

# LME49871

## High Performance, High Fidelity Current Feedback Audio Operational Amplifier

### General Description

The LME49871 is an ultra-low distortion, low noise, ultra high slew rate current feedback operational amplifier optimized and fully specified for high performance, high fidelity applications. Combining advanced leading-edge process technology with state-of-the-art circuit design, the LME49871 current feedback operational amplifier delivers superior signal amplification for outstanding performance. Operating on a wide supply range of  $\pm 5V$  to  $\pm 22V$ , the LME49871 combines extremely low voltage noise density ( $1.9nV/\sqrt{Hz}$ ) with very low THD+N (0.00012%) to easily satisfy the most demanding applications. To ensure that the most challenging loads are driven without compromise, the LME49871 has a high slew rate of  $\pm 1900V/\mu s$  and an output current capability of  $\pm 100mA$ . Further, dynamic range is maximized by an output stage that drives  $150\Omega$  loads to within 2.9V of either power supply voltage.

The LME49871's outstanding CMRR (88dB), PSRR (102dB), and  $V_{OS}$  (0.05mV) give the amplifier excellent operational amplifier DC performance.

The LME49871 is available in an 8-lead narrow body SOIC. Demonstration boards are available.

### Key Specifications

■ Power Supply Voltage Range	$\pm 5V$ to $\pm 22V$
■ THD+N ( $A_V = 1$ , $R_L = 100\Omega$ , $V_{OUT} = 2V_{P-P}$ , $f = 1kHz$ )	0.00021% (typ)
■ THD+N ( $A_V = 1$ , $R_L = 600\Omega$ , $V_{OUT} = 1.4V_{RMS}$ , $f = 1kHz$ )	0.00012% (typ)
■ Input Noise Density	$1.9nV/\sqrt{Hz}$ (typ)
■ Slew Rate	$\pm 1900V/\mu s$ (typ)
■ Bandwidth ( $A_V = 1$ , $R_L = 2k\Omega$ , $R_F = 800\Omega$ )	213MHz (typ)
■ Input Bias Current	1.8 $\mu A$ (typ)
■ Input Offset Voltage	0.05mV (typ)
■ PSRR	102dB (typ)
■ CMRR	90dB (typ)

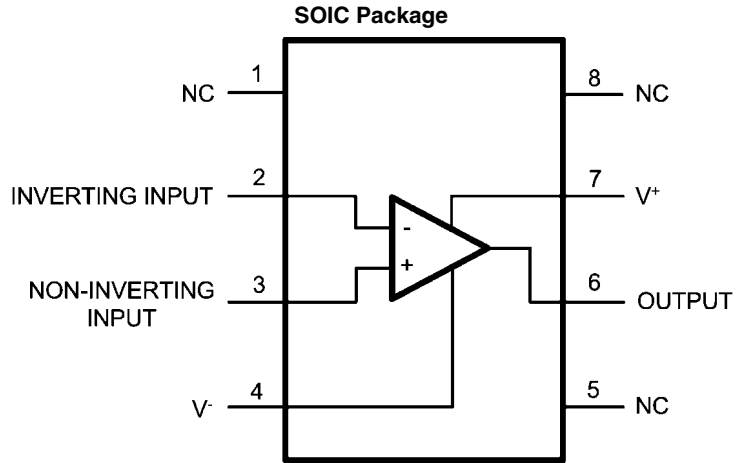
### Features

- Easily drives  $150\Omega$  loads
- Optimized for superior audio signal fidelity
- Output short circuit protection
- SOIC package

### Applications

- Ultra high quality audio amplification
- High fidelity preamplifiers
- High fidelity multimedia
- State of the art phono pre amps
- High performance professional audio
- High fidelity equalization and crossover networks
- High performance line drivers
- High performance line receivers
- High fidelity active filters

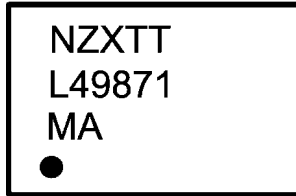
# Connection Diagrams



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Order Number LME49871MA  
See NS Package Number M08A

LME49871MA Top Mark



30042602

N = National Logo  
Z = Assembly plant code  
X = 1 Digit date code  
TT = Die traceability  
L49871 = LME49871  
MA = Package code

**Absolute Maximum Ratings** (Notes 1, 2)

If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/ Distributors for availability and specifications.

Power Supply Voltage ( $V_S = V^+ - V^-$ )	46V
Storage Temperature	-65°C to 150°C
Input Voltage ( $V^-$ ) - 0.7V to ( $V^+$ ) + 0.7V	
Output Short Circuit (Note 3)	Continuous
Power Dissipation	Internally Limited

ESD Rating (Note 4)	2000V
ESD Rating (Note 5)	
Pins 1, 4, 7 and 8	200V
Pins 2, 3, 5 and 6	100V
Junction Temperature	150°C
Thermal Resistance	
$\theta_{JA}$ (MA)	145°C/W
Temperature Range	
$T_{MIN} \leq T_A \leq T_{MAX}$	-40°C $\leq T_A \leq$ 85°C
Supply Voltage Range	$\pm 5.0V \leq V_S \leq \pm 22V$

**Electrical Characteristics** (Notes 1, 2) The following specifications apply for  $\pm 22V$ ,  $R_L = 2k\Omega$ ,  $R_{SOURCE} = 10\Omega$ ,  $f_{IN} = 1kHz$ , and  $T_A = 25^\circ C$ , unless otherwise specified.

Symbol	Parameter	Conditions	LME49871		Units (Limits)
			Typical	Limit	
			(Note 6)	(Note 7)	
THD+N	Total Harmonic Distortion + Noise	$A_V = 1$ , $f = 1kHz$ , $R_F = 1.2k\Omega$	0.00021		%
		$R_L = 100\Omega$ , $V_{OUT} = 3V_{RMS}$ $R_L = 600\Omega$ , $V_{OUT} = 1.4V_{RMS}$	0.00012		%
IMD	Intermodulation Distortion	$A_V = 1$ , $V_{IN} = 3V_{RMS}$ Two-tone, 60Hz & 7kHz 4:1	0.00009		%
BW	Bandwidth	$A_V = -1$ , $R_F = 800\Omega$	213		MHz
SR	Slew Rate	$V_{OUT} = 20V_{P-P}$ , $A_V = -5$	$\pm 1900$		V/ $\mu s$
FPBW	Full Power Bandwidth	$V_{OUT} = 20V_{P-P}$ , -3dB referenced to output magnitude at $f = 1kHz$ , $A_V = 1$	30		MHz
$t_s$	Settling Time	$A_V = -1$ , 10V step, 0.1% error range	50		ns
$e_n$	Equivalent Input Noise Voltage	$f_{BW} = 20Hz$ to 20kHz	0.26	0.6	$\mu V_{RMS}$ (max)
	Equivalent Input Noise Density	$f = 1kHz$ $f = 10Hz$	1.9 11.5	4.0	$nV/\sqrt{Hz}$ (max)
$i_n$	Current Noise Density	$f = 1kHz$	16		$pA/\sqrt{Hz}$
		$f = 10Hz$	160		$pA/\sqrt{Hz}$
$V_{OS}$	Input Offset Voltage		$\pm 0.05$	$\pm 1.0$	mV (max)
$\Delta V_{OS}/\Delta Temp$	Average Input Offset Voltage Drift vs Temperature	-40°C $\leq T_A \leq$ 85°C	0.29		$\mu V/^\circ C$
PSRR	Average Input Offset Voltage Shift vs Power Supply Voltage	$V_S = \pm 22V$ , $\Delta V_S = 30V$ (Note 8)	102	100	dB (min)
$I_B$	Input Bias Current	$V_{CM} = 0V$	1.8	6	$\mu A$ (max)
$\Delta I_{OS}/\Delta Temp$	Input Bias Current Drift vs Temperature	-40°C $\leq T_A \leq$ 85°C			
		Inverting input Non-inverting input	4.5 4.7		nA/ $^\circ C$ nA/ $^\circ C$
$I_{OS}$	Input Offset Current	$V_{CM} = 0V$	1.3	5	$\mu A$ (max)
$V_{IN-CM}$	Common-Mode Input Voltage Range	$V_S = \pm 22V$	$\pm 20.5$	( $V^+$ ) - 1.0 ( $V^-$ ) + 1.0	V (min) V (min)
CMRR	Common-Mode Rejection	-10V $\leq V_{CM} \leq$ 10V	90	86	dB (min)
$Z_{IN}$	Non-inverting-input Input Impedance	-10V $\leq V_{CM} \leq$ 10V	1.2		M $\Omega$
	Inverting-input Input Impedance	-10V $\leq V_{CM} \leq$ 10V	58		$\Omega$
$Z_T$	Transimpedance	$V_{OUT} = \pm 10V$			
		$R_L = 200\Omega$ $R_L = \infty$	4.2 4.7	2.0 2.65	M $\Omega$ (min) M $\Omega$ (min)

Symbol	Parameter	Conditions	LME49871		Units (Limits)
			Typical	Limit	
			(Note 6)	(Note 7)	
V <sub>OUTMAX</sub>	Maximum Output Voltage Swing	R <sub>L</sub> = 150Ω	±18.6	±17.6	V (min)
		R <sub>L</sub> = 600Ω	±19.4	±18.4	V (min)
I <sub>OUT</sub>	Output Current	R <sub>L</sub> = 150Ω, V <sub>S</sub> = ±22V	±100	±93	mA (min)
I <sub>OUT-CC</sub>	Instantaneous Short Circuit Current		±140		mA
R <sub>OUT</sub>	Output Resistance	f <sub>IN</sub> = 5MHz Open-Loop	10		Ω
I <sub>S</sub>	Total Quiescent Current	I <sub>OUT</sub> = 0mA	8.3	9.5	mA (max)

**Note 1:** "Absolute Maximum Ratings" indicate limits beyond which damage to the device may occur, including inoperability and degradation of device reliability and/or performance. Functional operation of the device and/or non-degradation at the *Absolute Maximum Ratings* or other conditions beyond those indicated in the *Recommended Operating Conditions* is not implied. The *Recommended Operating Conditions* indicate conditions at which the device is functional and the device should not be operated beyond such conditions. All voltages are measured with respect to the ground pin, unless otherwise specified.

**Note 2:** The *Electrical Characteristics* tables list guaranteed specifications under the listed *Recommended Operating Conditions* except as otherwise modified or specified by the *Electrical Characteristics Conditions* and/or Notes. Typical specifications are estimations only and are not guaranteed.

**Note 3:** Amplifier output connected to GND, any number of amplifiers within a package.

**Note 4:** Human body model, applicable std. JESD22-A114C.

**Note 5:** Machine model, applicable std. JESD22-A115-A.

**Note 6:** Typical values represent most likely parametric norms at T<sub>A</sub> = +25°C, and at the *Recommended Operation Conditions* at the time of product characterization and are not guaranteed.

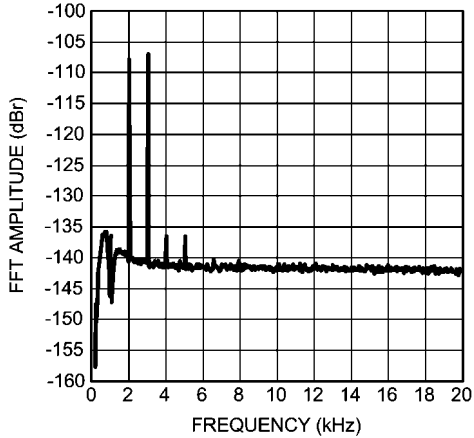
**Note 7:** Datasheet min/max specification limits are guaranteed by test or statistical analysis.

**Note 8:** PSRR is measured as follows: V<sub>OS</sub> is measured at two supply voltages, ±7V and ±22V. PSRR = |20log(ΔV<sub>OS</sub>/ΔV<sub>S</sub>)|.

## Typical Performance Characteristics

FFT of 1kHz Sinewave, 0dB Input Magnitude

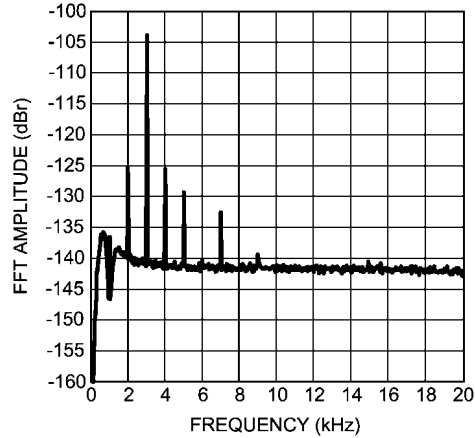
$$V_{OUT} = 3V_{RMS}, R_L = 1k\Omega, V_S = \pm 15V, A_V = 1$$



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FFT of 1kHz Sinewave, 0dB Input Magnitude

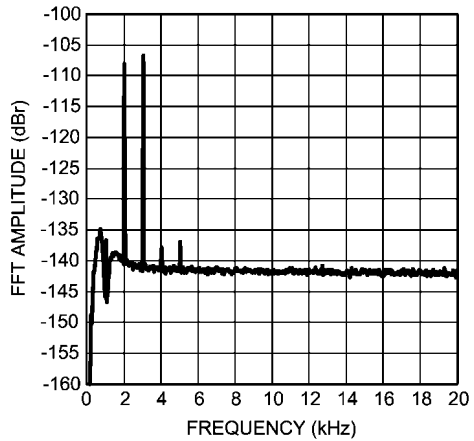
$$V_{OUT} = 3V_{RMS}, R_L = 100\Omega, V_S = \pm 15V, A_V = 1$$



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FFT of 1kHz Sinewave, 0dB Input Magnitude

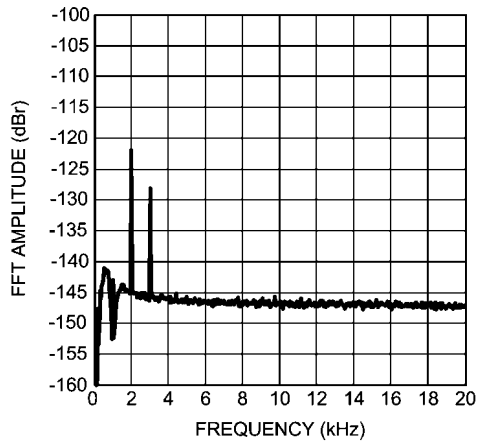
$$V_{OUT} = 3V_{RMS}, R_L = 600\Omega, V_S = \pm 15V, A_V = 1$$



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FFT of 1kHz Sinewave, 0dB Input Magnitude

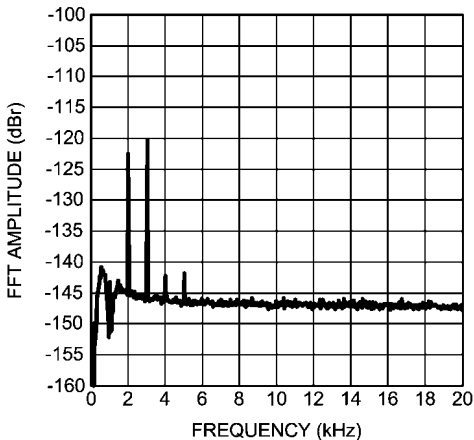
$$V_{OUT} = 1.4V_{RMS}, R_L = 1k\Omega, V_S = \pm 15V, A_V = 1$$



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FFT of 1kHz Sinewave, 0dB Input Magnitude

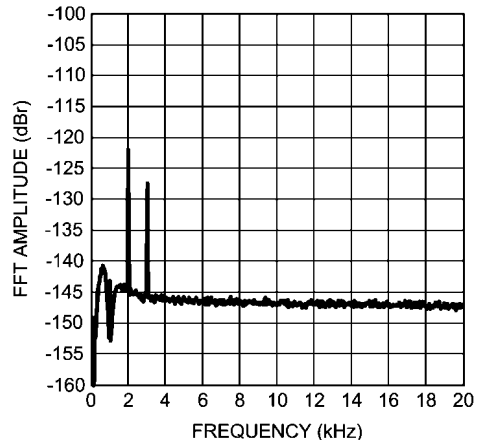
$$V_{OUT} = 1.4V_{RMS}, R_L = 100\Omega, V_S = \pm 15V, A_V = 1$$



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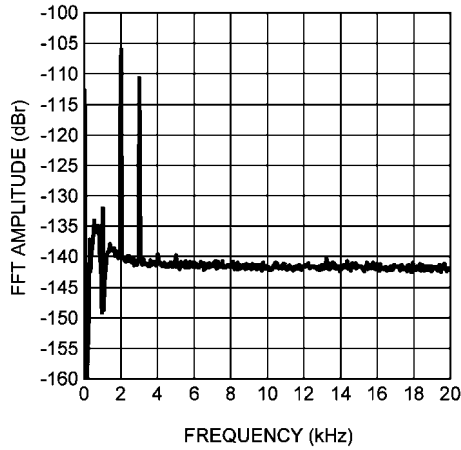
FFT of 1kHz Sinewave, 0dB Input Magnitude

$$V_{OUT} = 1.4V_{RMS}, R_L = 600\Omega, V_S = \pm 15V, A_V = 1$$



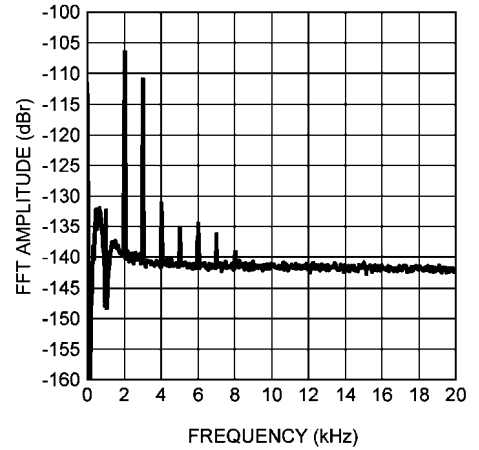
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FFT of 1kHz Sinewave, 0dB Input Magnitude  
 $V_{OUT} = 3V_{RMS}$ ,  $R_L = 1k\Omega$ ,  $V_S = \pm 22V$ ,  $A_V = 1$



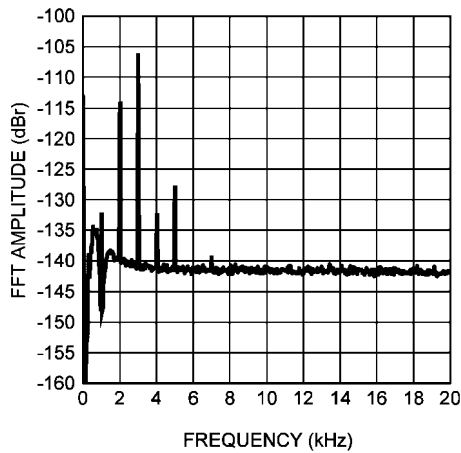
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FFT of 1kHz Sinewave, 0dB Input Magnitude  
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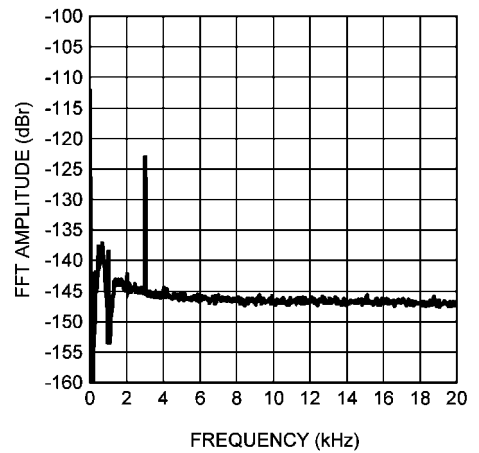
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FFT of 1kHz Sinewave, 0dB Input Magnitude  
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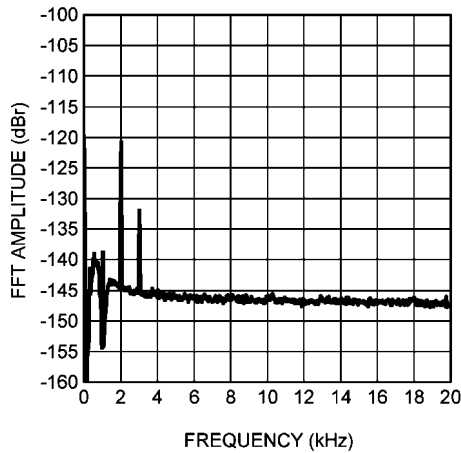
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FFT of 1kHz Sinewave, 0dB Input Magnitude  
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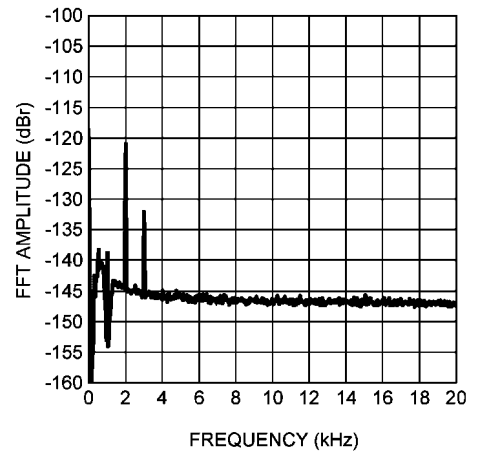
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FFT of 1kHz Sinewave, 0dB Input Magnitude  
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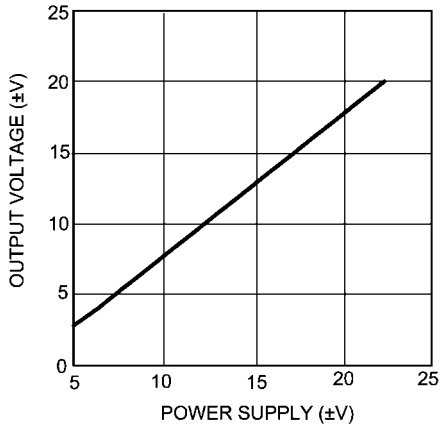
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FFT of 1kHz Sinewave, 0dB Input Magnitude  
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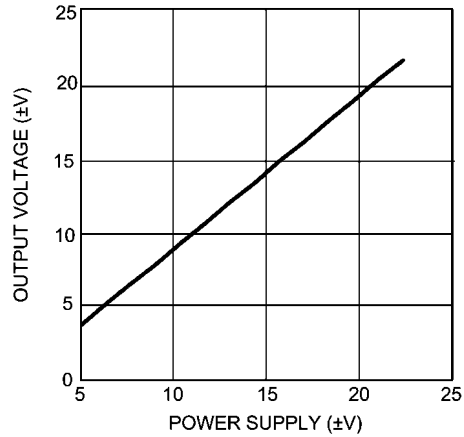
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**Output Voltage vs Supply Voltage**  
 $A_V = 1, R_L = 600\Omega, 1\% \text{ THD+N}$



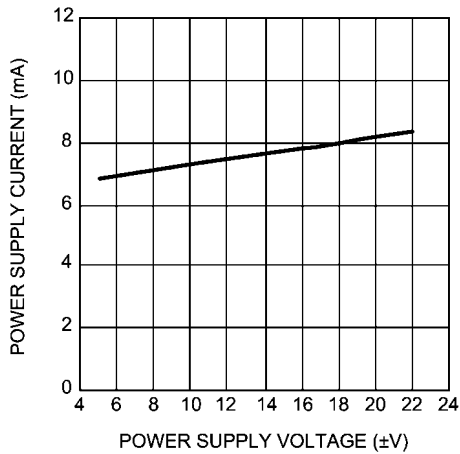
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**Output Voltage vs Supply Voltage**  
 $A_V = 1, R_L = \text{open}, 1\% \text{ THD+N}$



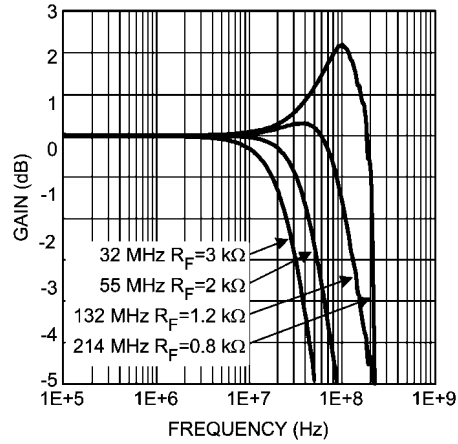
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**Supply Current ( $I_{CC}$ ) vs Power Supply**  
 $R_L = \text{open}$



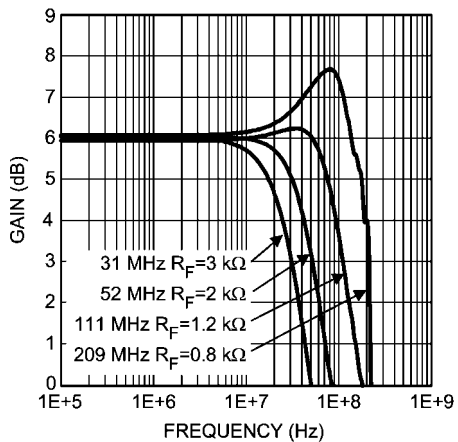
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**Gain vs Frequency**  
 $V_S = \pm 15V, G = -1$



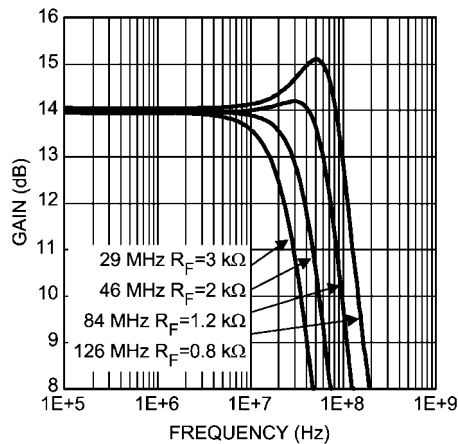
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**Gain vs Frequency**  
 $V_S = \pm 15V, G = -2$

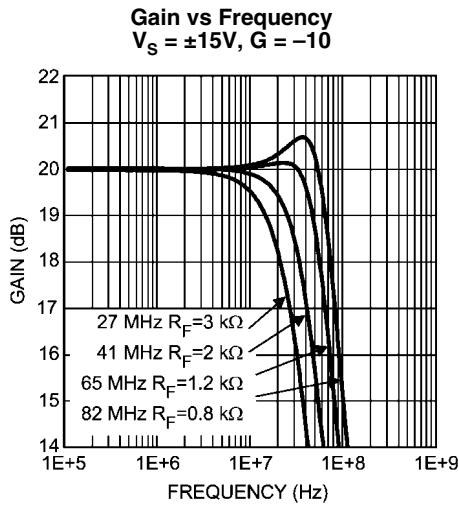


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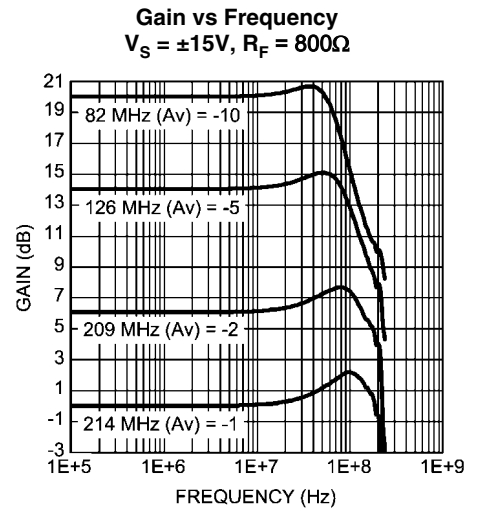
**Gain vs Frequency**  
 $V_S = \pm 15V, G = -5$



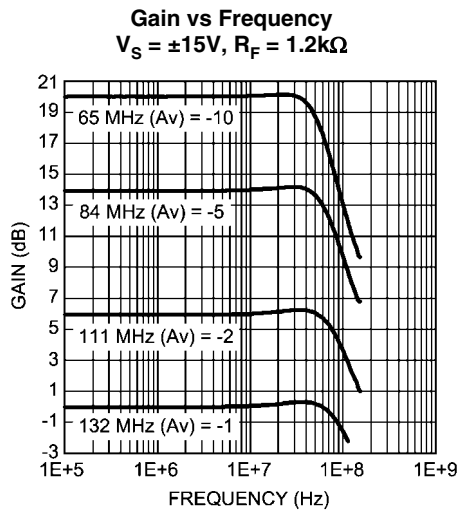
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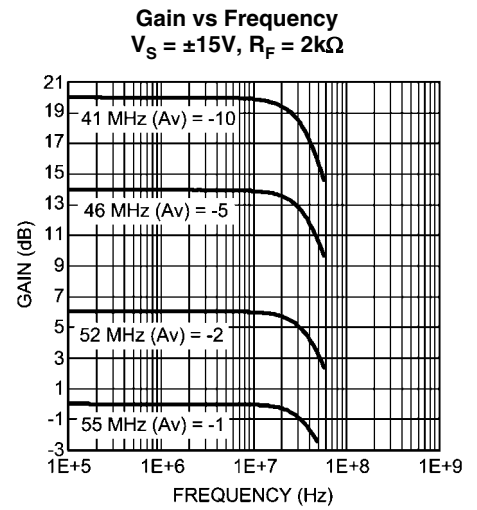
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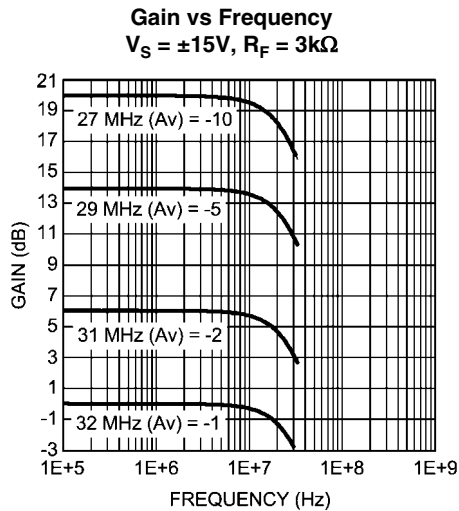
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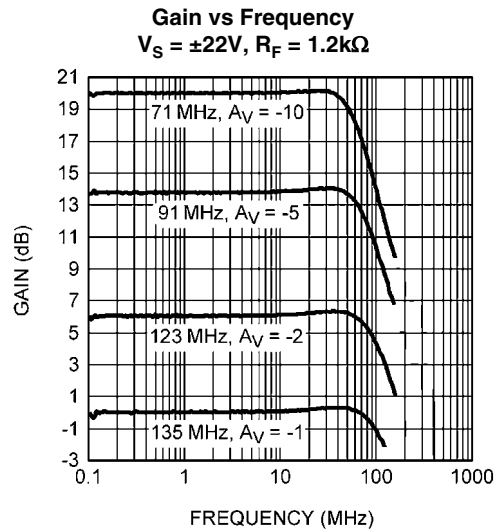
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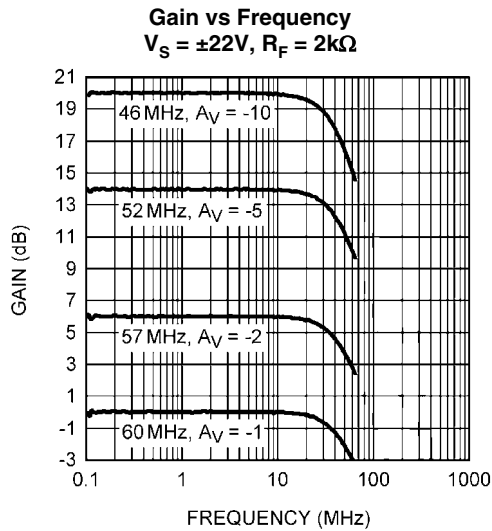


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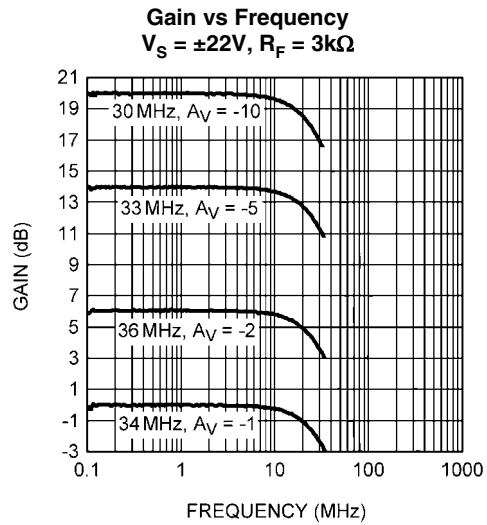


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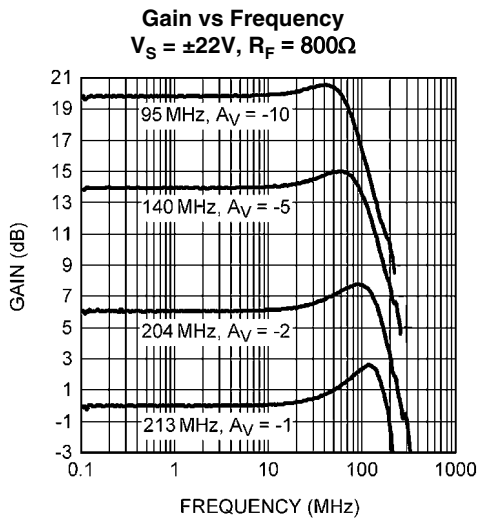




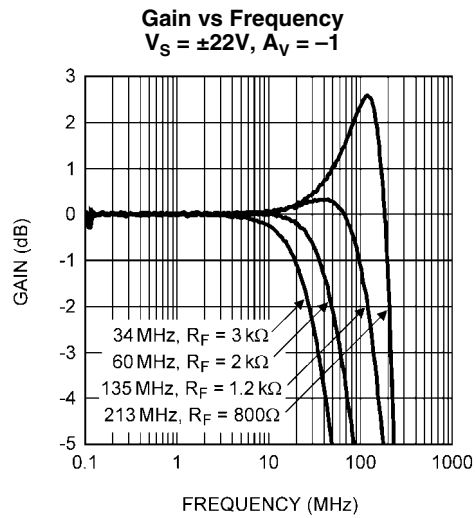
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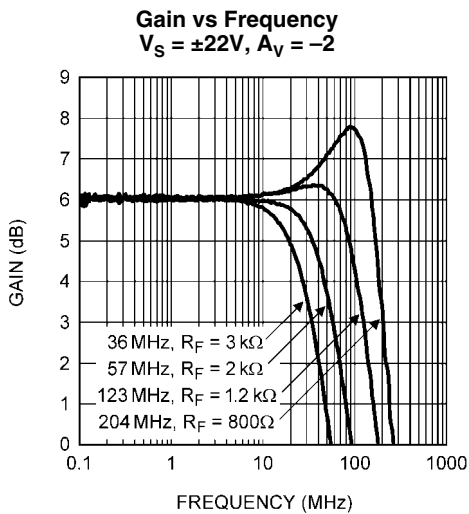
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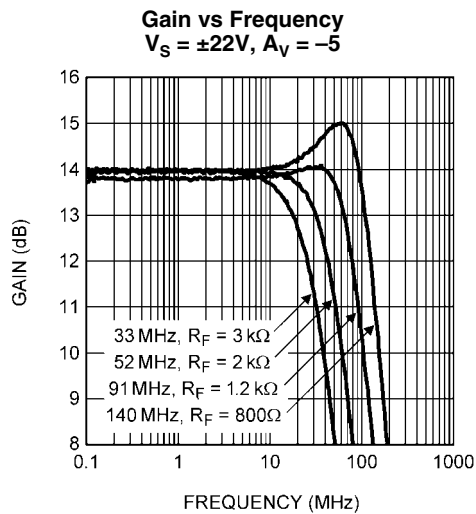
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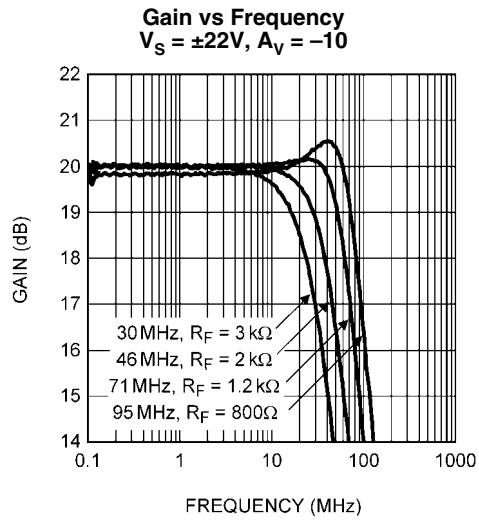
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## Application Information

### GENERAL AMPLIFIER FUNCTION

oltage feedback amplifiers have a small-signal bandwidth that is a function of the closed-loop gain. Conversely, the LME49871 current feedback amplifier features a small-signal bandwidth that is relatively independent of the closed-loop gain. This is shown in *Figure 1* where the LME49871's gain is  $-1$ ,  $-2$ ,  $-5$  and  $-10$ . Like all current feedback amplifiers, the LME49871's closed-loop bandwidth is a function of the feedback resistance value. Therefore,  $R_s$  must be varied to select the desired closed-loop gain.

### POWER SUPPLY BYPASSING AND LAYOUT CONSIDERATIONS

Properly placed and correctly valued supply bypassing is essential for optimized high-speed amplifier operation. The supply bypassing must maintain a wideband, low-impedance capacitive connection between the amplifier's supply pin and ground. This helps preserve high speed signal and fast transient fidelity. The bypassing is easily accomplished using a parallel combination of a  $10\mu\text{F}$  tantalum and a  $0.1\mu\text{F}$  ceramic capacitors for each power supply pin. The bypass capacitors should be placed as close to the amplifier power supply pins as possible.

### FEEDBACK RESISTOR SELECTION ( $R_f$ )

The value of the  $R_f$  is also a dominant factor in compensating the LME49871. For general applications, the LME49871 will maintain specified performance with an  $1.2\text{k}\Omega$  feedback resistor. Although this value will provide good results for most applications, it may be advantageous to adjust this value slightly for best pulse response optimized for the desired bandwidth. In addition to reducing bandwidth, increasing the feedback resistor value also reduces overshoot in the time domain response.

### SLEW RATE CONSIDERATIONS

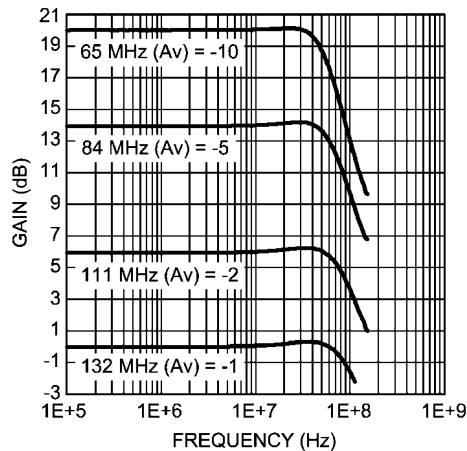
A current feedback amplifier's slew rate characteristics are different than that of voltage feedback amplifiers. A voltage feedback amplifier's slew rate limiting or non-linear amplifier behavior is dominated by the finite availability of the first stage tail current charging the second stage voltage amplifier's compensation capacitor. Conversely, a current feedback amplifier's slew rate is not constant. Transient current at the inverting input determines slew rate for both inverting and non-inverting gains. The non-inverting configuration slew rate is also determined by input stage limitations. Accordingly, variations of slew rates occur for different circuit topologies.

### DRIVING CAPACITIVE LOADS

The LME49871 can drive significantly higher capacitive loads than many current feedback amplifiers. Although the LME49871 can directly drive as much as  $100\text{pF}$  without oscillating, the resulting response will be a function of the feedback resistor value.

### CAPACITIVE FEEDBACK

It is quite common to place a small lead-compensation capacitor in parallel with a voltage feedback amplifier's feedback resistance,  $R_f$ . This compensation reduces the amplifier's peaking in the frequency domain and damps the transient response. Whereas this yields the expected results when used with voltage feedback amplifiers, this technique must not be used with current feedback amplifiers. The dynamic impedance of capacitors in the feedback loop reduces the amplifier's stability. Instead, reduced peaking in the frequency response and bandwidth limiting can be accomplished by adding an RC circuit to the amplifier's input.



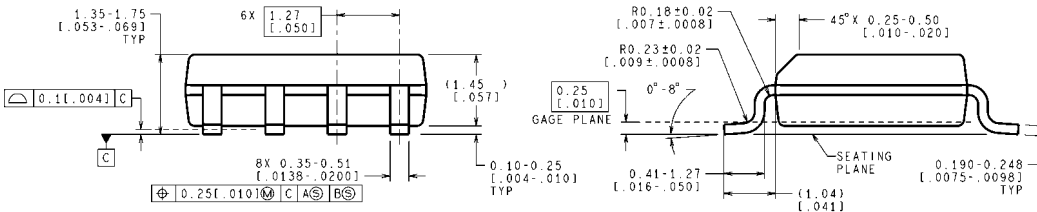
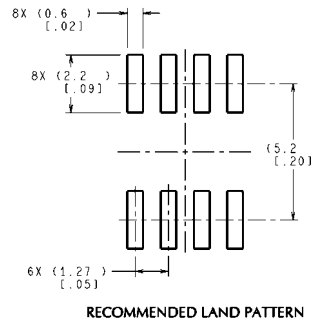
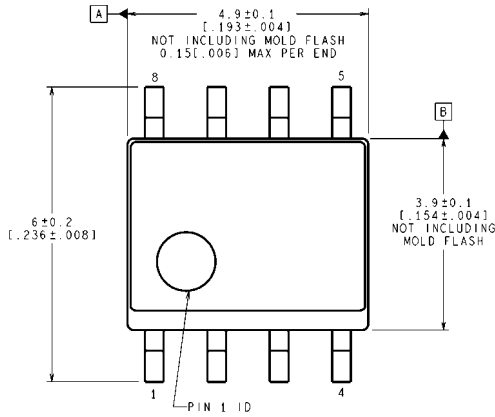
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FIGURE 1. Bandwidth as a function of gain

## Revision History

Rev	Date	Description
1.0	04/24/08	Initial release.
1.01	04/28/08	Changed the Limit values on $V_{IN-CM}$ from $-2.0$ and $+2.0$ to $-1.0$ and $+1.0$ .

**Physical Dimensions** inches (millimeters) unless otherwise noted



CONTROLLING DIMENSION IS MILLIMETER  
VALUES IN [ ] ARE INCHES  
DIMENSIONS IN ( ) FOR REFERENCE ONLY

**SOIC Package**  
**Order Number LME49871MA**  
**NS Package Number M08A**

M08A (Rev L)

## Notes

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Displays	<a href="http://www.national.com/displays">www.national.com/displays</a>	Green Compliance	<a href="http://www.national.com/quality/green">www.national.com/quality/green</a>
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LDOs	<a href="http://www.national.com/ldo">www.national.com/ldo</a>		
LED Lighting	<a href="http://www.national.com/led">www.national.com/led</a>		
PowerWise	<a href="http://www.national.com/powerwise">www.national.com/powerwise</a>		
Serial Digital Interface (SDI)	<a href="http://www.national.com/sdi">www.national.com/sdi</a>		
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