

### FEATURES

Excellent Video Specifications ( $R_L = 150 \Omega$ ,  $G = +2$ )

Gain Flatness 0.1 dB to 60 MHz

0.01% Differential Gain Error

0.02° Differential Phase Error

### Low Power

5.5 mA/Amp Max Power Supply Current (55 mW)

### High Speed and Fast Settling

600 MHz, -3 dB Bandwidth ( $G = +1$ )

500 MHz, -3 dB Bandwidth ( $G = +2$ )

1200 V/ $\mu$ s Slew Rate

16 ns Settling Time to 0.1%

### Low Distortion

-65 dBc THD,  $f_c = 5$  MHz

33 dBm Third Order Intercept,  $F_1 = 10$  MHz

-66 dB SFDR,  $f = 5$  MHz

-60 dB Crosstalk,  $f = 5$  MHz

### High Output Drive

Over 70 mA Output Current

Drives Up to Eight Back-Terminated 75  $\Omega$  Loads

(Four Loads/Side) While Maintaining Good  
Differential Gain/Phase Performance (0.01%/0.17°)

Available in 8-Lead Plastic DIP, SOIC and  $\mu$ SOIC Packages

### APPLICATIONS

A-to-D Driver

Video Line Driver

Differential Line Driver

Professional Cameras

Video Switchers

Special Effects

RF Receivers

### PRODUCT DESCRIPTION

The AD8002 is a dual, low-power, high-speed amplifier designed to operate on  $\pm 5$  V supplies. The AD8002 features unique transimpedance linearization circuitry. This allows it to drive video loads with excellent differential gain and phase performance on only 50 mW of power per amplifier. The AD8002 is a current feedback amplifier and features gain flatness of 0.1 dB to 60 MHz while offering differential gain and phase error of 0.01% and 0.02°. This makes the AD8002 ideal for professional video electronics such as cameras and video switchers. Additionally, the AD8002's low distortion and fast settling make it ideal for buffer high-speed A-to-D converters.

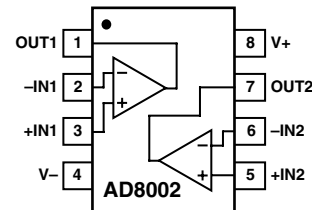
The AD8002 offers low power of 5.5 mA/amplifier max ( $V_S = \pm 5$  V) and can run on a single 12 V power supply, while capable of delivering over 70 mA of load current. It is offered in an 8-lead plastic DIP, SOIC, and  $\mu$ SOIC package. These features make this amplifier ideal for portable and battery-powered applications where size and power are critical.

### REV. D

Information furnished by Analog Devices is believed to be accurate and reliable. However, no responsibility is assumed by Analog Devices for its use, nor for any infringements of patents or other rights of third parties which may result from its use. No license is granted by implication or otherwise under any patent or patent rights of Analog Devices.

### FUNCTIONAL BLOCK DIAGRAM

8-Lead Plastic DIP, SOIC, and  $\mu$ SOIC



The outstanding bandwidth of 600 MHz along with 1200 V/ $\mu$ s of slew rate make the AD8002 useful in many general purpose high speed applications where dual power supplies of up to  $\pm 6$  V and single supplies from 6 V to 12 V are needed. The AD8002 is available in the industrial temperature range of  $-40^\circ\text{C}$  to  $+85^\circ\text{C}$ .

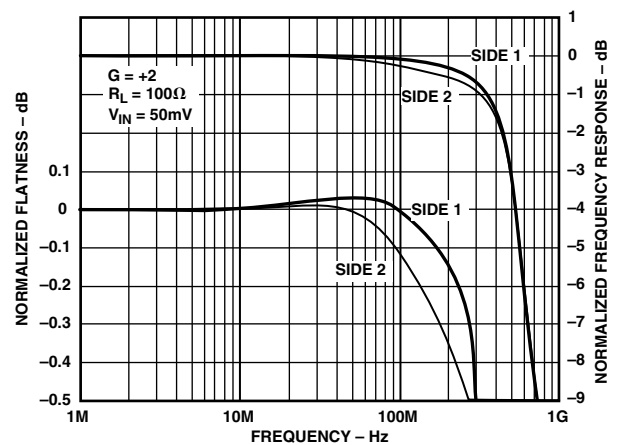


Figure 1. Frequency Response and Flatness,  $G = +2$

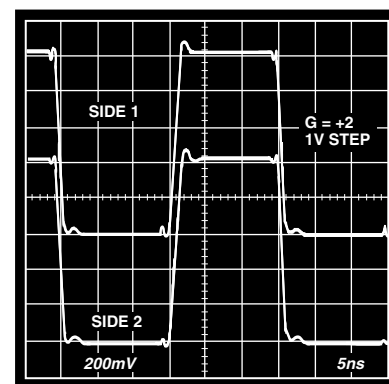


Figure 2. 1 V Step Response,  $G = +1$

# AD8002—SPECIFICATIONS (@ T<sub>A</sub> = 25°C, V<sub>S</sub> = ±5 V, R<sub>L</sub> = 100 Ω, R<sub>C</sub><sup>1</sup> = 75 Ω, unless otherwise noted.)

Model	Conditions	AD8002A			Unit	
		Min	Typ	Max		
<b>DYNAMIC PERFORMANCE</b>						
-3 dB Small Signal Bandwidth,	N Package	G = +2, R <sub>F</sub> = 750 Ω	500		MHz	
	R Package	G = +1, R <sub>F</sub> = 1.21 kΩ	600		MHz	
Bandwidth for 0.1 dB Flatness	R Package	G = +2, R <sub>F</sub> = 681 Ω	500		MHz	
	RM Package	G = +1, R <sub>F</sub> = 953 Ω	600		MHz	
Slew Rate	RM Package	G = +2, R <sub>F</sub> = 681 Ω	500		MHz	
	N Package	G = +1, R <sub>F</sub> = 1 kΩ	600		MHz	
Settling Time to 0.1% Rise and Fall Time	N Package	G = +2, R <sub>F</sub> = 750 Ω	60		MHz	
	R Package	G = +2, R <sub>F</sub> = 681 Ω	90		MHz	
Slew Rate	R Package	G = +2, R <sub>F</sub> = 681 Ω	60		MHz	
	RM Package	G = +2, V <sub>O</sub> = 2 V Step	700		V/μs	
Settling Time to 0.1% Rise and Fall Time		G = -1, V <sub>O</sub> = 2 V Step	1200		V/μs	
		G = +2, V <sub>O</sub> = 2 V Step	16		ns	
		G = +2, V <sub>O</sub> = 2 V Step, R <sub>F</sub> = 750 Ω	2.4		ns	
<b>NOISE/HARMONIC PERFORMANCE</b>						
Total Harmonic Distortion		f <sub>C</sub> = 5 MHz, V <sub>O</sub> = 2 V p-p G = +2, R <sub>L</sub> = 100 Ω	-65		dBc	
Crosstalk, Output to Output		f = 5 MHz, G = +2	-60		dB	
Input Voltage Noise		f = 10 kHz, R <sub>C</sub> = 0 Ω	2.0		nV/√Hz	
Input Current Noise		f = 10 kHz, +In	2.0		pA/√Hz	
		-In	18		pA/√Hz	
Differential Gain Error		NTSC, G = +2, R <sub>L</sub> = 150 Ω	0.01		%	
Differential Phase Error		NTSC, G = +2, R <sub>L</sub> = 150 Ω	0.02		Degree	
Third Order Intercept		f = 10 MHz	33		dBm	
1 dB Gain Compression		f = 10 MHz	14		dBm	
SFDR		f = 5 MHz	-66		dB	
<b>DC PERFORMANCE</b>						
Input Offset Voltage			2.0	6	mV	
		T <sub>MIN</sub> -T <sub>MAX</sub>	2.0	9	mV	
Offset Drift			10		μV/°C	
-Input Bias Current			5.0	25	±μA	
		T <sub>MIN</sub> -T <sub>MAX</sub>		35	±μA	
+Input Bias Current			3.0	6.0	±μA	
		T <sub>MIN</sub> -T <sub>MAX</sub>		10	±μA	
Open Loop Transresistance		T <sub>MIN</sub> -T <sub>MAX</sub> V <sub>O</sub> = ±2.5 V	250	900	kΩ	
		T <sub>MIN</sub> -T <sub>MAX</sub>	175		kΩ	
<b>INPUT CHARACTERISTICS</b>						
Input Resistance	+Input		10		MΩ	
	-Input		50		Ω	
Input Capacitance	+Input		1.5		pF	
Input Common-Mode Voltage Range			3.2		±V	
Common-Mode Rejection Ratio		V <sub>CM</sub> = ±2.5 V	49	54	dB	
	Offset Voltage	V <sub>CM</sub> = ±2.5 V, T <sub>MIN</sub> -T <sub>MAX</sub>	0.3	1.0	μA/V	
-Input Current		V <sub>CM</sub> = ±2.5 V, T <sub>MIN</sub> -T <sub>MAX</sub>	0.2	0.9	μA/V	
+Input Current						
<b>OUTPUT CHARACTERISTICS</b>						
Output Voltage Swing		R <sub>L</sub> = 150 Ω	2.7	3.1	±V	
Output Current <sup>2</sup>				70	mA	
Short Circuit Current <sup>2</sup>			85	110	mA	
<b>POWER SUPPLY</b>						
Operating Range			±3.0	±6.0	V	
Quiescent Current/Both Amplifiers		T <sub>MIN</sub> -T <sub>MAX</sub>		10.0	11.5	mA
		+V <sub>S</sub> = +4 V to +6 V, -V <sub>S</sub> = -5 V	60	75	dB	
Power Supply Rejection Ratio		-V <sub>S</sub> = -4 V to -6 V, +V <sub>S</sub> = +5 V	49	56	dB	
-Input Current		T <sub>MIN</sub> -T <sub>MAX</sub>	0.5	2.5	μA/V	
+Input Current		T <sub>MIN</sub> -T <sub>MAX</sub>	0.1	0.5	μA/V	

## NOTES

<sup>1</sup>R<sub>C</sub> is recommended to reduce peaking and minimize input reflections at frequencies above 300 MHz. However, R<sub>C</sub> is not required.

<sup>2</sup>Output current is limited by the maximum power dissipation in the package. See the power derating curves.

Specifications subject to change without notice.

## ABSOLUTE MAXIMUM RATINGS<sup>1</sup>

Supply Voltage . . . . .	13.2 V
Internal Power Dissipation <sup>2</sup>	
Plastic DIP Package (N) . . . . .	1.3 W
Small Outline Package (R) . . . . .	0.9 W
$\mu$ SOIC Package (RM) . . . . .	0.6 W
Input Voltage (Common Mode) . . . . .	$\pm V_S$
Differential Input Voltage . . . . .	$\pm 1.2$ V
Output Short Circuit Duration	Observe Power Derating Curves
Storage Temperature Range N, R, RM . . . . .	-65°C to +125°C
Operating Temperature Range (A Grade) . . . . .	-40°C to +85°C
Lead Temperature Range (Soldering 10 sec) . . . . .	300°C

## NOTES

<sup>1</sup>Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

<sup>2</sup>Specification is for device in free air:

8-Lead Plastic DIP Package:  $\theta_{JA} = 90^\circ\text{C}/\text{W}$

8-Lead SOIC Package:  $\theta_{JA} = 155^\circ\text{C}/\text{W}$

8-Lead  $\mu$ SOIC Package:  $\theta_{JA} = 200^\circ\text{C}/\text{W}$

## MAXIMUM POWER DISSIPATION

The maximum power that can be safely dissipated by the AD8002 is limited by the associated rise in junction temperature. The maximum safe junction temperature for plastic encapsulated devices is determined by the glass transition temperature of the plastic, approximately 150°C. Exceeding this limit temporarily may cause a shift in parametric performance due to a change in the stresses exerted on the die by the package. Exceeding a junction temperature of 175°C for an extended period can result in device failure.

While the AD8002 is internally short circuit protected, this may not be sufficient to guarantee that the maximum junction temperature (150°C) is not exceeded under all conditions. To ensure proper operation, it is necessary to observe the maximum power derating curves.

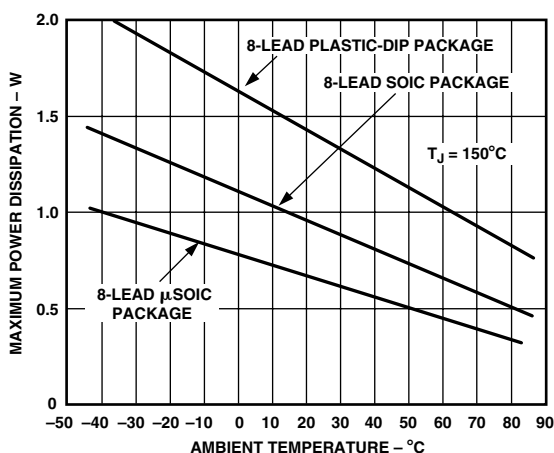


Figure 3. Plot of Maximum Power Dissipation vs. Temperature

## ORDERING GUIDE

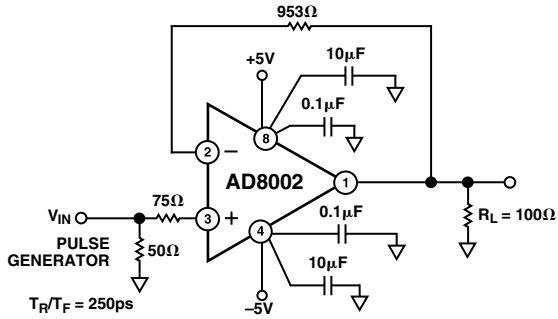
Model	Temperature Range	Package Description	Package Option	Brand Code
AD8002AN	-40°C to +85°C	8-Lead PDIP	N-8	Standard
AD8002AR	-40°C to +85°C	8-Lead SOIC	SO-8	Standard
AD8002AR-REEL	-40°C to +85°C	8-Lead SOIC 13" REEL	SO-8	Standard
AD8002AR-REEL7	-40°C to +85°C	8-Lead SOIC 7" REEL	SO-8	Standard
AD8002ARM	-40°C to +85°C	8-Lead $\mu$ SOIC	RM-8	HFA
AD8002ARM-REEL	-40°C to +85°C	8-Lead $\mu$ SOIC 13" REEL	RM-8	HFA
AD8002ARM-REEL7	-40°C to +85°C	8-Lead $\mu$ SOIC 7" REEL	RM-8	HFA

## CAUTION

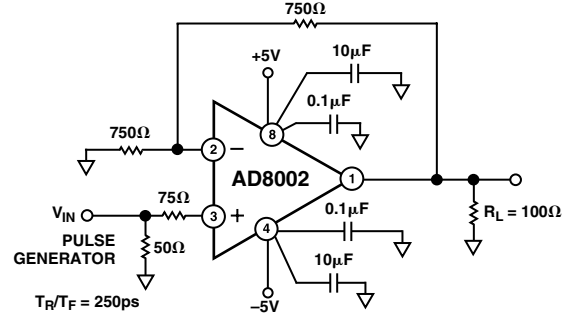
ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily accumulate on the human body and test equipment and can discharge without detection. Although the AD8002 features proprietary ESD protection circuitry, permanent damage may occur on devices subjected to high-energy electrostatic discharges. Therefore, proper ESD precautions are recommended to avoid performance degradation or loss of functionality.



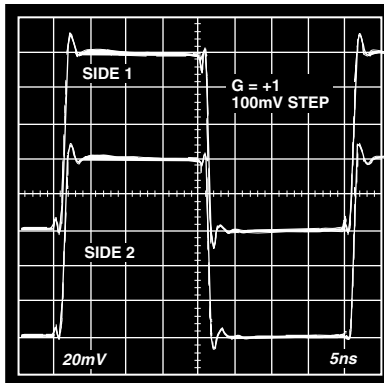
# AD8002—Typical Performance Characteristics



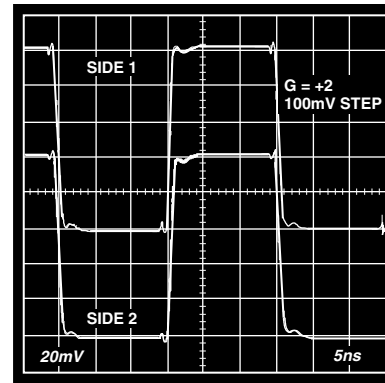
TPC 1. Test Circuit, Gain = +1



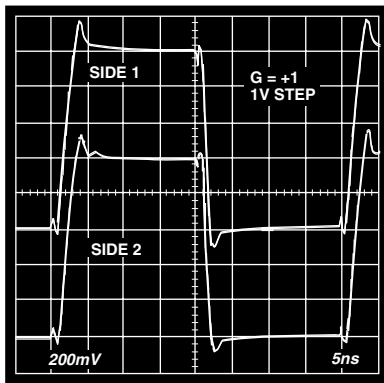
TPC 4. Test Circuit, Gain = +2



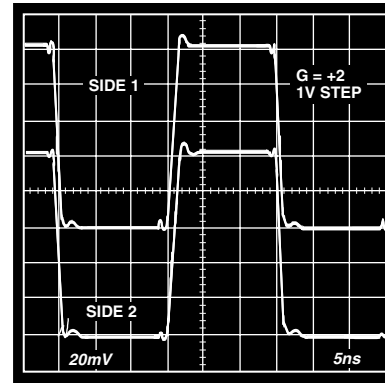
TPC 2. 100 mV Step Response, G = +1



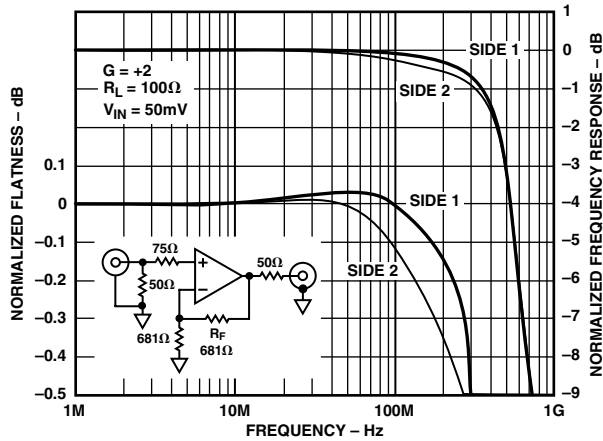
TPC 5. 100 mV Step Response, G = +2



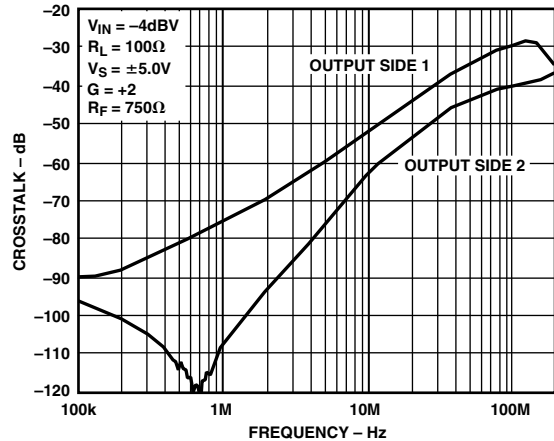
TPC 3. 1 V Step Response, G = +1



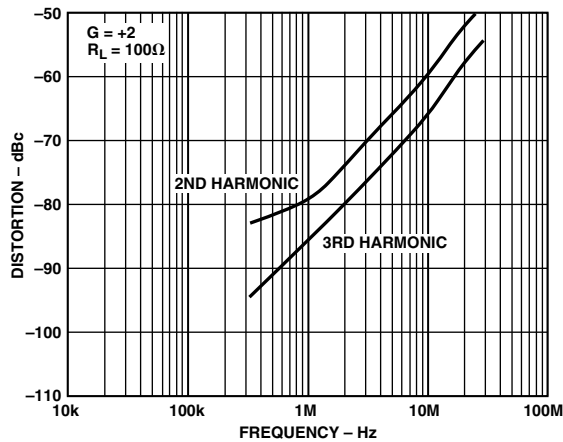
TPC 6. 1 V Step Response, G = +2



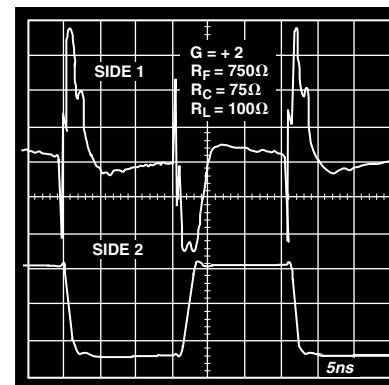
TPC 7. Frequency Response and Flatness,  $G = +2$



TPC 10. Crosstalk (Output-to-Output) vs. Frequency

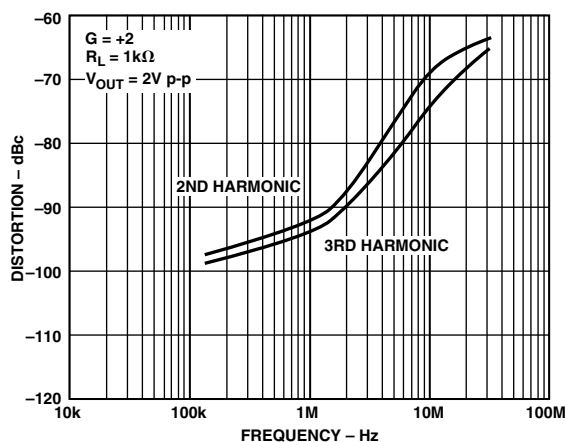


TPC 8. Distortion vs. Frequency,  $G = +2, R_L = 100 \Omega$

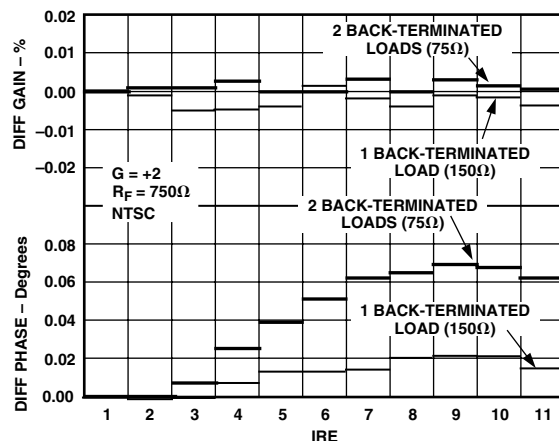


NOTES: SIDE 1:  $V_{IN} = 0V$ ; 8mV/div RTO  
SIDE 2: 1V STEP RTO; 400mV/div

TPC 11. Pulse Crosstalk, Worst Case, 1 V Step

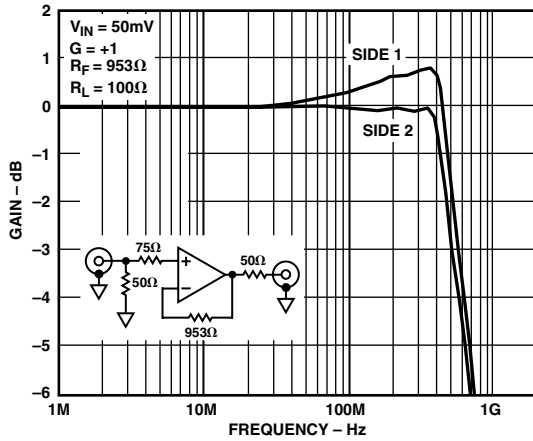


TPC 9. Distortion vs. Frequency,  $G = +2, R_L = 1 k\Omega$

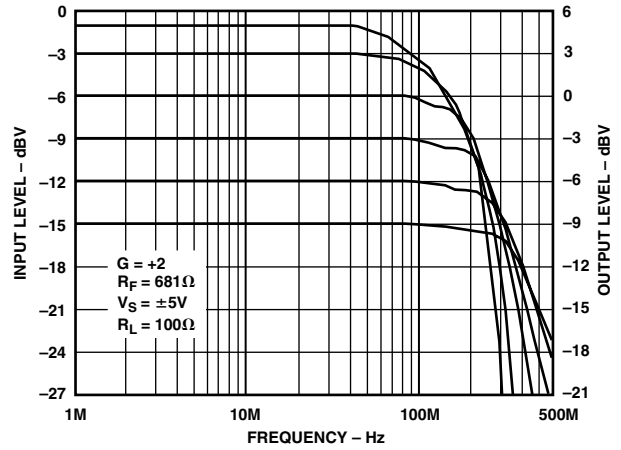


TPC 12. Differential Gain and Differential Phase (per Amplifier)

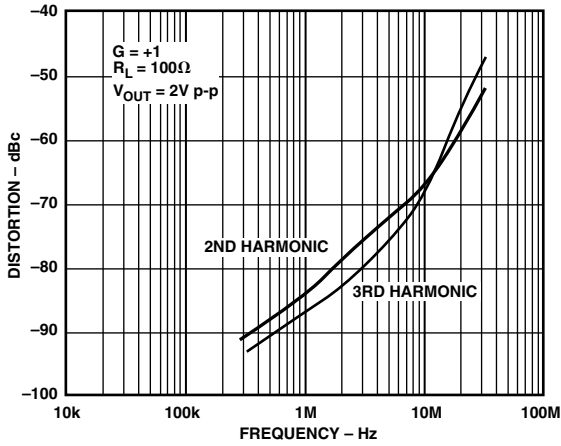
# AD8002



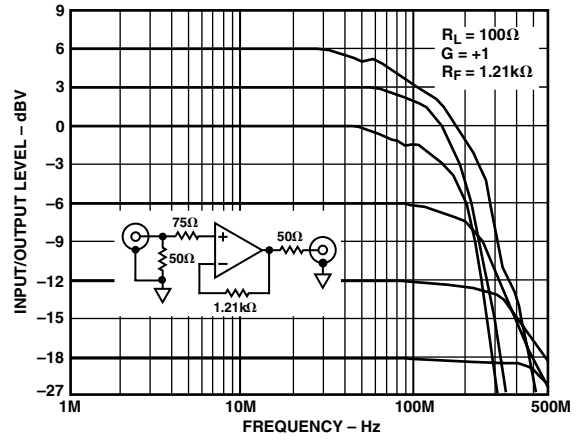
TPC 13. Frequency Response,  $G = +1$



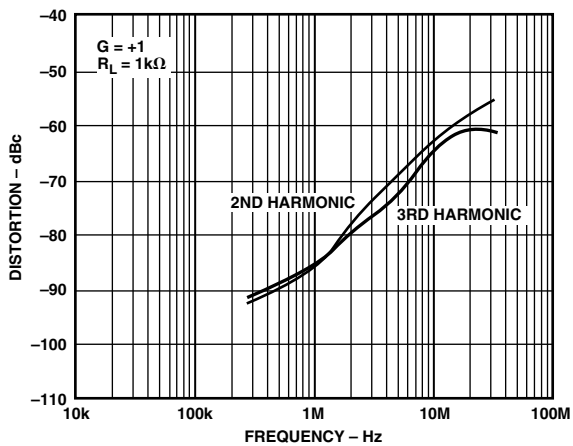
TPC 16. Large Signal Frequency Response,  $G = +2$



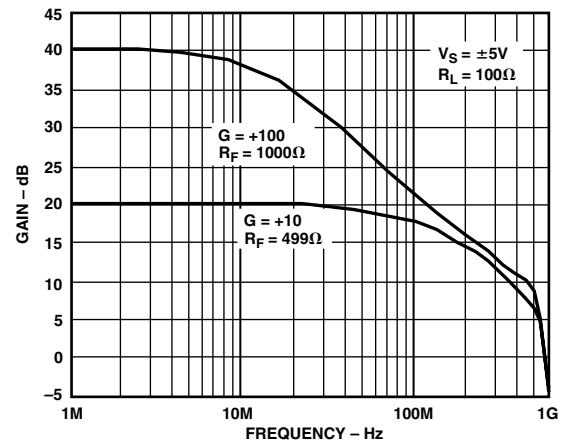
TPC 14. Distortion vs. Frequency,  $G = +1$ ,  $R_L = 100\ \Omega$



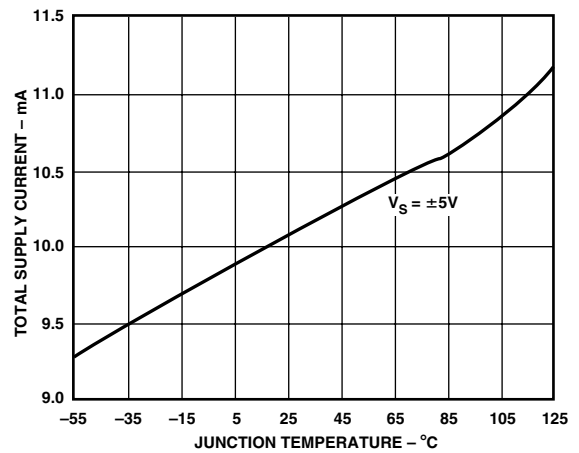
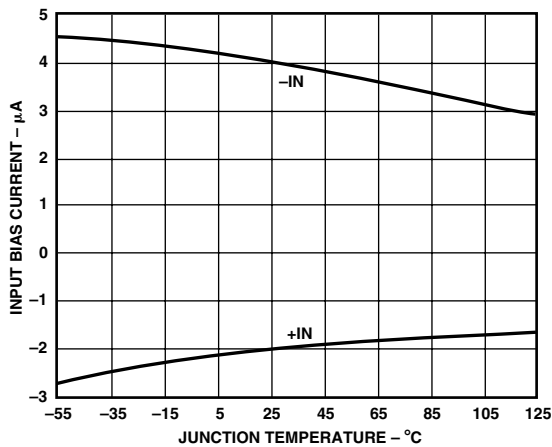
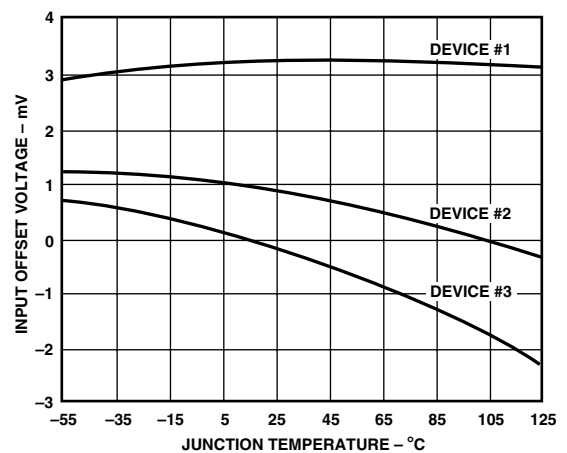
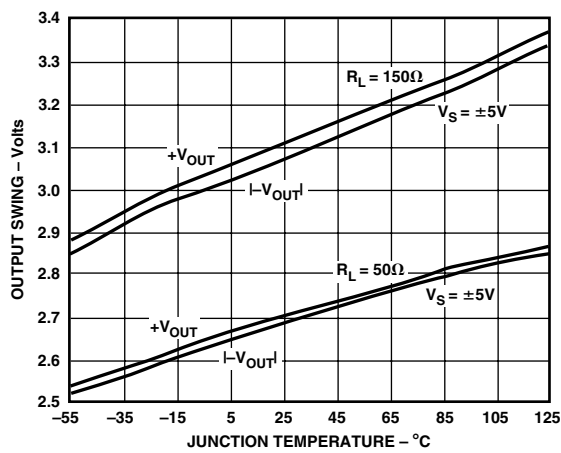
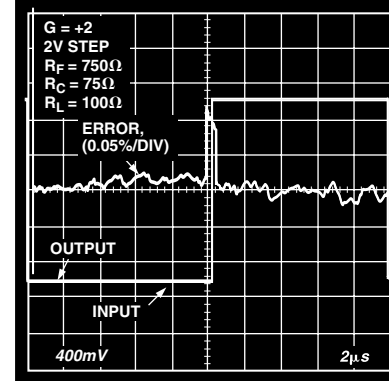
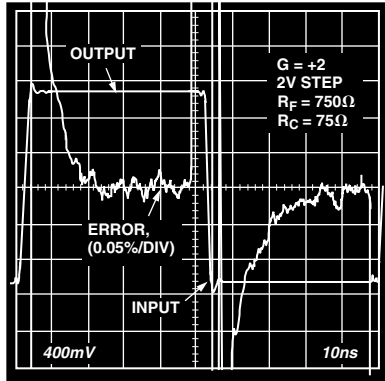
TPC 17. Large Signal Frequency Response,  $G = +1$



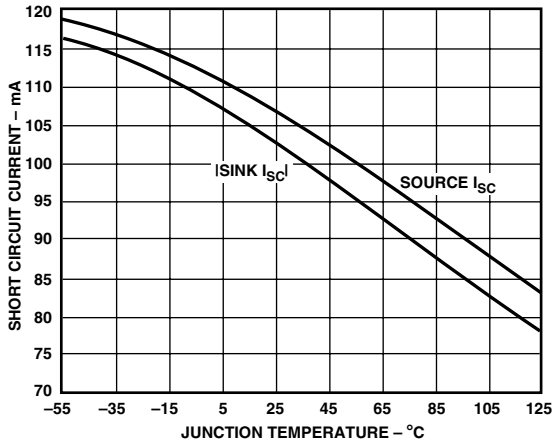
TPC 15. Distortion vs. Frequency,  $G = +1$ ,  $R_L = 1\ \text{k}\Omega$



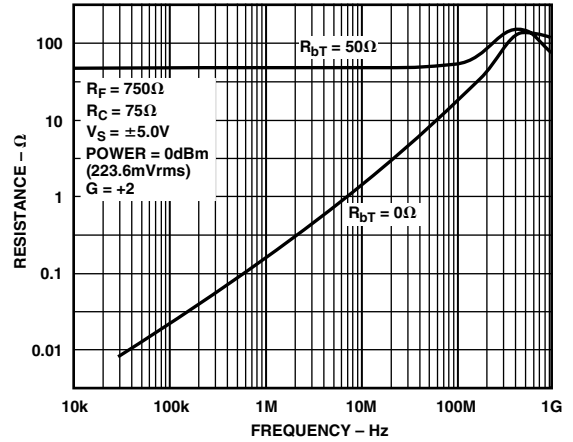
TPC 18. Frequency Response,  $G = +10$ ,  $G = +100$



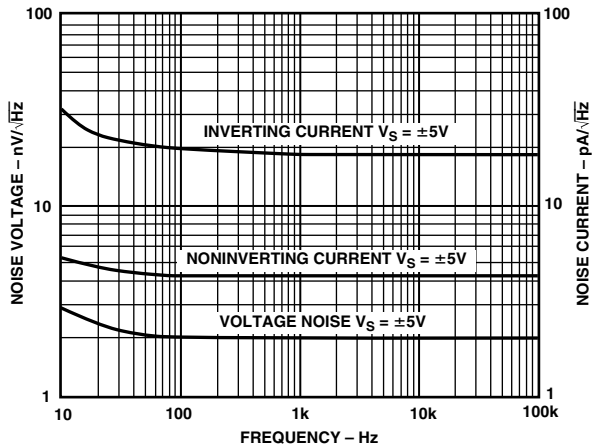
# AD8002



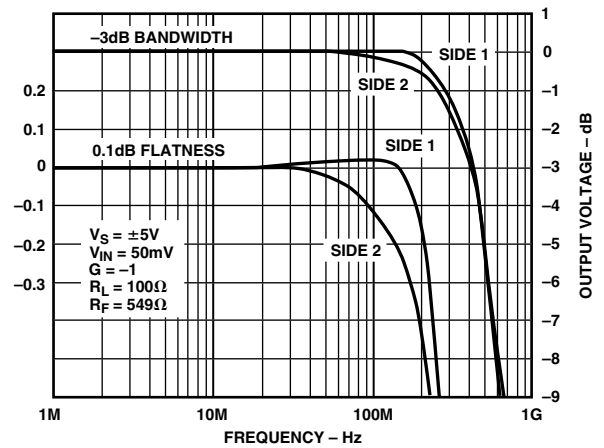
TPC 25. Short Circuit Current vs. Temperature



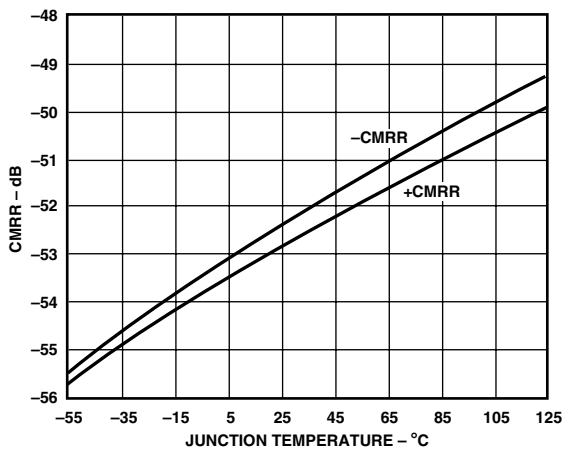
TPC 28. Output Resistance vs. Frequency



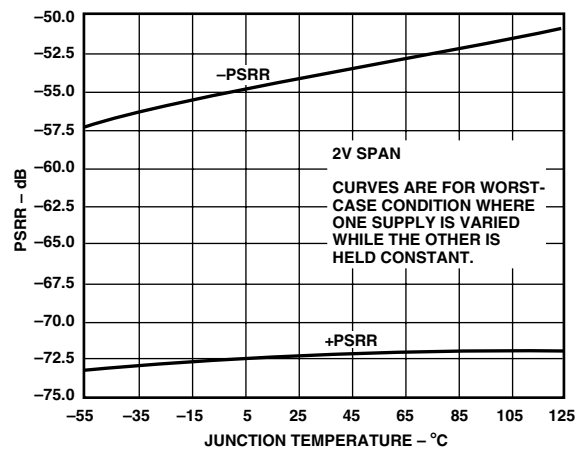
TPC 26. Noise vs. Frequency



TPC 29. -3 dB Bandwidth vs. Frequency,  $G = -1$

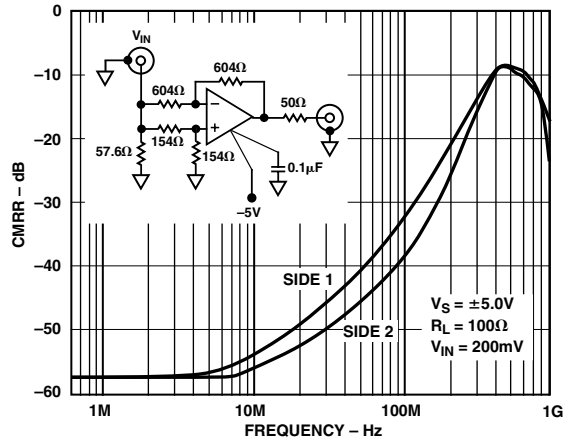


TPC 27. CMRR vs. Temperature

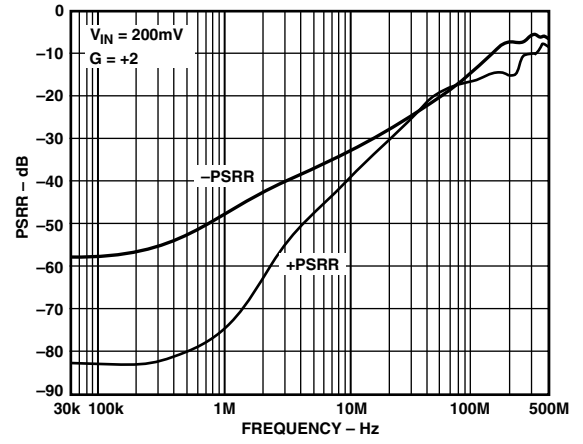


TPC 30. PSRR vs. Temperature

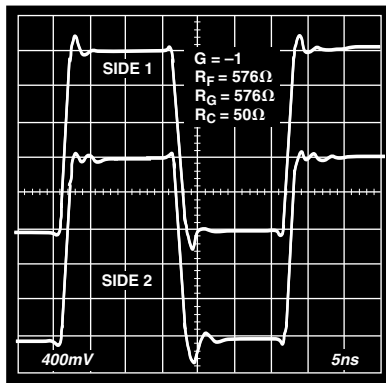




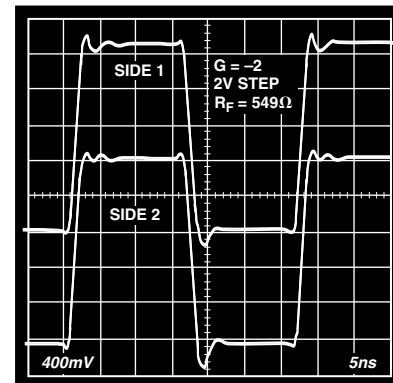
TPC 31. CMRR vs. Frequency



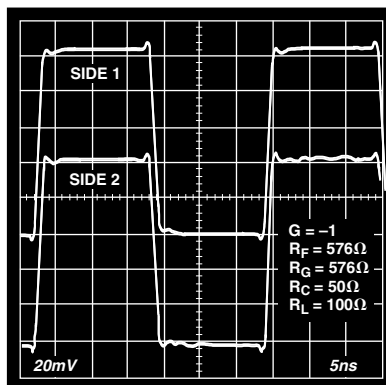
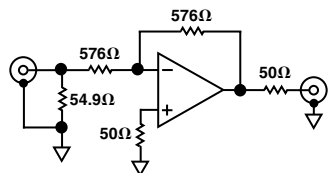
TPC 34. PSRR vs. Frequency



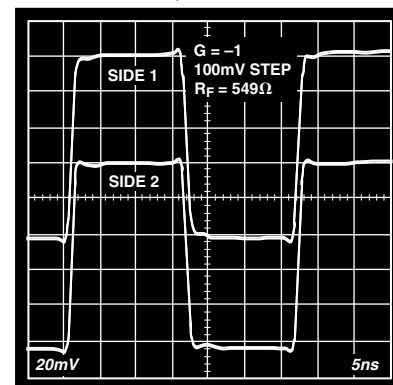
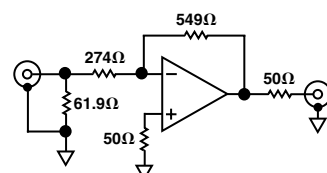
TPC 32. 2 V Step Response,  $G = -1$



TPC 35. 2 V Step Response,  $G = -2$



TPC 33. 100 mV Step Response,  $G = -1$



TPC 36. 100 mV Step Response,  $G = -2$

# AD8002

## THEORY OF OPERATION

A very simple analysis can put the operation of the AD8002, a current feedback amplifier, in familiar terms. Being a current feedback amplifier, the AD8002's open-loop behavior is expressed as transimpedance,  $\Delta V_O/\Delta I_{IN}$ , or  $T_Z$ . The open-loop transimpedance behaves just as the open-loop voltage gain of a voltage feedback amplifier, that is, it has a large dc value and decreases at roughly 6 dB/octave in frequency.

Since the  $R_{IN}$  is proportional to  $1/g_m$ , the equivalent voltage gain is just  $T_Z \times g_m$ , where the  $g_m$  in question is the transconductance of the input stage. This results in a low open-loop input impedance at the inverting input, a now familiar result. Using this amplifier as a follower with gain, Figure 4, basic analysis yields the following result.

$$\frac{V_O}{V_{IN}} = G \times \frac{T_Z(S)}{T_Z(S) + G \times R_{IN} + R1}$$

$$G = 1 + \frac{R1}{R2} \quad R_{IN} = 1/g_m \approx 50 \Omega$$

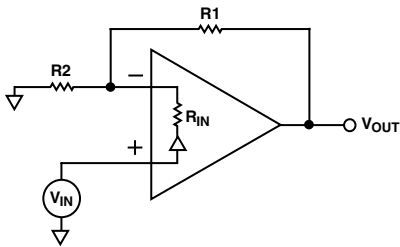


Figure 4.

Recognizing that  $G \times R_{IN} \ll R1$  for low gains, it can be seen to the first order that bandwidth for this amplifier is independent of gain (G).

Considering that additional poles contribute excess phase at high frequencies, there is a minimum feedback resistance below which peaking or oscillation may result. This fact is used to determine the optimum feedback resistance,  $R_F$ . In practice parasitic capacitance at the inverting input terminal will also add phase in the feedback loop, so picking an optimum value for  $R_F$  can be difficult.

Achieving and maintaining gain flatness of better than 0.1 dB at frequencies above 10 MHz requires careful consideration of several issues.

### Choice of Feedback and Gain Resistors

The fine scale gain flatness will, to some extent, vary with feedback resistance. It, therefore, is recommended that once optimum resistor values have been determined, 1% tolerance values should be used if it is desired to maintain flatness over a wide range of production lots. In addition, resistors of different construction have different associated parasitic capacitance and inductance. Surface mount resistors were used for the bulk of the characterization for this data sheet. It is not recommended that leaded components be used with the AD8002.

### Printed Circuit Board Layout Considerations

As expected for a wideband amplifier, PC board parasitics can affect the overall closed-loop performance. Of concern are stray capacitances at the output and the inverting input nodes. If a ground plane is to be used on the same side of the board as the signal traces, a space (5 mm min) should be left around the signal lines to minimize coupling. Additionally, signal lines connecting the feedback and gain resistors should be short enough so that their associated inductance does not cause high frequency gain errors. Line lengths on the order of less than 5 mm are recommended. If long runs of coaxial cable are being driven, dispersion and loss must be considered.

### Power Supply Bypassing

Adequate power supply bypassing can be critical when optimizing the performance of a high-frequency circuit. Inductance in the power supply leads can form resonant circuits that produce peaking in the amplifier's response. In addition, if large current transients must be delivered to the load, bypass capacitors (typically greater than 1  $\mu$ F) will be required to provide the best settling time and lowest distortion. A parallel combination of 4.7  $\mu$ F and 0.1  $\mu$ F is recommended. Some brands of electrolytic capacitors will require a small series damping resistor  $\approx 4.7 \Omega$  for optimum results.

### DC Errors and Noise

There are three major noise and offset terms to consider in a current feedback amplifier. For offset errors, refer to the equation below. For noise error, the terms are root-sum-squared to give a net output error. In the circuit shown in Figure 5 they are input offset ( $V_{IO}$ ), which appears at the output multiplied by the noise gain of the circuit ( $1 + R_F/R_I$ ), noninverting input current ( $I_{BN} \times R_N$ ), also multiplied by the noise gain, and the inverting input current, which, when divided between  $R_F$  and  $R_I$  and subsequently multiplied by the noise gain, always appears at the output as  $I_{BN} \times R_F$ . The input voltage noise of the AD8002 is a low 2 nV/ $\sqrt{Hz}$ . At low gains, though, the inverting input current noise times  $R_F$  is the dominant noise source. Careful layout and device matching contribute to better offset and drift specifications for the AD8002 compared to many other current feedback amplifiers. The typical performance curves in conjunction with the equations below can be used to predict the performance of the AD8002 in any application.

$$V_{OUT} = V_{IO} \times \left(1 + \frac{R_F}{R_I}\right) \pm I_{BN} \times R_N \times \left(1 + \frac{R_F}{R_I}\right) \pm I_{BI} \times R_F$$

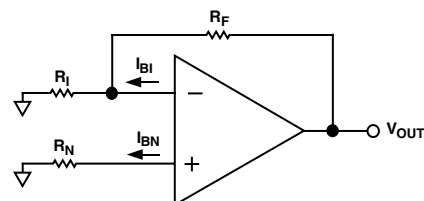


Figure 5. Output Offset Voltage

## Driving Capacitive Loads

The AD8002 was designed primarily to drive nonreactive loads. If driving loads with a capacitive component is desired, best frequency response is obtained by the addition of a small series resistance as shown in Figure 6.

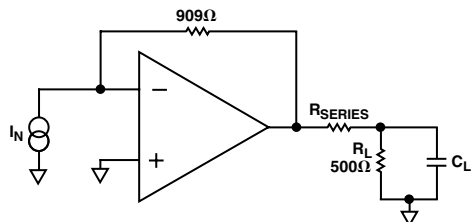


Figure 6. Driving Capacitive Loads

Figure 7 shows the optimum value for  $R_{SERIES}$  versus capacitive load. It is worth noting that the frequency response of the circuit when driving large capacitive loads will be dominated by the passive roll-off of  $R_{SERIES}$  and  $C_L$ .

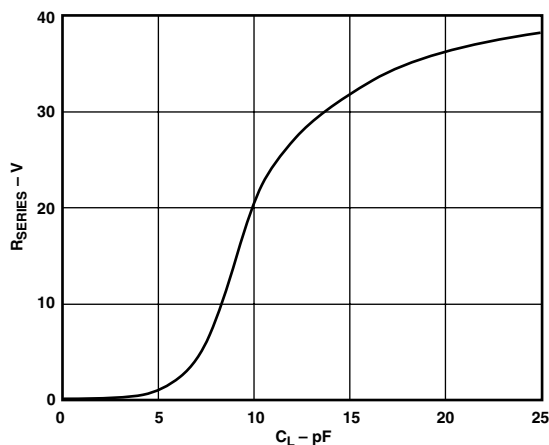


Figure 7. Recommended  $R_{SERIES}$  vs. Capacitive Load

## Communications

Distortion is a key specification in communications applications. Intermodulation distortion (IMD) is a measure of the ability of an amplifier to pass complex signals without the generation of spurious harmonics. The third order products are usually the most problematic since several of them fall near the fundamentals and do not lend themselves to filtering. Theory predicts that the third order harmonic distortion components increase in power at three times the rate of the fundamental tones. The specification of third order intercept as the virtual point where fundamental and harmonic power are equal is one standard measure of distortion performance. Op amps used in closed-loop applications do not always obey this simple theory. At a gain of two, the AD8002 has performance summarized in Figure 8. Here the worst third order products are plotted versus input power. The third order intercept of the AD8002 is 33 dBm at 10 MHz.

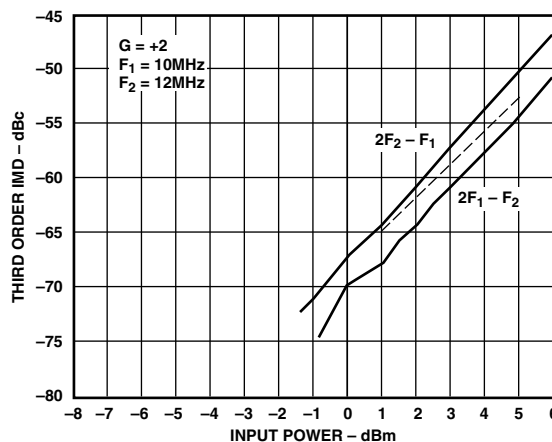


Figure 8. Third Order IMD;  $F_1 = 10$  MHz,  $F_2 = 12$  MHz

## Operation as a Video Line Driver

The AD8002 has been designed to offer outstanding performance as a video line driver. The important specifications of differential gain (0.01%) and differential phase (0.02°) meet the most exacting HDTV demands for driving one video load with each amplifier. The AD8002 also drives four back-terminated loads (two each), as shown in Figure 9, with equally impressive performance (0.01%, 0.07°). Another important consideration is isolation between loads in a multiple load application. The AD8002 has more than 40 dB of isolation at 5 MHz when driving two 75 Ω back-terminated loads.

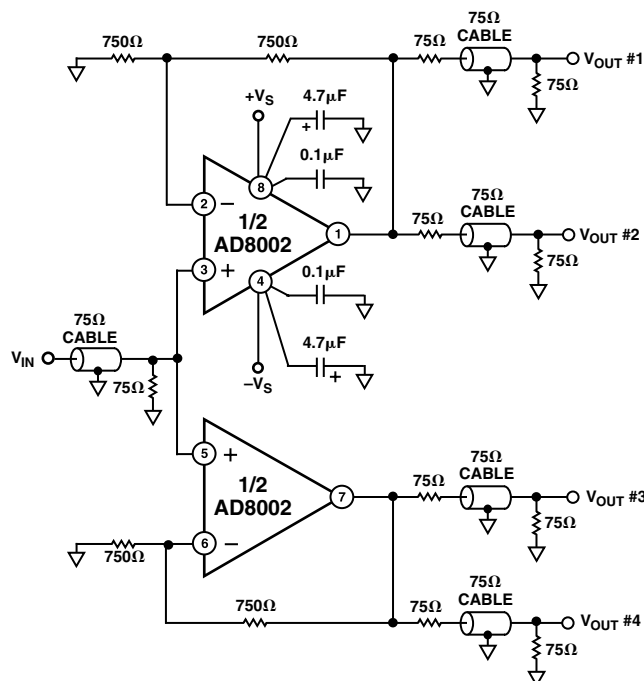


Figure 9. Video Line Driver

# AD8002

## Driving A-to-D Converters

The AD8002 is well suited for driving high-speed analog-to-digital converters such as the AD9058. The AD9058 is a dual 8-bit 50 MSPS ADC. In Figure 10, the AD8002 is shown driving the inputs of the AD9058 which are configured for 0 V to 2 V ranges. Bipolar input signals are buffered, amplified ( $-2\times$ ), and offset (by 1.0 V) into the proper input range of the ADC. Using

the AD9058's internal 2 V reference connected to both ADCs as shown in Figure 10 reduces the number of external components required to create a complete data acquisition system. The 20  $\Omega$  resistors in series with ADC inputs are used to help the AD8002s drive the 10 pF ADC input capacitance. The AD8002 adds only 100 mW to the power consumption, while not limiting the performance of the circuit.

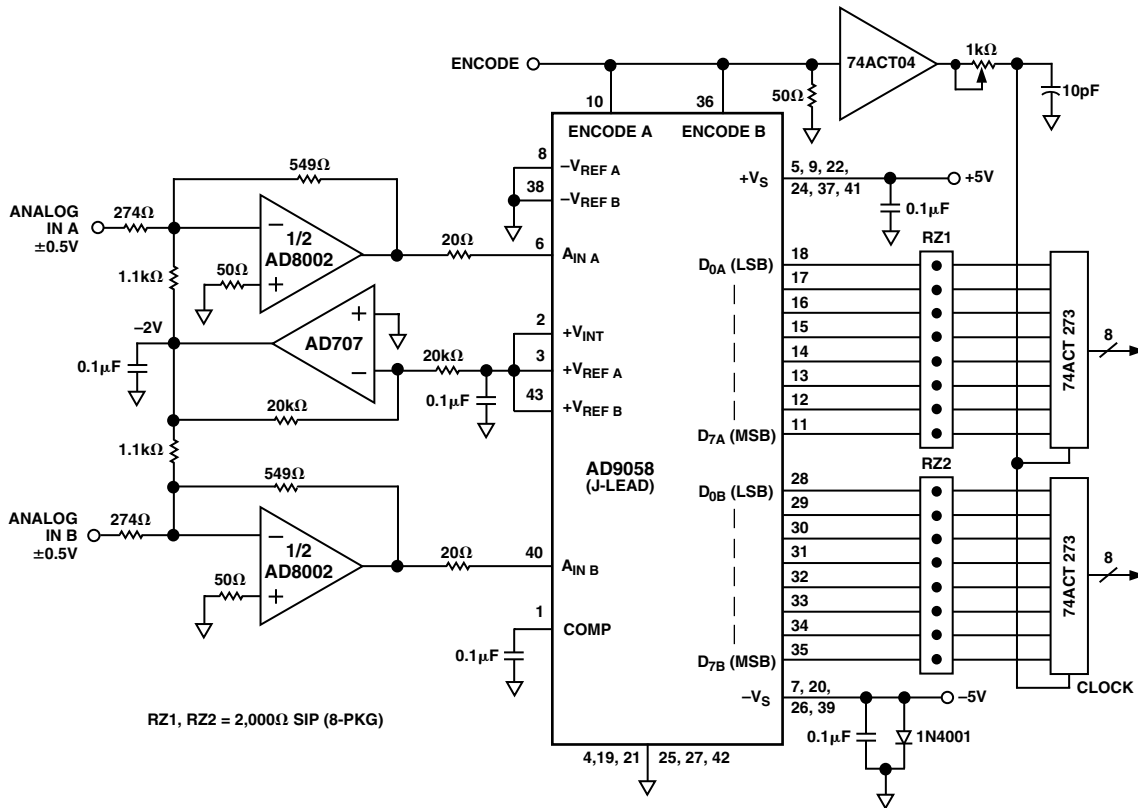


Figure 10. AD8002 Driving a Dual A-to-D Converter

### Single-Ended-to-Differential Driver Using an AD8002

The two halves of an AD8002 can be configured to create a single-ended-to-differential high-speed driver with a  $-3$  dB bandwidth in excess of 200 MHz, as shown in Figure 11. Although the individual op amps are each current feedback, the overall architecture yields a circuit with attributes normally associated with voltage feedback amplifiers, while offering the speed advantages inherent in current feedback amplifiers. In addition, the gain of the circuit can be changed by varying a single resistor,  $R_F$ , which is often not possible in a dual op amp differential driver.

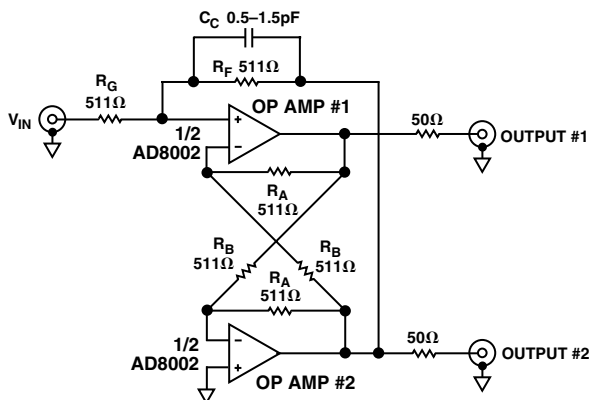


Figure 11. Differential Line Driver

The current feedback nature of the op amps, in addition to enabling the wide bandwidth, provides an output drive of more than 3 V p-p into a 20  $\Omega$  load for each output at 20 MHz. On the other hand, the voltage feedback nature provides symmetrical high impedance inputs and allows the use of reactive components in the feedback network.

The circuit consists of the two op amps, each configured as a unity gain follower by the 511  $\Omega$   $R_A$  feedback resistors between each op amp's output and inverting input. The output of each op amp has a 511  $\Omega$   $R_B$  resistor to the inverting input of the other op amp. Thus, each output drives the other op amp through a unity gain inverter configuration. By connecting the two amplifiers as cross-coupled inverters, their outputs are freed to be equal and opposite, assuring zero-output common-mode voltage.

With this circuit configuration, the common-mode signal of the outputs is reduced. If one output moves slightly higher, the negative input to the other op amp drives its output to go slightly lower and thus preserves the symmetry of the complementary outputs, which reduces the common-mode signal. The common-mode output signal was measured to be  $-50$  dB at 1 MHz.

Looking at this configuration overall, there are two high impedance inputs (the + inputs of each op amp), two low impedance outputs, and high open-loop gain. If we consider the two noninverting inputs and just the output of Op Amp #2, the structure looks like a voltage feedback op amp having two symmetrical, high-impedance inputs, and one output. The +input to Op Amp #2 is the noninverting input (it has the same polarity as Output #2) and the +input to Amplifier #1 is the inverting input (opposite polarity of Output #2).

With a feedback resistor  $R_F$ , an input resistor  $R_G$ , and grounding of the +input of Op Amp #2, a feedback amplifier is formed. This configuration is just like a voltage feedback amplifier in an inverting configuration if only Output #2 is considered. The addition of Output #1 makes the amplifier differential output.

The differential gain of this circuit is:

$$G = \frac{R_F}{R_G} \times \left( 1 + \frac{R_A}{R_B} \right)$$

The  $R_F/R_G$  term is the gain of the overall op amp configuration and is the same as for an inverting op amp except for the polarity. If Output #1 is used as the output reference, the gain is positive. The  $1 + R_A/R_B$  term is the noise gain of each individual op amp in its noninverting configuration.

The resulting architecture offers several advantages. First, the gain can be changed by changing a single resistor. Changing either  $R_F$  or  $R_G$  will change the gain as in an inverting op amp circuit. For most types of differential circuits, more than one resistor must be changed to change gain and still maintain good CMR.

Reactive elements can be used in the feedback network. This is in contrast to current feedback amplifiers that restrict the use of reactive elements in the feedback. The circuit described requires about 0.9 pF of capacitance in shunt across  $R_F$  in order to optimize peaking and realize a  $-3$  dB bandwidth of more than 200 MHz.

The peaking exhibited by the circuit is very sensitive to the value of this capacitor. Parasitics in the board layout on the order of tenths of picofarads will influence the frequency response and the value required for the feedback capacitor, so a good layout is essential.

The shunt capacitor type selection is also critical. A good microwave type chip capacitor with high Q was found to yield best performance. The part selected for this circuit was a muRata Erie part number MA280R9B.

The distortion was measured at 20 MHz with a 3 V p-p input and a 100  $\Omega$  load on each output. For Output #1 the distortion is  $-37$  dBc and  $-41$  dBc for the second and third harmonics respectively. For Output #2 the second harmonic is  $-35$  dBc and the third harmonic is  $-43$  dBc.

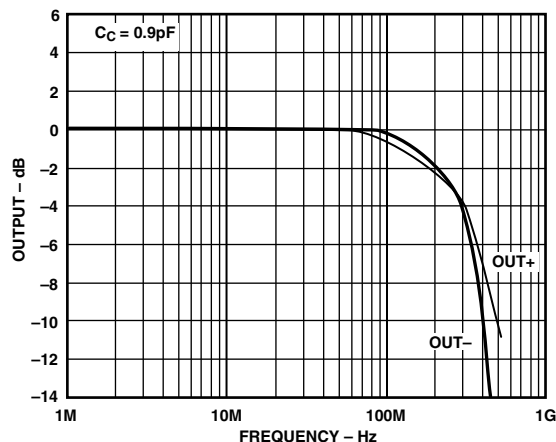


Figure 12. Differential Driver Frequency Response

# AD8002

## Layout Considerations

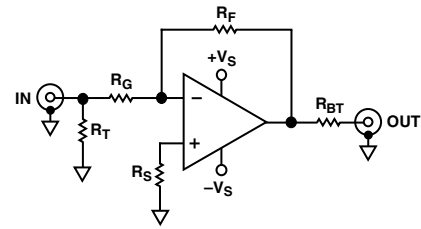
The specified high-speed performance of the AD8002 requires careful attention to board layout and component selection. Proper  $R_F$  design techniques and low parasitic component selection are mandatory.

The PCB should have a ground plane covering all unused portions of the component side of the board to provide a low impedance ground path. The ground plane should be removed from the area near the input pins to reduce stray capacitance.

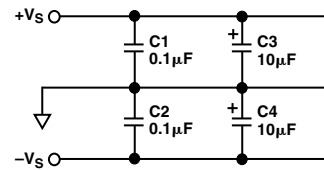
Chip capacitors should be used for supply bypassing (see Figure 13). One end should be connected to the ground plane and the other within 1/8 in. of each power pin. An additional large tantalum electrolytic capacitor (4.7  $\mu\text{F}$ –10  $\mu\text{F}$ ) should be connected in parallel, but not necessarily so close, to supply current for fast, large-signal changes at the output.

The feedback resistor should be located close to the inverting input pin in order to keep the stray capacitance at this node to a minimum. Capacitance variations of less than 1 pF at the inverting input will significantly affect high-speed performance.

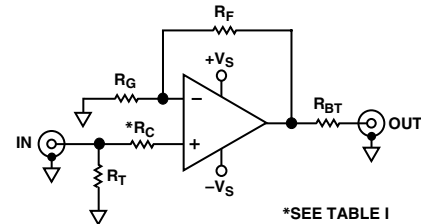
Stripline design techniques should be used for long signal traces (greater than about 1 in.). These should be designed with a characteristic impedance of 50  $\Omega$  or 75  $\Omega$  and be properly terminated at each end.



*Inverting Configuration*



*Supply Bypassing*



\*SEE TABLE I

*Noninverting Configuration*

Figure 13. Inverting and Noninverting Configurations

Table I. Recommended Component Values

Component	AD8002AN (DIP) Gain							AD8002AR (SOIC) Gain						
	-10	-2	-1	+1	+2	+10	+100	-10	-2	-1	+1	+2	+10	+100
$R_F$ ( $\Omega$ )	499	549	576	1210	750	499	1000	499	499	549	953	681	499	1000
$R_G$ ( $\Omega$ )	49.9	274	576	–	750	54.9	10	49.9	249	549	–	681	54.9	10
$R_{BT}$ (Nominal) ( $\Omega$ )	49.9	49.9	49.9	49.9	49.9	49.9	49.9	49.9	49.9	49.9	49.9	49.9	49.9	49.9
$R_C$ ( $\Omega$ )*				75	75	0	0				75	75	0	0
$R_S$ ( $\Omega$ )	49.9	49.9	49.9					49.9	49.9	49.9				
$R_T$ (Nominal) ( $\Omega$ )	–	61.9	54.9	49.9	49.9	49.9	49.9	–	61.9	54.9	49.9	49.9	49.9	49.9
Small Signal BW (MHz)	270	380	410	600	500	170	17	250	410	410	600	500	170	17
0.1 dB Flatness (MHz)	45	80	130	35	60	24	3	50	100	100	35	90	24	3

Component	AD8002ARM ( $\mu\text{SOIC}$ ) Gain						
	-10	-2	-1	+1	+2	+10	+100
$R_F$ ( $\Omega$ )	499	499	590	1000	681	499	1000
$R_G$ ( $\Omega$ )	49.9	249	590	–	681	54.9	10
$R_{BT}$ (Nominal) ( $\Omega$ )	49.9	49.9	49.9	49.9	49.9	49.9	49.9
$R_C$ ( $\Omega$ )*				75	75	0	0
$R_S$ ( $\Omega$ )	49.9	49.9	49.9				
$R_T$ (Nominal) ( $\Omega$ )	–	61.9	49.9	49.9	49.9	49.9	49.9
Small Signal BW (MHz)	270	400	410	600	450	170	19
0.1 dB Flatness (MHz)	60	100	100	35	70	35	3

\* $R_C$  is recommended to reduce peaking, and minimizes input reflections at frequencies above 300 MHz. However,  $R_C$  is not required.

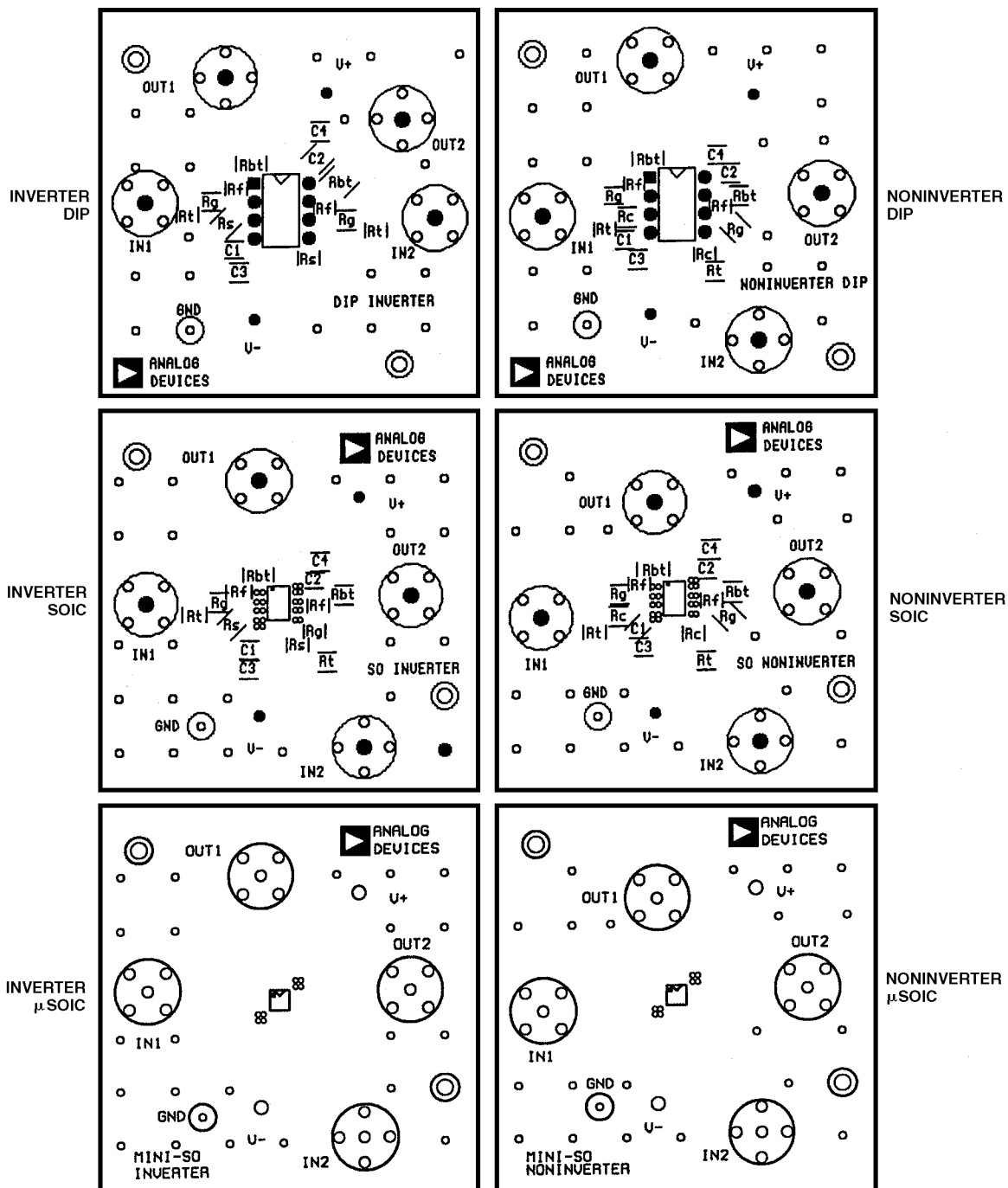


Figure 14. Board Layout (Silkscreen)

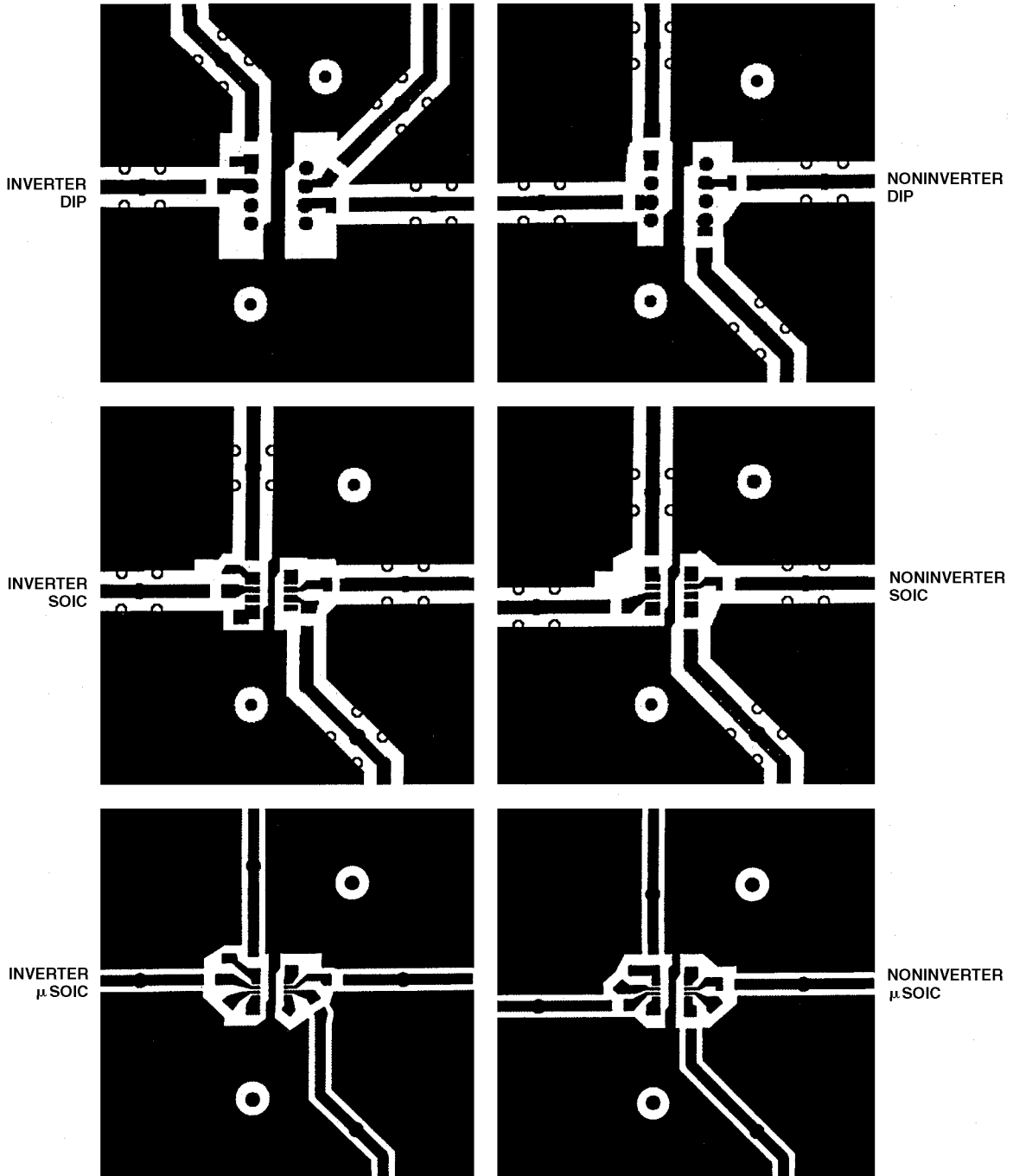


Figure 15. Board Layout (Component Layer)



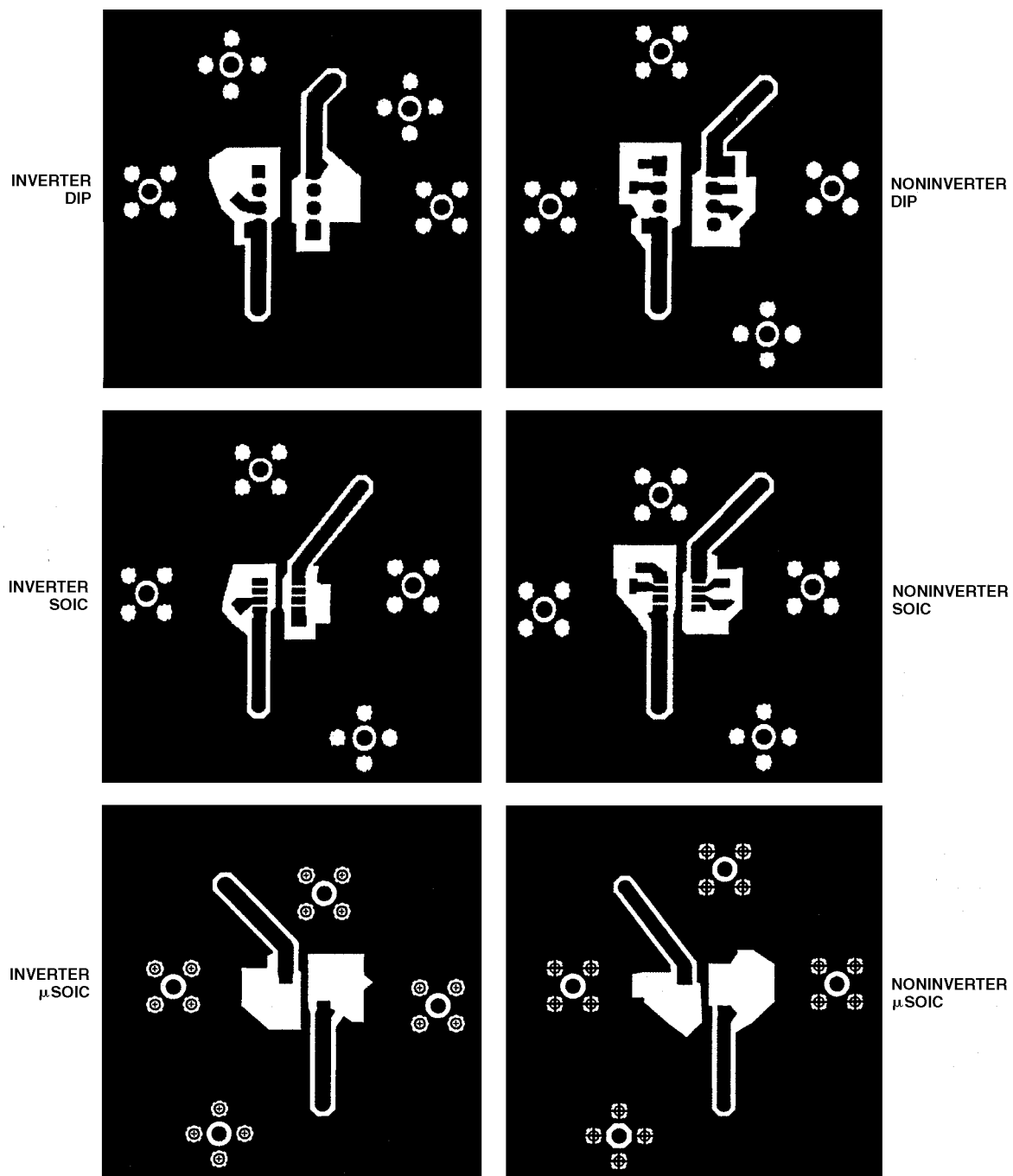
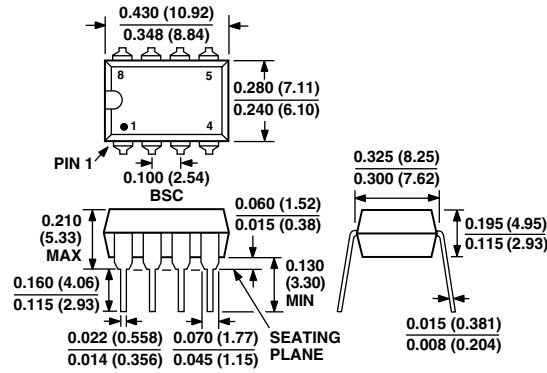


Figure 16. Board Layout (Solder Side) (Looking through the Board)

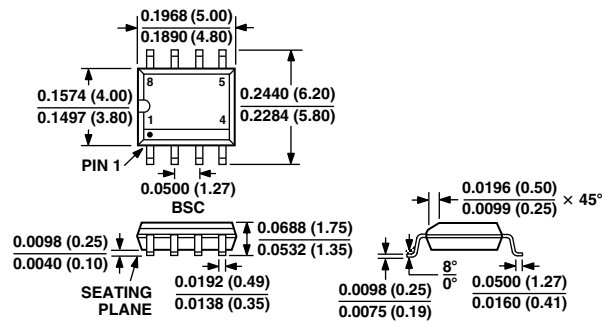
## OUTLINE DIMENSIONS

Dimensions shown in inches and (mm).

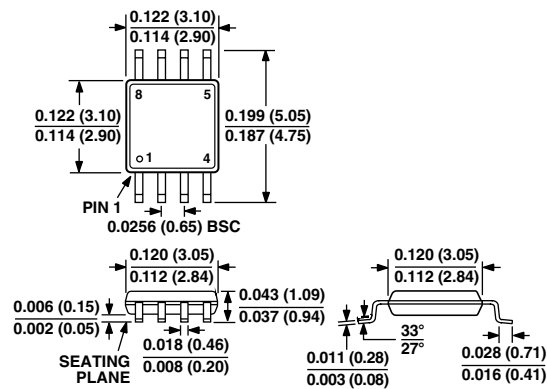
### 8-Lead Plastic DIP (N-8)



### 8-Lead SOIC (SO-8)



### 8-Lead $\mu$ SOIC (RM-8)



# Revision History–AD8002

**Location**

**Page**

Data Sheet changed from REV. C to REV. D.

MAX RATINGS changed ..... 3

