# 3A, 2MHz, Synchronous Step-Down Converter

### **General Description**

The RT8055 is a high efficiency synchronous, step-down DC/DC converter. Its input voltage range is from 2.6V to 5.5V and provides an adjustable regulated output voltage from 0.8V to 5V while delivering up to 3A of output current.

The internal synchronous low on-resistance power switches increase efficiency and eliminate the need for an external Schottky diode. The switching frequency is set by an external resistor. The 100% duty cycle provides low dropout operation extending battery life in portable systems. Current mode operation with external compensation allows the transient response to be optimized over a wide range of loads and output capacitors.

The RT8055 is operated in forced continuous PWM Mode which minimizes ripple voltage and reduces the noise and RF interference.

The RT8055 is available in the WDFN-10L 3x3 and SOP-8 (Exposed Pad) packages.

## **Ordering Information**

RT8055 PACKAGE Type
QW: WDFN-10L 3x3 (W-Type)
SP: SOP-8 (Exposed Pad-Option 2)
Lead Plating System
G: Green (Halogen Free and Pb Free)
Z: ECO (Ecological Element, Halogen Free)

#### Note:

Richtek Green products are :

- RoHS compliant and compatible with the current requirements of IPC/JEDEC J-STD-020.
- ▶ Suitable for use in SnPb or Pb-free soldering processes.

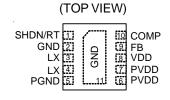
### **Features**

- High Efficiency: Up to 95%
- Low R<sub>DS(ON)</sub> Internal Switches :  $100m\Omega$
- Programmable Frequency : 300kHz to 2MHz
- No Schottky Diode Required
- 0.8V Reference Voltage Allows for Low Output Voltage
- Forced Continuous Mode Operation
- 100% Duty Cycle Operation
- Input Over Voltage Protection
- RoHS Compliant and Halogen Free

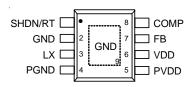
## **Applications**

- Portable Instruments
- Battery-Powered Equipment
- Notebook Computers
- Distributed Power Systems
- IP Phones
- Digital Cameras
- 3G/3.5G Data Card

## **Pin Configurations**



WDFN-10L 3x3



SOP-8 (Exposed Pad)



# **Marking Information**

RT8055GQW

JN=YM DNN JN=: Product Code YMDNN: Date Code RT8055 GSPYMDNN

RT8055GSP

RT8055GSP: Product Number

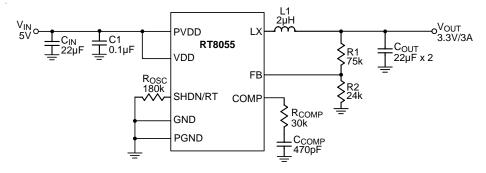
YMDNN: Date Code

RT8055ZQW



JN: Product Code YMDNN: Date Code

# **Typical Application Circuit**



**Table 1. Recommended Component Selection** 

V <sub>OUT</sub>	R1 (kΩ)	R2 (kΩ)	R <sub>COMP</sub> (kΩ)	C <sub>COMP</sub> (nF)	L1 (μH)	C <sub>OUT</sub> (μF)
3.3	75	24	30	0.47	2.2	22 x 2
2.5	51	24	27	0.47	2.2	22 x 2
1.8	30	24	22	0.47	2.2	22 x 2
1.5	21	24	18	0.47	2.2	22 x 2
1.2	12	24	15	0.47	1.0	22 x 2
1.0	6	24	13	0.47	1.0	22 x 2

3

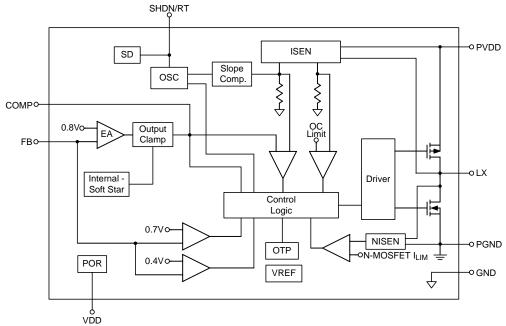


# **Functional Pin Description**

Pin No.		Din Nama	Din Franction
WDFN-10L 3x3	SOP-8	Pin Name	Pin Function
1	1	SHDN/RT	Shutdown Control or Frequency Setting Input. Connect a resistor to ground from this pin sets the switching frequency. Force this pin to $V_{DD}$ or GND causes the device to be shut down.
2, 11 (Exposed Pad)	2, 9 (Exposed Pad)	GND	Signal Ground. All small-signal components and compensation components should be connected to this ground, which in turn connects to PGND at one point. The exposed pad must be soldered to a large PCB and connected to GND for maximum power dissipation.
3, 4	3	LX	Internal Power MOSFET Switches Output. Connect this pin to the inductor.
5	4	PGND	Power Ground. Connect this pin close to the negative terminal of $C_{\text{IN}}$ and $C_{\text{OUT}}$ .
6, 7	5	PVDD	Power Supply Input. Decouple this pin to PGND with a capacitor.
8	6	VDD	Signal Supply Input. Decouple this pin to GND with a capacitor. Generally, $V_{\rm DD}$ is equal to PVDD.
9	7	FB	Feedback Pin. This pin receives the feedback voltage from a resistive divider connected across the output.
10	8	COMP	Error Amplifier Compensation Point. The current comparator threshold increases with this control voltage. Connect external compensation elements to this pin to stabilize the control loop.

# **Function Block Diagram**

Downloaded from Elcodis.com electronic components distributor



# Absolute Maximum Ratings (Note 1)

Supply Input Voltage, VDD, PVDD	
LX Pin Switch Voltage	
<30ns	
Other I/O Pin Voltages	
• LX Pin Switch Current	4A
<ul> <li>Power Dissipation, P<sub>D</sub> @ T<sub>A</sub> = 25°C</li> </ul>	
WDFN-10L 3x3	1.667W
SOP-8 (Exposed Pad)	1.333W
Package Thermal Resistance (Note 2)	
WDFN-10L 3x3, $\theta_{JA}$	60°C/W
WDFN-10L 3x3, $\theta_{JC}$	7.8°C/W
SOP-8 (Exposed Pad), $\theta_{JA}$	75°C/W
SOP-8 (Exposed Pad), θ <sub>JC</sub>	15°C/W
Junction Temperature	150°C
• Lead Temperature (Soldering, 10 sec.)	260°C
Storage Temperature Range	
ESD Susceptibility (Note 3)	
HBM (Human Body Mode)	2kV
MM (Machine Mode)	200V
Recommended Operating Conditions (Note 4)	

### **Electrical Characteristics**

( $V_{DD} = 3.3V$ ,  $T_A = 25$ °C, unless otherwise specified)

Parameter	Symbol	Test Conditions	Min	Тур	Max	Unit
Input Voltage Range	$V_{DD}$		2.6		5.5	V
Feedback Reference Voltage	$V_{REF}$		0.784	8.0	0.816	V
Feedback Leakage Current	I <sub>FB</sub>	V <sub>FB</sub> = 3.3V			0.1	μΑ
DC Bias Current		Active , V <sub>FB</sub> = 0.7V, Not Switching		500		μΑ
DC bias current		Shutdown			1	μΑ
Output Voltage Line Regulation	$\Delta V_{LINE}$	V <sub>IN</sub> = 2.6V to 5.5V		0.1		%N
Output Voltage Load Regulation	$\Delta V_{LOAD}$	$V_{IN} = 5V$ , $V_{OUT} = 3.3V$ , $I_{OUT} = 0A$ to $3A$		0.4		%
Error Amplifier Transconductance	gm			400		μΑ/V
Current Sense Transresistance	R <sub>S</sub>			0.4		Ω
RT Leakage Current		SHDN/RT = V <sub>IN</sub> = 5.5V			1	μΑ
		$R_{OSC} = 180k\Omega$	1.44	1.8	2.16	MHz
Switching Frequency		Adjustable Switching Frequency Range	0.3		2	MHz

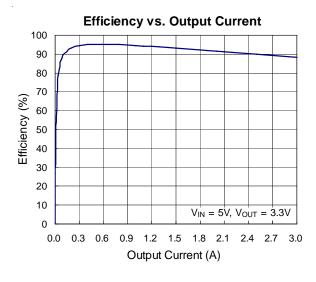
To be continued

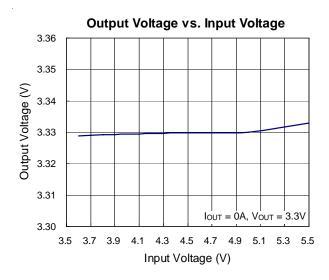


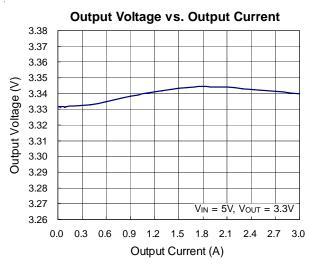
Parameter	Symbol	Test Conditions	Min	Тур	Max	Unit
Switch On Resistance, High	R <sub>DS(ON</sub>	I <sub>SW</sub> = 0.3A		100	160	mΩ
Switch On Resistance, Low	R <sub>DS(ON</sub>	$I_{SW} = 0.3A$		100	170	mΩ
Peak Current Limit	I <sub>LIM</sub>		3.5			Α
Under Voltage Lockout		V <sub>DD</sub> Rising @Full Temperature	2.33	2.4	2.57	V
Threshold (Note 5)		V <sub>DD</sub> Falling @Full Temperature	1.98	2.2	2.37	V
Shutdown Threshold	V <sub>SHDN</sub>	V <sub>SHDN</sub> Rising		V <sub>IN</sub> - 0.85	V <sub>IN</sub> – 0.4	V

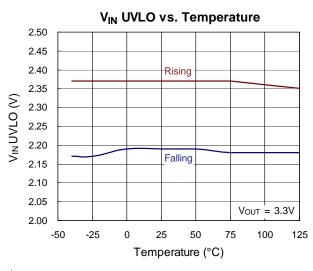
- **Note 1.** Stresses listed as the above "Absolute Maximum Ratings" may cause permanent damage to the device. These are for stress ratings. Functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may remain possibility to affect device reliability.
- Note 2.  $\theta_{JA}$  is measured in the natural convection at  $T_A = 25$ °C on a high effective thermal conductivity four layers test board of JEDEC 51-7 thermal measurement standard. The case point of  $\theta_{JC}$  is on the exposed pad for the package.
- Note 3. Devices are ESD sensitive. Handling precaution is recommended.
- Note 4. The device is not guaranteed to function outside its operating conditions.
- Note 5. Guaranteed by design.

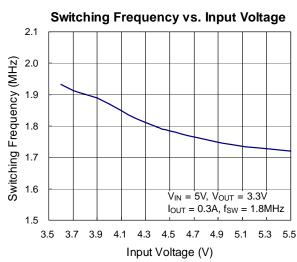
## **Typical Operating Characteristics**

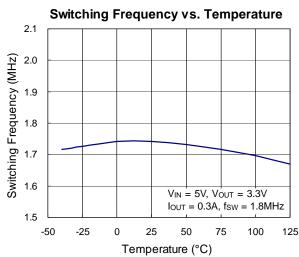




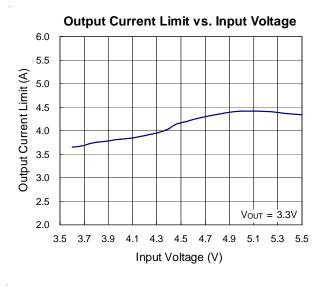


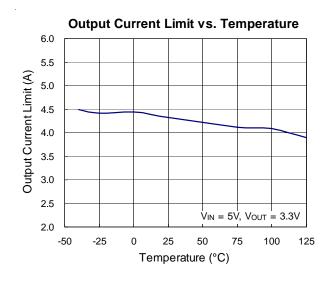


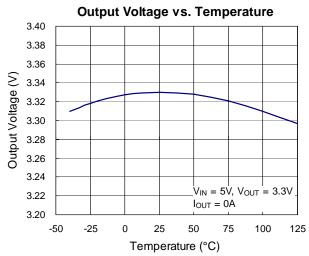


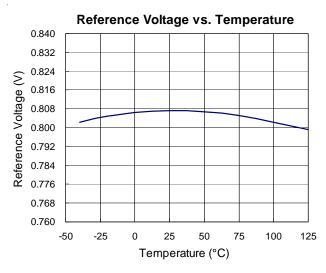


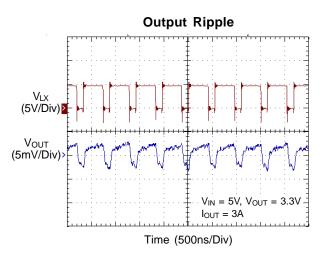


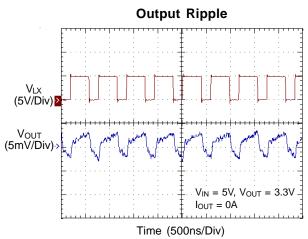


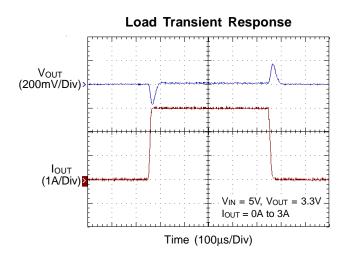


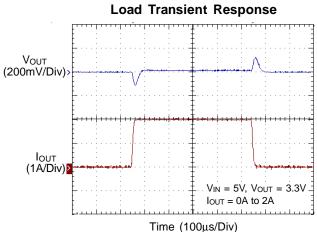


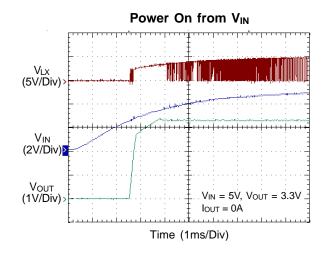


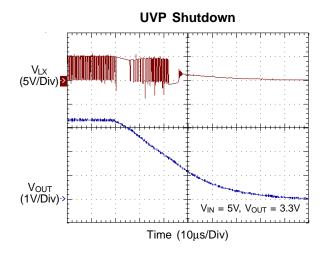














## **Application Information**

The basic RT8055 application circuit is shown in Typical Application Circuit. External component selection is determined by the maximum load current and begins with the selection of the inductor value and operating frequency followed by  $C_{\text{IN}}$  and  $C_{\text{OUT}}$ .

### **Output Voltage Setting**

The output voltage is set by an external resistive divider according to the following equation:

$$V_{OUT} = V_{REF} \times \left(1 + \frac{R1}{R2}\right)$$

where V<sub>REF</sub> equals to 0.8V typical.

The resistive divider allows the FB pin to sense a fraction of the output voltage as shown in Figure 1.

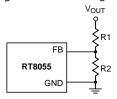


Figure 1. Setting the Output Voltage

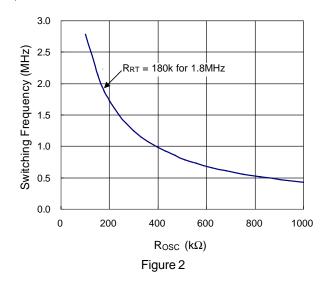
#### Soft-Start

The RT8055 contains an internal soft-start clamp that gradually raises the clamp on the COMP pin.

#### **Operating Frequency**

Selection of the operating frequency is a tradeoff between efficiency and component size. High frequency operation allows the use of smaller inductor and capacitor values. Operation at lower frequency improves efficiency by reducing internal gate charge and switching losses but requires larger inductance and/or capacitance to maintain low output ripple voltage.

The operating frequency of the RT8055 is determined by an external resistor that is connected between the SHDN/RT pin and GND. The value of the resistor sets the ramp current that is used to charge and discharge an internal timing capacitor within the oscillator. The RT resistor value can be determined by examining the frequency vs.  $R_{RT}$  curve. Although frequencies as high as 2MHz are possible, the minimum on-time of the RT8055 imposes a minimum limit on the operating duty cycle. The minimum on-time is typically 110ns. Therefore, the minimum duty cycle is equal to 100 x 110ns x f (Hz).



#### 100% Duty Cycle Operation

When the input supply voltage decreases toward the output voltage, the duty cycle increases toward the maximum on-time. Further reduction of the supply voltage forces the main switch to remain on for more than one cycle eventually reaching 100% duty cycle.

The output voltage will then be determined by the input voltage minus the voltage drop across the internal P-MOSFET and the inductor.

#### **Low Supply Operation**

The RT8055 is designed to operate down to an input supply voltage of 2.6V. One important consideration at low input supply voltages is that the  $R_{\rm DS(ON)}$  of the P-Channel and N-Channel power switches increases. The user should calculate the power dissipation when the RT8055 is used at 100% duty cycle with low input voltages to ensure that thermal limits are not exceeded.

### Slope Compensation and Inductor Peak Current

Slope compensation provides stability in constant frequency architectures by preventing sub-harmonic oscillations at duty cycles greater than 50%. It is accomplished internally by adding a compensating ramp to the inductor current signal. Normally, the maximum inductor peak current is reduced when slope compensation is added. In the RT8055, however, separated inductor current signals are used to monitor over current condition.



This keeps the maximum output current relatively constant regardless of duty cycle.

#### **Short Circuit Protection**

When the output is shorted to ground, the inductor current decays very slowly during a single switching cycle. A current runaway detector is used to monitor inductor current. As current increasing beyond the control of current loop, switching cycles will be skipped to prevent current runaway from occurring.

#### Inductor Selection

The inductor value and operating frequency determine the ripple current according to a specific input and output voltage. The ripple current  $\Delta I_L$  increases with higher  $V_{IN}$  and decreases with higher inductance.

$$\Delta I_{L} = \left[ \frac{V_{OUT}}{f \times L} \right] \times \left[ 1 - \frac{V_{OUT}}{V_{IN}} \right]$$

Having a lower ripple current reduces not only the ESR losses in the output capacitors but also the output voltage ripple. However, it requires a large inductor to achieve this goal.

For the ripple current selection, the value of  $\Delta I_L = 0.4 (I_{MAX})$  will be a reasonable starting point. The largest ripple current occurs at the highest  $V_{IN}$ . To guarantee that the ripple current stays below the specified maximum, the inductor value should be chosen according to the following equation :

$$L = \left[\frac{V_{OUT}}{f \times \Delta I_{L(MAX)}}\right] \times \left[1 - \frac{V_{OUT}}{V_{IN(MAX)}}\right]$$

The inductor's current rating (caused a 40°C temperature rising from 25°C ambient) should be greater than the maximum load current and its saturation current should be greater than the short circuit peak current limit.

#### CIN and COUT Selection

The input capacitance,  $C_{\text{IN}}$ , is needed to filter the trapezoidal current at the source of the top MOSFET. To prevent large ripple voltage, a low ESR input capacitor sized for the maximum RMS current should be used. RMS current is given by :

$$I_{RMS} = I_{OUT(MAX)} \frac{V_{OUT}}{V_{IN}} \sqrt{\frac{V_{IN}}{V_{OUT}}} - 1$$

This formula has a maximum at  $V_{IN} = 2V_{OUT}$ , where  $I_{RMS} = I_{OUT}/2$ . This simple worst-case condition is commonly used for design because even significant deviations do not offer much relief. Choose a capacitor rated at a higher temperature than required.

Several capacitors may also be paralleled to meet size or height requirements in the design.

The selection of  $C_{OUT}$  is determined by the effective series resistance (ESR) that is required to minimize voltage ripple and load step transients, as well as the amount of bulk capacitance that is necessary to ensure that the control loop is stable. Loop stability can be checked by viewing the load transient response as described in a later section. The output ripple,  $\Delta V_{OUT}$ , is determined by :

$$\Delta V_{OUT} \le \Delta I_L \left[ ESR + \frac{1}{8fC_{OUT}} \right]$$

The output ripple is highest at maximum input voltage since  $\Delta I_L$  increases with input voltage. Multiple capacitors placed in parallel may be needed to meet the ESR and RMS current handling requirements. Dry tantalum, special polymer, aluminum electrolytic and ceramic capacitors are all available in surface mount packages. Special polymer capacitors offer very low ESR but have lower capacitance density than other types. Tantalum capacitors have the highest capacitance density but it is important to only use types that have been surge tested for use in switching power supplies. Aluminum electrolytic capacitors have significantly higher ESR but can be used in cost-sensitive applications provided that consideration is given to ripple current ratings and long term reliability. Ceramic capacitors have excellent low ESR characteristics but can have a high voltage coefficient and audible piezoelectric effects. The high Q of ceramic capacitors with trace inductance can also lead to significant ringing.

#### **Using Ceramic Input and Output Capacitors**

Higher values, lower cost ceramic capacitors are now becoming available in smaller case sizes. Their high ripple current, high voltage rating and low ESR make them ideal for switching regulator applications. However, care must be taken when these capacitors are used at the input and output. When a ceramic capacitor is used at the input and the power is supplied by a wall adapter through long

wires, a load step at the output can induce ringing at the input,  $V_{DD}$ . At best, this ringing can couple to the output and be mistaken as loop instability. At worst, a sudden inrush of current through the long wires can potentially cause a voltage spike at  $V_{IN}$  large enough to damage the part.

#### **Thermal Considerations**

For continuous operation, do not exceed absolute maximum junction temperature. The maximum power dissipation depends on the thermal resistance of the IC package, PCB layout, rate of surrounding airflow, and difference between junction and ambient temperature. The maximum power dissipation can be calculated by the following formula:

$$P_{D(MAX)} = (T_{J(MAX)} - T_A) / \theta_{JA}$$

where  $T_{J(MAX)}$  is the maximum junction temperature,  $T_A$  is the ambient temperature, and  $\theta_{JA}$  is the junction to ambient thermal resistance.

For recommended operating condition specifications of the RT8055, the maximum junction temperature is 125°C and  $T_A$  is the ambient temperature. The junction to ambient thermal resistance,  $\theta_{JA}$ , is layout dependent. For SOP-8 (Exposed Pad) packages, the thermal resistance,  $\theta_{JA}$ , is 75°C/W on a standard JEDEC 51-7 four-layer thermal test board. For WDFN-10L 3x3 packages, the thermal resistance,  $\theta_{JA}$ , is 70°C/W on a standard JEDEC 51-7 four-layer thermal test board. The maximum power dissipation at  $T_A$  = 25°C can be calculated by the following formulas :

 $P_{D(MAX)} = (125^{\circ}C - 25^{\circ}C) / (75^{\circ}C/W) = 1.333W$  for SOP-8 (Exposed Pad) package

 $P_{D(MAX)} = (125^{\circ}C - 25^{\circ}C) / (70^{\circ}C/W) = 1.429W$  for WDFN-10L 3x3 package

The maximum power dissipation depends on the operating ambient temperature for fixed  $T_{J(MAX)}$  and thermal resistance,  $\theta_{JA}$ . For the RT8055 packages, the derating curves in Figure 4 allow the designer to see the effect of rising ambient temperature on the maximum power dissipation.

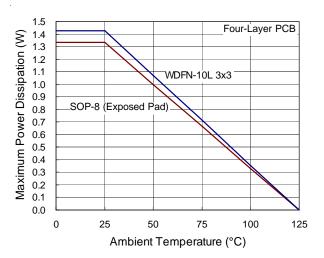


Figure 3. Derating Curves for RT8055 Package

#### **Layout Considerations**

Follow the PCB layout guidelines for optimal performance of RT8055.

- A ground plane is recommended. If a ground plane layer is not used, the signal and power grounds should be segregated with all small-signal components returning to the GND pin at one point that is then connected to the PGND pin close to the IC. The exposed pad should be connected to GND.
- Connect the terminal of the input capacitor(s), C<sub>IN</sub>, as close as possible to the PVDD pin. This capacitor provides the AC current into the internal power MOSFETs.
- LX node is with high frequency voltage swing and should be kept within small area. Keep all sensitive small-signal nodes away from the LX node to prevent stray capacitive noise pick-up.
- Flood all unused areas on all layers with copper. Flooding with copper will reduce the temperature rise of powercomponents.

You can connect the copper areas to any DC net (PVDD, VDD, VOUT, PGND, GND, or any other DC rail in your system).

Connect the FB pin directly to the feedback resistors. The resistor divider must be connected between V<sub>OUT</sub> and GND.

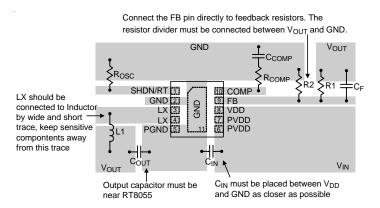


Figure 4. PCB Layout Guide

Recommended component selection for Typical Application

Table 1. Inductors

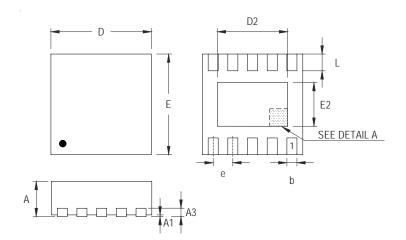
<b>Component Supplier</b>	Series	Inductance (µH)	DCR (mΩ)	Current Rating (mA)	Dimensions (mm)
TAIYO YUDEN	NR 8040	2	9	7800	8x8x4

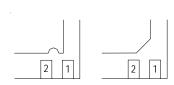
Table 2. Capacitors for C<sub>IN</sub> and C<sub>OUT</sub>

Component Supplier	Part No.	Capacitance (μF)	Case Size
TDK	C3225X5R0J226M	22	1210
TDK	C2012X5R0J106M	10	0805
Panasonic	ECJ4YB0J226M	22	1210
Panasonic	ECJ4YB1A106M	10	1210
TAIYO YUDEN	LMK325BJ226ML	22	1210
TAIYO YUDEN	JMK316BJ226ML	22	1206
TAIYO YUDEN	JMK212BJ106ML	10	0805



## **Outline Dimension**





**DETAIL A** 

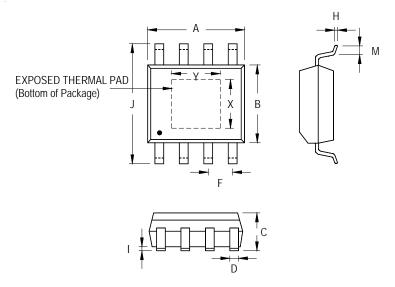
Pin #1 ID and Tie Bar Mark Options

Note: The configuration of the Pin #1 identifier is optional, but must be located within the zone indicated.

Symbol	Dimensions I	n Millimeters	Dimension	s In Inches
Symbol	Min	Max	Min	Max
А	0.700	0.800	0.028	0.031
A1	0.000	0.050	0.000	0.002
А3	0.175	0.250	0.007	0.010
b	0.180	0.300	0.007	0.012
D	2.950	3.050	0.116	0.120
D2	2.300	2.650	0.091	0.104
Е	2.950	3.050	0.116	0.120
E2	1.500	1.750	0.059	0.069
е	0.5	500	0.020	
L	0.350	0.450	0.014	0.018

W-Type 10L DFN 3x3 Package





Symbol		Dimensions I	n Millimeters	Dimension	s In Inches
Symb	101	Min	Max	Min	Max
Α		4.801	5.004	0.189	0.197
В		3.810	4.000	0.150	0.157
С		1.346	1.753	0.053	0.069
D		0.330	0.510	0.013	0.020
F		1.194	1.346 0.047		0.053
Н		0.170	0.254	0.007	0.010
I	1		0.152	0.000	0.006
J		5.791	6.200	0.228	0.244
М		0.406	1.270	0.016	0.050
Ontion 1	Χ	2.000	2.300	0.079	0.091
Option 1	Υ	2.000	2.300	0.079	0.091
Ontion 2	Χ	2.100	2.500	0.083	0.098
Option 2	Υ	3.000	3.500	0.118	0.138

8-Lead SOP (Exposed Pad) Plastic Package

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