

## LP3906

# Dual High-Current Step-Down DC/DC and Dual Linear Regulator with I2C Compatible Interface

### General Description

The LP3906 is a multi-function, programmable Power Management Unit, optimized for low power FPGAs, Microprocessors and DSPs. This device integrates two highly efficient 1.5A Step-Down DC/DC converters with dynamic voltage management (DVM), two 300mA Linear Regulators and a 400kHz I2C compatible interface to allow a host controller access to the internal control registers of the LP3906. The LP3906 additionally features programmable power-on sequencing and is offered in a tiny 5 x 4 x 0.8mm LLP-24 pin package.

### Key Specifications

#### Step-Down DC/DC Converter (Buck)

- 1.5A output current
- Programmable V<sub>out</sub> from:
  - Buck1 : 0.8V–2.0V
  - Buck2 : 1.0V–3.5V
- Up to 96% efficiency
- 2 MHz PWM switching frequency
- ±3% output voltage accuracy
- Automatic soft start

#### Linear Regulators (LDO)

- Programmable V<sub>OUT</sub> of 1.0V–3.5V
- ±3% output voltage accuracy
- 300 mA output currents
- 25 mV (typ) Dropout

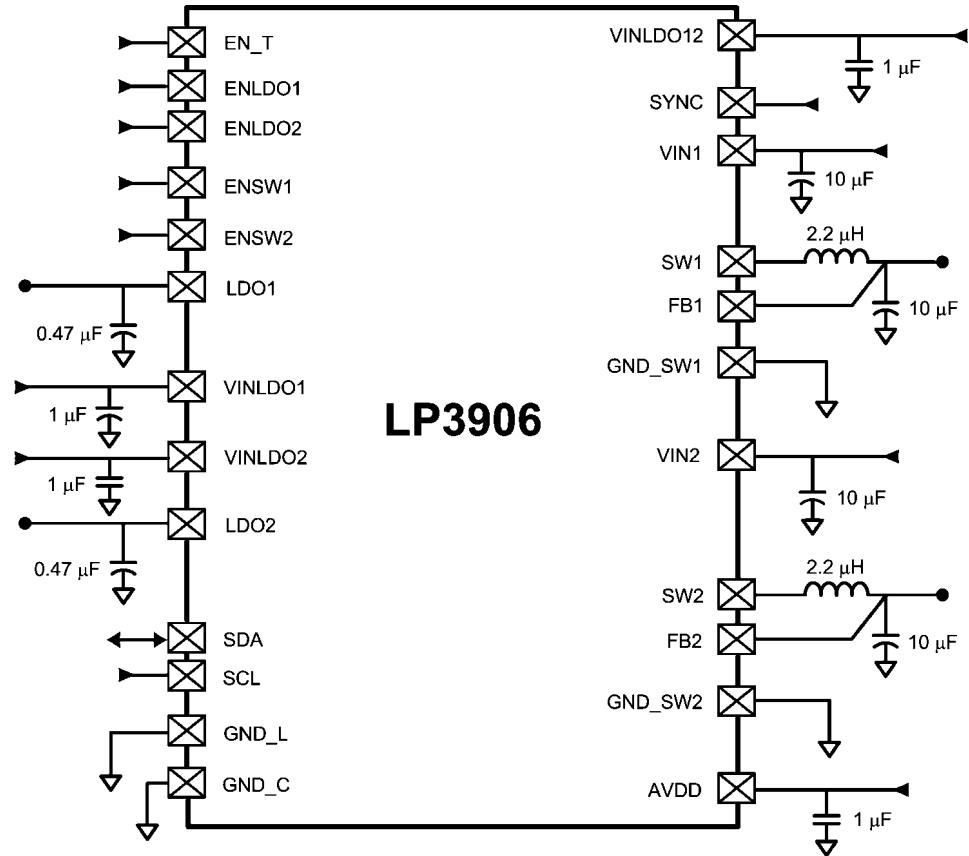
### Features

- Compatible with advanced applications processors and FPGAs
- 2 LDOs for powering Internal processor functions and I/Os
- High speed serial interface for independent control of device functions and settings
- Precision internal reference
- Thermal overload protection
- Current overload protection
- 24-lead 5 x 4 x 0.8 mm LLP package
- Software Programmable Regulators

### Applications

- FPGA, DSP core power
- Applications processors
- Peripheral I/O power

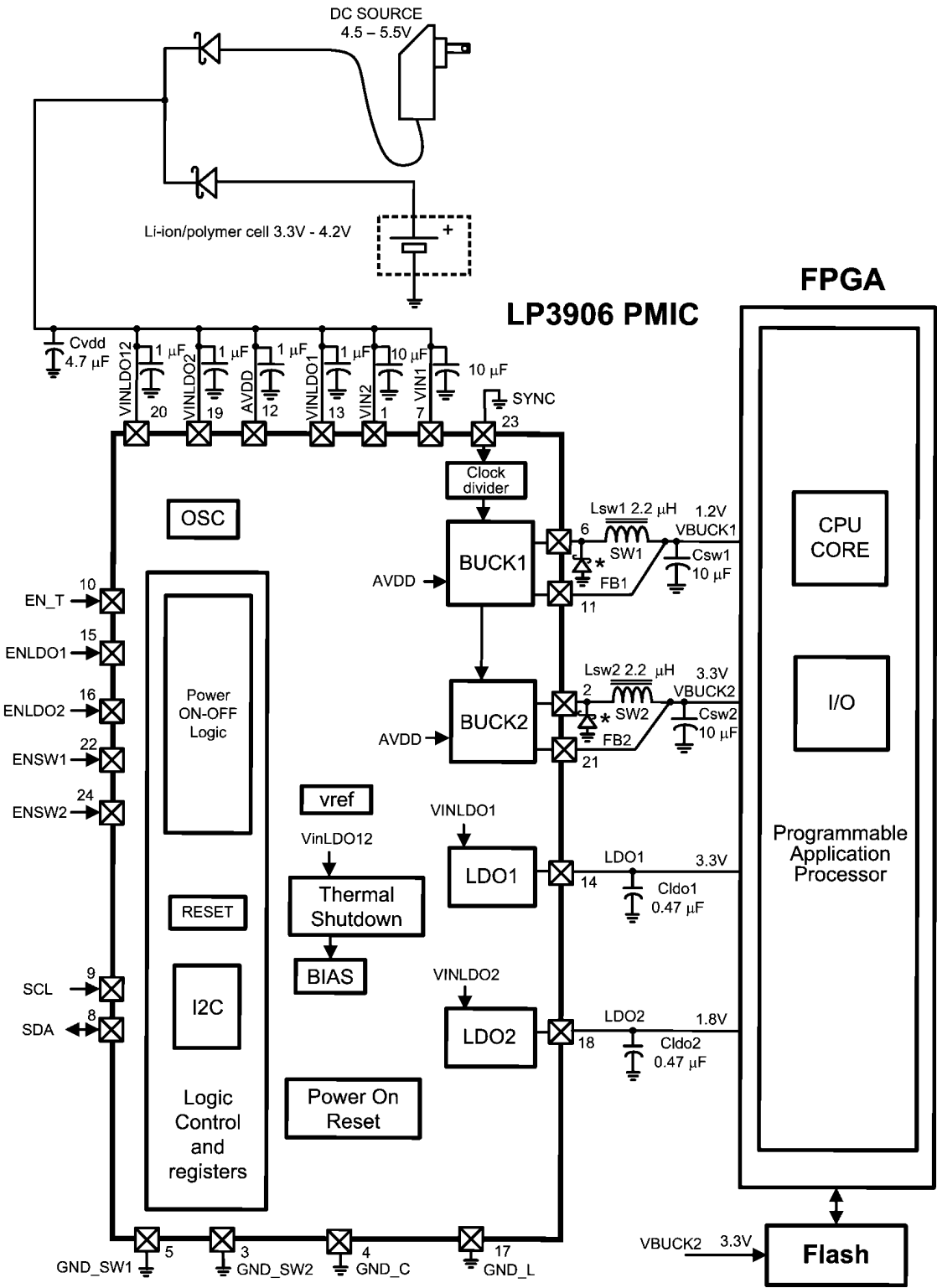
# Typical Application Circuit



**LP3906**

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FIGURE 1. Typical Application Circuit

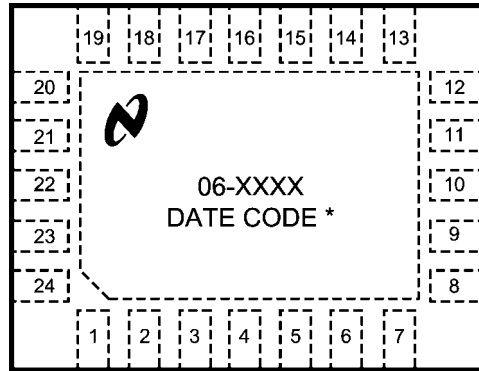


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\* For information about how schottky diodes can reduce noise in high load, high Vin applications, refer to "Buck Output Ripple Management" in the Application Notes section.

FIGURE 2. Typical Application Circuit

## Connection Diagram



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\* Refer to Package Marking in Ordering Information Table Below

**FIGURE 3. 24-Lead LLP Package (Top View)**

**Note:** The physical placement of the package marking will vary from part to part.

(\*) UZXYTT format: 'U' – wafer fab code; 'Z' – assembly code; 'XY' 2 digit date code; 'TT' – die run code

See [http://www.national.com/quality/marketing\\_conventions.html](http://www.national.com/quality/marketing_conventions.html) for more information on marking information.

## Ordering Information

Voltage Option	Order Number	Package Type	NSC Package Drawing	Package Marking	Supplied As
Voltage JXXI	LP3906SQ JXXI	24 lead LLP	SQA024AG	06-JXXI	1000 tape & reel
Voltage JXXI	LP3906SQX JXXI	24 lead LLP	SQA024AG	06-JXXI	4500 tape & reel
Voltage DJXI	LP3906SQ DJXI	24 lead LLP	SQA024AG	06-DJXI	1000 tape & reel
Voltage DJXI	LP3906SQX DJXI	24 lead LLP	SQA024AG	06-DJXI	4500 tape & reel
Voltage VPFP	LP3906SQ VPFP	24 lead LLP	SQA024AG	06-VPFP	1000 tape & reel
Voltage VPFP	LP3906SQX VPFP	24 lead LLP	SQA024AG	06-VPFP	4500 tape & reel
Voltage PPXP	LP3906SQ PPXP	24 lead LLP	SQA024AG	06-PPXP	1000 tape & reel
Voltage PPXP	LP3906SQX PPXP	24 lead LLP	SQA024AG	06-PPXP	4500 tape & reel

## Default Voltage Options

Regulator	Version JXXI	Version DJXI	Version VPFP	Version PPXP
	Default Voltages (V)	Default Voltages (V)	Default Voltages (V)	Default Voltages (V)
SW1	1.2	0.9	1.8	1.5
SW2	3.3	1.8	2.5	2.5
LDO1	3.3	3.3	1.5	3.3
LDO2	1.8	1.8	2.5	2.5

## Pin Descriptions

Pin	Pin Name	I/O	Type	Functional Description
1	VIN2	I	PWR	Power in from either DC source or Battery to Buck 2
2	SW2	O	PWR	Buck2 switcher output pin
3	GND_SW2	G	G	Buck2 NMOS Power Ground
4	GND_C	G	G	Non switching core ground pin
5	GND_SW1	G	G	Buck1 NMOS Power Ground
6	SW1	O	PWR	Buck1 switcher output pin
7	VIN1	I	PWR	Power in from either DC source or Battery to buck 1
8	SDA	I/O	D	I <sup>2</sup> C Data (Bidirectional)
9	SCL	I	D	I <sup>2</sup> C Clock
10	EN_T	I	D	Enable for preset power on sequence.
11	FB1	I	A	Buck1 input feedback terminal
12	AVDD	I	PWR	Analog Power for Buck converters.
13	VINLDO1	I	PWR	Power in from either DC source or Battery to input terminal of LDO1
14	LDO1	O	PWR	LDO1 Output
15	ENLDO1	I	D	LDO1 enable pin, a logic HIGH enables the LDO1
16	ENLDO2	I	D	LDO2 enable pin, a logic HIGH enables the LDO2
17	GND_L	G	G	LDO Ground
18	LDO2	O	PWR	LDO2 Output
19	VINLDO2	I	PWR	Power in from either DC source or battery to input terminal to LDO2
20	VinLDO12	I	PWR	Analog Power for Internal Functions (VREF, BIAS, I2C, Logic)
21	FB2	I	A	Buck2 input feedback terminal
22	ENSW1	I	D	Enable Pin for Buck1 switcher, a logic HIGH enables Buck1
23	SYNC	I	D	Frequency Synchronization pin which allows the user to connect an external clock signal PLL to synchronize the PMIC internal oscillator.
24	ENSW2	I	D	Enable Pin for Buck2 switcher, a logic HIGH enables Buck2

A: Analog Pin D: Digital Pin G: Ground Pin PWR: Power Pin I: Input Pin I/O: Input/Output Pin O: Output Pin

**Absolute Maximum Ratings** (Notes 1, 2)

If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/ Distributors for availability and specifications.

$V_{IN}$ , SDA, SCL	-0.3V to +6V
GND to GND SLUG	$\pm 0.3V$
Power Dissipation ( $P_{D\_MAX}$ ) ( $T_A=85^\circ C$ , $T_{MAX}=125^\circ C$ ,)(Note 5)	1.43 W
Junction Temperature ( $T_{J\_MAX}$ )	150°C
Storage Temperature Range	-65°C to +150°C
Maximum Lead Temperature (Soldering)	260°C

## ESD Ratings

Human Body Model (Note 4)

2 kV

**Operating Ratings** (Notes 1, 2, 7)**Bucks**

$V_{IN}$	2.7V to 5.5V
$V_{EN}$	0 to ( $V_{IN} + 0.3V$ )
Junction Temperature ( $T_J$ ) Range	-40°C to +125°C

Ambient Temperature ( $T_A$ ) Range (Note 6) -40°C to +85°C**Thermal Properties** (Notes 3, 5, 6)

Junction-to-Ambient Thermal Resistance

( $\theta_{JA}$ )SQA024AG

28°C/W

**Electrical Characteristics****General Electrical Characteristics** (Notes 1, 2, 7, 13)

Unless otherwise noted,  $V_{IN} = 3.6V$ . Typical values and limits appearing in normal type apply for  $T_J = 25^\circ C$ . Limits appearing in **boldface type** apply over the entire junction temperature range for operation, -40°C to +125°C.

Symbol	Parameter	Conditions	Min	Typ	Max	Units
$V_{POR}$	Power-On Reset Threshold	$V_{DD}$ Falling Edge		1.9		V
$T_{SD}$	Thermal Shutdown Threshold			160		°C
$T_{SDH}$	Thermal Shutdown Hysteresis			20		°C

**I<sup>2</sup>C Compatible Interface Electrical Specifications** (Note 13)

Unless otherwise noted,  $V_{IN} = 3.6V$ . Typical values and limits appearing in normal type apply for  $T_J = 25^\circ C$ . Limits appearing in **boldface type** apply over the entire junction temperature range for operation, -40°C to +125°C.

Symbol	Parameter	Conditions	Min	Typ	Max	Units
$F_{CLK}$	Clock Frequency				400	kHz
$t_{BF}$	Bus-Free Time Between Start and Stop	(Note 13)	1.3			$\mu s$
$t_{HOLD}$	Hold Time Repeated Start Condition	(Note 13)	0.6			$\mu s$
$t_{CLKLP}$	CLK Low Period	(Note 13)	1.3			$\mu s$
$t_{CLKHP}$	CLK High Period	(Note 13)	0.6			$\mu s$
$t_{SU}$	Set Up Time Repeated Start Condition	(Note 13)	0.6			$\mu s$
$t_{DATAHLD}$	Data Hold time	(Note 13)	0			$\mu s$
$t_{DATASU}$	Data Set Up Time	(Note 13)	100			ns
$T_{SU}$	Set Up Time for Start Condition	(Note 13)	0.6			$\mu s$
$T_{TRANS}$	Maximum Pulse Width of Spikes that Must be Suppressed by the Input Filter of Both DATA & CLK Signals.	(Note 13)		50		ns

## Low Drop Out Regulators, LDO1 and LDO2

Unless otherwise noted,  $V_{IN} = 3.6$ ,  $C_{IN} = 1.0 \mu\text{F}$ ,  $C_{OUT} = 0.47 \mu\text{F}$ . Typical values and limits appearing in normal type apply for  $T_J = 25^\circ\text{C}$ . Limits appearing in **boldface type** apply over the entire junction temperature range for operation,  $-40^\circ\text{C}$  to  $+125^\circ\text{C}$ . (Notes 2, 7, 8, 9, 10, 11, 12)

Symbol	Parameter	Conditions	Min	Typ	Max	Units
$V_{IN}$	Operational Voltage Range	VINLDO1 and VINLDO2 PMOS pins(Note 15)	<b>1.74</b>		<b>5.5</b>	V
$V_{OUT}$ Accuracy	Output Voltage Accuracy (Default $V_{OUT}$ )	Load current = 1 mA	<b>-3</b>		<b>3</b>	%
$\Delta V_{OUT}$	Line Regulation	$V_{IN} = (V_{OUT} + 0.3\text{V})$ to 5.0V, (Note 12), Load Current = 1 mA			<b>0.15</b>	%/V
	Load Regulation	$V_{IN} = 3.6\text{V}$ , Load Current = 1 mA to $I_{MAX}$			<b>0.011</b>	%/mA
$I_{SC}$	Short Circuit Current Limit	LDO1-2, $V_{OUT} = 0\text{V}$		500		mA
$V_{IN} - V_{OUT}$	Dropout Voltage	Load Current = 50 mA (Note 10)		25	<b>200</b>	mV
PSRR	Power Supply Ripple Rejection	$F = 10 \text{ kHz}$ , Load Current = $I_{MAX}$		45		dB
$\theta_n$	Supply Output Noise	$10 \text{ Hz} < F < 100 \text{ KHz}$		80		$\mu\text{Vrms}$
$I_Q$ (Notes 11, 14)	Quiescent Current "On"	$I_{OUT} = 0 \text{ mA}$		40		$\mu\text{A}$
	Quiescent Current "On"	$I_{OUT} = I_{MAX}$		60		$\mu\text{A}$
	Quiescent Current "Off"	EN is de-asserted(Note 16)		0.03		$\mu\text{A}$
$T_{ON}$	Turn On Time	Start up from shut-down		300		$\mu\text{s}$
$C_{OUT}$	Output Capacitor	Capacitance for stability $0^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$	<b>0.33</b>	0.47		$\mu\text{F}$
		$-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$	<b>0.68</b>	1.0		$\mu\text{F}$
		ESR	<b>5</b>		<b>500</b>	m $\Omega$

## Buck Converters SW1, SW2

Unless otherwise noted,  $V_{IN} = 3.6$ ,  $C_{IN} = 10 \mu\text{F}$ ,  $C_{OUT} = 10 \mu\text{F}$ ,  $L_{OUT} = 2.2 \mu\text{H}$  ceramic. Typical values and limits appearing in normal type apply for  $T_J = 25^\circ\text{C}$ . Limits appearing in **boldface type** apply over the entire junction temperature range for operation,  $-40^\circ\text{C}$  to  $+125^\circ\text{C}$ . (Notes 2, 7, 8, 9, 14)

Symbol	Parameter	Conditions	Min	Typ	Max	Units
$V_{OUT}$	Output Voltage Accuracy	Default $V_{OUT}$	<b>-3</b>		<b>+3</b>	%
	Line Regulation	$2.7 < V_{IN} < 5.5$ $I_O = 10 \text{ mA}$		0.089		%/V
	Load Regulation	$100 \text{ mA} < I_O < I_{MAX}$		0.0013		%/mA
Eff	Efficiency	Load Current = 250 mA		96		%
$I_{SHDN}$	Shutdown Supply Current	EN is de-asserted		0.01		$\mu\text{A}$
$f_{OSC}$	Sync Mode Clock Frequency	Synchronized from 13 MHz system clock		2.0		MHz
	Internal Oscillator Frequency			2.0		MHz
$I_{PEAK}$	Peak Switching Current Limit			2.0		A
$I_Q$ (Note 14)	Quiescent Current "On"	No load PFM Mode		33		$\mu\text{A}$
$R_{DSON} (P)$	Pin-Pin Resistance PFET			200		m $\Omega$
$R_{DSON} (N)$	Pin-Pin Resistance NFET			180		m $\Omega$
$T_{ON}$	Turn On Time	Start up from shut-down		500		$\mu\text{s}$
$C_{IN}$	Input Capacitor	Capacitance for stability	10			$\mu\text{F}$
$C_O$	Output Capacitor	Capacitance for stability	10			$\mu\text{F}$

## IO Electrical Characteristics

Unless otherwise noted: Typical values and limits appearing in normal type apply for  $T_J = 25^\circ\text{C}$ . Limits appearing in **boldface type** apply over the entire junction temperature range for operation,  $T_J = 0^\circ\text{C}$  to  $+125^\circ\text{C}$ . (Note 13)

Symbol	Parameter	Conditions	Limit		Units
			Min	Max	
$V_{IL}$	Input Low Level			<b>0.4</b>	V
$V_{IH}$	Input High Level		<b>1.2</b>		V

**Note 1:** Absolute Maximum Ratings indicate limits beyond which damage to the component may occur. Operating Ratings are conditions under which operation of the device is guaranteed. Operating Ratings do not imply guaranteed performance limits. For guaranteed performance limits and associated test conditions, see the Electrical Characteristics.

**Note 2:** All voltages are with respect to the potential at the GND pin.

**Note 3:** Internal thermal shutdown circuitry protects the device from permanent damage. Thermal shutdown engages at  $T_J = 160^\circ\text{C}$  (typ.) and disengages at  $T_J = 140^\circ\text{C}$  (typ.)

**Note 4:** The Human body model is a 100 pF capacitor discharged through a 1.5 k $\Omega$  resistor into each pin. (MILSTD - 883 3015.7)

**Note 5:** In applications where high power dissipation and/or poor package thermal resistance is present, the maximum ambient temperature may have to be derated. Maximum ambient temperature ( $T_{A-MAX}$ ) is dependent on the maximum operating junction temperature ( $T_{J-MAX-OP} = 125^\circ\text{C}$ ), the maximum power dissipation of the device in the application ( $P_{D-MAX}$ ), and the junction-to-ambient thermal resistance of the part/package in the application ( $\theta_{JA}$ ), as given by the following equation:  $T_{A-MAX} = T_{J-MAX-OP} - (\theta_{JA} \times P_{D-MAX})$ . See applications section.

**Note 6:** Junction-to-ambient thermal resistance is highly application and board-layout dependent. In applications where high maximum power dissipation exists, special care must be paid to thermal dissipation issues in board design.

**Note 7:** Min and Max limits are guaranteed by design, test, or statistical analysis. Typical numbers are not guaranteed, but do represent the most likely norm.

**Note 8:**  $C_{IN}$ ,  $C_{OUT}$ : Low-ESR Surface-Mount Ceramic Capacitors (MLCCs) used in setting electrical characteristics.

**Note 9:** The device maintains a stable, regulated output voltage without a load.

**Note 10:** Dropout voltage is the voltage difference between the input and the output at which the output voltage drops to 100 mV below its nominal value.

**Note 11:** Quiescent current is defined here as the difference in current between the input voltage source and the load at  $V_{OUT}$ .

**Note 12:**  $V_{IN}$  minimum for line regulation values is 1.8V.

**Note 13:** This specification is guaranteed by design.

**Note 14:** The  $I_q$  can be defined as the standing current of the LP3906 when the I2C bus is active and all other power blocks have been disabled via the I2C bus, or it can be defined as the I2C bus active, and the other power blocks are active under no load condition. These two values can be used by the system designer when the LP3906 is powered using a battery. If the user plans to use the HW enable pins to disable each block of the IC please contact the factory applications for IQ details.

**Note 15:** Pins 13, 19 can operate from  $V_{in}$  min of 1.74 to a  $V_{in}$  max of 5.5V this rating is only for the series pass pmos power fet. It allows the system design to use a lower voltage rating if the input voltage comes from a buck output.

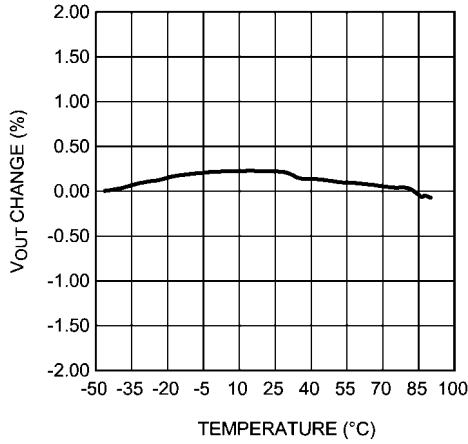
**Note 16:** The  $I_q$  exhibits a higher current draw when the EN pin is de-asserted because the I2C buffer pins draw an additional 2 $\mu\text{A}$



# Typical Performance Characteristics — LDO

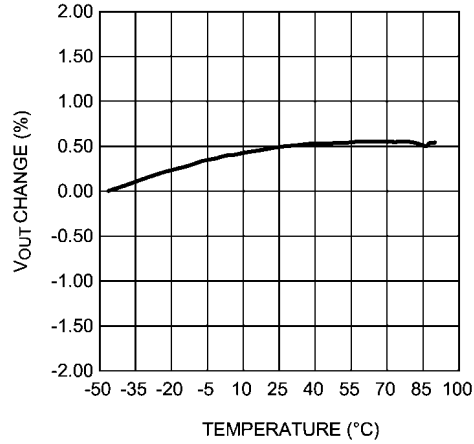
$T_A = 25^\circ\text{C}$  unless otherwise noted

**Output Voltage Change vs Temperature (LDO1)**  
 $V_{in} = 4.3\text{V}$ ,  $V_{out} = 3.3\text{V}$ , 100 mA load



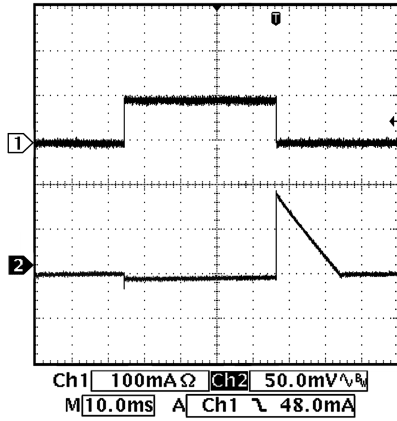
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**Output Voltage Change vs Temperature (LDO2)**  
 $V_{in} = 4.3\text{V}$ ,  $V_{out} = 1.8\text{V}$ , 100 mA load



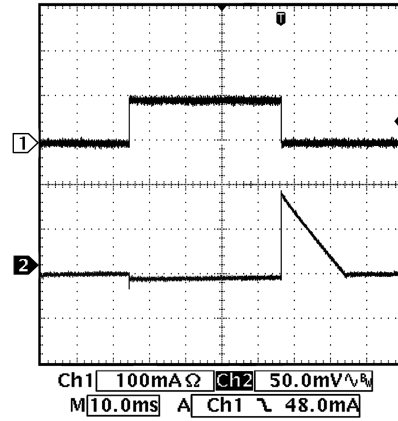
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**Load Transient (LDO1)**  
 $3.6\text{V}$   $V_{in}$ ,  $3.3\text{V}$   $V_{out}$ , 0 – 100 mA load



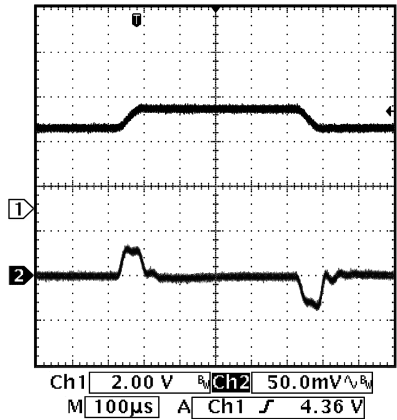
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**Load Transient (LDO2)**  
 $3.6\text{V}$   $V_{in}$ ,  $1.8\text{V}$   $V_{out}$ , 0 – 100 mA load



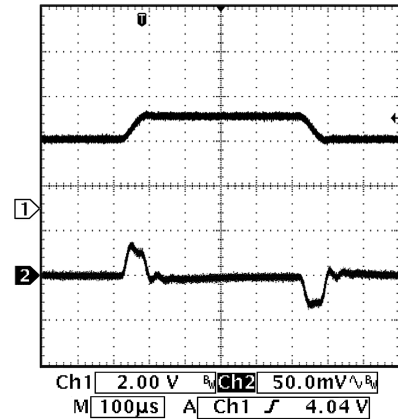
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**Line Transient (LDO1)**  
 $3.6 - 4.5\text{V}$   $V_{in}$ ,  $3.3\text{V}$   $V_{out}$ , 150 mA load



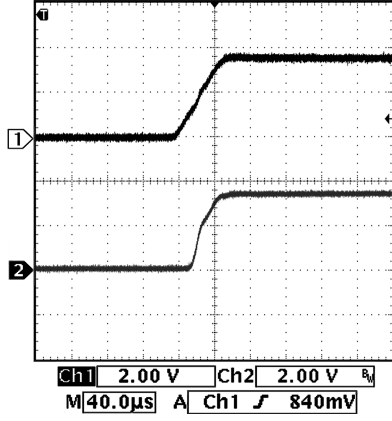
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**Line Transient (LDO2)**  
 $3 - 4.2\text{V}$   $V_{in}$ ,  $1.8\text{V}$   $V_{out}$ , 150 mA load



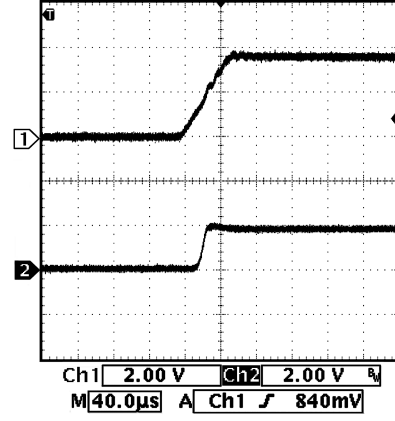
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Enable Start-up time (LDO1 )  
0-3.6 Vin, 3.3 Vout, 1mA load



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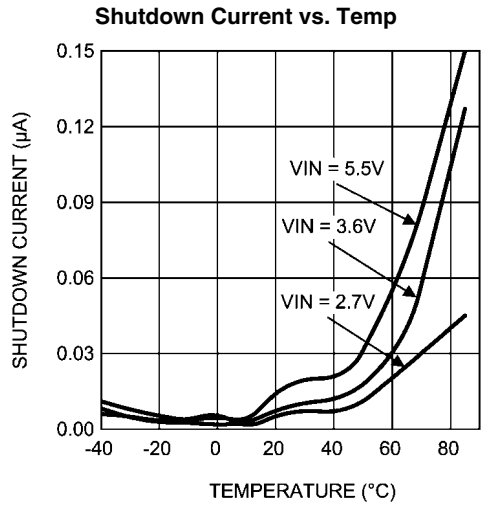
Enable Start-up time (LDO2)  
0 - 3.6 Vin, 1.8 Vout, 1 mA load



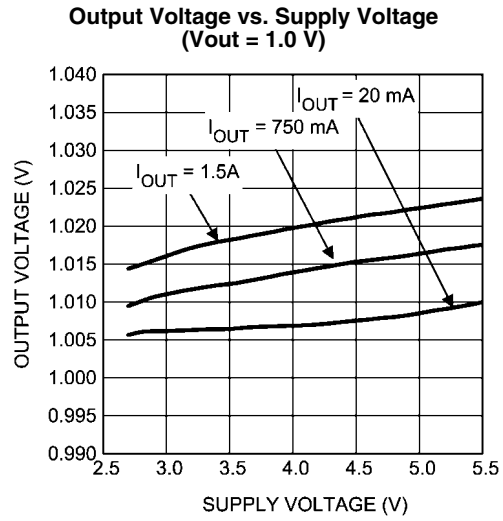
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# Typical Performance Characteristics — Buck

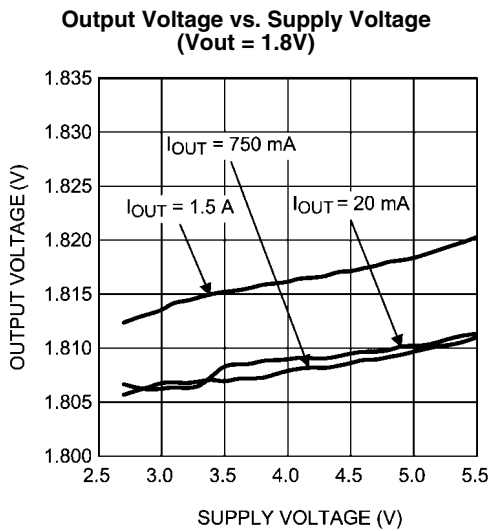
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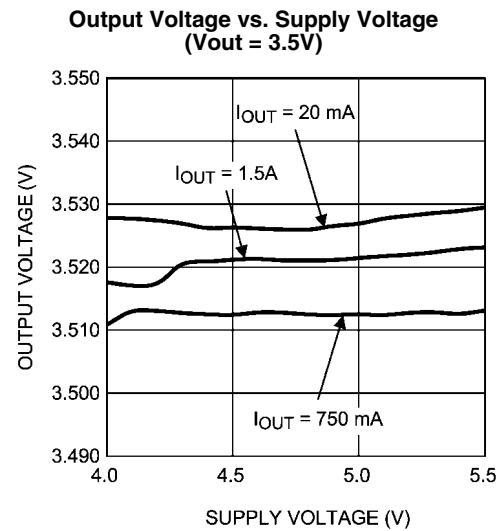
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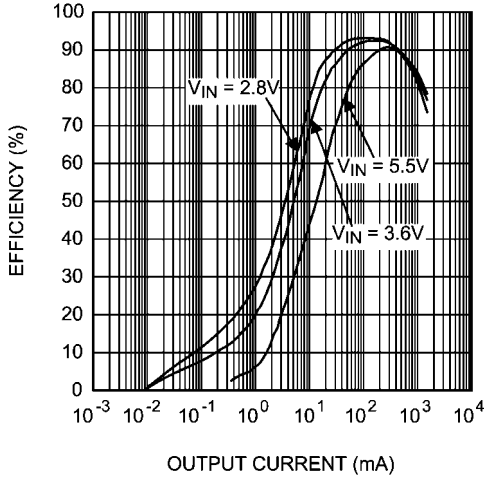


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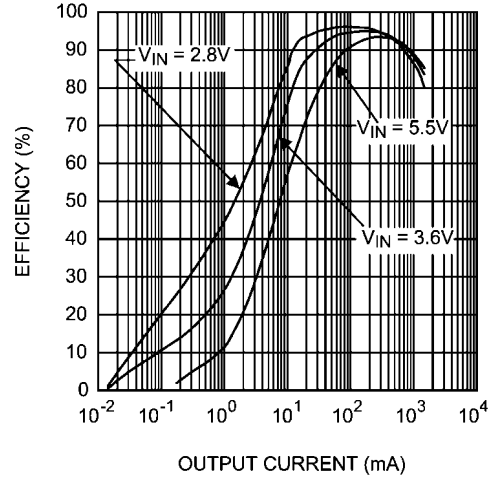
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**Buck 1 Efficiency vs Output Current  
(Forced PWM Mode,  $V_{out} = 1.2V$ ,  $L = 2.2\mu H$ )**



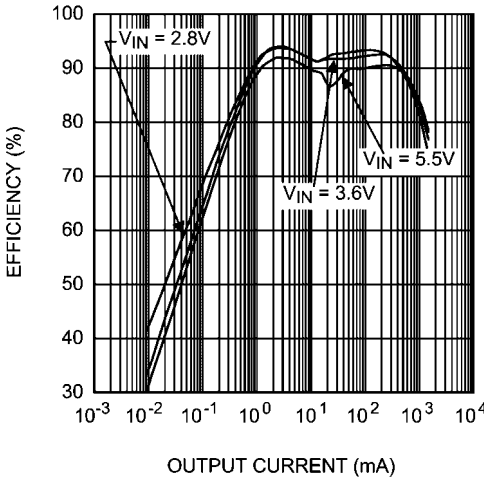
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**Buck 1 Efficiency vs Output Current  
(Forced PWM Mode,  $V_{out} = 2.0V$ ,  $L = 2.2\mu H$ )**



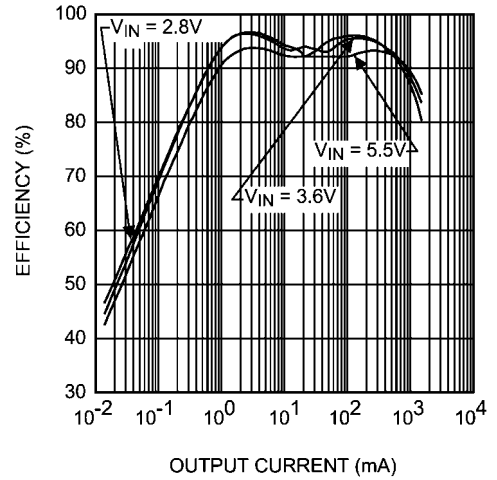
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**Buck 1 Efficiency vs Output Current  
(PFM to PWM mode,  $V_{out} = 1.2V$ ,  $L = 2.2\mu H$ )**



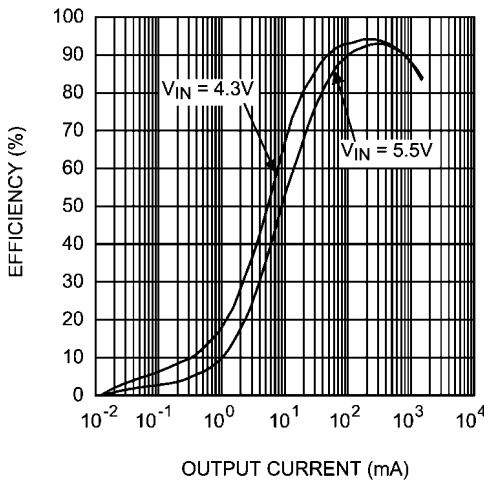
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**Buck 1 Efficiency vs Output Current  
(PFM to PWM mode,  $V_{out} = 2.0V$ ,  $L = 2.2\mu H$ )**



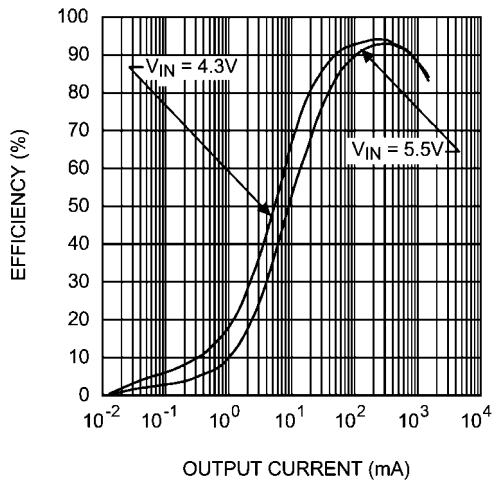
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**Buck 2 Efficiency vs Output Current  
(Forced PWM Mode,  $V_{out} = 1.8V$ ,  $L = 2.2\mu H$ )**



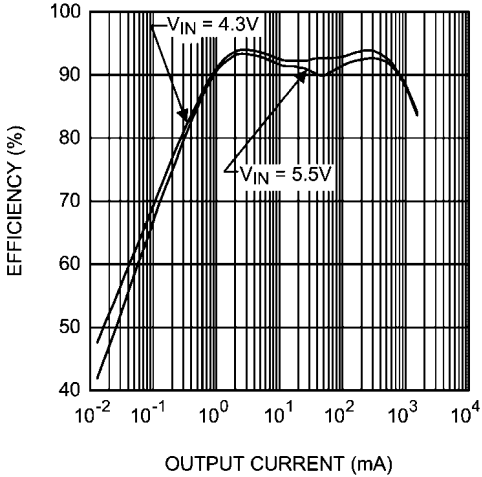
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**Buck 2 Efficiency vs Output Current  
(Forced PWM Mode,  $V_{out} = 3.3V$ ,  $L = 2.2\mu H$ )**



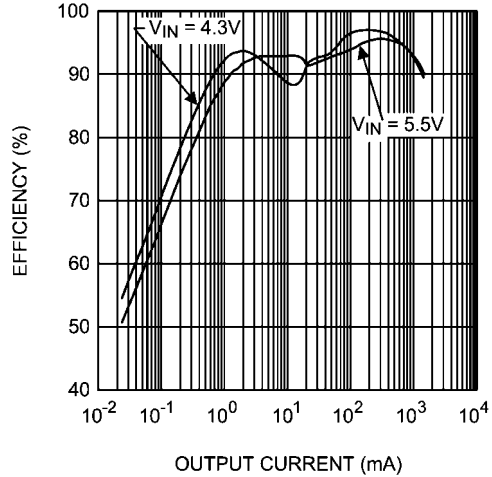
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**Buck 2 Efficiency vs Output Current  
(PFM to PWM Mode,  $V_{out}=1.8V$ ,  $L=2.2\mu H$ )**



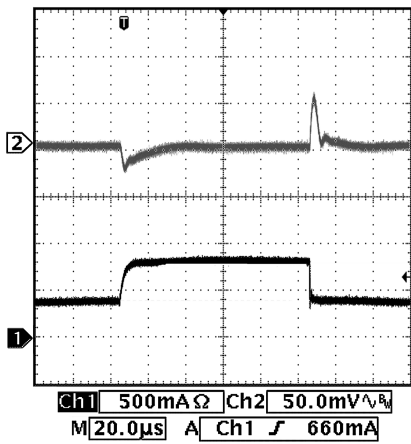
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**Buck 2 Efficiency vs Output Current  
(PFM to PWM Mode,  $V_{out}=3.3V$ ,  $L=2.2\mu H$ )**



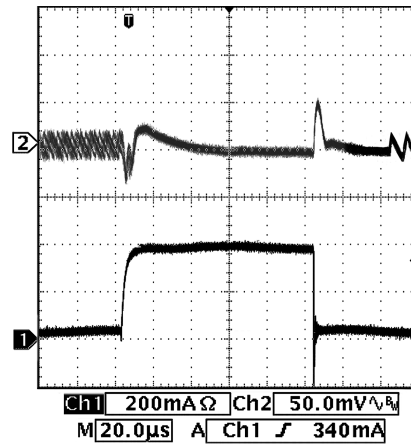
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**Load Transient Response  
 $V_{out} = 1.2V$  (PWM Mode)**



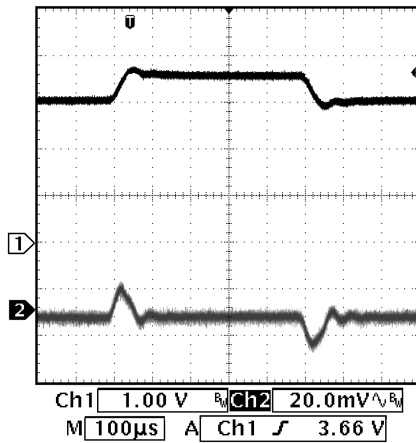
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**Mode Change by Load Transient  
 $V_{out} = 1.2V$  (PWM to PFM)**



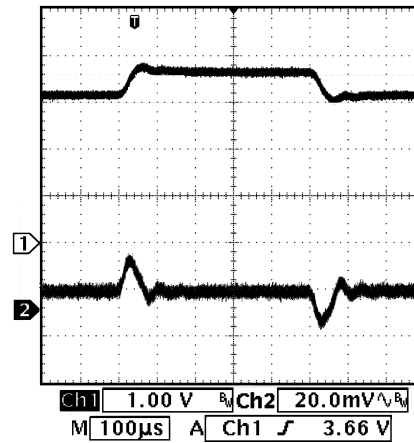
20197856

**Line Transient Response  
 $V_{in} = 3 - 3.6V$ ,  $V_{out} = 1.2V$ , 250 mA load**



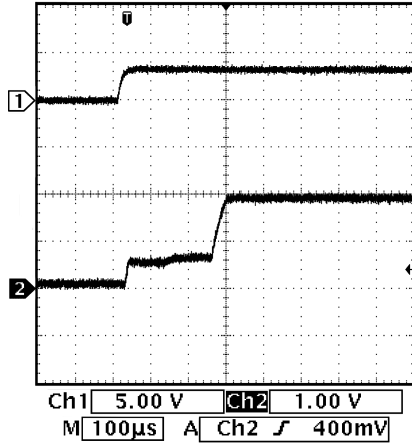
20197857

**Line Transient Response  
 $V_{in} = 3 - 3.6V$ ,  $V_{out} = 3.3V$ , 250 mA load**



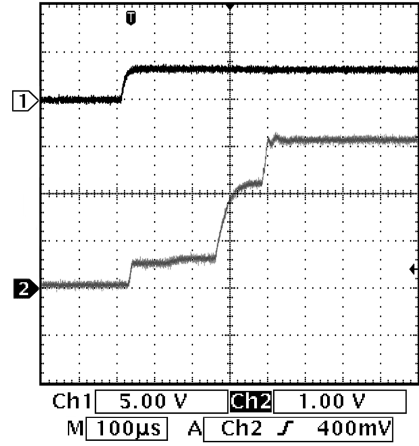
20197858

Start up into PWM Mode  
Vout = 1.8 V, 1.2 A load



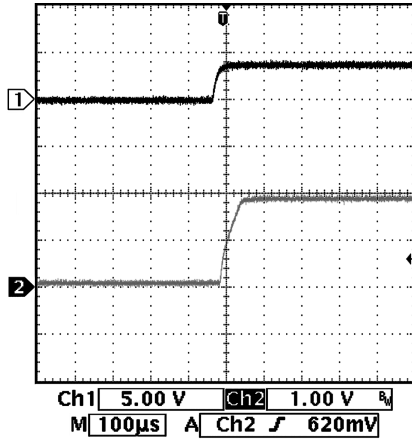
20197859

Start up into PWM Mode  
Vout = 3.3 V, 1.2 A load



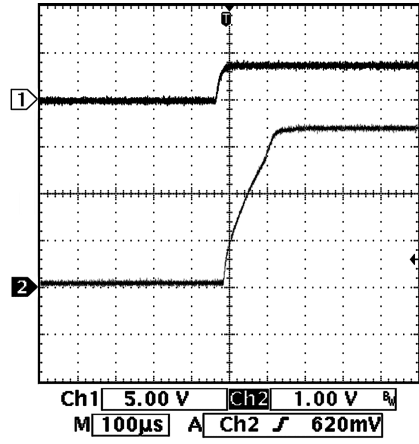
20197860

Start up into PFM Mode  
Vout = 1.8 V, 30 mA load



20197861

Start up into PFM Mode  
Vout = 3.3 V, 30 mA load



20197862

# DC/DC Converters

## OVERVIEW

The LP3906 supplies the various power needs of the application by means of two Linear Low Drop Regulators LDO1 and LDO2 and two Buck converters SW1 and SW2. The table here under lists the output characteristics of the various regulators.

### SUPPLY SPECIFICATION

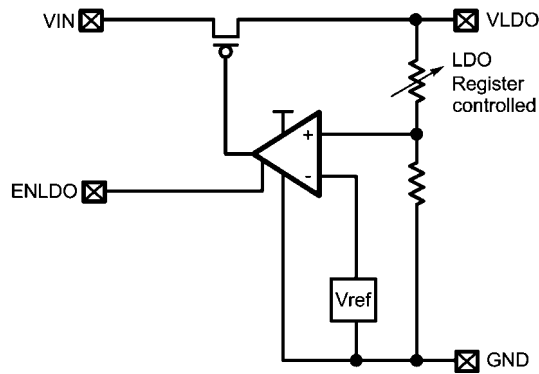
Supply	Load	Output		
		V <sub>OUT</sub> Range(V)	Resolution (mV)	I <sub>MAX</sub> Maximum Output Current (mA)
LDO1	analog	1.0 to 3.5	100	300
LDO2	analog	1.0 to 3.5	100	300
SW1	digital	0.8 to 2.0	50	1500
SW2	digital	1.0 to 3.5	100	1500

\*For default values of the regulators, please consult Default Voltage Options Table page 3

### LINEAR LOW DROP-OUT REGULATORS (LDOS)

LDO1 and LDO2 are identical linear regulators targeting analog loads characterized by low noise requirements. LDO1 and LDO2 are enabled through the ENLDO pin or through the corresponding LDO1 or LDO2 control register. The output

voltages of both LDOs are register programmable. The default output voltages are factory programmed during Final Test, which can be tailored to the specific needs of the system designer.



### NO-LOAD STABILITY

The LDOs will remain stable and in regulation with no external load. This is an important consideration in some circuits, for example CMOS RAM keep-alive applications.

### LDO1 AND LDO2 CONTROL REGISTERS

LDO1 and LDO2 can be configured by means of the LDO1 and LDO2 control registers. The output voltage is pro-

grammable in steps of 100mV from 1.0V to 3.5V by programming bits D4-0 in the LDO Control registers. Both LDO1 and LDO2 are enabled by applying a logic 1 to the ENLDO1 and ENLDO2 pin. Enable/disable control is also provided through enable bit of the LDO1 and LDO2 control registers. The value of the enable LDO bit in the register is logic 1 by default. The output voltage can be altered while the LDO is enabled.

## SW1, SW2: Synchronous Step Down Magnetic DC/DC Converters

### FUNCTIONAL DESCRIPTION

The LP3906 incorporates two high efficiency synchronous switching buck regulators, SW1 and SW2 that deliver a constant voltage from a single Li-Ion battery to the portable system processors. Using a voltage mode architecture with synchronous rectification, both bucks have the ability to deliver up to 1500mA depending on the input voltage and output voltage (voltage head room), and the inductor chosen (maximum current capability).

There are three modes of operation depending on the current required - PWM, PFM, and shutdown. PWM mode handles current loads of approximately 70mA or higher, delivering voltage precision of +/-3% with 90% efficiency or better. Lighter output current loads cause the device to automatically switch into PFM for reduced current consumption ( $I_Q = 15 \mu\text{A}$  typ.) and a longer battery life. The Standby operating mode turns off the device, offering the lowest current consumption. PWM or PFM mode is selected automatically or PWM mode can be forced through the setting of the buck control register.

Both SW1 and SW2 can operate up to a 100% duty cycle (PMOS switch always on) for low drop out control of the output voltage. In this way the output voltage will be controlled down to the lowest possible input voltage.

Additional features include soft-start, under-voltage lock-out, current overload protection, and thermal overload protection.

### CIRCUIT OPERATION DESCRIPTION

A buck converter contains a control block, a switching PFET connected between input and output, a synchronous rectifying NFET connected between the output and ground (BCK-GND pin) and a feedback path. During the first portion of each switching cycle, the control block turns on the internal PFET switch. This allows current to flow from the input through the inductor to the output filter capacitor and load. The inductor limits the current to a ramp with a slope of

$$\frac{V_{IN} - V_{OUT}}{L}$$

by storing energy in a magnetic field. During the second portion of each cycle, the control block turns the PFET switch off, blocking current flow from the input, and then turns the NFET synchronous rectifier on. The inductor draws current from ground through the NFET to the output filter capacitor and load, which ramps the inductor current down with a slope of

$$\frac{-V_{OUT}}{L}$$

The output filter stores charge when the inductor current is high, and releases it when low, smoothing the voltage across the load.

### PWM OPERATION

During PWM operation the converter operates as a voltage-mode controller with input voltage feed forward. This allows the converter to achieve excellent load and line regulation. The DC gain of the power stage is proportional to the input voltage. To eliminate this dependence, feed forward voltage inversely proportional to the input voltage is introduced.

### INTERNAL SYNCHRONOUS RECTIFICATION

While in PWM mode, the buck uses an internal NFET as a synchronous rectifier to reduce rectifier forward voltage drop and associated power loss. Synchronous rectification provides a significant improvement in efficiency whenever the output voltage is relatively low compared to the voltage drop across an ordinary rectifier diode.

### CURRENT LIMITING

A current limit feature allows the converter to protect itself and external components during overload conditions. PWM mode implements current limiting using an internal comparator that trips at 2.0 A (typ). If the output is shorted to ground the device enters a timed current limit mode where the NFET is turned on for a longer duration until the inductor current falls below a low threshold, ensuring inductor current has more time to decay, thereby preventing runaway.

A current limit feature allows the buck to protect itself and external components during overload conditions PWM mode implements cycle-by-cycle current limiting using an internal comparator that trips at 2000mA (typical).

### PFM OPERATION

At very light loads, the converter enters PFM mode and operates with reduced switching frequency and supply current to maintain high efficiency.

The part will automatically transition into PFM mode when either of two conditions occurs for a duration of 32 or more clock cycles:

- A. The inductor current becomes discontinuous
- or
- B. The peak PMOS switch current drops below the  $I_{MODE}$  level

$$\left( \text{Typically } I_{MODE} < 66 \text{ mA} + \frac{V_{IN}}{160\Omega} \right)$$

During PFM operation, the converter positions the output voltage slightly higher than the nominal output voltage during PWM operation, allowing additional headroom for voltage drop during a load transient from light to heavy load. The PFM comparators sense the output voltage via the feedback pin and control the switching of the output FETs such that the output voltage ramps between 0.8% and 1.6% (typical) above the nominal PWM output voltage. If the output voltage is below the 'high' PFM comparator threshold, the PMOS power switch is turned on. It remains on until the output voltage exceeds the 'high' PFM threshold or the peak current exceeds the  $I_{PFM}$  level set for PFM mode. The typical peak current in PFM mode is:

$$I_{PFM} = 66 \text{ mA} + \frac{V_{IN}}{80\Omega}$$

Once the PMOS power switch is turned off, the NMOS power switch is turned on until the inductor current ramps to zero. When the NMOS zero-current condition is detected, the NMOS power switch is turned off. If the output voltage is below the 'high' PFM comparator threshold (see figure below), the PMOS switch is again turned on and the cycle is repeated until the output reaches the desired level. Once the output reaches the 'high' PFM threshold, the NMOS switch is turned on briefly to ramp the inductor current to zero and then both output switches are turned off and the part enters an ex-



tremely low power mode. Quiescent supply current during this 'sleep' mode is less than 30  $\mu$ A, which allows the part to achieve high efficiencies under extremely light load conditions. When the output drops below the 'low' PFM threshold, the cycle repeats to restore the output voltage to  $\sim 1.6\%$  above the nominal PWM output voltage.

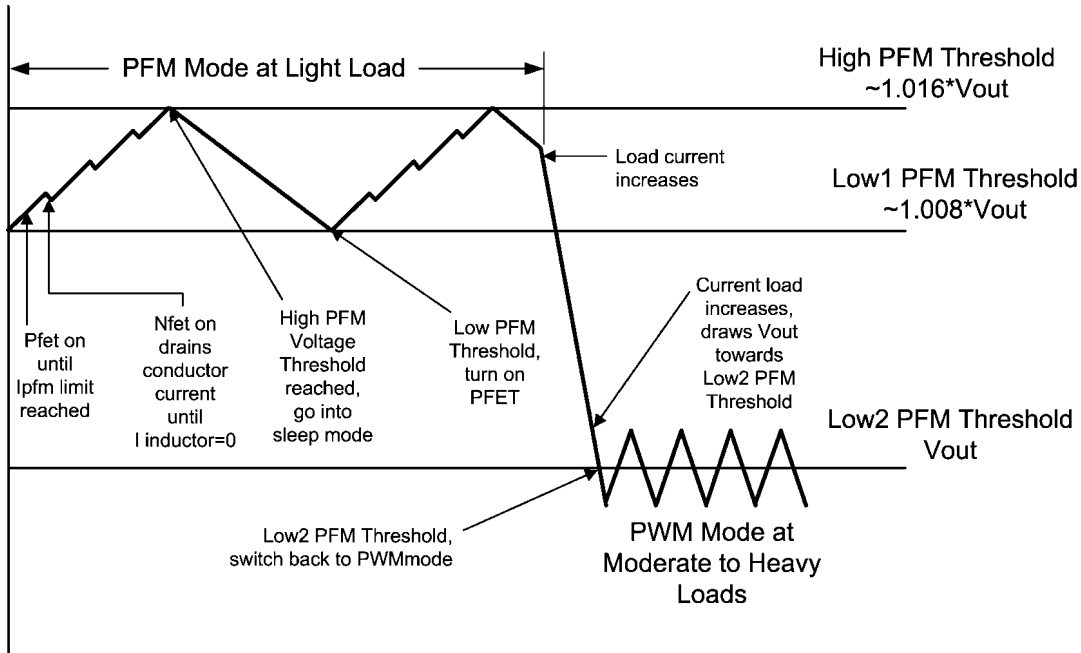
If the load current should increase during PFM mode (see figure below) causing the output voltage to fall below the 'low2' PFM threshold, the part will automatically transition into fixed-frequency PWM mode.

**SW1, SW2 OPERATION**

SW1 and SW2 have selectable output voltages ranging from 0.8V to 3.5V (typ.). Both SW1 and SW2 in the LP3906 are I<sup>2</sup>C register controlled and are enabled by default through the

internal state machine of the LP3906 following a Power-On event that moves the operating mode to the Active state. (see Power On Sequence). The SW1 and SW2 output voltages revert to default values when the power on sequence has been completed. The default output voltage for each buck converter is factory programmable. (See Application Notes). SW1, SW2 can be enabled/disabled through the corresponding control register.

The Modulation mode PWM/PFM is by default automatic and depends on the load as described above in the functional description. The modulation mode can be overridden by setting I<sup>2</sup>C bit to a logic 1 in the corresponding buck control register, forcing the buck to operate in PWM mode regardless of the load condition.



**SHUTDOWN MODE**

During shutdown the PFET switch, reference, control and bias circuitry of the converters are turned off. The NFET switch will be on in shutdown to discharge the output. When the converter is enabled, soft start is activated. It is recommended to disable the converter during the system power up and under voltage conditions when the supply is less than 2.8V.

**SOFT START**

The soft-start feature allows the power converter to gradually reach the initial steady state operating point, thus reducing start-up stresses and surges. The two LP3906 buck converters have a soft-start circuit that limits in-rush current during start-up. During start-up the switch current limit is increased in steps. Soft start is activated only if EN goes from logic low to logic high after VIN reaches 2.8V. Soft start is implemented by increasing switch current limit in steps of 213 mA, 425 mA, 850 mA and 1700 mA (typ. Switch current limit). The start-up time thereby depends on the output capacitor and load current demanded at start-up.

**LOW DROPOUT OPERATION**

The LP3906 can operate at 100% duty cycle (noswitching; PMOS switch completely on) for low drop out support of the output voltage. In this way the output voltage will be controlled

down to the lowest possible input voltage. When the device operates near 100% duty cycle, output voltage ripple is approximately 25 mV. The minimum input voltage needed to support the output voltage is

$$V_{IN, MIN} = I_{LOAD} * (R_{DSON, PFET} + R_{INDUCTOR}) + V_{OUT}$$

- $I_{LOAD}$  Load current
- $R_{DSON, PFET}$  Drain to source resistance of PFET switch in the triode region
- $R_{INDUCTOR}$  Inductor resistance

**FLEXIBLE POWER SEQUENCING OF MULTIPLE POWER SUPPLIES**

The LP3906 provides several options for power on sequencing. The two bucks can be individually controlled with ENSW1 and ENSW2. The two LDOs can also be individually controlled with ENLDO1 and ENLDO2.

If the user desires a set power on sequence, all four enables should be tied LOW so that the regulators don't automatically enable when power is supplied. The user can then program the chip through I<sup>2</sup>C and raise EN\_T from LOW to HIGH to activate the power on sequencing.

**POWER ON**

EN\_T assertion causes the LP3906 to emerge from Standby mode to Full Operation mode at a preset timing sequence. By default, the enables for the LDOs and Bucks are internally pulled up, which causes the part to turn ON automatically. If the user wishes to have a preset timing sequence to power on the regulators, the external regulator enables must be tied LOW. Otherwise, simply tie the enables of each specific regulator HIGH.

EN\_T is edge triggered with rising edge signaling the chip to power on. The EN\_T input is deglitched and the default is set at 1 ms. As shown in the next 2 diagrams, a rising EN\_T edge will start a power on sequence, while a falling EN\_T edge will start a shutdown sequence. If EN\_T is high, toggling the external enables of the regulators will have no effect on the chip.

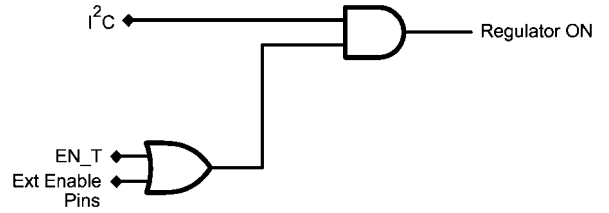
**Default Power ON Sequence:**

t <sub>1</sub> (ms)	t <sub>2</sub> (ms)	t <sub>3</sub> (ms)	t <sub>4</sub> (ms)
1.5	2.0	3	6

**Note:** LP3906 The default Power on delays can be reprogrammed at final test or by using I<sup>2</sup>C registers to 1, 1.5, 2, 3, 6, or 11 ms.

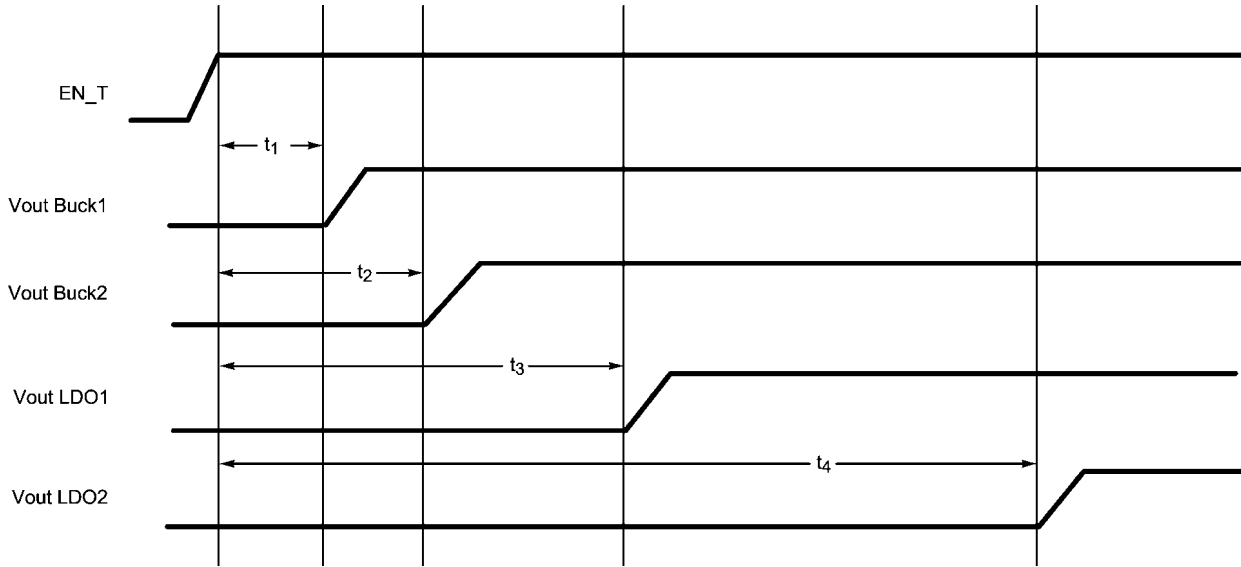
The regulators can also be programmed through I<sup>2</sup>C to turn on and off. By default, the I<sup>2</sup>C enables for the regulators are ON.

The regulators are on following the pattern below:  
 Regulators on = (I<sup>2</sup>C enable) AND (External pin enable OR EN\_T high).



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## LP3906 Default Power-Up Sequence



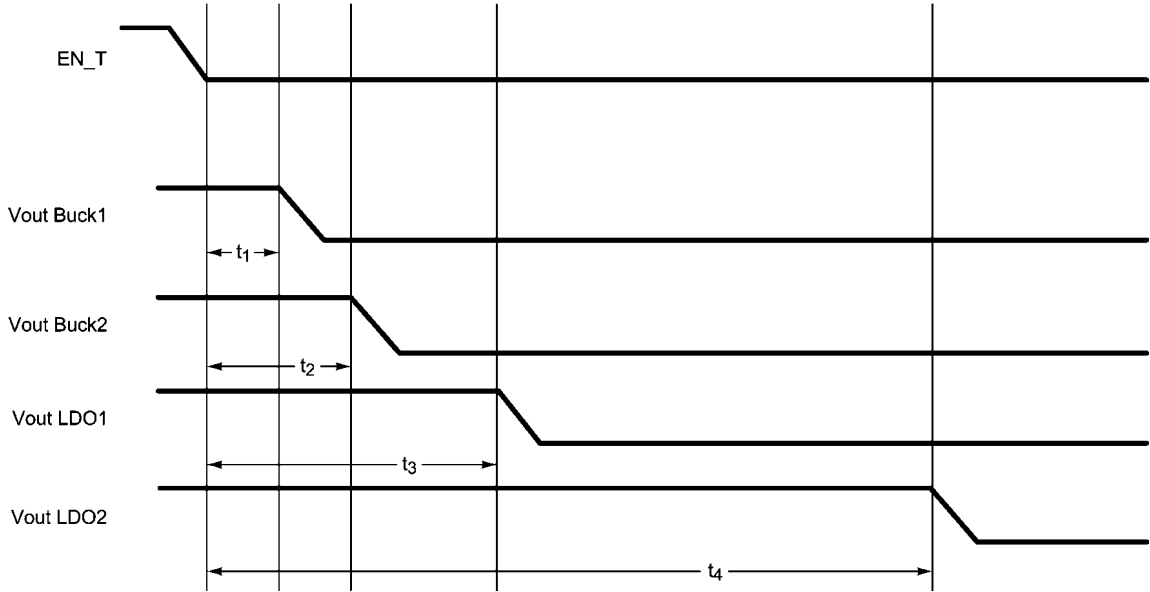
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## Power-On Timing Specification

Symbol	Description	Min	Typ	Max	Units
$t_1$	Programmable Delay from EN_T assertion to $V_{CC}$ -Buck1 On		1.5		ms
$t_2$	Programmable Delay from EN_T assertion to $V_{CC}$ -Buck2 On		2		ms
$t_3$	Programmable Delay from EN_T assertion to $V_{CC}$ -LDO1 On		3		ms
$t_4$	Programmable Delay from EN_T assertion to $V_{CC}$ -LDO2 On		6		ms

**Note:** LP3906 The default Power on delays can be reprogrammed at final test or I<sup>2</sup>C to 1, 1.5, 2, 3, 6, or 11 ms.

## LP3906 Default Power-Off Sequence



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Symbol	Description	Min	Typ	Max	Units
$t_1$	Programmable Delay from EN_T deassertion to $V_{CC\_Buck1}$ Off		1.5		ms
$t_2$	Programmable Delay from EN_T deassertion to $V_{CC\_Buck2}$ Off		2		ms
$t_3$	Programmable Delay from EN_T deassertion to $V_{CC\_LDO1}$ Off		3		ms
$t_4$	Programmable Delay from EN_T deassertion to $V_{CC\_LDO2}$ Off		6		ms

**Note:** LP3906 The default Power on delays can be reprogrammed at final test to 0, .5, 1, 2, 5, or 10 ms. Default setting is the same as the on sequence.

### Power-On-Reset

The LP3906 is equipped with an internal Power-On-Reset (“POR”) circuit that will reset the logic when  $V_{DD} < V_{POR}$ . This guarantees that the logic is properly initialized when  $V_{DD}$  ris-

es above the minimum operating voltage of the Logic and the internal oscillator that clocks the Sequential Logic in the Control section.

## I<sup>2</sup>C Compatible Serial Interface

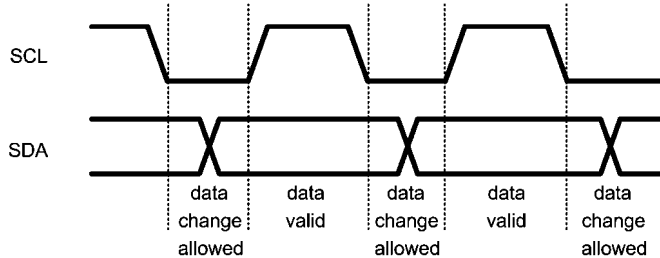
### I<sup>2</sup>C SIGNALS

The LP3906 features an I<sup>2</sup>C compatible serial interface, using two dedicated pins: SCL and SDA for I<sup>2</sup>C clock and data respectively. Both signals need a pull-up resistor according to the I<sup>2</sup>C specification. The LP3906 interface is an I<sup>2</sup>C slave that is clocked by the incoming SCL clock.

Signal timing specifications are according to the I<sup>2</sup>C bus specification. The maximum bit rate is 400 kbit/s. See I<sup>2</sup>C specification from Philips for further details.

### I<sup>2</sup>C DATA VALIDITY

The data on the SDA line must be stable during the HIGH period of the clock signal (SCL), e.g. - the state of the data line can only be changed when CLK is LOW.



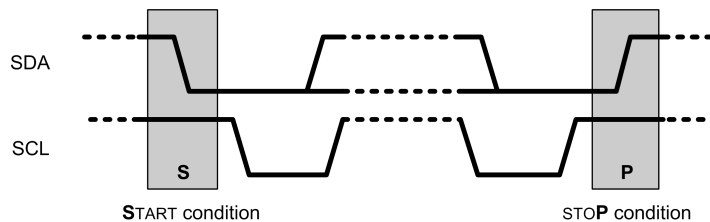
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### I<sup>2</sup>C Signals: Data Validity

### I<sup>2</sup>C START AND STOP CONDITIONS

START and STOP bits classify the beginning and the end of the I<sup>2</sup>C session. START condition is defined as the SDA signal transitioning from HIGH to LOW while the SCL line is HIGH. STOP condition is defined as the SDA transitioning from LOW to HIGH while the SCL is HIGH. The I<sup>2</sup>C master

always generates START and STOP bits. The I<sup>2</sup>C bus is considered to be busy after START condition and free after STOP condition. During data transmission, I<sup>2</sup>C master can generate repeated START conditions. First START and repeated START conditions are equivalent, function-wise.



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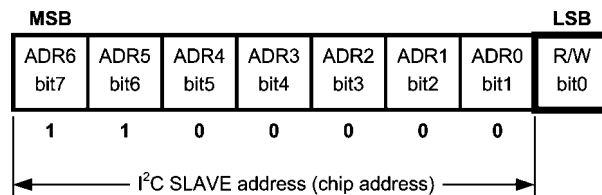
### START and STOP Conditions

### TRANSFERRING DATA

Every byte put on the SDA line must be eight bits long, with the most significant bit (MSB) being transferred first. Each byte of data has to be followed by an acknowledge bit. The acknowledged related clock pulse is generated by the master. The transmitter releases the SDA line (HIGH) during the acknowledge clock pulse. The receiver must pull down the SDA line during the 9th clock pulse, signifying acknowledgement. A receiver which has been addressed must generate an acknowledgement ("ACK") after each byte has been received. After the START condition, the I<sup>2</sup>C master sends a chip address. This address is seven bits long followed by an eighth

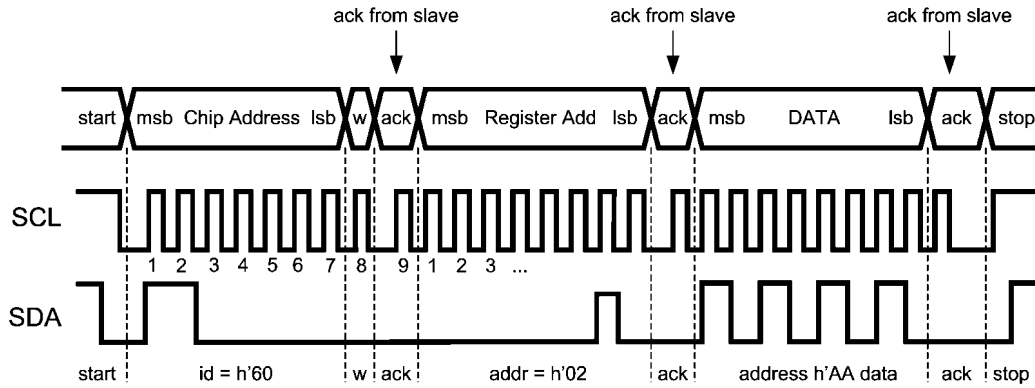
bit which is a data direction bit (R/W). Please note that according to industry I<sup>2</sup>C standards for 7-bit addresses, the MSB of an 8-bit address is removed, and communication actually starts with the 7th most significant bit. For the eighth bit (LSB), a "0" indicates a WRITE and a "1" indicates a READ. The second byte selects the register to which the data will be written. The third byte contains data to write to the selected register.

LP3906 has a chip address of 60'h, which is factory programmed.



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### I<sup>2</sup>C Chip Address

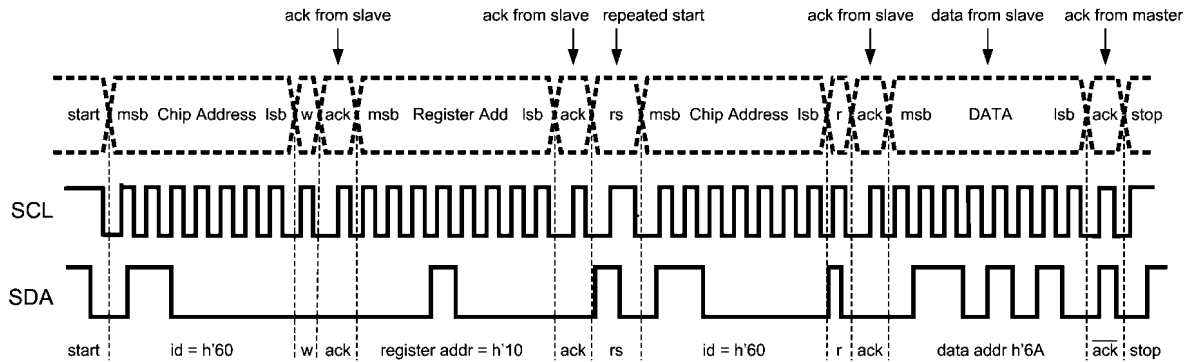


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w = write (SDA = "0")  
 r = read (SDA = "1")  
 ack = acknowledge (SDA pulled down by either master or slave)  
 rs = repeated start  
 id = LP3906 chip address : 0x60

**I2C Write Cycle**

When a READ function is to be accomplished, a WRITE function must precede the READ function, as shown in the Read Cycle waveform.



20197824

**I2C Read Cycle**

## LP3906 Control Registers

Register Address	Register Name	Read/Write	Register Description
0x02	ICRA	R	Interrupt Status Register A
0x07	SCR1	R/W	System Control 1 Register
0x10	BKLD0EN	R/W	Buck and LDO Output Voltage Enable Register
0x11	BKLD0SR	R	Buck and LDO Output Voltage Status Register
0x20	VCCR	R/W	Voltage Change Control Register 1
0x23	B1TV1	R/W	Buck 1 Target Voltage 1 Register
0x24	B1TV2	R/W	Buck 1 Target Voltage 2 Register
0x25	B1RC	R/W	Buck 1 Ramp Control
0x29	B2TV1	R/W	Buck 2 Target Voltage 1 Register
0x2A	B2TV2	R/W	Buck 2 Target Voltage 2 Register
0x2B	B2RC	R/W	Buck 2 Ramp Control
0x38	BFCR	R/W	Buck Function Register
0x39	LDO1VCR	R/W	LDO1 Voltage control Registers
0x3A	LDO2VCR	R/W	LDO2 Voltage control Registers

**INTERRUPT STATUS REGISTER (ISRA) 0X02**

This register informs the user of the temperature status of the chip.

	D7-2	D1	D0
Name	—	Temp 125°C	—
Access	—	R	—
Data	Reserved	Status bit for thermal warning PMIC T>125°C 0 – PMIC Temp. < 125°C 1 – PMIC Temp. > 125°C	Reserved
Reset	0	0	0

**CONTROL 1 REGISTER (SCR1) 0X07**

This register allows the user to select the preset delay sequence for power-on timing, to switch between PFM and PWM mode for the bucks, and also to select between an internal and external clock for the bucks.

The external LDO and SW enables should be pulled LOW to allow the blocks to sequence correctly through assertion of the EN\_T pin.

	D7	D6-4	D3	D2	D1	D0
Name	—	EN_DLY	—	FPWM2	FPWM1	ECEN
Access	—	R/W	—	R/W	R/W	R/W
Data	Reserved	Selects the preset delay sequence from EN_T assertion (shown below)	Reserved	Buck 2 PWM /PFM Mode select 0 – Auto Switch PFM - PWM operation 1 – PWM Mode Only	Buck 1 PWM /PFM Mode select 0 – Auto Switch PFM - PWM operation 1 – PWM Mode Only	External Buck Clock Select 0 – Internal 2 MHz Oscillator clock 1 – External 13 MHz Oscillator clock
Reset	0	010	1	0	0	0

**EN\_DLY PRESET DELAY SEQUENCE AFTER EN\_T ASSERTION**

EN_DLY<2:0>	Delay (ms)			
	Buck1	Buck2	LDO1	LDO2
000	1	1	1	1
001	1	1.5	2	2
010	1.5	2	3	6
011	1.5	2	1	1
100	1.5	2	3	6
101	1.5	1.5	2	2
110	3	2	1	1.5
111	2	3	6	11



**BUCK AND LDO OUTPUT VOLTAGE ENABLE REGISTER (BKLD0EN) – 0X10**

This register controls the enables for the Bucks and LDOs.

	D7	D6	D5	D4	D3	D2	D1	D0
Name	—	LDO2EN	—	LDO1EN	—	BK2EN	—	BK1EN
Access	—	R/W	—	R/W	—	R/W	—	R/W
Data	Reserved	0 – Disable 1 – Enable	Reserved	0 – Disable 1 – Enable	Reserved	0 – Disable 1 – Enable	Reserved	0 – Disable 1 – Enable
Reset	0	1	1	1	0	1	0	1

**BUCK AND LDO STATUS REGISTER (BKLDOSR) – 0X11**

This register monitors whether the Bucks and LDOs meet the voltage output specifications.

	D7	D6	D5	D4	D3	D2	D1	D0
Name	BKS_OK	LDOS_OK	LDO2_OK	LDO1_OK	—	BK2_OK	—	BK1_OK
Access	R	R	R	R	—	R	—	R
Data	0 – Buck 1-2 Not Valid 1 – Bucks Valid	0 – LDO 1-2 Not Valid 1 – LDOs Valid	0 – LDO2 Not Valid 1 – LDO2 Valid	0 – LDO1 Not Valid 1 – LDO1 Valid	Reserved	0 – Buck2 Not Valid 1 – Buck2 Valid	Reserved	0 – Buck1 Not Valid 1 – Buck1 Valid
Reset	0	0	0	0	0	0	0	0

**BUCK VOLTAGE CHANGE CONTROL REGISTER 1 (VCCR) – 0X20**

This register selects and controls the output target voltages for the buck regulators.

	D7-6	D5	D4	D3-2	D1	D0
Name	—	B2VS	B2GO	—	B1VS	B1GO
Access	—	R/W	R/W	—	R/W	R/W
Data	Reserved	Buck2 Target Voltage Select 0 – B2VT1 1 – B2VT2	Buck2 Voltage Ramp CTRL 0 – Hold 1 – Ramp to B2VS selection	Reserved	Buck1 Target Voltage Select 0 – B1VT1 1 – B1VT2	Buck1 Voltage Ramp CTRL 0 – Hold 1 – Ramp to B1VS selection
Reset	00	0	0	00	0	0

**BUCK1 TARGET VOLTAGE 1 REGISTER (B1TV1) – 0X23**

This register allows the user to program the output target voltage of Buck 1.

	D7-5	D4-0
Name	—	BK1_VOUT1
Access	—	R/W
Data	Reserved	Buck1 Output Voltage (V)
		5'h00 Ext Ctrl
		5'h01 0.80
		5'h02 0.85
		5'h03 0.90
		5'h04 0.95
		5'h05 1.00
		5'h06 1.05
		5'h07 1.10
		5'h08 1.15
		5'h09 1.20
		5'h0A 1.25
		5'h0B 1.30
		5'h0C 1.35
		5'h0D 1.40
		5'h0E 1.45
		5'h0F 1.50
		5'h10 1.55
		5'h11 1.60
		5'h12 1.65
5'h13 1.70		
5'h14 1.75		
5'h15 1.80		
5'h16 1.85		
5'h17 1.90		
5'h18 1.95		
5'h19 2.00		
5'h1A–5'h1F 2.00		
Reset	000	Factory Programmed Default

**BUCK 1 TARGET VOLTAGE 2 REGISTER (B1TV2) – 0X24**

This register allows the user to program the output target voltage of Buck 1.

	D7-5	D4-0
Name	—	BK1_VOUT2
Access	—	R/W
Data	Reserved	Buck1 Output Voltage (V)
		5'h00 Ext Ctrl
		5'h01 0.80
		5'h02 0.85
		5'h03 0.90
		5'h04 0.95
		5'h05 1.00
		5'h06 1.05
		5'h07 1.10
		5'h08 1.15
		5'h09 1.20
		5'h0A 1.25
		5'h0B 1.30
		5'h0C 1.35
		5'h0D 1.40
		5'h0E 1.45
		5'h0F 1.50
		5'h10 1.55
		5'h11 1.60
		5'h12 1.65
5'h13 1.70		
5'h14 1.75		
5'h15 1.80		
5'h16 1.85		
5'h17 1.90		
5'h18 1.95		
5'h19 2.00		
5'h1A–5'h1F 2.00		
Reset	000	Factory Programmed Default

**BUCK 1 RAMP CONTROL REGISTER (B1RC) - 0x25**

This register allows the user to program the rate of change between the target voltages of Buck 1.

	D7	D6-4	D3-0	
Name	----	----	B1RS	
Access	----	----	R/W	
Data	Reserved	Reserved	Data Code	Ramp Rate mV/us
			4h'0	Instant
			4h'1	1
			4h'2	2
			4h'3	3
			4h'4	4
			4h'5	5
			4h'6	6
			4h'7	7
			<b>4h'8</b>	<b>8</b>
			4h'9	9
			4h'A	10
4h'B - 4h'F	10			
Reset	0	010	1000	

**BUCK 2 TARGET VOLTAGE 1 REGISTER (B2TV1) – 0X29**

This register allows the user to program the output target voltage of Buck 2.

	D7-5	D4-0
Name	—	BK2_VOUT1
Access	—	R/W
Data	Reserved	Buck2 Output Voltage (V)
		5'h00 Ext Ctrl
		5'h01 1.0
		5'h02 1.1
		5'h03 1.2
		5'h04 1.3
		5'h05 1.4
		5'h06 1.5
		5'h07 1.6
		5'h08 1.7
		5'h09 1.8
		5'h0A 1.9
		5'h0B 2.0
		5'h0C 2.1
		5'h0D 2.2
		5'h0E 2.4
		5'h0F 2.5
		5'h10 2.6
		5'h11 2.7
		5'h12 2.8
5'h13 2.9		
5'h14 3.0		
5'h15 3.1		
5'h16 3.2		
5'h17 3.3		
5'h18 3.4		
5'h19 3.5		
5'h1A–5'h1F 3.5		
Reset	000	Factory Programmed Default

**BUCK 2 TARGET VOLTAGE 2 REGISTER (B2TV2) – 0X2A**

This register allows the user to program the output target voltage of Buck 2.

	D7-5	D4-0
Name	—	BK2_VOUT2
Access	—	R/W
Data	Reserved	Buck2 Output Voltage (V)
		5'h00 Ext Ctrl
		5'h01 1.0
		5'h02 1.1
		5'h03 1.2
		5'h04 1.3
		5'h05 1.4
		5'h06 1.5
		5'h07 1.6
		5'h08 1.7
		5'h09 1.8
		5'h0A 1.9
		5'h0B 2.0
		5'h0C 2.1
		5'h0D 2.2
		5'h0E 2.4
		5'h0F 2.5
		5'h10 2.6
		5'h11 2.7
		5'h12 2.8
5'h13 2.9		
5'h14 3.0		
5'h15 3.1		
5'h16 3.2		
5'h17 3.3		
5'h18 3.4		
5'h19 3.5		
5'h1A–5'h1F 3.5		
Reset	000	Factory Programmed Default

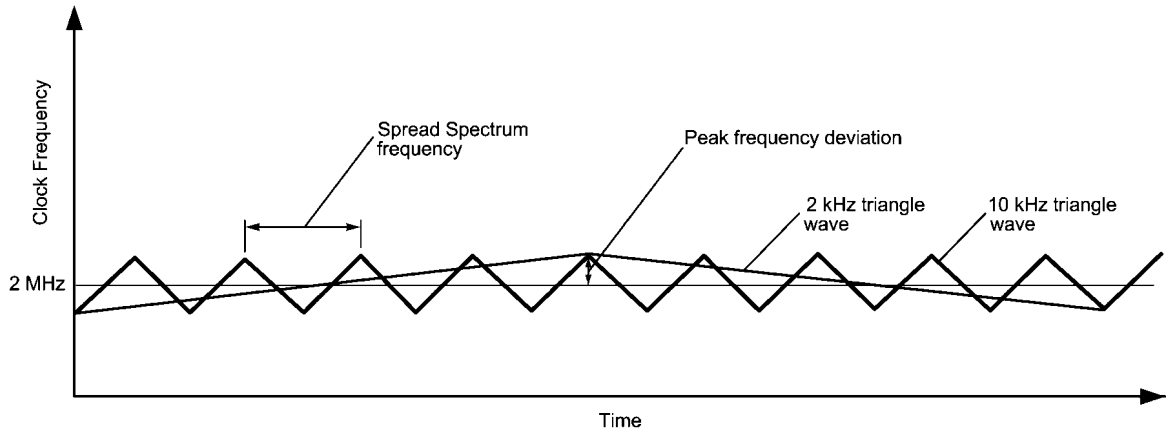
**BUCK 2 RAMP CONTROL REGISTER (B2RC) - 0x2B**

This register allows the user to program the rate of change between the target voltages of Buck 2

	D7	D6-4	D3-0	
Name	----	----	B2RS	
Access	----	----	R/W	
Data	Reserved	Reserved	Data Code	Ramp Rate mV/us
			4h'0	Instant
			4h'1	1
			4h'2	2
			4h'3	3
			4h'4	4
			4h'5	5
			4h'6	6
			4h'7	7
			<b>4h'8</b>	<b>8</b>
			4h'9	9
			4h'A	10
4h'B - 4h'F	10			
Reset	0	010	1000	

**BUCK FUNCTION REGISTER (BFCR) – 0x38**

This register allows the Buck switcher clock frequency to be spread across a wider range, allowing for less Electro-magnetic Interference (EMI). The spread spectrum modulation frequency refers to the rate at which the frequency ramps up and down, centered at 2 MHz.



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	D7-2	D1	D0
Name	—	BK_SLOMOD	BK_SSEN
Access	—	R/W	R/W
Data	Reserved	Buck Spread Spectrum Modulation 0 – 10 kHz triangular wave 1 – 2 kHz triangular wave	Spread Spectrum Function Output 0 – Disabled 1 – Enabled
Reset	000010	1	0

**LDO1 CONTROL REGISTER (LDO1VCR) – 0X39**

This register allows the user to program the output target voltage of LDO 1.

	D7-5	D4-0	
Name	—	LDO1_OUT	
Access	—	R/W	
Data	Reserved	LDO1 Output voltage (V)	
		5'h00	1.0
		5'h01	1.1
		5'h02	1.2
		5'h03	1.3
		5'h04	1.4
		5'h05	1.5
		5'h06	1.6
		5'h07	1.7
		5'h08	1.8
		5'h09	1.9
		5'h0A	2.0
		5'h0B	2.1
		5'h0C	2.2
		5'h0D	2.3
		5'h0E	2.4
		5'h0F	2.5
		5'h10	2.6
		5'h11	2.7
		5'h12	2.8
5'h13	2.9		
5'h14	3.0		
5'h15	3.1		
5'h16	3.2		
5'h17	3.3		
5'h18	3.4		
5'h19	3.5		
5'h1A–5'h1F	3.5		
Reset	000	Factory Programmed Default	

**LDO2 CONTROL REGISTER (LDO2VCR) – 0X3A**

This register allows the user to program the output target voltage of LDO 2.

	D7-5	D4-0	
Name	—	LDO2_OUT	
Access	—	R/W	
Data	Reserved	LDO2 Output voltage (V)	
		5'h00	1.0
		5'h01	1.1
		5'h02	1.2
		5'h03	1.3
		5'h04	1.4
		5'h05	1.5
		5'h06	1.6
		5'h07	1.7
		5'h08	1.8
		5'h09	1.9
		5'h0A	2.0
		5'h0B	2.1
		5'h0C	2.2
		5'h0D	2.3
		5'h0E	2.4
		5'h0F	2.5
		5'h10	2.6
		5'h11	2.7
		5'h12	2.8
5'h13	2.9		
5'h14	3.0		
5'h15	3.1		
5'h16	3.2		
5'h17	3.3		
5'h18	3.4		
5'h19	3.5		
5'h1A–5'h1F	3.5		
Reset	000	Factory Programmed Default	

## Application Notes

### SYSTEM CLOCK INPUT (SYNC) PIN

Pin 23 of the chip allows for a system clock input in order to synchronize the buck converters in PWM mode. This is useful if the user wishes to force the bucks to work synchronously with the system. Otherwise, the user should tie the pin to GND and the bucks will operate on an internal 2 MHz clock.

The signal applied to the SYNC pin must be 13 MHz as per application processor specifications, but we can be contacted to modify that specification if so desired. Upon inputting the 13 MHz clock signal, the bucks will scale it down and continue to run at 2 MHz based off the 13 MHz clock.

### ANALOG POWER SIGNAL ROUTING

All power inputs should be tied to the main VDD source (i.e. battery), unless the user wishes to power it from another source. (i.e. external LDO output).

The analog VDD inputs power the internal bias and error amplifiers, so they should be tied to the main VDD. The analog VDD inputs must have an input voltage between 2.7 and 5.5 V, as specified on pg. 6 of the datasheet.

The other  $V_{INs}$  ( $V_{INLDO1}$ ,  $V_{INLDO2}$ ,  $V_{IN1}$ ,  $V_{IN2}$ ) can actually have inputs lower than 2.7V, as long as it's higher than the programmed output (+0.3V, to be safe).

The analog and digital grounds should be tied together outside of the chip to reduce noise coupling.

### COMPONENT SELECTION

#### Inductors for SW1 and SW2

There are two main considerations when choosing an inductor; the inductor should not saturate and the inductor current ripple is small enough to achieve the desired output voltage ripple. Care should be taken when reviewing the different saturation current ratings that are specified by different manufacturers. Saturation current ratings are typically specified at 25°C, so ratings at maximum ambient temperature of the application should be requested from the manufacturer.

There are two methods to choose the inductor saturation current rating:

#### Method 1:

The saturation current is greater than the sum of the maximum load current and the worst case average to peak inductor current. This can be written as follows:

$$I_{sat} > I_{outmax} + I_{ripple}$$

$$\text{where } I_{ripple} = \left(\frac{1}{f}\right) \times \left(\frac{V_{IN} - V_{OUT}}{2L}\right) \times \left(\frac{V_{OUT}}{V_{IN}}\right)$$

- $I_{RIPPLE}$ :** Average to peak inductor current
- $I_{OUTMAX}$ :** Maximum load current
- $V_{IN}$ :** Maximum input voltage to the buck
- L:** Min inductor value including worse case tolerances (30% drop can be considered for method 1)
- f:** Minimum switching frequency (1.6 MHz)
- $V_{OUT}$ :** Buck Output voltage

#### Method 2:

A more conservative and recommended approach is to choose an inductor that has saturation current rating greater than the maximum current limit of 2375 mA.

Given a peak-to-peak current ripple ( $I_{pp}$ ) the inductor needs to be at least

$$L \geq \left(\frac{V_{IN} - V_{OUT}}{I_{PP}}\right) \times \left(\frac{V_{OUT}}{V_{IN}}\right) \times \left(\frac{1}{f}\right)$$

Inductor	Value	Unit	Description	Notes
$L_{SW1,2}$	2.2	$\mu\text{H}$	SW1,2 inductor	D.C.R. 70 m $\Omega$

### External Capacitors

The regulators on the LP3906 require external capacitors for regulator stability. These are specifically designed for portable applications requiring minimum board space and smallest components. These capacitors must be correctly selected for good performance.

### LDO CAPACITOR SELECTION

#### Input Capacitor

An input capacitor is required for stability. It is recommended that a 1.0  $\mu\text{F}$  capacitor be connected between the LDO input pin and ground (this capacitance value may be increased without limit).

This capacitor must be located a distance of not more than 1 cm from the input pin and returned to a clean analog ground. Any good quality ceramic, tantalum, or film capacitor may be used at the input.

**Important:** Tantalum capacitors can suffer catastrophic failures due to surge currents when connected to a low impedance source of power (like a battery or a very large capacitor). If a tantalum capacitor is used at the input, it must be guaranteed by the manufacturer to have a surge current rating sufficient for the application.

There are no requirements for the ESR (Equivalent Series Resistance) on the input capacitor, but tolerance and temperature coefficient must be considered when selecting the capacitor to ensure the capacitance will remain approximately 1.0  $\mu\text{F}$  over the entire operating temperature range.

#### Output Capacitor

The LDOs on the LP3906 are designed specifically to work with very small ceramic output capacitors. A 1.0  $\mu\text{F}$  ceramic capacitor (temperature types Z5U, Y5V or X7R) with ESR between 5 m $\Omega$  to 500 m $\Omega$ , are suitable in the application circuit.

It is also possible to use tantalum or film capacitors at the device output,  $C_{OUT}$  (or  $V_{OUT}$ ), but these are not as attractive for reasons of size and cost.

The output capacitor must meet the requirement for the minimum value of capacitance and also have an ESR value that is within the range 5 m $\Omega$  to 500 m $\Omega$  for stability.

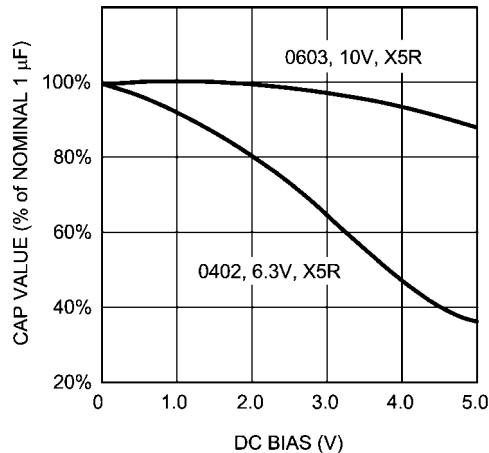
### Capacitor Characteristics

The LDOs are designed to work with ceramic capacitors on the output to take advantage of the benefits they offer. For capacitance values in the range of 0.47  $\mu\text{F}$  to 4.7  $\mu\text{F}$ , ceramic capacitors are the smallest, least expensive and have the lowest ESR values, thus making them best for eliminating high frequency noise. The ESR of a typical 1.0  $\mu\text{F}$  ceramic capacitor is in the range of 20 m $\Omega$  to 40 m $\Omega$ , which easily meets the ESR requirement for stability for the LDOs.

For both input and output capacitors, careful interpretation of the capacitor specification is required to ensure correct device operation. The capacitor value can change greatly, depending on the operating conditions and capacitor type.



In particular, the output capacitor selection should take account of all the capacitor parameters, to ensure that the specification is met within the application. The capacitance can vary with DC bias conditions as well as temperature and frequency of operation. Capacitor values will also show some decrease over time due to aging. The capacitor parameters are also dependent on the particular case size, with smaller sizes giving poorer performance figures in general. As an example, the graph below shows a typical graph comparing different capacitor case sizes in a Capacitance vs. DC Bias plot.



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**Graph Showing a Typical Variation in Capacitance vs. DC Bias**

As shown in the graph, increasing the DC Bias condition can result in the capacitance value that falls below the minimum value given in the recommended capacitor specifications table. Note that the graph shows the capacitance out of spec for the 0402 case size capacitor at higher bias voltages. It is therefore recommended that the capacitor manufacturers' specifications for the nominal value capacitor are consulted for all conditions, as some capacitor sizes (e.g. 0402) may not be suitable in the actual application.

The ceramic capacitor's capacitance can vary with temperature. The capacitor type X7R, which operates over a temperature range of  $-55^{\circ}\text{C}$  to  $+125^{\circ}\text{C}$ , will only vary the capacitance to within  $\pm 15\%$ . The capacitor type X5R has a similar tolerance over a reduced temperature range of  $-55^{\circ}\text{C}$  to  $+85^{\circ}\text{C}$ . Many large value ceramic capacitors, larger than  $1\ \mu\text{F}$  are manufactured with Z5U or Y5V temperature characteristics. Their capacitance can drop by more than 50% as the temperature varies from  $25^{\circ}\text{C}$  to  $85^{\circ}\text{C}$ . Therefore X7R is recommended over Z5U and Y5V in applications where the ambient temperature will change significantly above or below  $25^{\circ}\text{C}$ .

Tantalum capacitors are less desirable than ceramic for use as output capacitors because they are more expensive when comparing equivalent capacitance and voltage ratings in the  $0.47\ \mu\text{F}$  to  $4.7\ \mu\text{F}$  range.

Another important consideration is that tantalum capacitors have higher ESR values than equivalent size ceramics. This means that while it may be possible to find a tantalum capacitor with an ESR value within the stable range, it would have to be larger in capacitance (which means bigger and more costly) than a ceramic capacitor with the same ESR value. It should also be noted that the ESR of a typical tantalum will increase about 2:1 as the temperature goes from  $25^{\circ}\text{C}$  down to  $-40^{\circ}\text{C}$ , so some guard band must be allowed.

### Input Capacitor Selection for SW1 and SW2

A ceramic input capacitor of  $10\ \mu\text{F}$ ,  $6.3\text{V}$  is sufficient for the magnetic dc/dc converters. Place the input capacitor as close as possible to the input of the device. A large value may be used for improved input voltage filtering. The recommended capacitor types are X7R or X5R. Y5V type capacitors should not be used. DC bias characteristics of ceramic capacitors must be considered when selecting case sizes like 0805 and 0603. The input filter capacitor supplies current to the PFET switch of the dc/dc converter in the first half of each cycle and reduces voltage ripple imposed on the input power source. A ceramic capacitor's low ESR (Equivalent Series Resistance) provides the best noise filtering of the input voltage spikes due to fast current transients. A capacitor with sufficient ripple current rating should be selected. The input current ripple can be calculated as:

$$I_{\text{rms}} = I_{\text{outmax}} \sqrt{\frac{V_{\text{OUT}}}{V_{\text{IN}}} \left( 1 - \frac{V_{\text{OUT}}}{V_{\text{IN}}} + \frac{r^2}{12} \right)}$$

$$\text{where } r = \frac{(V_{\text{in}} - V_{\text{out}}) \times V_{\text{out}}}{L \times f \times I_{\text{outmax}} \times V_{\text{in}}}$$

The worse case is when  $V_{\text{IN}} = 2V_{\text{OUT}}$

### Output Capacitor Selection for SW1, SW2

A  $10\ \mu\text{F}$ ,  $6.3\text{V}$  ceramic capacitor should be used on the output of the sw1 and sw2 magnetic dc/dc converters. The output capacitor needs to be mounted as close as possible to the output of the device. A large value may be used for improved input voltage filtering. The recommended capacitor types are X7R or X5R. Y5V type capacitors should not be used. DC bias characteristics of ceramic capacitors must be considered when selecting case sizes like 0805 and 0603. DC bias characteristics vary from manufacturer to manufacturer and DC bias curves should be requested from them and analyzed as part of the capacitor selection process.

The output filter capacitor of the magnetic dc/dc converter smoothes out current flow from the inductor to the load, helps maintain a steady output voltage during transient load changes and reduces output voltage ripple. These capacitors must be selected with sufficient capacitance and sufficiently low ESD to perform these functions.

The output voltage ripple is caused by the charging and discharging of the output capacitor and also due to its ESR and can be calculated as follows:

$$V_{\text{pp-c}} = \frac{I_{\text{ripple}}}{4 \times f \times C}$$

Voltage peak-to-peak ripple due to ESR can be expressed as follows:

$$V_{\text{PP-ESR}} = 2 \times I_{\text{RIPPLE}} \times R_{\text{ESR}}$$

Because the  $V_{\text{PP-C}}$  and  $V_{\text{PP-ESR}}$  are out of phase, the rms value can be used to get an approximate value of the peak-to-peak ripple:

$$V_{\text{pp-rms}} = \sqrt{V_{\text{pp-c}}^2 + V_{\text{pp-esr}}^2}$$

Note that the output voltage ripple is dependent on the inductor current ripple and the equivalent series resistance of the output capacitor ( $R_{ESR}$ ). The  $R_{ESR}$  is frequency dependent as well as temperature dependent. The  $R_{ESR}$  should be calculated with the applicable switching frequency and ambient temperature.

Capacitor	Min Value	Unit	Description	Recommended Type
C <sub>LDO1</sub>	0.47	μF	LDO1 output capacitor	Ceramic, 6.3V, X5R
C <sub>LDO2</sub>	0.47	μF	LDO2 output capacitor	Ceramic, 6.3V, X5R
C <sub>SW1</sub>	10.0	μF	SW1 output capacitor	Ceramic, 6.3V, X5R
C <sub>SW2</sub>	10.0	μF	SW2 output capacitor	Ceramic, 6.3V, X5R

#### I<sup>2</sup>C Pullup Resistor

Both I<sup>2</sup>C\_SDA and I<sup>2</sup>C\_SCL terminals need to have pullup resistors connected to VINLDO12 or to the power supply of the I<sup>2</sup>C master. The values of the pull-up resistors (typ. ~1.8kΩ) are determined by the capacitance of the bus. Too large of a resistor combined with a given bus capacitance will result in a rise time that would violate the max. rise time spec-

ification. A too small resistor will result in a contention with the pull-down transistor on either slave(s) or master.

#### Operation without I<sup>2</sup>C Interface

Operation of the LP3906 without the I<sup>2</sup>C interface is possible if the system can operate with default values for the LDO and Buck regulators. (Read below: Factory programmable options). The I<sup>2</sup>C-less system must rely on the correct default output values of the LDO and Buck converters.

#### Factory Programmable Options

The following options are EPROM programmed during final test of the LP3906. The system designer that needs specific options is advised to contact the local National Semiconductor sales office.

Factory programmable options	Current value
Enable delay for power on	code 010 (see Control 1 register section)
SW1 ramp speed	8 mV/μs
SW2 ramp speed	8 mV/μs

The I<sup>2</sup>C Chip ID address is offered as a metal mask option. The current value equals **0x60**.

## MODE BOUNCE

PFM-PWM transition at low load current.

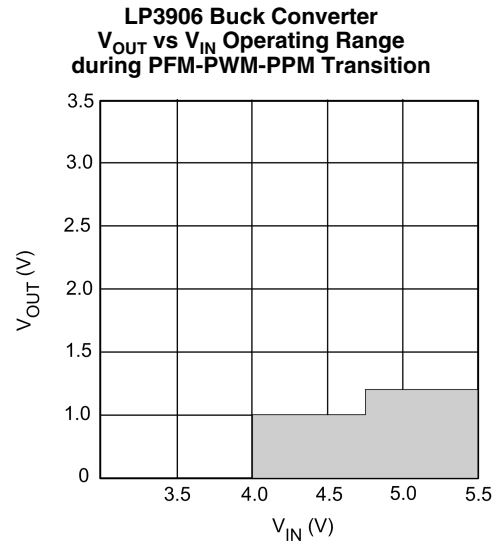
To improve efficiency at lower load currents LP3906 buck converters employ an automatically invoked PFM mode for the low load operation. The PFM mode operates with a much lower value quiescent current ( $I_Q$ ) than the PWM mode of operation that is used in the higher load currents.

As shown in the datasheet section about SW operation, there is a DC voltage difference between the two modes of operation, with  $V_{out}$  PFM being typically 1.2% higher than  $V_{out}$  PWM. So there is a DC voltage level transition and some associated dynamic perturbation at the mode transition point.

The transition between the two modes of operation has an associated hysteresis in the transition current value. That is, the transition point for increasing current (PFM to PWM) is at a higher value than the decreasing current (PWM to PFM). This hysteresis is to ensure that in the event that the load current values equals the PFM PWM transition value, the device will not make multiple transitions between modes; this reduces the noise at this load by eliminating multiple transitions between modes (also known as mode bounce).

Under some conditions of high  $V_{in}$  and Low  $V_{out}$  the hysteresis value is reduced and some amount of mode bounce can occur. Under these conditions, the regulator still maintains DC regulation, however the output ripple is more pronounced. Refer to the attached  $V_{out}$  vs  $V_{in}$  chart below that shows the

operational area that may exhibit this increased output ripple. If the application is expected to be operated in the area of concern AND have a static load current of the transition current value, the user can avoid the possible noise increase by invoking the components' "Force PWM mode".



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**High Vin-High Load Operation**

Additional information is provided when the IC is operated at extremes of Vin and regulator loads. These are described in terms of the Junction temperature and, Buck output ripple management.

**Junction Temperature**

The maximum junction temperature TJ-MAX-OP of 125°C of the IC package.

The following equations demonstrate junction temperature determination, ambient temperature TA-MAX and Total chip power must be controlled to keep TJ below this maximum:

$$TJ-MAX-OP = TA-MAX + (\theta JA) [ \text{ }^\circ\text{C/ Watt} ] * (PD-MAX) \text{ [Watts]}$$

Total IC power dissipation PD-MAX is the sum of the individual power dissipation of the four regulators plus a minor amount for chip overhead. Chip overhead is Bias, TSD & LDO analog.

$$PD-MAX = P_{LDO1} + P_{LDO2} + P_{BUCK1} + P_{BUCK2} + (0.0001A * Vin) \text{ [Watts].}$$

**Power dissipation of LDO1**

$$P_{LDO1} = (Vin_{LDO1} - Vout_{LDO1}) * Iout_{LDO1} \text{ [V*A]}$$

**Power dissipation of LDO2**

$$P_{LDO2} = (Vin_{LDO2} - Vout_{LDO2}) * Iout_{LDO2} \text{ [V*A]}$$

**Power dissipation of Buck1**

$$P_{Buck1} = P_{IN} - P_{OUT} = Vout_{Buck1} * Iout_{Buck1} * (1 - \eta_1) / \eta_1 \text{ [V*A]}$$

$\eta_1$  = efficiency of buck 1

**Power dissipation of Buck2**

$$P_{Buck2} = P_{IN} - P_{OUT} = Vout_{Buck2} * Iout_{Buck2} * (1 - \eta_2) / \eta_2 \text{ [V*A]}$$

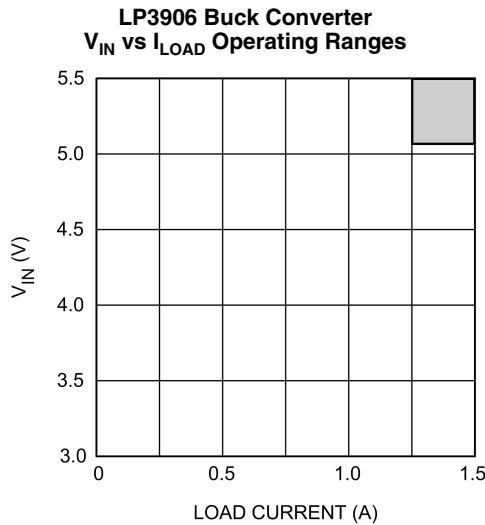
$\eta_2$  = efficiency of buck 2

$\eta$  is the efficiency for the specific condition taken from efficiency graphs.

**Buck Output Ripple Management**

If Vin and ILoad increase, the output ripple associated with the Buck Regulators also increases. The figure below shows the safe operating area. To ensure operation in the area of concern it is recommended that the system designer circumvents the output ripple issues to install schottky diodes on the Bucks(s) that are expected to perform under these extreme corner conditions.

(Schottky diodes are recommended to reduce the output ripple if the system requirements include this shaded area of operation. Vin > 5.2 V and Iload > 1.24 A)



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## Thermal Performance of the LLP Package

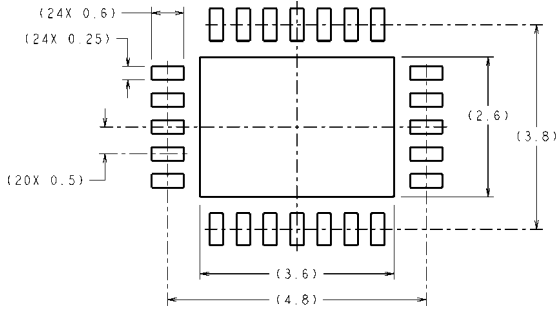
The LP3906 is a monolithic device with integrated power FETs. For that reason, it is important to pay special attention to the thermal impedance of the LLP package and to the PCB layout rules in order to maximize power dissipation of the LLP package.

The LLP package is designed for enhanced thermal performance and features an exposed die attach pad at the bottom center of the package that creates a direct path to the PCB for maximum power dissipation. Compared to the traditional leaded packages where the die attach pad is embedded inside the molding compound, the LLP reduces one layer in the thermal path.

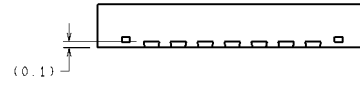
The thermal advantage of the LLP package is fully realized only when the exposed die attach pad is soldered down to a thermal land on the PCB board with thermal vias planted un-

derneath the thermal land. Based on thermal analysis of the LLP package, the junction-to-ambient thermal resistance ( $\theta_{JA}$ ) can be improved by a factor of two when the die attach pad of the LLP package is soldered directly onto the PCB with thermal land and thermal vias, as opposed to an alternative with no direct soldering to a thermal land. Typical pitch and outer diameter for thermal vias are 1.27mm and 0.33mm respectively. Typical copper via barrel plating is 1oz, although thicker copper may be used to further improve thermal performance. The LP3906 die attach pad is connected to the substrate of the IC and therefore, the thermal land and vias on the PCB board need to be connected to ground (GND pin). For more information on board layout techniques, refer to Application Note AN-1187 "Leadless Lead frame Package (LLP)." on <http://www.national.com> This application note also discusses package handling, solder stencil and the assembly process.

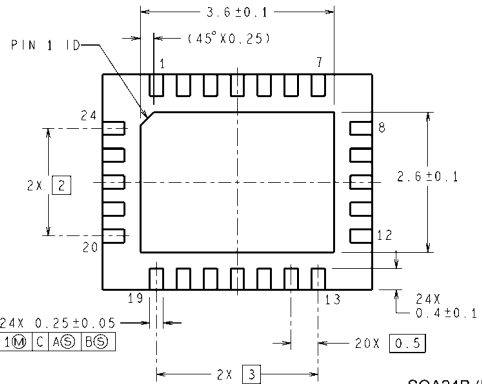
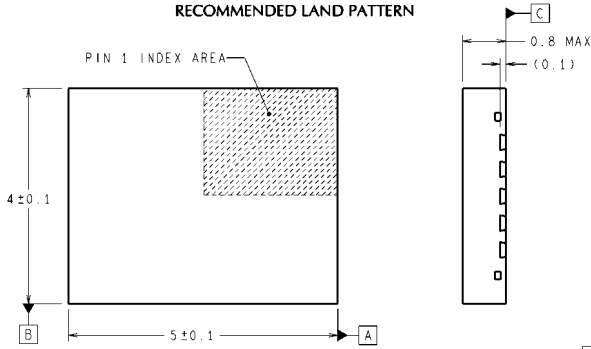
**Physical Dimensions** inches (millimeters) unless otherwise noted



**DIMENSIONS ARE IN MILLIMETERS**  
DIMENSIONS IN ( ) FOR REFERENCE ONLY



**RECOMMENDED LAND PATTERN**



5 X 4 X 0.8 mm 24-Pin LLP Package

SQA24B (Rev A)

# Notes

LP3906

## Notes

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