# Optocoupler, Phototriac Output, Zero Crossing, High dV/dt, Low Input Current 



## DESCRIPTION

The IL410 and IL4108 consists of a GaAs IRLED optically coupled to a photosensitive zero crossing TRIAC network. The TRIAC consists of two inverse parallel connected monolithic SCRs. These three semiconductors are assembled in a six pin dual in-line package.
High input sensitivity is achieved by using an emitter follower phototransistor and a cascaded SCR predriver resulting in an LED trigger current of less than 2 mA (DC). The use of a proprietary $\mathrm{dV} / \mathrm{dt}$ clamp results in a static $\mathrm{dV} / \mathrm{dt}$ of greater than $10 \mathrm{kV} / \mathrm{ms}$. This clamp circuit has a MOSFET that is enhanced when high dV/dt spikes occur between MT1 and MT2 of the TRIAC. When conducting, the FET clamps the base of the phototransistor, disabling the first stage SCR predriver.
The zero cross line voltage detection circuit consists of two enhancement MOSFETS and a photodiode. The inhibit voltage of the network is determined by the enhancement voltage of the N -channel FET. The P -channel FET is enabled by a photocurrent source that permits the FET to conduct the main voltage to gate on the N -channel FET. Once the main voltage can enable the N -channel, it clamps the base of the phototransistor, disabling the first stage SCR predriver.
The $600 \mathrm{~V}, 800 \mathrm{~V}$ blocking voltage permits control of off-line voltages up to $240 \mathrm{~V}_{\mathrm{AC}}$, with a safety factor of more than two, and is sufficient for as much as $380 \mathrm{~V}_{\mathrm{AC}}$.
The IL410, IL4108 isolates low-voltage logic from $120 \mathrm{~V}_{\mathrm{AC}}$, $240 \mathrm{~V}_{\mathrm{AC}}$, and $380 \mathrm{~V}_{\mathrm{AC}}$ lines to control resistive, inductive, or capacitive loads including motors, solenoids, high current thyristors or TRIAC and relays.

## FEATURES

- High input sensitivity
- $I_{F T}=2 \mathrm{~mA}, \mathrm{PF}=1.0$
- $\mathrm{I}_{\mathrm{FT}}=5 \mathrm{~mA}, \mathrm{PF} \leq 1.0$
- 300 mA on-state current
- Zero voltage crossing detector


## RoHS

 complant- $600 \mathrm{~V}, 800 \mathrm{~V}$ blocking voltage
- High static dV/dt $10 \mathrm{kV} / \mu \mathrm{s}$
- Very low leakage $<10 \mu \mathrm{~A}$
- Isolation test voltage 5300 VRMS
- Small 6 pin DIP package
- Compliant to RoHS Directive 2002/95/EC and in accordance to WEEE 2002/96/EC


## APPLICATIONS

- Solid-state relays
- Industrial controls
- Office equipment
- Consumer appliances


## AGENCY APPROVALS

- UL1577, file no. E52744 system code H or J, double protection
- CSA 93751
- DIN EN 60747-5-5 (VDE 0884) available with option 1



## Note

(1) Also available in tubes, do not put T on the end.

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| ABSOLUTE MAXIMUM RATINGS (1) $\left(\mathrm{T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}\right.$, unless otherwise specified) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PARAMETER | TEST CONDITION | PART | SYMBOL | VALUE | UNIT |
| INPUT |  |  |  |  |  |
| Reverse voltage |  |  | $\mathrm{V}_{\mathrm{R}}$ | 6 | V |
| Forward current |  |  | $\mathrm{I}_{\mathrm{F}}$ | 60 | mA |
| Surge current |  |  | $\mathrm{I}_{\text {FSM }}$ | 2.5 | A |
| Power dissipation |  |  | $\mathrm{P}_{\text {diss }}$ | 100 | mW |
| Derate from $25^{\circ} \mathrm{C}$ |  |  |  | 1.33 | $\mathrm{mW} /{ }^{\circ} \mathrm{C}$ |
| OUTPUT |  |  |  |  |  |
| Peak off-state voltage |  | IL410 | $\mathrm{V}_{\text {DRM }}$ | 600 | V |
|  |  | IL4108 | $\mathrm{V}_{\text {DRM }}$ | 800 | V |
| RMS on-state current |  |  | $\mathrm{I}_{\text {TM }}$ | 300 | mA |
| Single cycle surge current |  |  |  | 3 | A |
| Total power dissipation |  |  | $\mathrm{P}_{\text {diss }}$ | 500 | mW |
| Derate from $25^{\circ} \mathrm{C}$ |  |  |  | 6.6 | $\mathrm{mW} /{ }^{\circ} \mathrm{C}$ |
| COUPLER |  |  |  |  |  |
| Isolation test voltage between emitter and detector | $\mathrm{t}=1 \mathrm{~s}$ |  | VISO | 5300 | $\mathrm{V}_{\text {RMS }}$ |
| Pollution degree (DIN VDE 0109) |  |  |  | 2 |  |
| Creepage distance |  |  |  | $\geq 7$ | mm |
| Clearance distance |  |  |  | $\geq 7$ | mm |
| Comparative tracking index per DIN IEC112/VDE 0303 part 1, group Illa per DIN VDE 6110 |  |  | CTI | $\geq 175$ |  |
| Isolation resistance | $\mathrm{V}_{10}=500 \mathrm{~V}, \mathrm{~T}_{\text {amb }}=25^{\circ} \mathrm{C}$ |  | $\mathrm{R}_{\mathrm{IO}}$ | $\geq 10^{12}$ | $\Omega$ |
|  | $\mathrm{V}_{\mathrm{IO}}=500 \mathrm{~V}, \mathrm{~T}_{\mathrm{amb}}=100^{\circ} \mathrm{C}$ |  | $\mathrm{R}_{10}$ | $\geq 10^{11}$ | $\Omega$ |
| Storage temperature range |  |  | $\mathrm{T}_{\text {stg }}$ | -55 to +150 | ${ }^{\circ} \mathrm{C}$ |
| Ambient temperature |  |  | $\mathrm{T}_{\text {amb }}$ | -55 to + 100 | ${ }^{\circ} \mathrm{C}$ |
| Soldering temperature ${ }^{(2)}$ | max. $\leq 10$ s dip soldering $\geq 0.5 \mathrm{~mm}$ from case bottom |  | $\mathrm{T}_{\text {sld }}$ | 260 | ${ }^{\circ} \mathrm{C}$ |

## Notes

(1) Stresses in excess of the absolute maximum ratings can cause permanent damage to the device. Functional operation of the device is not implied at these or any other conditions in excess of those given in the operational sections of this document. Exposure to absolute maximum ratings for extended periods of the time can adversely affect reliability.
(2) Refer to reflow profile for soldering conditions for surface mounted devices (SMD). Refer to wave profile for soldering conditions for through hole devices (DIP).

## Optocoupler, Phototriac Output, Zero Crossing, High dV/dt, Low Input Current

| PARAMETER | TEST CONDITION | PART | SYMBOL | MIN. | TYP. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT |  |  |  |  |  |  |  |
| Forward voltage | $\mathrm{I}_{\mathrm{F}}=10 \mathrm{~mA}$ |  | $\mathrm{V}_{\mathrm{F}}$ |  | 1.16 | 1.35 | V |
| Reverse current | $\mathrm{V}_{\mathrm{R}}=6 \mathrm{~V}$ |  | $\mathrm{I}_{\mathrm{R}}$ |  | 0.1 | 10 | $\mu \mathrm{A}$ |
| Input capacitance | $\mathrm{V}_{\mathrm{F}}=0 \mathrm{~V}, \mathrm{f}=1 \mathrm{MHz}$ |  | $\mathrm{C}_{\text {IN }}$ |  | 25 |  | pF |
| Thermal resistance, junction to ambient |  |  | $\mathrm{R}_{\text {thja }}$ |  | 750 |  | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| OUTPUT |  |  |  |  |  |  |  |
| Off-state voltage | $\mathrm{I}_{\mathrm{D} \text { (RMS) }}=70 \mu \mathrm{~A}$ | IL410 | $\mathrm{V}_{\mathrm{D} \text { (RMS) }}$ | 424 | 460 |  | V |
|  |  | IL4108 | $\mathrm{V}_{\mathrm{D} \text { (RMS) }}$ | 565 |  |  | V |
| Repetitive peak off-state voltage | $\mathrm{I}_{\text {DRM }}=100 \mu \mathrm{~A}$ | IL410 | $\mathrm{V}_{\text {DRM }}$ | 600 |  |  | V |
|  |  | IL4108 | $\mathrm{V}_{\text {DRM }}$ | 800 |  |  | V |
| Off-state current | $\begin{gathered} \mathrm{V}_{\mathrm{D}}=\mathrm{V}_{\mathrm{DRM}}, \mathrm{~T}_{\mathrm{amb}}=100^{\circ} \mathrm{C}, \\ \mathrm{I}_{\mathrm{F}}=0 \mathrm{~mA} \end{gathered}$ |  | $I_{\text {d (RMS })^{1}}$ |  | 10 | 100 | $\mu \mathrm{A}$ |
| On-state voltage | $\mathrm{I}_{\mathrm{T}}=300 \mathrm{~mA}$ |  | $\mathrm{V}_{\text {TM }}$ |  | 1.7 | 3 | V |
| On-state current | $\mathrm{PF}=1, \mathrm{~V}_{\mathrm{T}(\mathrm{RMS})}=1.7 \mathrm{~V}$ |  | $\mathrm{I}_{\text {TM }}$ |  |  | 300 | mA |
| Surge (non-repetitive), on-state current | $\mathrm{f}=50 \mathrm{~Hz}$ |  | $\mathrm{I}_{\text {TSM }}$ |  |  | 3 | A |
| Trigger current 1 | $\mathrm{V}_{\mathrm{D}}=5 \mathrm{~V}$ |  | $\mathrm{I}_{\mathrm{FT} 1}$ |  |  | 2 | mA |
| Trigger current 2 | $\begin{gathered} \mathrm{V}_{\mathrm{OP}}=220 \mathrm{~V}_{\mathrm{RMS}}, \mathrm{f}=50 \mathrm{~Hz}, \\ \mathrm{~T}_{\mathrm{j}}=100^{\circ} \mathrm{C}, \mathrm{t}_{\mathrm{plF}}>10 \mathrm{~ms} \\ \hline \end{gathered}$ |  | IfT2 |  |  | 6 | mA |
| Trigger current temp. gradient |  |  | $\Delta \mathrm{l}_{\mathrm{FT} 1} / \Delta \mathrm{T}_{\mathrm{j}}$ |  | 7 | 14 | $\mu \mathrm{A} /{ }^{\circ} \mathrm{C}$ |
|  |  |  | $\Delta \mathrm{l}_{\mathrm{FT} 2} / \Delta \mathrm{T}_{\mathrm{j}}$ |  | 7 | 14 | $\mu \mathrm{A} /{ }^{\circ} \mathrm{C}$ |
| Inhibit voltage temp. gradient |  |  | $\Delta \mathrm{V}_{\text {DINH }} / \Delta \mathrm{T}_{\mathrm{j}}$ |  | -20 |  | $\mathrm{mV} /{ }^{\circ} \mathrm{C}$ |
| Off-state current in inhibit state | $\mathrm{I}_{\mathrm{F}}=\mathrm{I}_{\mathrm{FT} 1}, \mathrm{~V}_{\text {DRM }}$ |  | I DINH |  | 50 | 200 | $\mu \mathrm{A}$ |
| Holding current |  |  | $\mathrm{I}_{\mathrm{H}}$ |  | 65 | 500 | $\mu \mathrm{A}$ |
| Latching current | $\mathrm{V}_{\mathrm{T}}=2.2 \mathrm{~V}$ |  | $\mathrm{I}_{\mathrm{L}}$ |  |  | 500 | $\mu \mathrm{A}$ |
| Zero cross inhibit voltage | $\mathrm{I}_{\mathrm{F}}=$ Rated $\mathrm{I}_{\text {FT }}$ |  | $\mathrm{V}_{\mathrm{IH}}$ |  | 15 | 25 | V |
| Turn-on time | $\mathrm{V}_{\mathrm{RM}}=\mathrm{V}_{\mathrm{DM}}=\mathrm{V}_{\mathrm{D}(\mathrm{RMS})}$ |  | $\mathrm{t}_{\text {on }}$ |  | 35 |  | $\mu \mathrm{s}$ |
| Turn-off time | $\mathrm{PF}=1, \mathrm{I}_{\mathrm{T}}=300 \mathrm{~mA}$ |  | $\mathrm{t}_{\text {off }}$ |  | 50 |  | $\mu \mathrm{s}$ |
| Critical rate of rise of off-state voltage | $\mathrm{V}_{\mathrm{D}}=0.67 \mathrm{~V}_{\text {DRM }}, \mathrm{T}_{\mathrm{j}}=25^{\circ} \mathrm{C}$ |  | $\mathrm{dV} / \mathrm{dt}_{\mathrm{cr}}$ | 10000 |  |  | V/ $/$ s |
|  | $\mathrm{V}_{\mathrm{D}}=0.67 \mathrm{~V}_{\text {DRM }}, \mathrm{T}_{\mathrm{j}}=80^{\circ} \mathrm{C}$ |  | $\mathrm{dV} / \mathrm{dt}_{\text {cra }}$ | 5000 |  |  | V/ $/$ s |
| Critical rate of rise of voltage at current commutation | $\begin{gathered} V_{D}=230 V_{\text {RMS }}, \\ \mathrm{I}_{\mathrm{D}}=300 \mathrm{~mA} \mathrm{RMS}^{\circ}, \mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C} \end{gathered}$ |  | $\mathrm{dV} / \mathrm{dt}_{\text {cra }}$ |  | 8 |  | V/ $/$ s |
|  | $\begin{gathered} V_{D}=230 V_{\text {RMS }}, \\ I_{D}=300 \mathrm{~mA}_{\text {RMS }}, \mathrm{T}_{J}=85^{\circ} \mathrm{C} \end{gathered}$ |  | $\mathrm{dV} / \mathrm{dt}_{\text {cra }}$ |  | 7 |  | V/ $/$ s |
| Critical rate of rise of on-state current commutation | $\begin{gathered} \mathrm{V}_{\mathrm{D}}=230 \mathrm{~V}_{\mathrm{RMS}}, \\ \mathrm{I}_{\mathrm{D}}=300 \mathrm{~mA}_{\mathrm{RMS}}, \mathrm{~T}_{J}=25^{\circ} \mathrm{C} \end{gathered}$ |  | $\mathrm{dl} / \mathrm{dt}_{\text {cra }}$ |  | 12 |  | A/ms |
| Thermal resistance, junction to ambient |  |  | $\mathrm{R}_{\text {thja }}$ |  | 150 |  | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| COUPLER |  |  |  |  |  |  |  |
| Critical rate of rise of coupled input/output voltage | $\mathrm{I}_{\mathrm{T}}=0 \mathrm{~A}, \mathrm{~V}_{\mathrm{RM}}=\mathrm{V}_{\mathrm{DM}}=\mathrm{V}_{\mathrm{D}(\mathrm{RMS})}$ |  | $\mathrm{dV}_{10} / \mathrm{dt}^{\text {d }}$ | 10000 |  |  | V/ $/$ s |
| Common mode coupling capacitance |  |  | $\mathrm{C}_{\text {CM }}$ |  | 0.01 |  | pF |
| Capacitance (input to output) | $\mathrm{f}=1 \mathrm{MHz}, \mathrm{V}_{10}=0 \mathrm{~V}$ |  | $\mathrm{C}_{10}$ |  | 0.8 |  | pF |
| Isolation resistance | $\mathrm{V}_{10}=500 \mathrm{~V}, \mathrm{~T}_{\text {amb }}=25^{\circ} \mathrm{C}$ |  | $\mathrm{R}_{10}$ |  | $\geq 10^{12}$ |  | $\Omega$ |
|  | $\mathrm{V}_{\mathrm{IO}}=500 \mathrm{~V}, \mathrm{~T}_{\mathrm{amb}}=100^{\circ} \mathrm{C}$ |  | $\mathrm{R}_{\text {IO }}$ |  | $\geq 10^{11}$ |  | $\Omega$ |

## Note

- Minimum and maximum values are testing requirements. Typical values are characteristics of the device and are the result of engineering evaluation. Typical values are for information only and are not part of the testing requirements.

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TYPICAL CHARACTERISTICS $\left(T_{a m b}=25^{\circ} \mathrm{C}\right.$, unless otherwise specified)


Fig. 1 - Forward Voltage vs. Forward Current


Fig. 2 - Peak LED Current vs. Duty Factor, $\tau$


Fig. 3 - Maximum LED Power Dissipation


Fig. 4 - Typical Output Characteristics


Fig. 5 - Current Reduction


Fig. 6 - Current Reduction


Fig. 3 - Typical Trigger Delay Time


Fig. 7 - Off-State Current in Inhibited State vs. $\mathrm{I}_{\mathrm{F}} / \mathrm{I}_{\mathrm{FT}} 25^{\circ} \mathrm{C}$


Fig. 8 - Power Dissipation 40 Hz to 60 Hz Line Operation


Fig. 9 - Typical Static Inhibit Voltage Limit

## TRIGGER CURRENT VS. TEMPERATURE AND VOLTAGE

The trigger current of the IL410, 4108 has a positive temperature gradient and also is dependent on the terminal voltage as shown as the fig. 11.


Fig. 11 - Trigger Current vs.
Temperature and Operating Voltage ( 50 Hz )

For the operating voltage $250 \mathrm{~V}_{\mathrm{RMS}}$ over the temperature range $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$, the $\mathrm{I}_{\mathrm{F}}$ should be at least 2.3 x of the $\mathrm{I}_{\mathrm{FT} 1}$ ( 1.3 mA, max.).
Considering - $30 \%$ degradation over time, the trigger current minimum is $\mathrm{I}_{\mathrm{F}}=1.3 \times 2.3 \times 130 \%=4 \mathrm{~mA}$

## INDUCTIVE AND RESISTIVE LOADS

For inductive loads, there is phase shift between voltage and current, shown in the fig. 12.


Fig. 12 - Waveforms of Resistive and Inductive Loads

The voltage across the triac will rise rapidly at the time the current through the power handling triac falls below the holding current and the triac ceases to conduct. The rise rate of voltage at the current commutation is called commutating $\mathrm{dV} / \mathrm{dt}$. There would be two potential problems for ZC phototriac control if the commutating $\mathrm{dV} / \mathrm{dt}$ is too high. One is lost control to turn off, another is failed to keep the triac on.

## Lost control to turn off

If the commutating $\mathrm{dV} / \mathrm{dt}$ is too high, more than its critical rate ( $\mathrm{dV} / \mathrm{dt}_{\text {crq }}$ ), the triac may resume conduction even if the LED drive current $I_{F}$ is off and control is lost.
In order to achieve control with certain inductive loads of power factors is less than 0.8, the rate of rise in voltage (dV/dt) must be limited by a series RC network placed in parallel with the power handling triac. The RC network is called snubber circuit. Note that the value of the capacitor increases as a function of the load current as shown in fig. 13.

## Failed to keep on

As a zero-crossing phototriac, the commutating $\mathrm{dV} / \mathrm{dt}$ spikes can inhibit one half of the TRIAC from keeping on If the spike potential exceeds the inhibit voltage of the zero cross detection circuit, even if the LED drive current $\mathrm{I}_{\mathrm{F}}$ is on.

This hold-off condition can be eliminated by using a snubber and also by providing a higher level of LED drive current. The higher LED drive provides a larger photocurrent which causes the triac to turn-on before the commutating spike has activated the zero cross detection circuit. Fig. 14 shows the relationship of the LED current for power factors of less than 1.0. The curve shows that if a device requires 1.5 mA for a resistive load, then 1.8 times ( 2.7 mA ) that amount would be required to control an inductive load whose power factor is less than 0.3 without the snubber to dump the spike.


Fig. 10 - Shunt Capacitance vs. Load Current


Fig. 11 - Normalized LED Trigger Current vs. Power Factor

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## APPLICATIONS

Direct switching operation:
The IL410, IL4108 isolated switch is mainly suited to control synchronous motors, valves, relays and solenoids. Fig. 15 shows a basic driving circuit. For resistive load the snubber circuit $R_{S} C_{S}$ can be omitted due to the high static $d V / d t$ characteristic.


Fig. 15 - Basic Direct Load Driving Circuit

Indirect switching operation:
The IL410, IL4108 switch acts here as an isolated driver and thus enables the driving of power thyristors and power triacs by microprocessors. Fig. 16 shows a basic driving circuit of inductive load. The resister R1 limits the driving current pulse which should not exceed the maximum permissible surge current of the IL410, IL4108. The resister $\mathrm{R}_{\mathrm{G}}$ is needed only for very sensitive thyristors or triacs from being triggered by noise or the inhibit current.


Fig. 16 - Basic Power Triac Driver Circuit

PACKAGE DIMENSIONS in millimeters


ISO method A


Option 6


Option 7



## Disclaimer

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