | Short-Circuit Current | $\mathrm{G}=1$ | $\pm 15 \mathrm{~V}$ | $\bullet$ | $\pm 50$ | $\pm 105$ |  | mA |
| SR | Slew Rate | $\begin{aligned} & \mathrm{G}=-2, \mathrm{~V}_{\text {OUT }}= \pm 12 \mathrm{~V}, \mathrm{P} 2=0 \mathrm{~V} \\ & \text { Measured at } \mathrm{V}_{\text {OUT }}= \pm 10 \mathrm{~V} \\ & \hline \end{aligned}$ | $\pm 15 \mathrm{~V}$ | $\bullet$ | 550 | 900 |  | V/us |
| $I_{S}$ | Supply Current | $\mathrm{G}=1$ | $\begin{aligned} & \pm 15 \mathrm{~V} \\ & \pm 5 \mathrm{~V} \end{aligned}$ | $\bullet$ |  | $\begin{aligned} & 8.0 \\ & 7.6 \end{aligned}$ | $\begin{aligned} & 11.0 \\ & 10.4 \end{aligned}$ | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \end{aligned}$ |

Note 1: Absolute Maximum Ratings are those values beyond which the life of a device may be impaired.
Note 2: The inputs are protected by diodes connected to $\mathrm{V}{ }^{+}$and $\mathrm{V}_{S}{ }^{-}$. If an input goes beyond the supply range, the input current should be limited to 10 mA .
Note 3: A heat sink may be required to keep the junction temperature below absolute maximum.
Note 4: The LT1995C and LT1995I are guaranteed functional over the operating temperature range of $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$.
Note 5: The LT1995C is guaranteed to meet specified performance from $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$. The LT1995C is designed, characterized and expected to meet specified performance from $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ but is not tested or QA sampled at these temperatures. The LT1995I is guaranteed to meet specified performance from $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$.

Note 6: Thermal resistance $\left(\theta_{\mathrm{JA}}\right)$ varies with the amount of PC board metal connected to the leads. The specified values are for short traces connected to the leads. If desired, the thermal resistance can be reduced slightly in the MS package to about $130^{\circ} \mathrm{C} / \mathrm{W}$ by connecting the used leads to a larger metal area. A substantial reduction in thermal resistance down to about $50^{\circ} \mathrm{C} / \mathrm{W}$ can be achieved by connecting the Exposed Pad on the bottom of the DD package to a large PC board metal area which is either open-circuited or connected to $\mathrm{V}_{S}$.
Note 7: Input offset voltage is pulse tested and is exclusive of warm-up drift. $V_{O S}$ and $V_{O S} T C$ refer to the input offset of the difference amplifier configuration. The equivalent input offset of the internal op amp can be calculated from $V_{O S \_O A}=V_{O S} \bullet G /(G+1)$.
Note 8: Full Power bandwidth is calculated from the slew rate measurement: FPBW = SR/2 $2 \mathrm{~V}_{\mathrm{p}}$.
Note 9: This parameter is not $100 \%$ tested.
Note 10: The input offset of the internal op amp is calculated from the input offset voltage: $V_{O S \_O A}=V_{O S} \bullet G /(G+1)$.

## TYPICAL PERFOROIAOCE CHARACTERISTICS (Difference Amplifier Configuration)



## TYPICAL PERFORMANCE CHARACTERISTICS (Difierence Amplifier Configuration)



## TYPICAL PERFORMANCE CHARACTERISTICS (Ditference Anpilier Configuration)



TYPICAL PGRFORMRACE CHARACTERISTICS (Difference Ampilier Conifiguation)


## PIn FUПCTIOnS (Difference Amplifier Configuration)

P1 (Pin 1): Noninverting Gain-of-1 Input. Connects a 4k internal resistor to the op amp's noninverting input.
P2 (Pin 2): Noninverting Gain-of-2 Input. Connects a $2 k$ internal resistor to the op amp's noninverting input.
P4 (Pin 3): Noninverting Gain-of-4 Input. Connects a 1k internal resistor to the op amp's noninverting input.
$V_{S}{ }^{-}$(Pin 4): Negative Supply Voltage.
REF (Pin 5): Reference Voltage. Sets the output level when the difference between the inputs is zero. Connects a 4 k internal resistor to the op amp's non inverting input.

OUT (Pin 6): Output Voltage. $\mathrm{V}_{\text {OUT }}=\mathrm{V}_{\text {REF }}+1 \cdot\left(\mathrm{~V}_{\mathrm{P} 1}-\mathrm{V}_{\mathrm{M} 1}\right)$ $+2 \cdot\left(\mathrm{~V}_{\mathrm{P} 2}-\mathrm{V}_{\mathrm{M} 2}\right)+4 \cdot\left(\mathrm{~V}_{\mathrm{P} 4}-\mathrm{V}_{\mathrm{M} 4}\right)$.
$\mathrm{V}_{\mathrm{S}}{ }^{+}$(Pin 7): Positive Supply Voltage.
M4 (Pin 8): Inverting Gain-of-4 Input. Connects a 1k internal resistor to the op amp's inverting input.
M2 (Pin 9): Inverting Gain-of-2 Input. Connects a $2 k$ internal resistor to the op amp's inverting input.
M1 (Pin 10): Inverting Gain-of-1 Input. Connects a 4k internal resistor to the op amp's inverting input.

## BLOCK DIAGRAM



## APPLICATIONS INFORMATION

## Configuration Flexibility

The LT1995 combines a high speed precision operational amplifier with eight ratio-matched on-chip resistors. The resistor configuration and pinout of the device is shown in the Block Diagram. The topology is extremely versatile and provides for simple realizations of most classic functional configurations including difference amplifiers, inverting gain stages, noninverting gain stages (including Hi-Z input buffers) and summing amplifiers. The LT1995 delivers load currents of at least 30mA, making it ideal for cable driving applications as well.
The input voltage range depends on gain and configuration. ESD diodes will clamp any input voltage that exceeds the supply potentials by more than several tenths of a volt; and the internal op amp input ports must remain at least 1.75 V within the rails to assure normal operation of the part. The output will swing to within one and a half volts of
the rails, which in low supply voltage and high gain configurations will create a limitation on the usable input range. It should be noted that while the internal op amp can withstand transient differential input voltages of up to 10 V without damage, this does generate large supply current increases (tens of mA ) as required for high slew rates. If the device is used with sustained differential input across the internal op amp (such as when the output is clipping), the average supply current will increase, excessive power dissipation will result, and the part may be damaged (i.e., the LT1995 is not recommended for use in comparator applications or with the output clipped).

## Difference Amplifier

The LT1995 can be connected as a classic difference amplifier with an output function given by:

$$
V_{\text {OUT }}=G \cdot\left(V_{\text {IN }^{+}}-V_{\text {IN }}^{-}\right)+V_{\text {REF }}
$$

## APPLICATIONS InFORMATION

As shown in Figure 1, the options for fixed gain G include: $1,1.33,1.67,2,3,4,5,6$ and 7 , all achieved by pinstrapping alone. With split-supply applications where the output is to be ground referenced, the $\mathrm{V}_{\text {REF }}$ input is simply tied to ground. The input common mode voltage is rejected by the high CMRR of the part within the usable input range.

## Inverting Gain Amplifier

The LT1995 can be connected as an inverting gain amplifier with an output function given by:

$$
V_{\text {OUT }}=-\left(G \cdot V_{\text {IN }}^{-}\right)+V_{\text {REF }}
$$

As shown in Figure 1, the options for fixed gain G include: 1, 1.33, 1.67, 2, 3, 4, 5, 6 and 7, all achieved by pin strapping alone. The $\mathrm{V}_{\mathrm{IN}}{ }^{+}$connection used in the difference amp configuration is simply tied to ground (or a low impedance potential equal to the input signal bias to create an input "virtual ground"). With split-supply applications where the output is to be ground referenced, the $\mathrm{V}_{\text {REF }}$ input is simply tied to ground as well.

## Noninverting Gain Buffer Amplifier

The LT1995 can be connected as a high input impedance noninverting gain buffer amplifier with an output function given by:

$$
\mathrm{V}_{\text {OUT }}=\mathrm{G} \cdot \mathrm{~V}_{\text {IN }}
$$

As shown in Figure 2, the options for fixed gain G include: $1,1.14,1.2,1.33,1.4,1.6,2,2.33,2.66,3,4,5,6,7$ and 8 , all achieved by pin strapping alone. With single supply applications, the grounded M input pins may be tied to a low impedance potential equal to the input signal bias to create a "virtual ground" for both the input and output signals. While there is no input attenuation from $\mathrm{V}_{\text {IN }}$ to the internal noninverting op amp port in these configurations, the $P$ connections vary to minimize offset by providing balanced input resistances to the internal op amp.

## Noninverting Gain Amplifier Input Attenuation

The LT1995 can also be connected as a noninverting gain amplifier having an input attenuation network to provide a wide range of additional noninverting gain options. In combination with the feedback configurations for gains of $G$ shown in Figure 2 (connections to the M inputs), the P and REF inputs may be connected to form several resistor divider attenuation ratios A , so that a compound output function is given by:
$V_{\text {OUT }}=A \cdot G \cdot V_{\text {IN }}$
As shown in Figure 3, the options for fixed attenuation A include $0.875,0.857,0.833,0.8,0.75,0.714,0.667,0.625$ and 0.571 , all achieved by pin strapping alone. With just the attenuation configurations of Figure 3 and the feedback configurations of Figure 2, seventy-three unique composite gains in the range of 1 to 8 are available (many options for gain below unity also exist). Figure 3 does not include the additional pin-strap configurations offering A values of $0.5,0.429,0.375,0.333,0.286,0.25,0.2,0.167$, 0.143 and 0.125 , as these values tend to compromise the low noise performance of the part and don't generally contribute many more unique gain options. It should be noted that with these configurations some degree of imbalance will generally exist between the effective resistances $R_{p}$ and $R_{M}$ seen by the internal op amp input ports, noninverting and inverting, respectively. Depending on the specific combination of $A$ and $G$, the following DC offset error due to op amp input bias current ( $\mathrm{I}_{\mathrm{B}}$ ) should be anticipated: The $\mathrm{I}_{\mathrm{B}}$ of the internal op amp is typically $0.6 \mu \mathrm{~A}$ and is prepackage tested to a limit of $2 \mu \mathrm{~A}$. Additional output-referred offset $=I_{B} \bullet\left(R_{P}-R_{M}\right) \cdot G$. In some configurations, this could be as much as $1.7 \mathrm{mV} \cdot \mathrm{G}$ additional output offset. The I Ios of the internal op amp is typically 120 nA and is prepackage tested to a limit of 350nA. The Electrical Characteristics table includes the effects of $\mathrm{I}_{\mathrm{B}}$ and $\mathrm{I}_{\mathrm{OS}}$.

## APPLICATIONS INFORMATION



Figure 1. Difference (and Inverting) Amplifier Configurations

Table 1. Pin Use, Input Range, Input Resistance, Bandwidth in Difference Amplifier Configuration

| GAIN | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ | $\mathbf{6}$ | $\mathbf{7}$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Use of P1/M1 | $\mathrm{V}_{\text {IN }}$ | Open | $\mathrm{V}_{\text {IN }}$ | Open | $\mathrm{V}_{\text {IN }}$ | Open | $\mathrm{V}_{\text {IN }}$ |
| Use of P2/M2 | Open | $\mathrm{V}_{\text {IN }}$ | $\mathrm{V}_{\text {IN }}$ | Open | Open | $\mathrm{V}_{\text {IN }}$ | $\mathrm{V}_{\text {IN }}$ |
| Use of P4/M4 | Open | Open | Open | $\mathrm{V}_{\text {IN }}$ | $\mathrm{V}_{\text {IN }}$ | $\mathrm{V}_{\text {IN }}$ | $\mathrm{V}_{\text {IN }}$ |
| Positive Input Range: $\mathrm{V}_{\text {REF }}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{S}}= \pm 15 \mathrm{~V}$ | $\pm 15 \mathrm{~V}$ | $\pm 15 \mathrm{~V}$ | $\pm 15 \mathrm{~V}$ | $\pm 15 \mathrm{~V}$ | $\pm \pm 15 \mathrm{~V}$ | $\pm 15 \mathrm{~V}$ | $\pm 15 \mathrm{~V}$ |
| Positive Input Range: $\mathrm{V}_{\text {REF }}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{S}}= \pm 5 \mathrm{~V}$ | $\pm 5 \mathrm{~V}$ | $\pm 4.88 \mathrm{~V}$ | $\pm 4.33 \mathrm{~V}$ | $\pm 4.06 \mathrm{~V}$ | $\pm 3.9 \mathrm{~V}$ | $\pm 3.79 \mathrm{~V}$ | $\pm 3.71 \mathrm{~V}$ |
| Positive Input Range: $\mathrm{V}_{\text {REF }}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{S}}= \pm 2.5 \mathrm{~V}$ | $\pm 1.5 \mathrm{~V}$ | $\pm 1.13 \mathrm{~V}$ | $\pm 1 \mathrm{~V}$ | $\pm 0.94 \mathrm{~V}$ | $\pm 0.9 \mathrm{~V}$ | $\pm 0.88 \mathrm{~V}$ | $\pm 0.86 \mathrm{~V}$ |
| Positive Input Resistance | 8 k | 6 k | 5.33 k | 5 k | 4.8 k | 4.67 k | 4.57 k |
| Minus Input Resistance | 4 k | 2 k | 1.33 k | 1 k | $800 \Omega$ | $667 \Omega$ | $571 \Omega$ |
| Ref Input Resistance | 8 k | 6 k | 5.33 k | 5 k | 4.8 k | 4.67 k | 4.57 k |
| Input Common Mode Resistance, $\mathrm{V}_{\text {REF }}=0 \mathrm{~V}$ | 4 k | 3 k | 2.67 k | 2.5 k | 2.4 k | 2.33 k | 2.29 k |
| Input Differential Mode Resistance, $\mathrm{V}_{\text {REF }}=0 \mathrm{~V}$ | 8 k | 4 k | 2.67 k | 2 k | 1.6 k | 1.33 k | 1.14 k |
| -3dB Bandwidth | 32 MHz | 27 MHz | 27 MHz | 23 MHz | 18 MHz | 16 MHz | 15 MHz |

APPLICATIONS InFORMATION


Figure 2. Noninverting Buffer Amplifier Configurations (Hi-Z Input)

## APPLICATIONS INFORMATION



Figure 3. Noninverting Amplifier Input Attenuation Configurations ( $\mathrm{A}>0.5$ )

## AC-Coupling Methods for Single Supply Operation

The LT1995 can be used in many single-supply applications using AC-coupling without additional biasing circuitry.
AC-coupling the LT1995 in a difference amplifier configuration (as in Figure 1) is a simple matter of adding coupling capacitors to each input and the output as shown in the example of Figure 5. The input voltage $V_{\text {BIAS }}$ applied to the REF pin establishes the quiescent voltage on the input and output pins. The V ${ }_{\text {BIAS }}$ signal should have a low source impedance to avoid degrading the CMRR ( $0.5 \Omega$ for 1 dB CMRR change typically).


Figure 4. Unique Noninverting Gain Configurations

## APPLICATIONS INFORMATION

Using the LT1995 as an AC-coupled inverting gain stage, the REF pin and the relevant P inputs may all be driven from a $\mathrm{V}_{\text {BIAS }}$ source as depicted in the example of Figure 6, thus establishing the quiescent voltage on the input and output pins. The $V_{\text {BIAS }}$ signal will only have to source the bias current $\left(I_{B}\right)$ of the noninverting input of the internal op amp ( $0.6 \mu \mathrm{~A}$ typically), so a high $\mathrm{V}_{\text {BIAS }}$ source impedance ( $\mathrm{R}_{\mathrm{S}}$ ) will cause the quiescent level of the amplifier output to deviate from the intended $V_{\text {BIAS }}$ level by $I_{B} \bullet R_{S}$.

In operation as a noninverting gain stage, the P and REF inputs may be configured as a "supply splitter," thereby providing a convenient mid-supply operating point. Figure 7 illustrates the three attenuation configurations that generate $50 \%$ mid-supply biasing levels with no external components aside from the desired coupling capacitors. As with the DC-coupled input attenuation ratios, $A$, a compound output function including the feedback gain parameter G is given by:

$$
V_{\text {OUT }}=A \cdot G \cdot V_{\text {IN }}
$$

Figure 5. AC-Coupled Difference Amplifier General Configuation ( $G=5$ Example)


Figure 6. AC-Coupled Inverting Gain Amplifier General Configuration ( $\mathrm{G}=5$ Example)

*CONFIGURE M INPUTS FOR DESIRED G PARAMETER; REFER TO FIGURE 2 FOR CONNECTIONS. ANY M INPUTS SHOWN GROUNDED IN FIGURE 2 SHOULD INSTEAD BE CAPACITIVELY COUPLED TO GROUND

Figure 7. AC-Coupled Noninverting Amplifier Input Attenuation Configurations (Supply Splitting)

## APPLICATIONS INFORMATION

If one of the A parameter configurations in Figure 3 is preferred, or the use of an external biasing source is desired, the $P$ and REF input connections shown grounded in a Figure 3 circuit may be instead driven by a $V_{\text {BIAS }}$ voltage to establish a quiescent operating point for the input and output pins. The $\mathrm{V}_{\text {IN }}$ connections of the Figure 3 circuit are then driven via a coupling capacitor. Any grounded M inputs for the desired G configuration (refer to Figure 2) must be individually or collectively AC-coupled to ground. Figure 8 illustrates a complete example circuit of an externally biased AC-coupled noninverting amplifier. The V ${ }_{\text {BIAS }}$ source impedance should be low (a few ohms) to avoid degrading the inherent accuracy of the LT1995. 0.013\% of additional Gain Error for each ohm of resistance on the REF pin is typical.


Figure 8. AC-Coupled Noninverting Amplifier with External Bias Source (Example)

## Resistor Considerations

The resistors in the LT1995 are very well matched, low temperature coefficientthin film based elements. Although their absolute tolerance is fairly wide (typically $\pm 5 \%$ but $\pm 25 \%$ worst case), the resistor matching is to within $0.2 \%$
at room temperature, and to within $0.3 \%$ over temperature. The temperature coefficient of the resistors is typically $-30 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$. The resistors have been sized to accommodate 15 V across each resistor, or in terms of power, 225 mW in the 1 k resistors, 113 mW in the 2 k resistors, and 56 mW in the 4 k resistors.

## Power Supply Considerations

As with any high speed amplifier, the LT1995 printed circuit layout should utilize good power supply decoupling practices. Good decoupling will typically consist of one or more capacitors employing the shortest practical interconnection traces and direct vias to a ground plane. This practice minimizes inductance at the supply pins so the impedance is low at the operating frequencies of the part, thereby suppressing feedback or crosstalk artifacts that might otherwise lead to extended settling times, frequency response anomalies, or even oscillation. For high speed parts like the LT1995, 10nF ceramics are suitable close-in bypass capacitors, and if high currents are being delivered to a load, additional $4.7 \mu \mathrm{~F}$ capacitors in parallel can help minimize induced power supply transients.
Because unused input pins are connected via resistors to the input of the op amp, excessive capacitances on these pins will degrade the rise time, slew rate, and step response of the output. Therefore, these pins should not be connected to large traces which would add capacitance when not in use.

Since the LT1995 has a wide operating supply voltage range, it is possible to place the part in situations of relatively high power dissipation that may cause excessive die temperatures to develop. Maximum junction temperature $\left(T_{J}\right)$ is calculated from the ambient temperature $\left(T_{A}\right)$

## APPLICATIONS INFORMATION

and power dissipation $\left(\mathrm{P}_{\mathrm{D}}\right)$ as follows for a nominal PCB layout:

$$
T_{J}=T_{A}+\left(P_{D} \bullet \theta_{\mathrm{JA}}\right)
$$

For example, in order to maintain a maximum junction temperature of $150^{\circ} \mathrm{C}$ at $85^{\circ} \mathrm{C}$ ambient in an MS10 package, the power must be limited to 0.4 W . It is important to note that when operating at $\pm 15 \mathrm{~V}$ supplies, the quiescent current alone will typically account for 0.24 W , so careful thermal management may be required if high load currents and high supply voltages are involved. By additional copper area contact to the supply pins or effective thermal coupling to extended ground plane(s), the thermal impedance can be reduced to $130^{\circ} \mathrm{C} / \mathrm{W}$ in the MS10 package. A substantial reduction in thermal impedance of the DD10 package down to about $50^{\circ} \mathrm{C} / \mathrm{W}$ can be achieved by connecting the Exposed Pad on the bottom of the package to a large PC board metal area which is either opencircuited or connected to $\mathrm{V}_{S}{ }^{-}$.


Figure 9. Optional Frequency Compensation Network for ( $1 \leq \mathbf{G} \leq 2$ )

## Frequency Compensation

The LT1995 comfortably drives heavy resistive loads such as back-terminated cables and provides nicely damped responses for all gain configurations when doing so. Small capacitances are included in the on-chip resistor network to optimize bandwidth in the basic difference gain configurations of Figure 1. For the noninverting configurations of Figure 2, where the gain parameter G is 2 or less, significant overshoot can occur when driving light loads. For these low gain cases, providing an RC output network as shown in Figure 9 to create an artificial load at high frequency will assure good damping behavior.


Figure 10. Step Response of Circuit in Figure 9

## PACKAGE DESCRIPTION

MS Package
10-Lead Plastic MSOP
(Reference LTC DWG \# 05-08-1661)


NOTE:

1. DIMENSIONS IN MILLIMETER/(INCH)
2. DRAWING NOT TO SCALE
3. DIMENSION DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS

MOLD FLASH, PROTRUSIONS OR GATE BURRS SHALL NOT EXCEED 0.152mm (.006") PER SIDE
4. DIMENSION DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSIONS

INTERLEAD FLASH OR PROTRUSIONS SHALL NOT EXCEED 0.152 mm (.006") PER SIDE
5. LEAD COPLANARITY (BOTTOM OF LEADS AFTER FORMING) SHALL BE 0.102 mm (.004") MAX


DETAIL "A"



Package
10-Lead Plastic DFN (3mm $\times 3 \mathrm{~mm}$ )
(Reference LTC DWG \# 05-08-1699)


RECOMMENDED SOLDER PAD PITCH AND DIMENSIONS


NOTE:

1. DRAWING TO BE MADE A JEDEC PACKAGE OUTLINE MO-229 VARIATION OF (WEED-2). CHECK THE LTC WEBSITE DATA SHEET FOR CURRENT STATUS OF VARIATION ASSIGNMENT
2. DRAWING NOT TO SCALE
3. ALL DIMENSIONS ARE IN MILLIMETERS
4. DIMENSIONS OF EXPOSED PAD ON BOTTOM OF PACKAGE DO NOT INCLUDE MOLD FLASH. MOLD FLASH, IF PRESENT, SHALL NOT EXCEED 0.15mm ON ANY SIDE
5. EXPOSED PAD SHALL BE SOLDER PLATED
6. SHADED AREA IS ONLY A REFERENCE FOR PIN 1 LOCATION ON THE TOP AND BOTTOM OF PACKAGE

## TYPICAL APPLICATIONS

High Input Impedance Precision Gain of 2 Configuration


OA to 2A Current Source


Tracking Negative Reference


Current Sense with Alarm


Single Supply Video Line Driver


## RELATGD PARTS

| PART NUMBER | DESCRIPTION | COMMENTS |
| :--- | :--- | :--- |
| LT1363 | $70 \mathrm{MHz}, 1000 \mathrm{~V} / \mu \mathrm{s}$ Op Amp | 50ns Settling Time to 0.1\%, CLOAD Stable |
| LT1990 | High Voltage Difference Amplifier | $\pm 250 \mathrm{~V}$ Common Mode Voltage, Micropower, Pin Selectable G = 1, 10 |
| LT1991 | Precision Gain Selectable Amplifier | Micropower, Precision, Pin Selectable G =-13 to 14 |
| LTC1992 | Fully Differential Amplifier | Differential Input and Output, Rail-to-Rail Output, IS $=1.2 \mathrm{~mA}$, CLOAD Stable <br> to 10,000pF, Adjustable Common Mode Voltage |
| LTC6910-x | Programmable Gain Amplifiers | 3 Gain Configurations, Rail-to-Rail Input and Output |


[^0]:    $\boldsymbol{\mathcal { Y }}$, LTC and LT are registered trademarks of Linear Technology Corporation. All other trademarks are the property of their respective owners.

