

Austin LynxTM 12 V SIP Non-isolated Power Modules: 10 – 14Vdc input; 1.2Vdc to 5.5Vdc Output; 10A Output Current

RoHS Compliant

Applications

- Distributed power architectures
- Intermediate bus voltage applications
- Telecommunications equipment
- Servers and storage applications
- Networking equipment

Features

- Compliant to RoHS EU Directive 2002/95/EC (-Z versions)
- Compliant to ROHS EU Directive 2002/95/EC with lead solder exemption (non-Z versions)
- **-** Delivers up to 10A of output current
- High efficiency 93% at 3.3V full load $(V_{\text{IN}} = 12.0V)$
- Small size and low profile: 50.8 mm x 12.7 mm x 8.10 mm (2.00 in x 0.50 in x 0.320 in)
- Low output ripple and noise
- High Reliability: Calculated MTBF = 4.4 M hours at 25° C Full-load
- Line Regulation: 0.3% (typical)
- Load Regulation: 0.4% (typical)
- **Temperature Regulation: 0.4% (typical)**
- Remote On/Off
- Remote Sense
- **•** Output overcurrent protection (non-latching)
- Overtemperature protection
- Wide operating temperature range (-40°C to 85°C)
- UL* 60950-1Recognized, CSA[†] C22.2 No. 60950-1-03 Certified, and *VDE*‡ 0805:2001-12 (EN60950-1) Licensed
- ISO** 9001 and ISO 14001 certified manufacturing facilities

Description

Austin Lynx[™] 12V SIP (Single Inline Package) power modules are non-isolated DC-DC converters that can deliver up to 10A of output current with full load efficiency of 93% at 3.3V output. These modules provide a precisely regulated output voltage ranging from 1.2Vdc to 5.5Vdc over a wide range of input voltage (V_{IN} = 10 – 14Vdc). Their open-frame construction and small footprint enable designers to develop cost- and space-efficient solutions. Standard features include remote On/Off, remote sense, output voltage adjustment, overcurrent and overtemperature protection.

* *UL* is a registered trademark of Underwriters Laboratories, Inc. † *CSA* is a registered trademark of Canadian Standards Association. ‡ *VDE* is a trademark of Verband Deutscher Elektrotechniker e.V.

^{**} ISO is a registered trademark of the International Organization of Standards

Absolute Maximum Ratings

Stresses in excess of the absolute maximum ratings can cause permanent damage to the device. These are absolute stress ratings only, functional operation of the device is not implied at these or any other conditions in excess of those given in the operations sections of the data sheet. Exposure to absolute maximum ratings for extended periods can adversely affect the device reliability.

Electrical Specifications

Unless otherwise indicated, specifications apply over all operating input voltage, resistive load, and temperature conditions.

CAUTION: This power module is not internally fused. An input line fuse must always be used.

This power module can be used in a wide variety of applications, ranging from simple standalone operation to being part of a complex power architecture. To preserve maximum flexibility, internal fusing is not included, however, to achieve maximum safety and system protection, always use an input line fuse. The safety agencies require a fastacting fuse with a maximum rating of 15 A (see Safety Considerations section). Based on the information provided in this data sheet on inrush energy and maximum dc input current, the same type of fuse with a lower rating can be used. Refer to the fuse manufacturer's data sheet for further information.

Electrical Specifications (continued)

Electrical Specifications (continued)

General Specifications

Feature Specifications

Unless otherwise indicated, specifications apply over all operating input voltage, resistive load, and temperature conditions. See Feature Descriptions for additional information.

Characteristic Curves

The following figures provide typical characteristics for the Austin Lynx™ 12 V SIP modules at 25°C.

Figure 1. Converter Efficiency versus Output Current (Vout =1.2Vdc).

Figure 2. Converter Efficiency versus Output Current (Vout = 1.5Vdc).

Figure3. Converter Efficiency versus Output Current (Vout = 1.8Vdc).

Figure 4. Converter Efficiency versus Output Current (Vout = 2.5Vdc).

Figure 5. Converter Efficiency versus Output Current (Vout = 3.3Vdc).

Figure 6. Converter Efficiency versus Output Current (Vout = 5.0Vdc).

Characteristic Curves (continued)

The following figures provide typical characteristics for the Austin LynxTM 12 V SIP modules at 25°C.

Figure 8. Typical Output Ripple and Noise (Vin = 12.0V dc, Vo = 2.5 Vdc, Io=10A).

Figure 9. Typical Output Ripple and Noise (Vin = 12.0V dc, Vo = 5.0 Vdc, Io=10A).

Figure 10. Transient Response to Dynamic Load Change from 50% to 100% of full load (Vo = 3.3Vdc).

Figure 11. Transient Response to Dynamic Load Change from 100% to 50% of full load (Vo = 3.3 Vdc).

Figure 12. Transient Response to Dynamic Load Change from 50% to 100% of full load (Vo = 3.3 Vdc, Cext = 2x150 μF Polymer Capacitors).

Characteristic Curves (continued)

The following figures provide typical characteristics for the Austin LynxTM 12 V SIP modules at 25°C.

Figure 13. Transient Response to Dynamic Load Change from 100% of 50% full load (Vo = 3.3 Vdc, Cext = 2x150 μF Polymer Capacitors).

Figure 15. Typical Start-Up Using Remote On/Off with Low-ESR external capacitors (Co= 5000μ**F) (Vin = 12.0Vdc, Vo = 5.0Vdc, Io = 10.0A, Co = 1050**μ**F).**

Figure 16. Typical Start-Up with application of Vin with low-ESR polymer capacitors at the output (7x150 μF) (Vin = 12Vdc, Vo = 5.0Vdc, Io = 10A, Co = 1050 μF).

Figure 17 Typical Start-Up Using Remote On/Off with Prebias (Vin = 12.0Vdc, Vo = 2.5Vdc, Io = 1.0A, Vbias =1.2Vdc).

Figure 18. Output short circuit Current (Vin = 12.0Vdc, Vo = 0.75Vdc).

Characteristic Curves (continued)

The following figures provide thermal derating curves for the Austin LynxTM 12 V SIP modules.

Figure 19. Derating Output Current versus Local Ambient Temperature and Airflow (Vin = 12.0 Vdc, Vo=0.75Vdc).

Figure 20. Derating Output Current versus Local Ambient Temperature and Airflow (Vin = 12.0Vdc, Vo=1.8 Vdc).

Figure 21. Derating Output Current versus Local Ambient Temperature and Airflow (Vin = 12.0Vdc, Vo=3.3 Vdc).

Figure 22. Derating Output Current versus Local Ambient Temperature and Airflow (Vin = 12.0 Vdc, Vo=5.0 Vdc).

Test Configurations

Figure 23. Input Reflected Ripple Current Test Setup.

to avoid measurement errors due to socket contact

resistance.

Figure 24. Output Ripple and Noise Test Setup.

NOTE: All voltage measurements to be taken at the module terminals, as shown above. If sockets are used then Kelvin connections are required at the module terminals to avoid measurement errors due to socket contact resistance.

Figure 25. Output Voltage and Efficiency Test Setup.

Efficiency
$$
\eta = \frac{V_0. I_0}{V_{IN} I_{IN}}
$$
 x 100 %

Design Considerations

Input Filtering

Austin Lynx[™] 12V SIP module should be connected to a low-impedance source. A highly inductive source can affect the stability of the module. An input capacitance must be placed directly adjacent to the input pin of the module, to minimize input ripple voltage and ensure module stability.

In a typical application, 4x47 µF low-ESR tantalum capacitors (AVX part #: TPSE476M025R0100, 47µF 25V 100 mΩ ESR tantalum capacitor) will be sufficient to provide adequate ripple voltage at the input of the module. To minimize ripple voltage at the input, low ESR ceramic capacitors are recommended at the input of the module. Figure 26 shows input ripple voltage (mVpp) for various outputs with 4x47 µF tantalum capacitors and with 4x22 µF ceramic capacitor (TDK part #: C4532X5R1C226M) at full load.

Output Voltage (Vdc)

Figure 26. Input ripple voltage for various output with 4x22 µF polymer and 4x47 µF ceramic capacitors at the input (full load).

Design Considerations (continued)

Output Filtering

The Austin LynxTM 12 V SIP module is designed for low output ripple voltage and will meet the maximum output ripple specification with 1 µF ceramic and 10 µF tantalum capacitors at the output of the module. However, additional output filtering may be required by the system designer for a number of reasons. First, there may be a need to further reduce the output ripple and noise of the module. Second, the dynamic response characteristics may need to be customized to a particular load step change.

To reduce the output ripple and improve the dynamic response to a step load change, additional capacitance at the output can be used. Low ESR polymer and ceramic capacitors are recommended to improve the dynamic response of the module. For stable operation of the module, limit the capacitance to less than the maximum output capacitance as specified in the electrical specification table.

Safety Considerations

For safety agency approval the power module must be installed in compliance with the spacing and separation requirements of the end-use safety agency standards, i.e., UL 60950-1, CSA C22.2 No. 60950-1-03, and VDE 0850:2001-12 (EN60950-1) Licensed.

For the converter output to be considered meeting the requirements of safety extra-low voltage (SELV), the input must meet SELV requirements. The power module has extra-low voltage (ELV) outputs when all inputs are ELV.

The input to these units is to be provided with a fastacting fuse with a maximum rating of 20A in the positive input lead.

Feature Description

Remote On/Off

The Austin Lynx[™] 12V SIP power modules feature an On/Off pin for remote On/Off operation. If not using the remote On/Off pin, leave the pin open (module will be On). The On/Off pin signal (Von/Off) is referenced to ground. To switch the module on and off using remote On/Off, connect an open collector npn transistor between the On/Off pin and the ground pin (See Figure 27).

During a logic-high (On/Off pin is pulled high internal to the module) when the transistor is in the Off state, the power module is ON. The maximum allowable leakage current of the transistor when Von/off = $V_{IN,max}$ is 10µA. During a logic-low when the transistor is turned-on, the power module is OFF. During this state VOn/Off is less than 0.3V and the maximum IOn/Off = 1mA.

Figure 27. Remote On/Off Implementation.

Overcurrent Protection

To provide protection in a fault (output overload) condition, the unit is equipped with internal current-limiting circuitry and can endure current limiting continuously. At the point of current-limit inception, the unit enters hiccup mode. The unit operates normally once the output current is brought back into its specified range. The typical average output current during hiccup is 3 A.

Input Undervoltage Lockout

At input voltages below the input undervoltage lockout limit, module operation is disabled. The module will begin to operate at an input voltage above the undervoltage lockout turn-on threshold.

Overtemperature Protection

To provide over temperature protection in a fault condition, the unit relies upon the thermal protection feature of the controller IC. The unit will shutdown if the thermal reference point T_{ref} , exceeds 125 $^{\circ}$ C (typical), but

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the thermal shutdown is not intended as a guarantee that the unit will survive temperatures beyond its rating. The module will automatically restart after it cools down.

Output Voltage Programming

The output voltage adjustment feature allows the output voltage set point to be increased or decreased by connecting an external resistor between the TRIM pin and Vo pin (decrease output voltage) or GND pin (increase output voltage).

To trim up output voltage set point using an external resistor, connect *Rtrim-up* between the TRIM and GND pins (Figure 28). The value of *Rtrim-up* resistor is defined as:

$$
Rtrim - up = \left[\frac{10500}{Vo - Vo, set} - 1000\right]\Omega
$$

Rtrim-up is the external resistor in Ω

Vo,set is the nominal output voltage

Vo is the desired trim-up voltage

For example, to trim up the output voltage of the 1.5V module (AXA010A0M93-SR) by 8% to 1.62V, *Rtrim-up* is calculated as follows:

Vo,set = 1.5V *Vo* = 1.62V:

$$
Rtrim - up = \left[\frac{10500}{1.62 - 1.5} - 1000\right]
$$

$$
Rtrim - up = 86.5k\Omega
$$

Figure 28. Circuit configuration for programming output voltage using an external resistor.

To trim down output voltage set point using an external resistor, connect *Rtrim-down* between TRIM and Vo pins (Figure 29). The value of *Rtrim-down* resistor is defined as:

$$
Rtrim - down = \left[\frac{(Vo - 0.7)15000}{Vo, set - Vo} - 1000\right] \Omega
$$

Feature Descriptions (continued)

Figure 29. Circuit configuration to trim-down output voltage using an external resistor

Rtrim-down is the external resistor in Ω *Vo,set* is the nominal output voltage *Vo*, is the desired trim-down voltage

For example, to trim down the output voltage of the 2.5V module (AXA010A0G93-SR) by 8% to 2.3V, *Rtrim-down* is calculated as follows:

Vo,set = 2.5V

Vo = 2.3V

$$
Rtrim - down = \left[\frac{(2.3 - 0.7)15000}{2.5 - 2.3} - 1000\right] \Omega
$$

$$
Rtrim - down = 119k\Omega
$$

The amount of power delivered by the module is defined as the voltage at the output terminals multiplied by the output current. When using the trim feature, the output voltage of the module can be increased, which at the same output current would increase the power output of the module. Care should be taken to ensure that the maximum output power of the module remains at or below the maximum rated power ($P_{max} = V_{o,set} \times I_{o,max}$).

Remote Sense

The Austin Lynx[™] 12V SIP power modules have a Remote Sense feature to minimize the effects of distribution losses by regulating the voltage at the Remote Sense and GND pins (See Figure 30). The voltage between the Sense pin and Vo pin must not exceed 0.5V. Although both the Remote Sense and the TRIM features can increase the output voltage Vo, the maximum increase is not the sum of both. The maximum

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Vo increase is the larger of either the Remote Sense or TRIM.

The amount of power delivered by the module is defined as the output voltage multiplied by the output current (Vo x Io). When using Remote Sense and/or TRIM, the output voltage of the module can increase, which if the same output is maintained, increases the power output by the module. Make sure that the maximum output power of the module remains at or below the maximum rated power. When the Remote Sense feature is not being used, leave the Remote Sense pin unconnected.

Figure 30. Remote sense circuit configuration

Thermal Considerations

Power modules operate in a variety of thermal environments; however, sufficient cooling should always be provided to help ensure reliable operation.

Considerations include ambient temperature, airflow, module power dissipation, and the need for increased reliability. A reduction in the operating temperature of the module will result in an increase in reliability. The thermal data presented here is based on physical measurements taken in a wind tunnel. The test set-up is shown in Figure 32. Note that the airflow is parallel to the short axis of the module as shown in figure 31. The derating data applies to airflow in either direction of the module's short axis.

Figure 32. Thermal Test Set-up.

Figure 31. Tref Temperature measurement location.

The thermal reference point, T_{ref} used in the specifications is shown in Figure 31. For reliable operation this temperature should not exceed 115°C. The output power of the module should not exceed the rated power of the module (Vo,set x Io,max).

Please refer to the Application Note "Thermal Characterization Process For Open-Frame Board-Mounted Power Modules" for a detailed discussion of thermal aspects including maximum device temperatures.

Heat Transfer via Convection

Increased airflow over the module enhances the heat transfer via convection. Thermal derating curves showing the maximum output current that can be delivered at different local ambient temperatures (T_A) for airflow conditions ranging from natural convection and up to 2m/s (400 ft./min) are shown in the Characteristics Curves section.

Layout Considerations

Copper paths must not be routed beneath the power module. For additional layout guide-lines, refer to the FLTR100V10 application note.

Mechanical Outline

Dimensions are in inches and (millimeters).

Tolerances: x.xx in. \pm 0.02 in. (x.x mm \pm 0.5 mm) [unless otherwise indicated] x.xxx in \pm 0.010 in. (x.xx mm \pm 0.25 mm)

Recommended Pad Layout

Dimensions are in inches and (millimeters).

Tolerances: x.xx in. \pm 0.02 in. (x.x mm \pm 0.5 mm) [unless otherwise indicated]

x.xxx in \pm 0.010 in. (x.xx mm \pm 0.25 mm)

RECOMMENDED HOLE PATTERN
COMPONENT-SIDE FOOTPRINT

Post solder Cleaning and Drying Considerations

Post solder cleaning is usually the final circuit-board assembly process prior to electrical board testing. The result of inadequate cleaning and drying can affect both the reliability of a power module and the testability of the finished circuit-board assembly. For guidance on appropriate soldering, cleaning and drying procedures, refer to *Board Mounted Power Modules: Soldering and Cleaning* Application Note.

Through-Hole Lead-Free Soldering Information

The RoHS-compliant through-hole products use the SAC (Sn/Ag/Cu) Pb-free solder and RoHS-compliant components. They are designed to be processed through single or dual wave soldering machines. The pins have an RoHS-compliant finish that is compatible with both Pb and Pb-free wave soldering processes. A maximum preheat rate of 3°C/s is suggested. The wave preheat process should be such that the temperature of the power module board is kept below 210°C. For Pb solder, the recommended pot temperature is 260°C, while the Pb-free solder pot is 270°C max. Not all RoHS-compliant through-hole products can be processed with paste-through-hole Pb or Pb-free reflow process. If additional information is needed, please consult with your Lineage Power technical representative for more details.

Ordering Information

Please contact your Lineage Power Sales Representative for pricing, availability and optional features.

Table 3. Device Codes

-Z refers to RoHS-compliant versions

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