# Low Voltage, High Current, LED Driver Demoboard 

## General Description

The HV9910BDB3 demoboard is a high current LED driver designed to drive one LED or two LEDs in series at currents up to 1.0A from a $10-30 \mathrm{~V}$ DC input. The demoboard uses Supertex's HV9910B Universal LED driver IC to drive a buck converter.

The HV9910BDB3 can be configured to operate in either a constant frequency mode (for driving a single LED) or in a constant off-time mode (for driving two LEDs).

The output current can be adjusted in two ways - either with linear dimming using the onboard potentiometer or with PWM dimming by applying a TTL - compatible square wave signal at the PWMD terminal. Using linear dimming, the output current of the HV9910DB1 can be lowered to about 0.01 A (note: zero output current can be obtained only by PWM dimming).

Specifications

| Parameter | Value |
| :--- | ---: |
| Input voltage | $10-30 \mathrm{VDC}$ |
| Output voltage - <br> constant frequency mode | $2.0-4.5 \mathrm{~V}$ |
| Output voltage - <br> constant off-time mode | $4.0-8.0 \mathrm{~V}$ |
| Maximum output current | $1.0 \mathrm{~A} \pm 10 \%$ |
| Output current ripple (typ) | $20 \%$ (peak-peak) |
| Efficiency (@ 12V input) | $86 \%$ (for one LED) |
| Open LED protection | $93 \%$ (for two LEDs) |
| Output short circuit protection | yes |
| Dimensions | no |

## Connection Diagram



## Connections

1. Input Connection: Connect the input DC voltage between VIN and GND terminals of connector J1 as shown in the connection diagram.
2. Output Connection: Connect the LEDs between LED+ (anode of LED string) and LED- (cathode of LED string) of connector J2.
a. If the load is one LED, short the $\boldsymbol{R T}$ and $\operatorname{FREQ}$ terminals of connector J4 using a jumper.
b. If the load is two LEDs, short the $\boldsymbol{R T}$ and OFFT terminals of connector J4 using a jumper.

## 3. PWM Dimming Connection:

a. If no PWM dimming is required, short PWMD and VDD terminals of connector J3.
b. If PWM dimming is required, connect the TTL-compatible PWM source between PWMD and GND terminals of connector J3. The recommended PWM dimming frequency is $\leq 1.0 \mathrm{kHz}$.

## Frequently Asked Questions

## 1. Why does the demoboard have two operating modes?

Constant frequency mode limits the maximum output voltage to less then $50 \%$ of the minimum input voltage. So, in this case, if we use only the constant frequency mode, the maximum output voltage will have to be less than 5 V . Constant off-time mode removes this limitation and allows the output voltage become higher. However, in order to achieve reasonable noise immunity and to limit the switching frequency variation over the input voltage range, it is not recommended to operate the HV9910DB3 with the output voltage exceeding $80 \%$ of the input voltage, even in the constant off-time mode. Please refer to application note AN-H50 on the Supertex website for more details.
2. If the minimum input voltage in my application is higher (say 20V), does that mean I can drive a 9V LED string in the constant frequency mode or an 16V LED string in the constant off-time mode using the demoboard?

Although a larger LED string can be driven using the demoboard in these conditions, the demoboard will not be able to drive the LED at 1A.

The HV9910B is a constant peak current controller. The average LED current is equal to the peak current set (using the sense resistor) minus one-half of the ripple current in the inductor.

Higher output voltages lead to larger ripple current values, which will reduce the maximum LED current the board can deliver.
3. How can I compute the maximum LED current the demoboard can deliver if I use a higher input voltage and a higher LED string voltage?

| Parameters Minimum input voltage <br>  Maximum LED string voltage <br> Switching frequency (constant freq  <br>  Off-Time (constant off-time mode) <br>  HV9910B CS threshold voltage <br> Sense Resistor  <br> Inductor  | $\begin{aligned} & =\mathrm{V}_{\text {IN,MIN }} \\ & =\mathrm{V}_{\mathrm{O}, \mathrm{MAX}} \\ & =\mathrm{f}_{\mathrm{S}} \\ & =\mathrm{T}_{\text {OFF }} \\ & =\mathrm{V}_{\mathrm{CS}} \\ & =\mathrm{R}_{\mathrm{CS}} \\ & =\mathrm{L} \end{aligned}$ | (100kHz) <br> (5.1 $\mu \mathrm{s}$ ) <br> (0.25V) <br> (0.22 $)$ <br> $(220 \mu \mathrm{H})$ |
| :---: | :---: | :---: |
| Constant Off-Time Mode | Constant Frequency Mode |  |
| $\begin{gathered} \Delta I=\frac{\mathrm{V}_{\mathrm{O}, \mathrm{MAX}} \cdot \mathrm{~T}_{\mathrm{OFF}}}{\mathrm{~L}} \\ \mathrm{I}_{\mathrm{LED}}=\frac{\mathrm{V}_{\mathrm{CS}}}{\mathrm{R}_{\mathrm{CS}}}-\frac{\Delta \mathrm{I}}{2} \\ \text { Maximum Switching Frequency } \left.=\frac{\left\{1-\frac{\mathrm{V}_{\mathrm{O}, \mathrm{MAX}}}{\mathrm{~V}_{\mathrm{IN}, \mathrm{MIN}}}\right\}}{\mathrm{T}_{\mathrm{OFF}}}\right\} \end{gathered}$ | $\begin{gathered} \Delta I=\frac{V_{\mathrm{O}, \text { MAX }} \cdot\left\{1-\frac{\mathrm{V}_{\mathrm{O}, \text { MAX }}}{\mathrm{V}_{\mathrm{IN,MIN}}}\right\}}{\mathrm{L} \cdot \mathrm{f}_{\mathrm{S}}} \\ \mathrm{I}_{\mathrm{LED}}=\frac{\mathrm{V}_{\mathrm{CS}}}{\mathrm{R}_{\mathrm{CS}}}-\frac{\Delta \mathrm{l}}{2} \end{gathered}$ |  |

## Frequently Asked Questions (cont.)

4. If the constant off-time mode allows a wider LED voltage range, why not use that mode exclusively? Why do we need the constant frequency mode?

Although the constant off-time mode allows the demoboard to operate at a higher output voltage, the LED ripple current is directly proportional to the output voltage in this mode. This makes it difficult to get a good load regulation of the LED current in the constant off-time mode with a wide variation in the LED string voltage (in this case it will be a $1: 4$ variation). At lower LED voltage values, the ripple will be lower and the LED current would be higher.

By switching between the two modes depending on the load, we can get a better current accuracy without having to adjust the LD voltage or the sense resistor.

5. Why is the efficiency of the demoboard higher with a load of two LEDs compared to a single LED load?

Losses in the HV9910BDB3 occur due mainly due to two factors:
a. Conduction losses in the FET and diode
b. Switching losses in the FET

Switching losses are dependent on the switching frequency, input voltage and total parasitic capacitance at the node. At higher switching frequencies, the switching losses are higher.

Conduction losses are dependent on the duty cycle. Since the voltage drop on the FET is smaller than the voltage drop on the diode (the on-resistance of the FET is very small), the higher the duty cycle, the smaller is the conduction loss. Please note that we are ignoring the losses in the inductor, which will be identical in both cases.

Also, efficiency $=\mathrm{P}_{\text {OUT }} / \mathrm{P}_{\text {IN }}=\mathrm{P}_{\text {OUT }} /\left(\mathrm{P}_{\text {OUT }}+\right.$ losses $)=1 /\left(1+\right.$ losses $\left./ \mathrm{P}_{\text {OUT }}\right)$, where $\mathrm{P}_{\text {OUT }}$ is the output power and $\mathrm{P}_{\text {IN }}$ is the input power. So, if the output power is higher, the fixed switching losses are a smaller fraction of the output power and thereby the efficiency is higher.

Comparing the operation of the converter in both modes at 12 V input for this particular demoboard, the following are the differences:
a. Output power is higher with 2 LEDs as the load
b. Switching frequency in the constant off-time mode is 55 kHz , whereas it is 100 kHz in the constant frequency mode
c. Duty cycle of operation is about higher in the constant off-time mode by a factor of 2 than in the constant frequency mode

All the above factors favor the higher load voltage and thus the demoboard has a higher efficiency when the load is larger.

## Frequently Asked Questions (cont.)

6. Why are the LED current rise and fall times during PWM dimming different when the load changes from one LED to two LEDs?

The LED current rise time is directly proportional to $\mathrm{V}_{\mathbb{I N}}-\mathrm{V}_{\text {OUT }}$ and the fall time is proportional to $\mathrm{V}_{\text {OUT }}$ (where $\mathrm{V}_{\text {IN }}$ is the input voltage and $V_{\text {OUT }}$ is the output voltage). Since $V_{\text {OUT }}$ is higher with two LEDs, the rise time will be larger and the fall time will be smaller.

## Typical Results

## Constant Frequency Mode:

The HV9910BDB3 is designed to be operated in the constant frequency mode when the load is a single LED. In this mode, the line regulation of the LED current is less than $2 \%$ and full-load efficiency greater than $80 \%$.


Fig. 1. Efficiency vs. Input Voltage Plot

## Efficiency vs. Load Voltage

(@ $\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}$ )


Fig. 3. Efficiency vs. Load Voltage Plot


Fig. 2. Line Regulation of LED Current Plot

Load Regulation (@ $\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}$ )


Fig. 4. Load Regulation of LED Current Plot

## Constant Off-Time Mode:

The HV9910BDB3 is designed to be operated in the constant off-time mode when the load is two LEDs in series. In this mode, the line regulation of the LED current is less than $2 \%$ and the efficiency greater than $80 \%$.


Fig. 5. Efficiency vs. Input Voltage Plot

Efficiency vs. Load Voltage
$\left(@ V_{\text {IN }}=12 \mathrm{~V}\right)$


Fig. 7. Efficiency vs. Load Voltage Plot


Fig. 6. Line Regulation of LED Current Plot


Fig. 8. Load Regulation of LED Current Plot

The variation in the switching frequency, when the HV9910BDB3 is operated in the constant off-time mode, is shown in Figs. 9 and 10.


Fig. 9. Switching Frequency vs. Input Voltage Plot


Fig. 10. Switching Frequency vs. Load Voltage Plot

## Waveforms

## Constant Frequency mode (LED Voltage $=3.3 \mathrm{~V}$ ):



Fig.11. Steady State Waveforms in Constant Frequency Mode

| C1 (Yellow) | $\vdots$ | Drain Voltage (10V/div) |
| :--- | :--- | :--- |
| C4 (Green) | $\vdots$ | LED Current $(200 \mathrm{~mA} / \mathrm{div})$ |
| Time Base | $\vdots$ | $5 \mu \mathrm{~s} /$ div |

## Waveforms (cont.)


(a) PWM Dimming Performance

Time Scale : $500 \mu \mathrm{~s} / \mathrm{div}$

(a) PWM Dimming Rise Time

Time Scale

(b) PWM Dimming Fall Time

Time Scale
$10 \mu \mathrm{~s} / \mathrm{div}$

Fig.12. PWM Dimming Performance in Constant Frequency Mode

| C1 (Yellow) | $:$ | PWMD Input Voltage (2V/div) |
| :--- | :--- | :--- |
| C4 (Green) | $:$ | LED Current (200mA/div) |

## Waveforms (cont.)

## Constant Off-time mode (LED Voltage $=6.4 \mathrm{~V}$ ):



Fig.13. Steady State Waveforms in Constant Frequency Mode

| C1 (Yellow) | $:$ | Drain Voltage $(10 \mathrm{~V} / \mathrm{div})$ |
| :--- | :--- | :--- |
| C4 (Green) | $\vdots$ | LED Current $(200 \mathrm{~mA} / \mathrm{div})$ |
| Time Base | $:$ | $10 \mu \mathrm{~s} /$ div |

## Waveforms (cont.)


(a) PWM Dimming Performance

Time Scale

(b) PWM Dimming Rise Time

Time Scale
$10 \mu \mathrm{~s} / \mathrm{div}$

(a) PWM Dimming Fall Time

Time Scale
$10 \mu \mathrm{~s} / \mathrm{div}$

Fig.14. PWM Dimming Performance in Constant Frequency Mode
C1 (Yellow)
PWMD Input Voltage (2V/div)
C4 (Green) $\quad: \quad$ LED Current (200mA/div)

## Schematic Diagram



HV9910BDB3

Bill of Materials

| $\begin{gathered} \text { Item } \\ \# \end{gathered}$ | Quantity | Ref Des | Description | Package | Manufacturer | Manufacturer's Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2 | C1,C2 | $100 \mu \mathrm{~F}, 35 \mathrm{~V}$, electrolytic capacitor | SMT | Panasonic | EEV-FK1V101P |
| 2 | 2 | C3,C4 | $2.2 \mu \mathrm{~F}, 50 \mathrm{~V}, \mathrm{X} 7 \mathrm{R}$ ceramic chip capacitor | SMD1206 | Murata | GRM31CR71H225KA88L |
| 3 | 1 | C5 | $0.1 \mu \mathrm{~F}, 16 \mathrm{~V}$ X7R ceramic chip capacitor | SMD0805 | Panasonic | ECJ-2VB1C104K |
| 4 | 1 | C6 | $2.2 \mu \mathrm{~F}, 16 \mathrm{~V}$ X7R ceramic chip capacitor | SMD0805 | TDK Corp | C2012X7R1C225K |
| 5 | 1 | D1 | 40V, 1A schottky diode | SMA | Diodes Inc | B140-13 |
| 6 | 2 | J1,J2 | 2 position, 5 mm pitch, vertical header | Thru-Hole | On Shore Tech | EDSTL130/02 |
| 7 | 2 | J3, J4 | 3 position, 0.100 " pitch, vertical header | Thru-Hole | Molex | 22-03-2031 |
| 8 | 1 | L1 | $220 \mathrm{uH}, 1.3 \mathrm{~A}$ rms, 2.4 A sat inductor | SMT | Coiltronics | DR127-221-R |
| 9 | 1 | Q1 | $40 \mathrm{~V}, 45 \mathrm{~m} \Omega$, 10nC N -channel FET | SOT-23 | Vishay | Si2318DS |
| 10 | 1 | R2 | $147 \mathrm{~K} \Omega, 1 / 8 \mathrm{~W}, 1 \%$ chip resistor | SMD0805 | - | - |
| 11 | 1 | R3 | $1 \mathrm{k} \Omega, 1 / 8 \mathrm{~W}, 1 \%$ chip resistor | SMD0805 | - | - |
| 12 | 1 | R4 | 0.22 , 1/4W, $1 \%$ chip resistor | SMD1206 | - | - |
| 13 | 1 | R5 | 226k $\Omega, 1 / 8 \mathrm{~W}, 1 \%$ chip resistor | SMD0805 | - | - |
| 14 | 1 | R6 | $5 \mathrm{~K} \Omega$ top adjust trimpot | SMT | Bourns Inc | 3361P-1-502G |
| 15 | 1 | R7 | $105 \mathrm{k} \Omega, 1 / 8 \mathrm{~W}, 1 \%$ chip resistor | SMD0805 | - | - |
| 16 | 1 | U1 | Universal LED Driver | SO-8 | Supertex | HV9910BLG-G |

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