

LM4562

LM4562 Dual High Performance, High Fidelity Audio Operational Amplifier

Dual High Performance, High Fidelity Audio Operational Amplifier

General Description

The LM4562 is part of the ultra-low distortion, low noise, high slew rate operational amplifier series optimized and fully specified for high performance, high fidelity applications. Combining advanced leading-edge process technology with state-of-the-art circuit design, the LM4562 audio operational amplifiers deliver superior audio signal amplification for outstanding audio performance. The LM4562 combines extremely low voltage noise density ($2.7\text{nV}/\sqrt{\text{Hz}}$) with vanishingly low THD+N (0.00003%) to easily satisfy the most demanding audio applications. To ensure that the most challenging loads are driven without compromise, the LM4562 has a high slew rate of $\pm 20\text{V}/\mu\text{s}$ and an output current capability of $\pm 26\text{mA}$. Further, dynamic range is maximized by an output stage that drives $2\text{k}\Omega$ loads to within 1V of either power supply voltage and to within 1.4V when driving 600Ω loads.

The LM4562's outstanding CMRR (120dB), PSRR (120dB), and V_{OS} (0.1mV) give the amplifier excellent operational amplifier DC performance.

The LM4562 has a wide supply range of $\pm 2.5\text{V}$ to $\pm 17\text{V}$. Over this supply range the LM4562's input circuitry maintains excellent common-mode and power supply rejection, as well as maintaining its low input bias current. The LM4562 is unity gain stable. This Audio Operational Amplifier achieves outstanding AC performance while driving complex loads with values as high as 100pF .

The LM4562 is available in 8-lead narrow body SOIC, 8-lead Plastic DIP, and 8-lead Metal Can TO-99. Demonstration boards are available for each package.

Key Specifications

- Power Supply Voltage Range $\pm 2.5\text{V}$ to $\pm 17\text{V}$
- THD+N ($A_V = 1$, $V_{OUT} = 3\text{V}_{RMS}$, $f_{IN} = 1\text{kHz}$)

$R_L = 2\text{k}\Omega$	0.00003% (typ)
$R_L = 600\Omega$	0.00003% (typ)
■ Input Noise Density	$2.7\text{nV}/\sqrt{\text{Hz}}$ (typ)
■ Slew Rate	$\pm 20\text{V}/\mu\text{s}$ (typ)
■ Gain Bandwidth Product	55MHz (typ)
■ Open Loop Gain ($R_L = 600\Omega$)	140dB (typ)
■ Input Bias Current	10nA (typ)
■ Input Offset Voltage	0.1mV (typ)
■ DC Gain Linearity Error	0.000009%

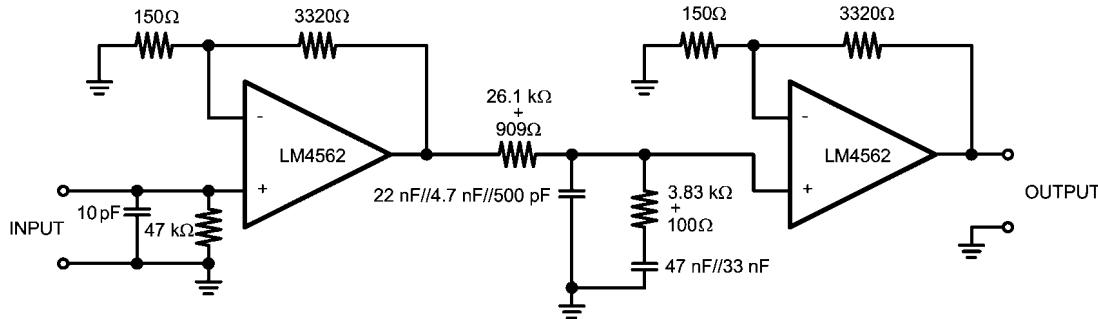
Features

- Easily drives 600Ω loads
- Optimized for superior audio signal fidelity
- Output short circuit protection
- PSRR and CMRR exceed 120dB (typ)
- SOIC, DIP, TO-99 metal can packages

Applications

- Ultra high quality audio amplification
- High fidelity preamplifiers
- High fidelity multimedia
- State of the art phono pre amps
- High performance professional audio
- High fidelity equalization and crossover networks
- High performance line drivers
- High performance line receivers
- High fidelity active filters

Typical Application

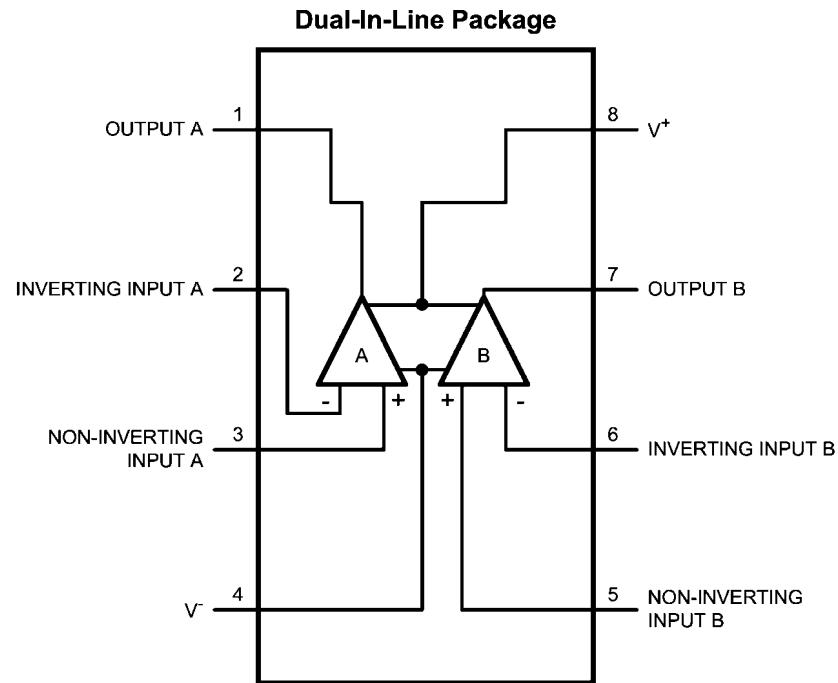


Note: 1% metal film resistors, 5% polypropylene capacitors

Passively Equalized RIAA Phono Preamplifier

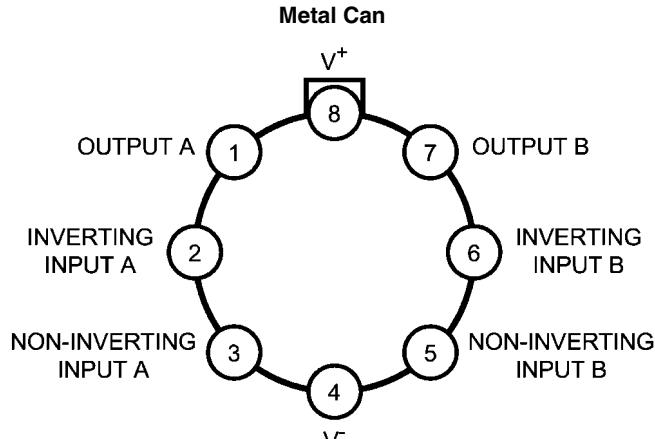
201572k5

Connection Diagrams



20157255

Order Number LM4562MA
See NS Package Number — M08A
Order Number LM4562NA
See NS Package Number — N08E



201572f3

Order Number LM4562HA
See NS Package Number — H08C

Absolute Maximum Ratings (Note 1, Note 2)

If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/Distributors for availability and specifications.

Power Supply Voltage ($V_S = V^+ - V^-$)	36V	ESD Susceptibility (Note 5) Pins 1, 4, 7 and 8	200V
Storage Temperature	-65°C to 150°C	Pins 2, 3, 5 and 6	100V
Input Voltage (V^-) - 0.7V to (V^+) + 0.7V	Continuous	Junction Temperature	150°C
Output Short Circuit (Note 3)	Internally Limited	Thermal Resistance θ_{JA} (SO)	145°C/W
Power Dissipation	2000V	θ_{JA} (NA)	102°C/W
ESD Susceptibility (Note 4)		θ_{JA} (HA)	150°C/W
		θ_{JC} (HA)	35°C/W
		Temperature Range $T_{MIN} \leq T_A \leq T_{MAX}$	-40°C ≤ T_A ≤ 85°C
		Supply Voltage Range $\pm 2.5V \leq V_S \leq \pm 17V$	

Electrical Characteristics for the LM4562 (Note 1, Note 2)

The specifications apply for $V_S = \pm 15V$, $R_L = 2k\Omega$, $f_{IN} = 1kHz$, $T_A = 25^\circ C$, unless otherwise specified.

Symbol	Parameter	Conditions	LM4562		Units (Limits)
			Typical	Limit	
			(Note 6)	(Note 7)	
THD+N	Total Harmonic Distortion + Noise	$A_V = 1$, $V_{OUT} = 3V_{rms}$ $R_L = 2k\Omega$ $R_L = 600\Omega$	0.00003 0.00003	0.00009	% (max)
IMD	Intermodulation Distortion	$A_V = 1$, $V_{OUT} = 3V_{RMS}$ Two-tone, 60Hz & 7kHz 4:1	0.00005		%
GBWP	Gain Bandwidth Product		55	45	MHz (min)
SR	Slew Rate		±20	±15	V/μs (min)
FPBW	Full Power Bandwidth	$V_{OUT} = 1V_{P-P}$, -3dB referenced to output magnitude at $f = 1kHz$	10		MHz
t_s	Settling time	$A_V = -1$, 10V step, $C_L = 100pF$ 0.1% error range	1.2		μs
e_n	Equivalent Input Noise Voltage	$f_{BW} = 20Hz$ to $20kHz$	0.34	0.65	μV_{RMS} (max)
	Equivalent Input Noise Density	$f = 1kHz$ $f = 10Hz$	2.7 6.4	4.7	nV/√Hz (max)
i_n	Current Noise Density	$f = 1kHz$ $f = 10Hz$	1.6 3.1		pA/√Hz
V_{OS}	Offset Voltage		±0.1	±0.7	mV (max)
$\Delta V_{OS}/\Delta Temp$	Average Input Offset Voltage Drift vs Temperature	-40°C ≤ T_A ≤ 85°C	0.2		μV/°C
PSRR	Average Input Offset Voltage Shift vs Power Supply Voltage	$\Delta V_S = 20V$ (Note 8)	120	110	dB (min)
ISO_{CH-CH}	Channel-to-Channel Isolation	$f_{IN} = 1kHz$ $f_{IN} = 20kHz$	118 112		dB
I_B	Input Bias Current	$V_{CM} = 0V$	10	72	nA (max)
$\Delta I_{OS}/\Delta Temp$	Input Bias Current Drift vs Temperature	-40°C ≤ T_A ≤ 85°C	0.1		nA/°C
I_{OS}	Input Offset Current	$V_{CM} = 0V$	11	65	nA (max)
V_{IN-CM}	Common-Mode Input Voltage Range		+14.1 -13.9	(V+) - 2.0 (V-) + 2.0	V (min)
CMRR	Common-Mode Rejection	-10V < V_{cm} < 10V	120	110	dB (min)
Z_{IN}	Differential Input Impedance		30		kΩ
	Common Mode Input Impedance	-10V < V_{cm} < 10V	1000		MΩ

Symbol	Parameter	Conditions	LM4562		Units (Limits)
			Typical	Limit	
			(Note 6)	(Note 7)	
A_{VOL}	Open Loop Voltage Gain	$-10V < V_{out} < 10V, R_L = 600\Omega$	140	125	dB (min)
		$-10V < V_{out} < 10V, R_L = 2k\Omega$	140		
		$-10V < V_{out} < 10V, R_L = 10k\Omega$	140		
V_{OUTMAX}	Maximum Output Voltage Swing	$R_L = 600\Omega$	± 13.6	± 12.5	V (min)
		$R_L = 2k\Omega$	± 14.0		
		$R_L = 10k\Omega$	± 14.1		
I_{OUT}	Output Current	$R_L = 600\Omega, V_S = \pm 17V$	± 26	± 23	mA (min)
I_{OUT-CC}	Instantaneous Short Circuit Current		+53 -42		mA
R_{OUT}	Output Impedance	$f_{IN} = 10kHz$			Ω
		Closed-Loop	0.01		
		Open-Loop	13		
C_{LOAD}	Capacitive Load Drive Overshoot	100pF	16		%
I_S	Total Quiescent Current	$I_{OUT} = 0mA$	10	12	mA (max)

Note 1: Absolute Maximum Ratings indicate limits beyond which damage to the device may occur.

Note 2: Operating Ratings indicate conditions for which the device is functional, but do not guarantee specific performance limits. For guaranteed specifications and test conditions, see the Electrical Characteristics. The guaranteed specifications apply only for the test conditions listed. Some performance characteristics may degrade when the device is not operated under the listed test conditions.

Note 3: Amplifier output connected to GND, any number of amplifiers within a package.

Note 4: Human body model, 100pF discharged through a $1.5k\Omega$ resistor.

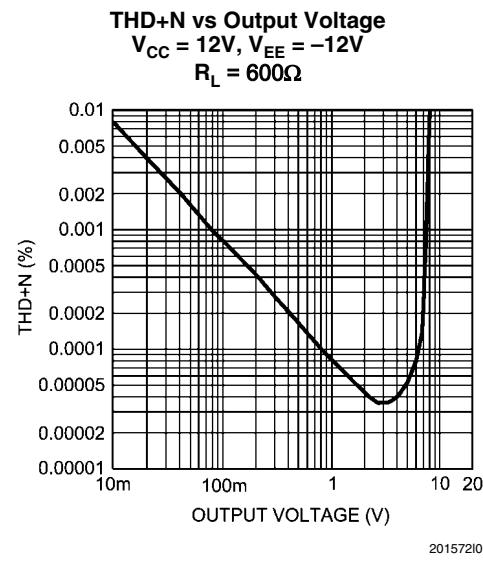
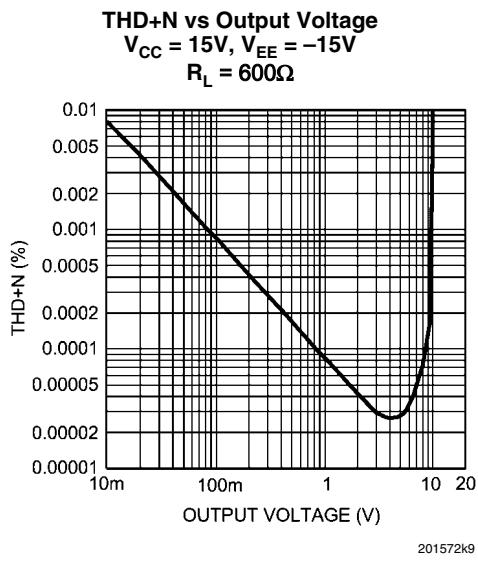
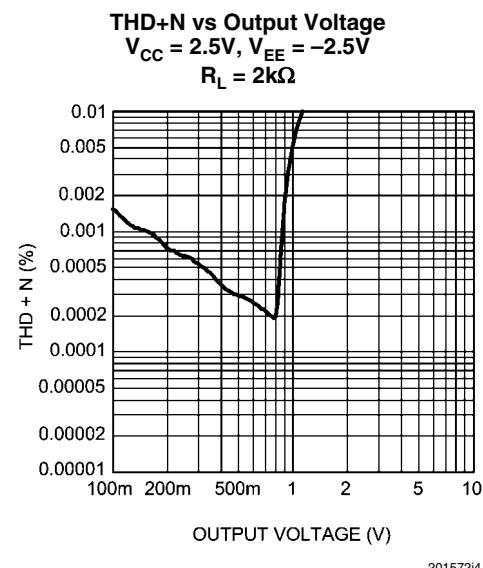
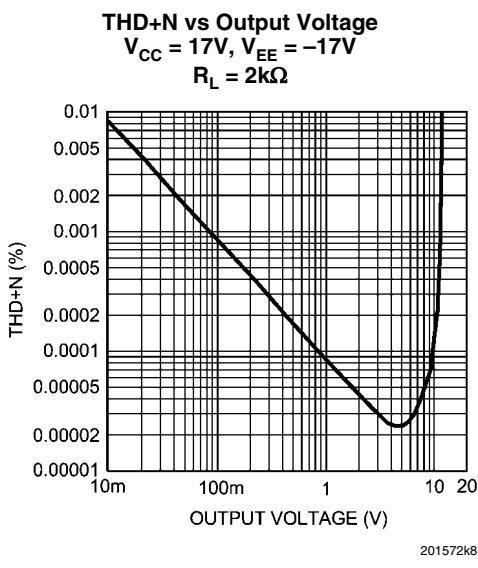
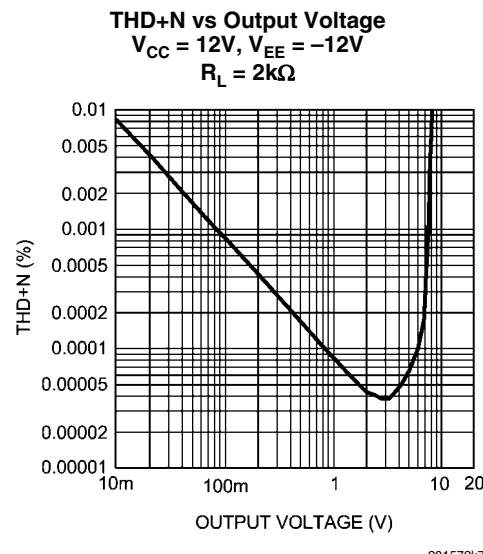
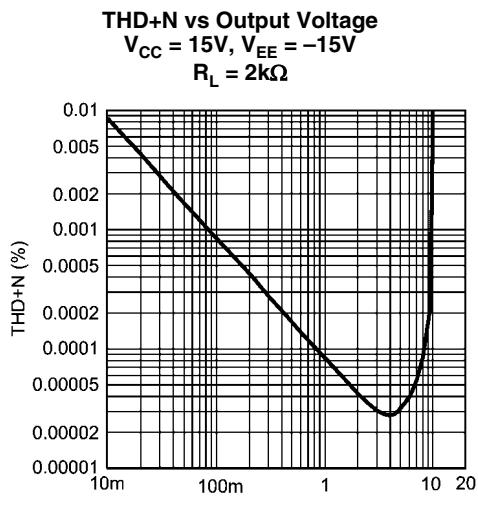
Note 5: Machine Model ESD test is covered by specification EIAJ IC-121-1981. A 200pF cap is charged to the specified voltage and then discharged directly into the IC with no external series resistor (resistance of discharge path must be under 50Ω).

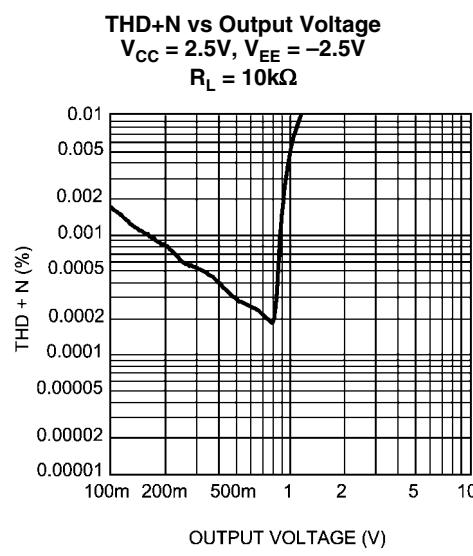
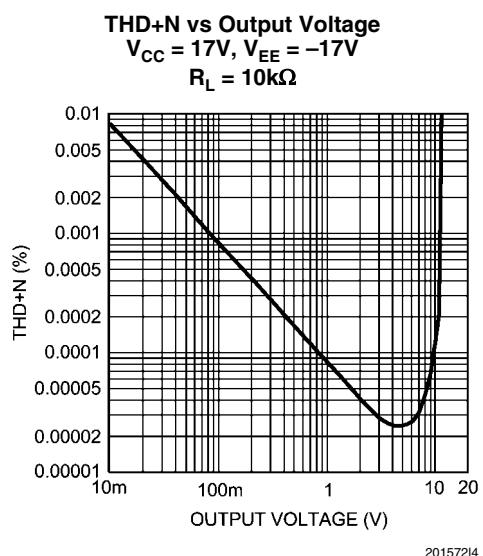
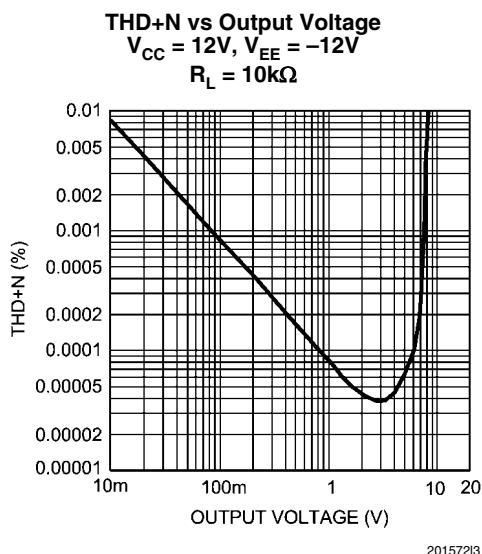
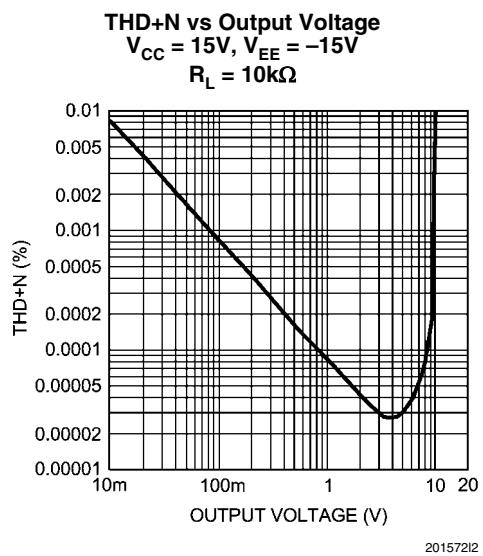
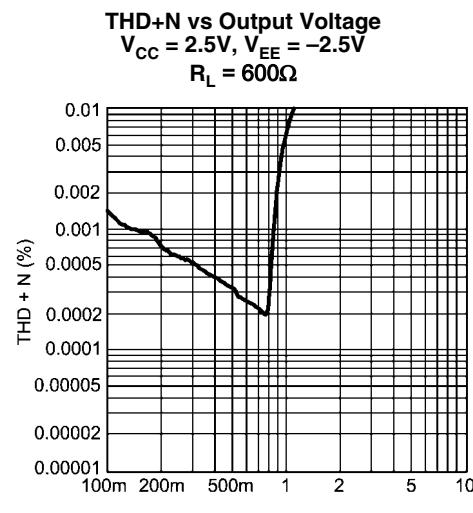
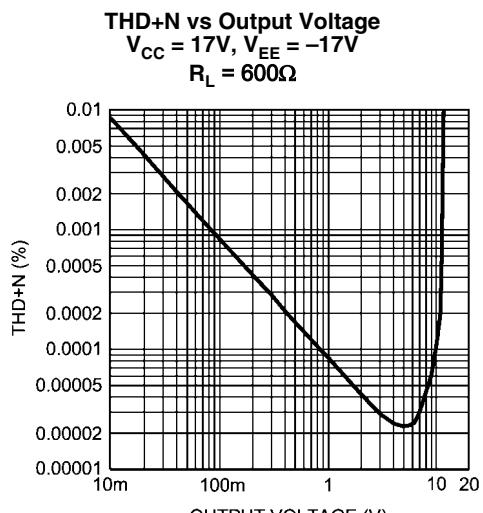
Note 6: Typical specifications are specified at $+25^\circ C$ and represent the most likely parametric norm.

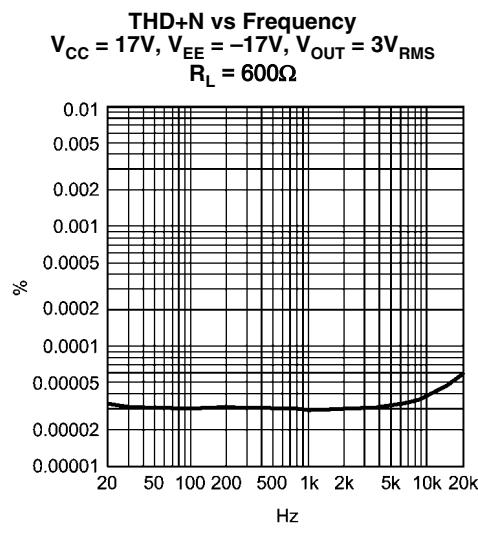
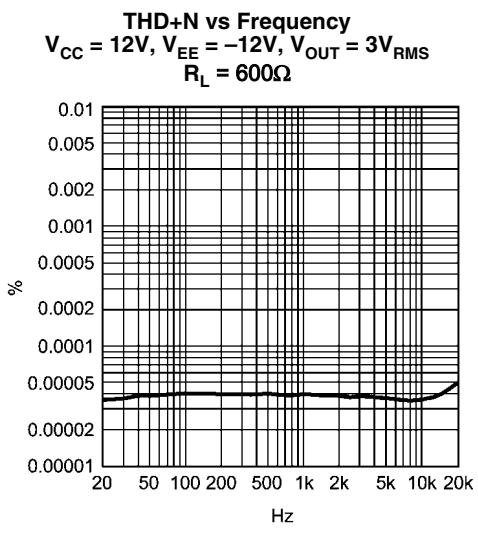
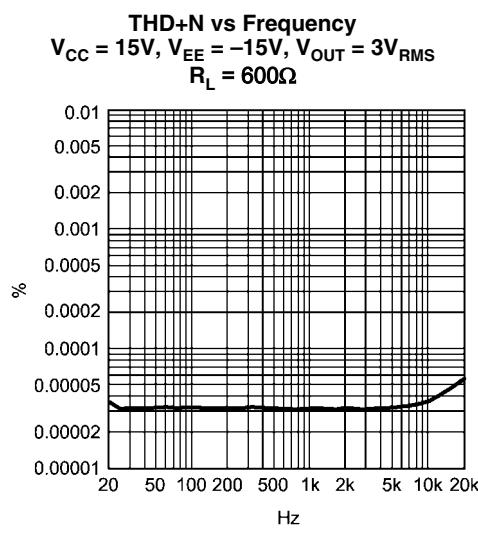
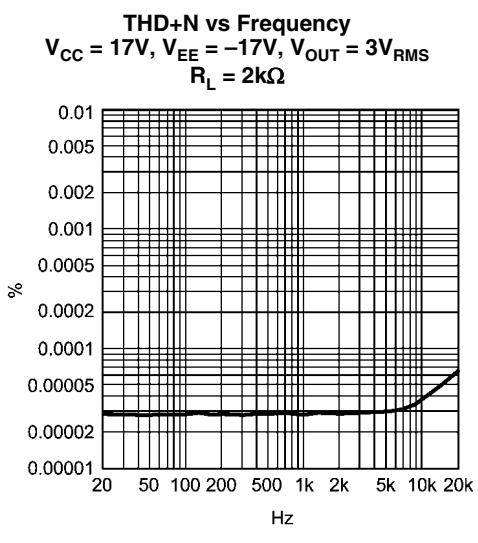
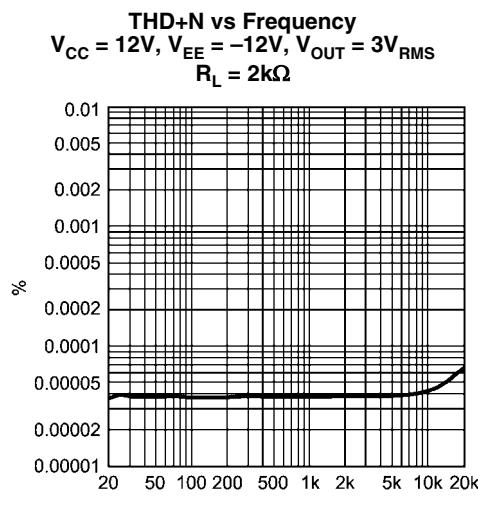
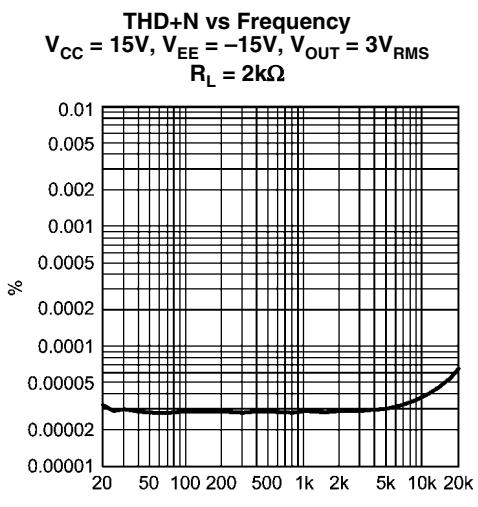
Note 7: Tested limits are guaranteed to National's AOQL (Average Outgoing Quality Level).

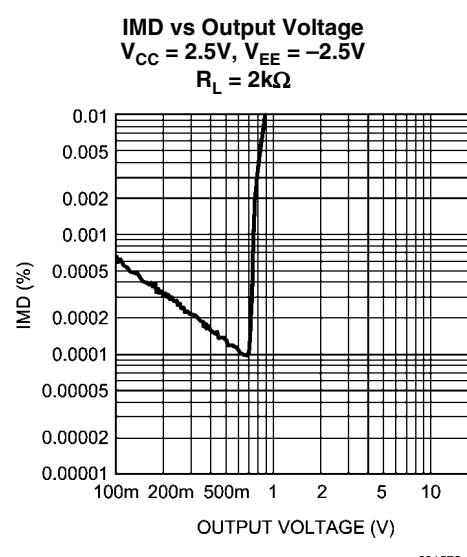
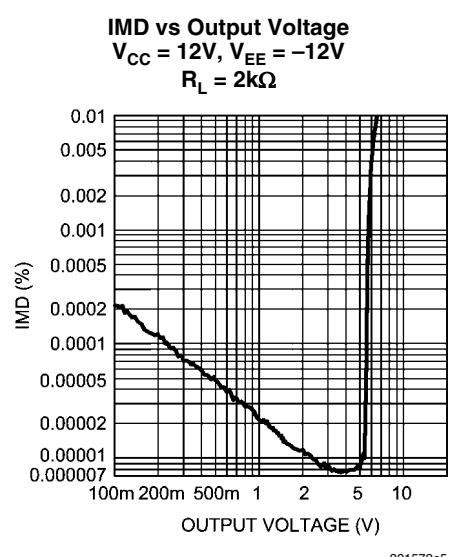
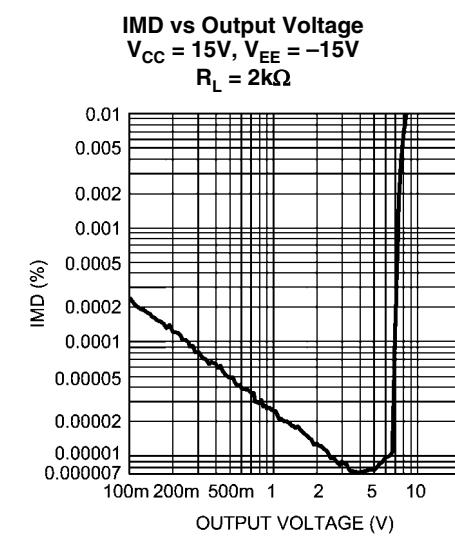
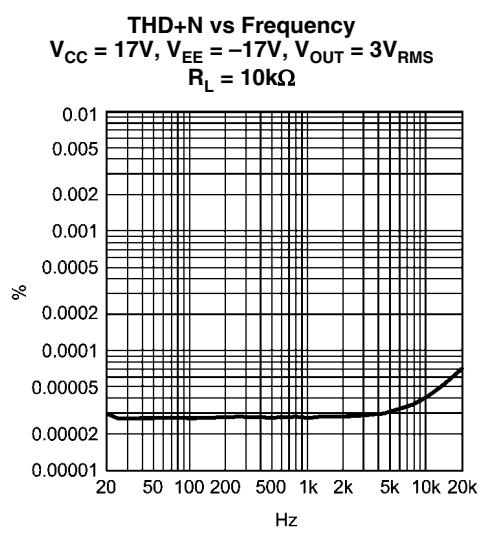
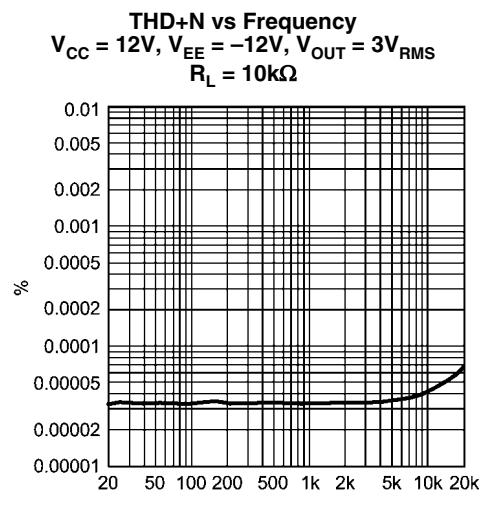
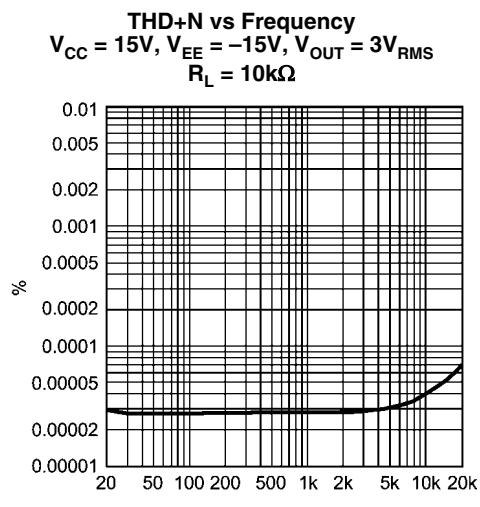
Note 8: PSRR is measured as follows: V_{OS} is measured at two supply voltages, $\pm 5V$ and $\pm 15V$. $PSRR = 20\log(\Delta V_{OS}/\Delta V_S) I$.

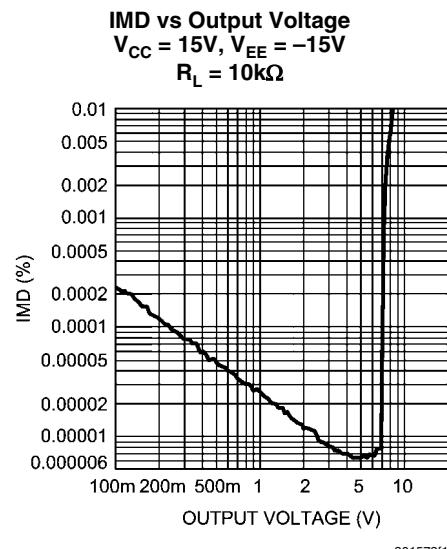
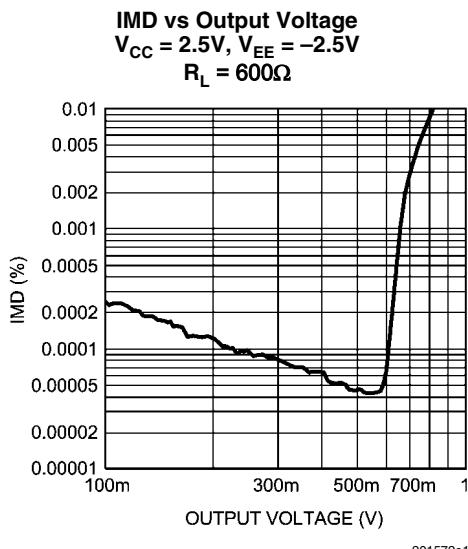
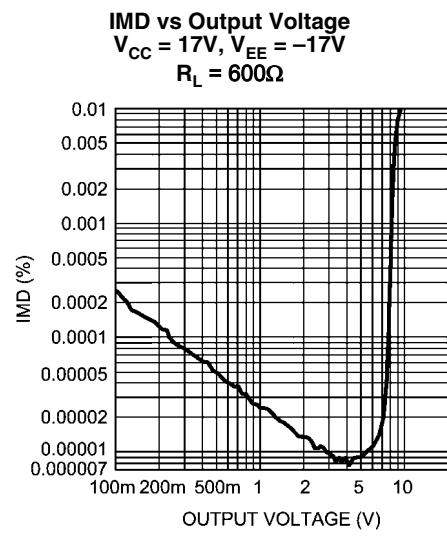
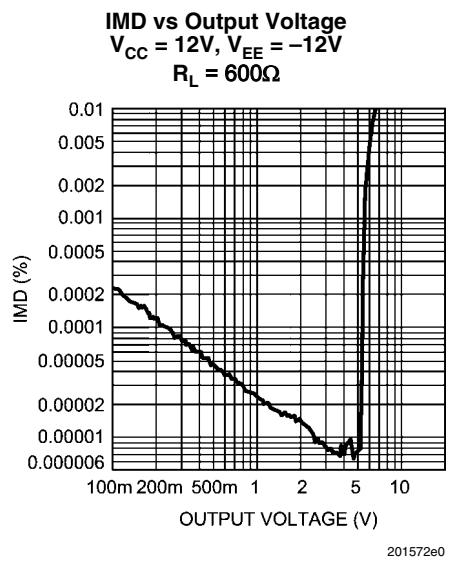
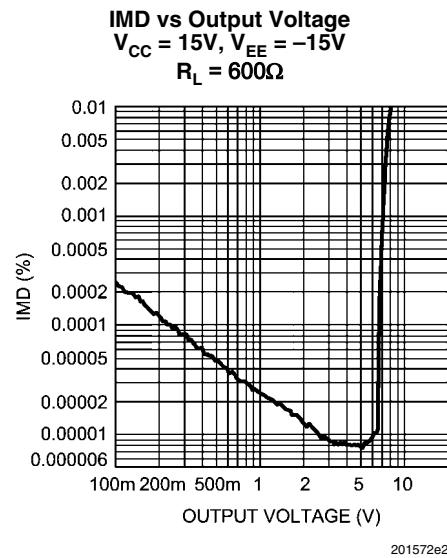
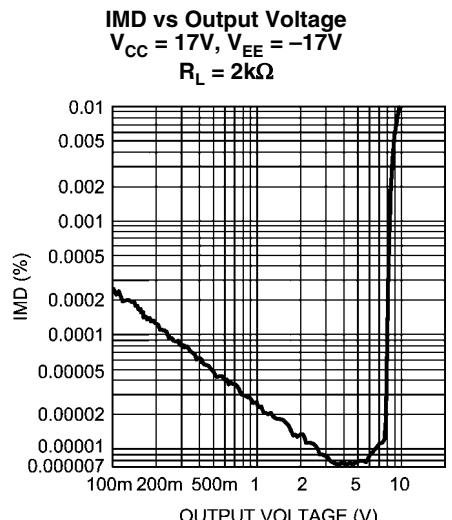
Typical Performance Characteristics

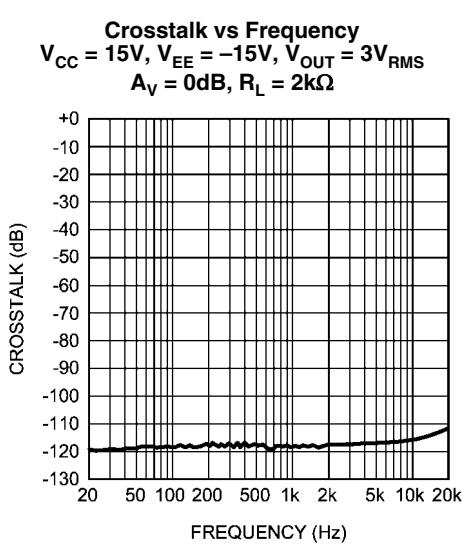
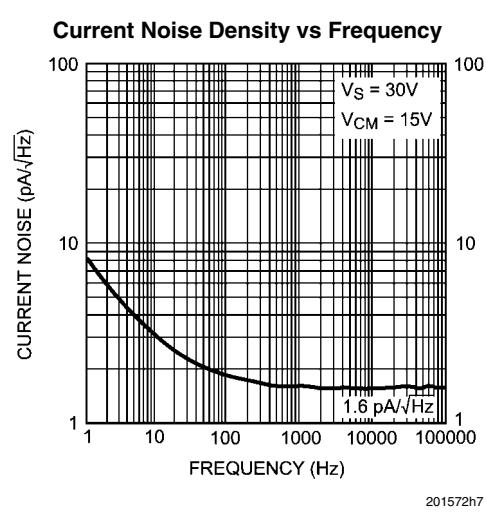
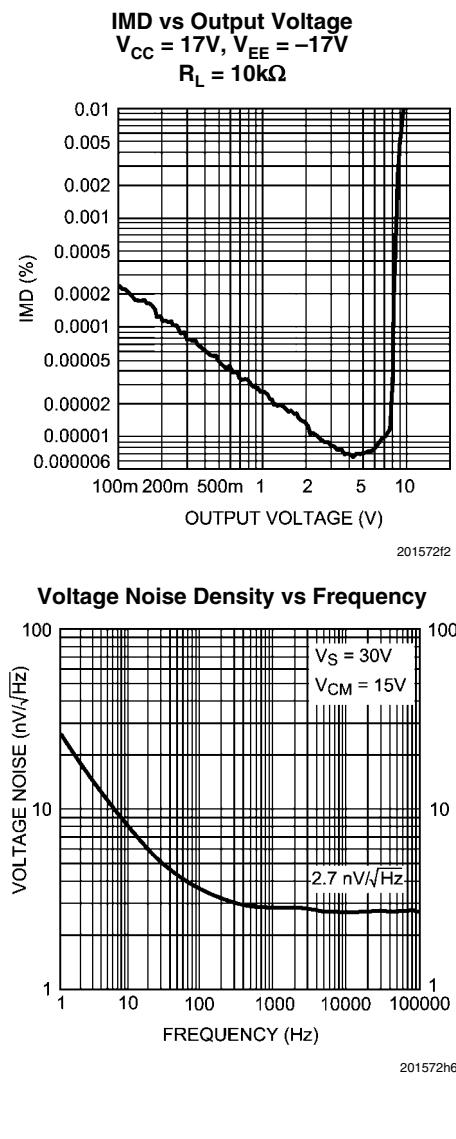
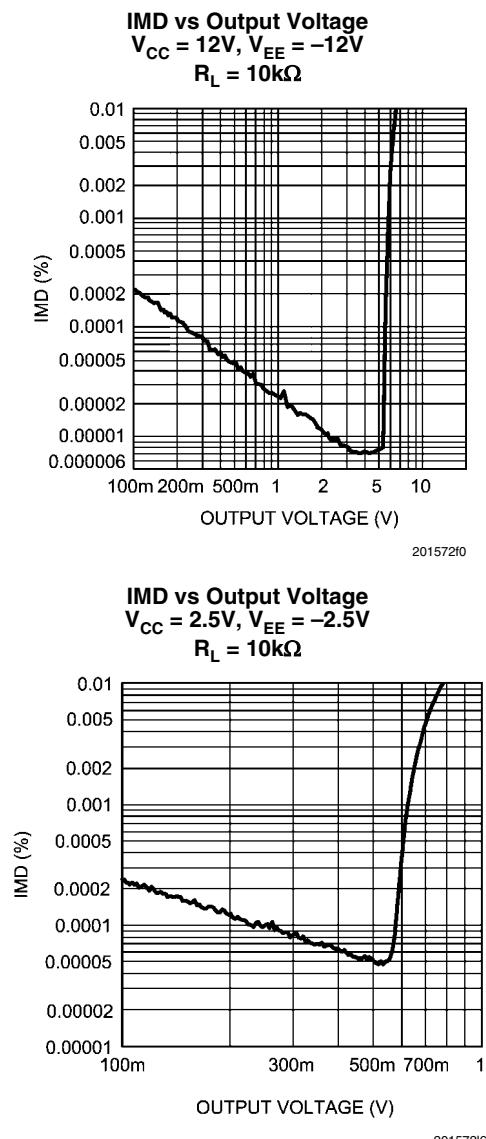




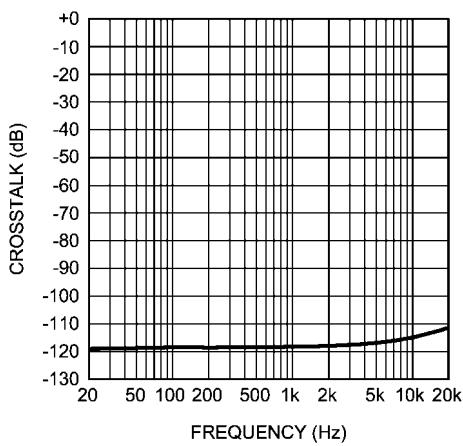




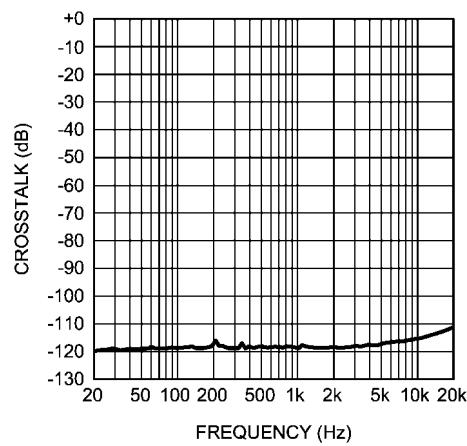




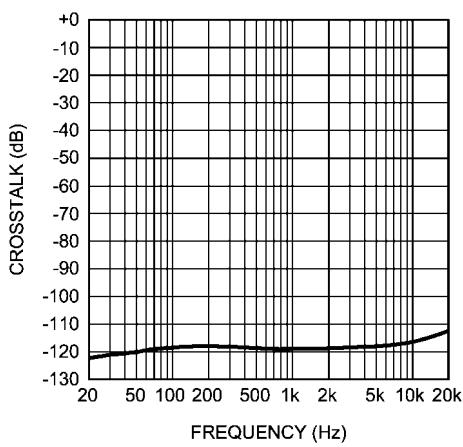
Crosstalk vs Frequency
 $V_{CC} = 15V$, $V_{EE} = -15V$, $V_{OUT} = 10V_{RMS}$
 $A_V = 0\text{dB}$, $R_L = 2k\Omega$



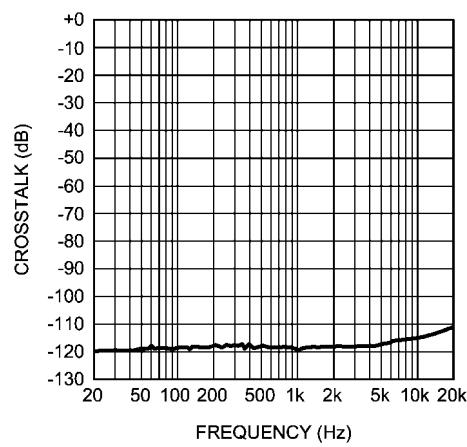
Crosstalk vs Frequency
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 $A_V = 0\text{dB}$, $R_L = 2k\Omega$



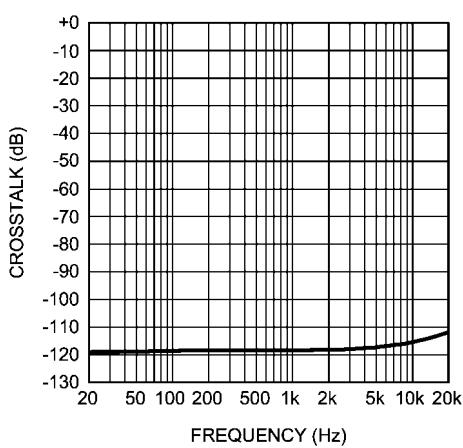
Crosstalk vs Frequency
 $V_{CC} = 12V$, $V_{EE} = -12V$, $V_{OUT} = 10V_{RMS}$
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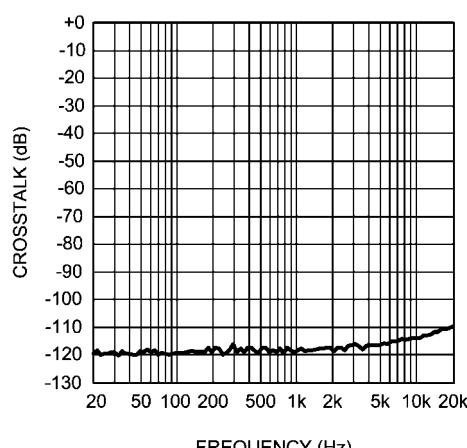
Crosstalk vs Frequency
 $V_{CC} = 17V$, $V_{EE} = -17V$, $V_{OUT} = 3V_{RMS}$
 $A_V = 0\text{dB}$, $R_L = 2k\Omega$

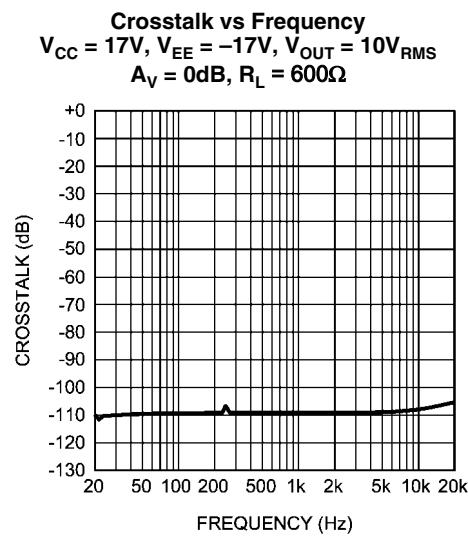
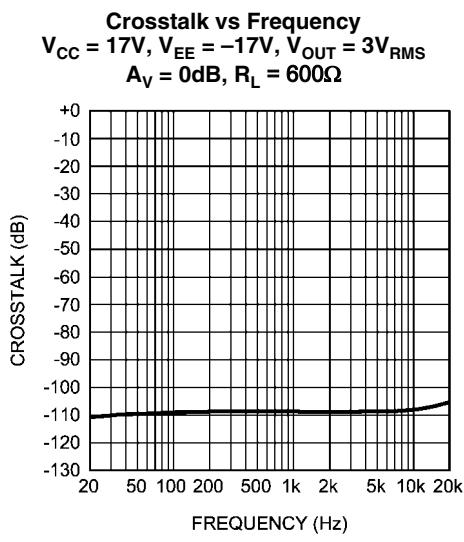
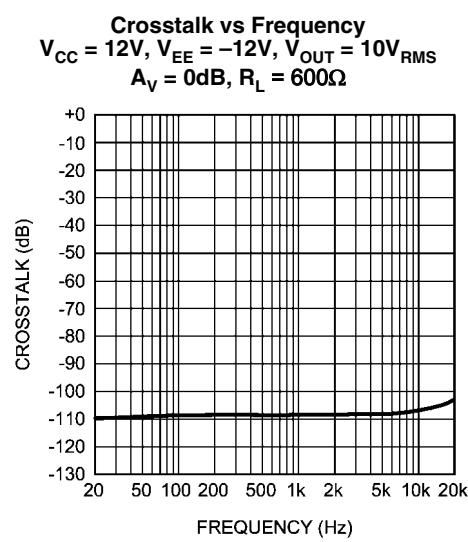
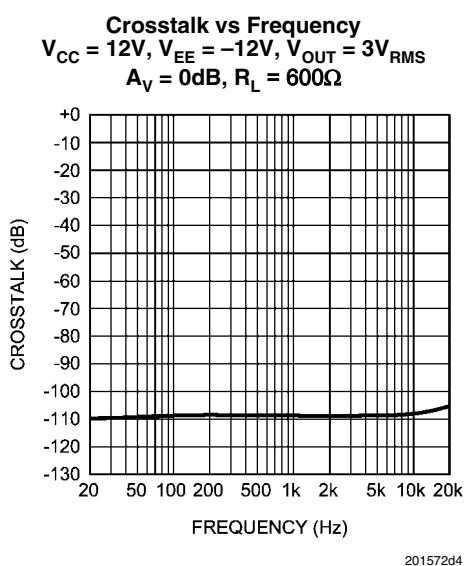
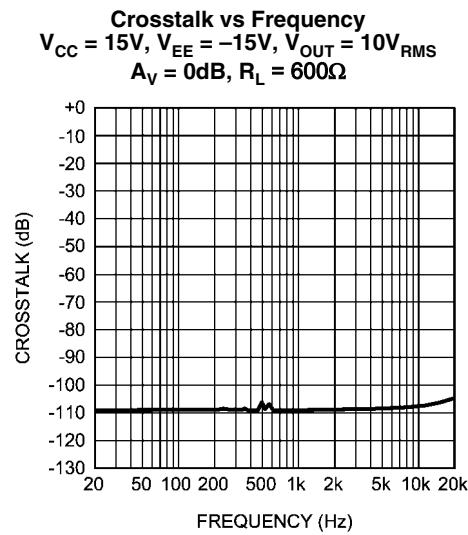
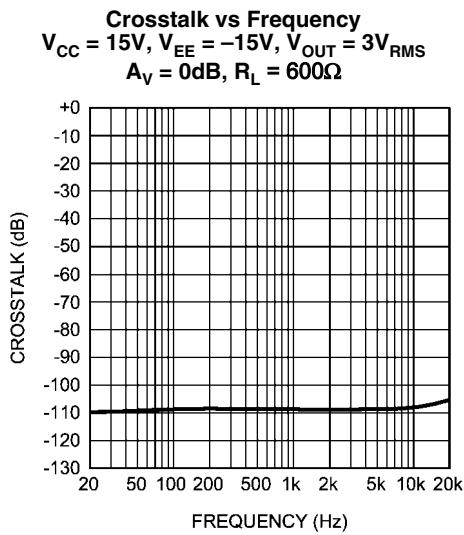


Crosstalk vs Frequency
 $V_{CC} = 17V$, $V_{EE} = -17V$, $V_{OUT} = 10V_{RMS}$
 $A_V = 0\text{dB}$, $R_L = 2k\Omega$

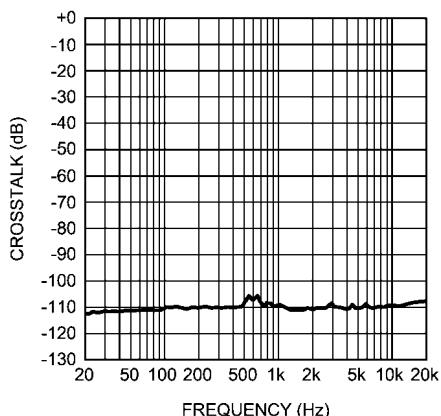


Crosstalk vs Frequency
 $V_{CC} = 2.5V$, $V_{EE} = -2.5V$, $V_{OUT} = 1V_{RMS}$
 $A_V = 0\text{dB}$, $R_L = 2k\Omega$

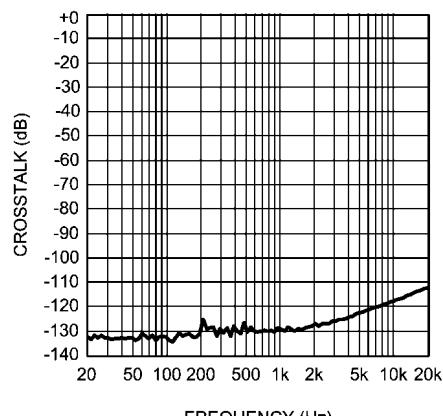




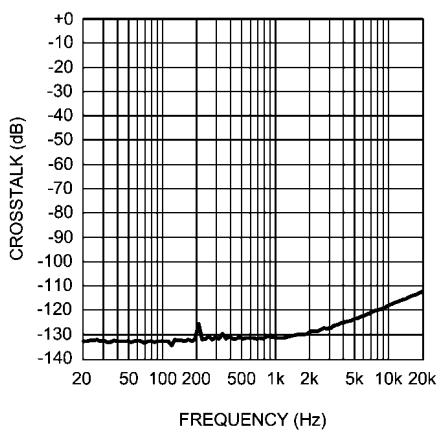
Crosstalk vs Frequency
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 $A_V = 0dB$, $R_L = 600\Omega$



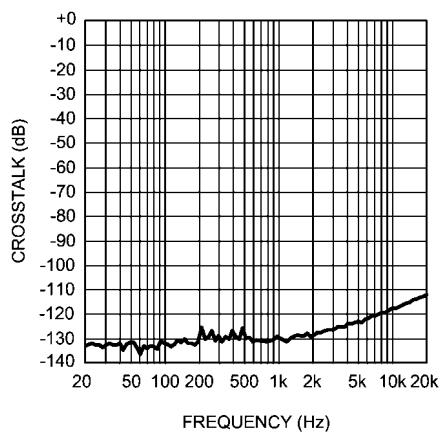
Crosstalk vs Frequency
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 $A_V = 0dB$, $R_L = 10k\Omega$



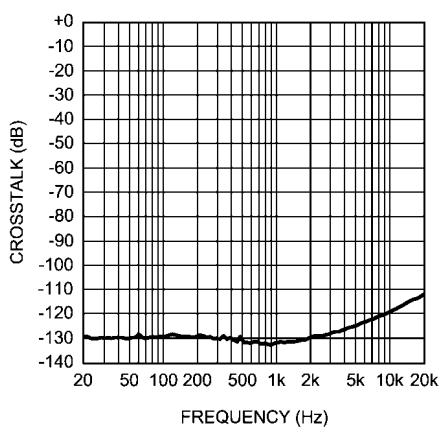
Crosstalk vs Frequency
 $V_{CC} = 15V$, $V_{EE} = -15V$, $V_{OUT} = 10V_{RMS}$
 $A_V = 0dB$, $R_L = 10k\Omega$



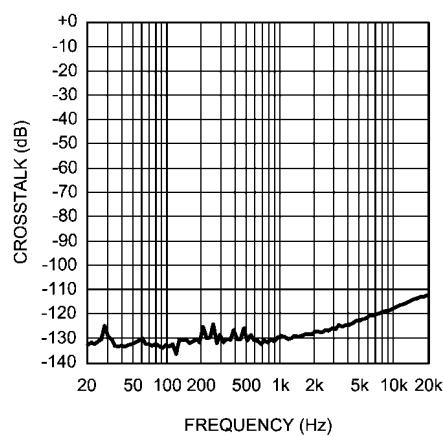
Crosstalk vs Frequency
 $V_{CC} = 12V$, $V_{EE} = -12V$, $V_{OUT} = 3V_{RMS}$
 $A_V = 0dB$, $R_L = 10k\Omega$



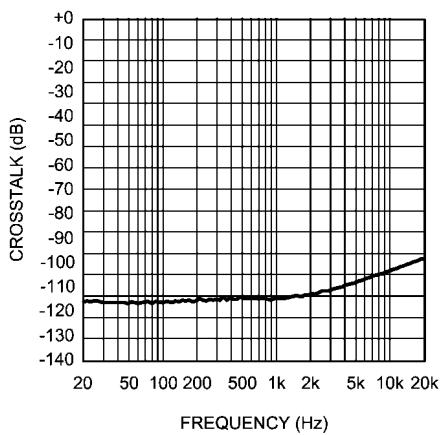
Crosstalk vs Frequency
 $V_{CC} = 12V$, $V_{EE} = -12V$, $V_{OUT} = 10V_{RMS}$
 $A_V = 0dB$, $R_L = 10k\Omega$



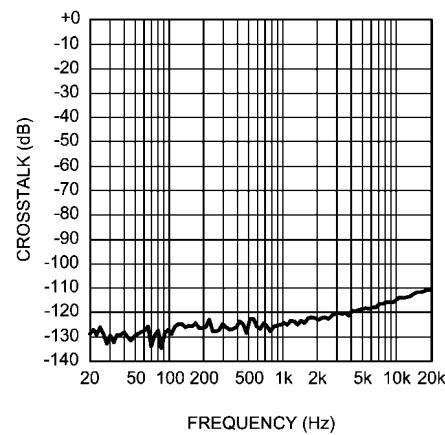
Crosstalk vs Frequency
 $V_{CC} = 17V$, $V_{EE} = -17V$, $V_{OUT} = 3V_{RMS}$
 $A_V = 0dB$, $R_L = 10k\Omega$



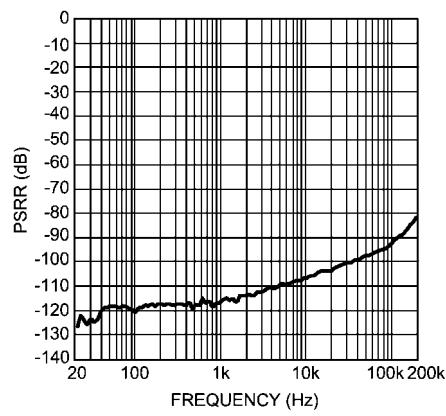
Crosstalk vs Frequency
 $V_{CC} = 17V$, $V_{EE} = -17V$, $V_{OUT} = 10V_{RMS}$
 $A_V = 0dB$, $R_L = 10k\Omega$



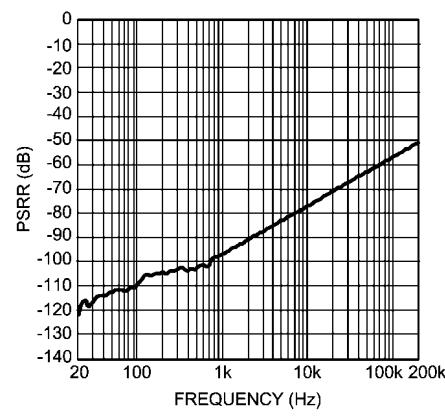
Crosstalk vs Frequency
 $V_{CC} = 2.5V$, $V_{EE} = -2.5V$, $V_{OUT} = 1V_{RMS}$
 $A_V = 0dB$, $R_L = 10k\Omega$



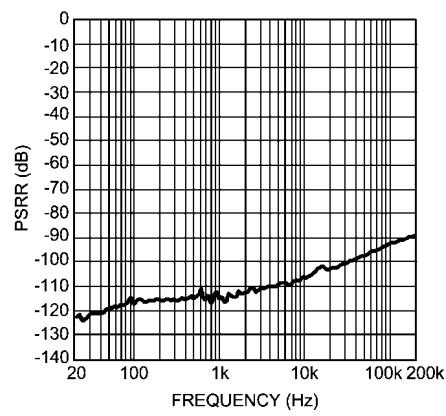
PSRR+ vs Frequency
 $V_{CC} = 15V$, $V_{EE} = -15V$
 $R_L = 10k\Omega$, $f = 200kHz$, $V_{RIPPLE} = 200mVpp$



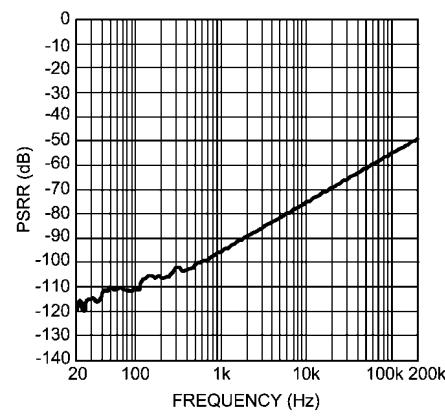
PSRR- vs Frequency
 $V_{CC} = 15V$, $V_{EE} = -15V$
 $R_L = 10k\Omega$, $f = 200kHz$, $V_{RIPPLE} = 200mVpp$



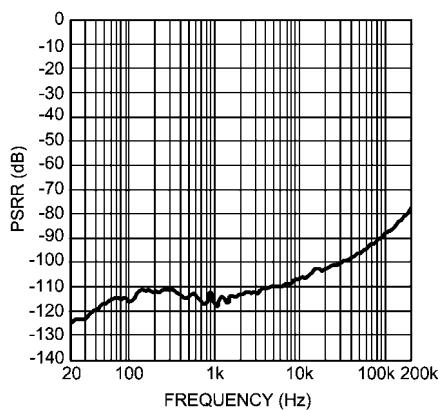
PSRR+ vs Frequency
 $V_{CC} = 15V$, $V_{EE} = -15V$
 $R_L = 2k\Omega$, $f = 200kHz$, $V_{RIPPLE} = 200mVpp$



PSRR- vs Frequency
 $V_{CC} = 15V$, $V_{EE} = -15V$
 $R_L = 2k\Omega$, $f = 200kHz$, $V_{RIPPLE} = 200mVpp$

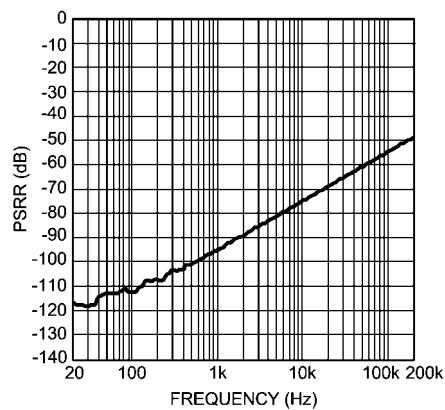


PSRR+ vs Frequency
 $V_{CC} = 15V, V_{EE} = -15V$
 $R_L = 600\Omega, f = 200kHz, V_{RIPPLE} = 200mVpp$



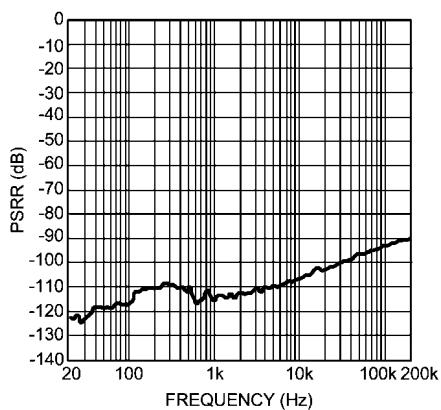
201572p0

PSRR- vs Frequency
 $V_{CC} = 15V, V_{EE} = -15V$
 $R_L = 600\Omega, f = 200kHz, V_{RIPPLE} = 200mVpp$



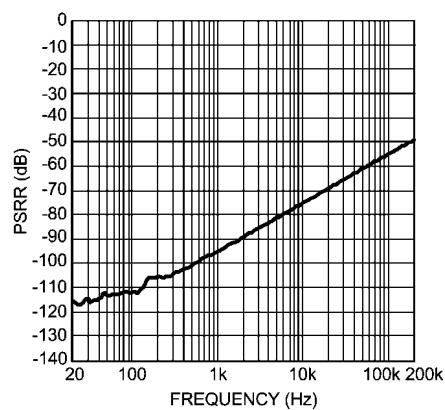
201572p3

PSRR+ vs Frequency
 $V_{CC} = 12V, V_{EE} = -12V$
 $R_L = 10k\Omega, f = 200kHz, V_{RIPPLE} = 200mVpp$



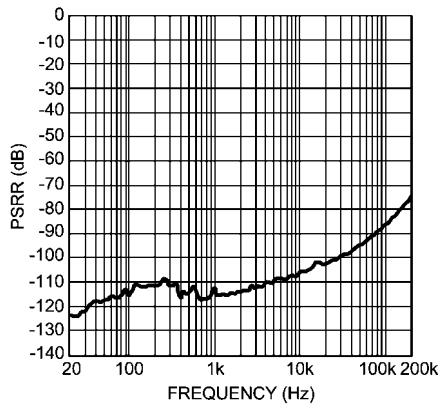
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PSRR- vs Frequency
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 $R_L = 10k\Omega, f = 200kHz, V_{RIPPLE} = 200mVpp$



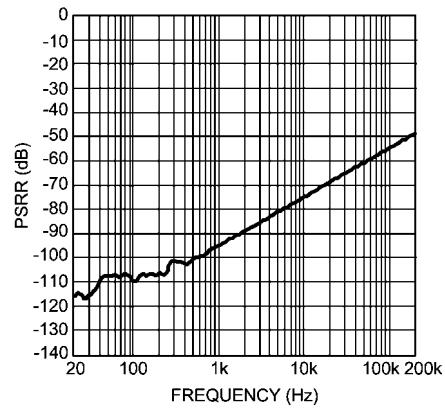
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PSRR+ vs Frequency
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 $R_L = 2k\Omega, f = 200kHz, V_{RIPPLE} = 200mVpp$



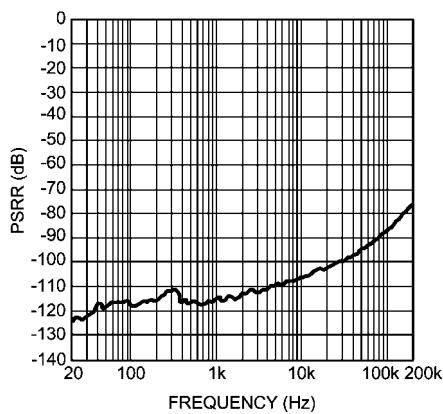
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PSRR- vs Frequency
 $V_{CC} = 12V, V_{EE} = -12V$
 $R_L = 2k\Omega, f = 200kHz, V_{RIPPLE} = 200mVpp$

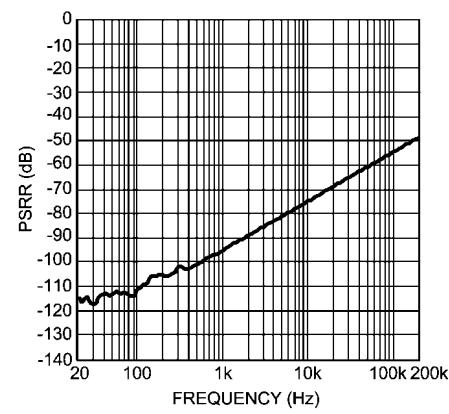


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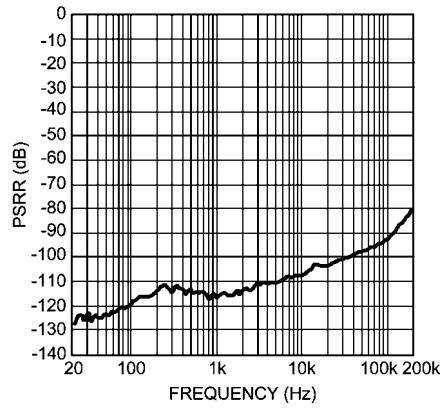
PSRR+ vs Frequency
 $V_{CC} = 12V, V_{EE} = -12V$
 $R_L = 600\Omega, f = 200kHz, V_{RIPPLE} = 200mVpp$



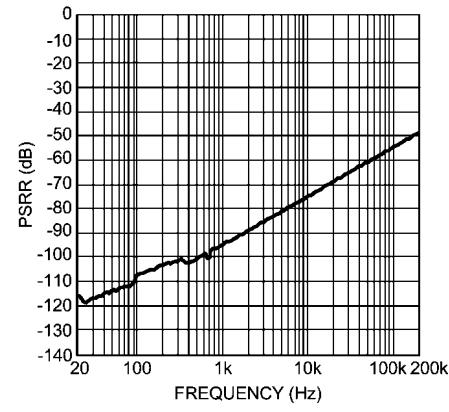
PSRR- vs Frequency
 $V_{CC} = 12V, V_{EE} = -12V$
 $R_L = 600\Omega, f = 200kHz, V_{RIPPLE} = 200mVpp$



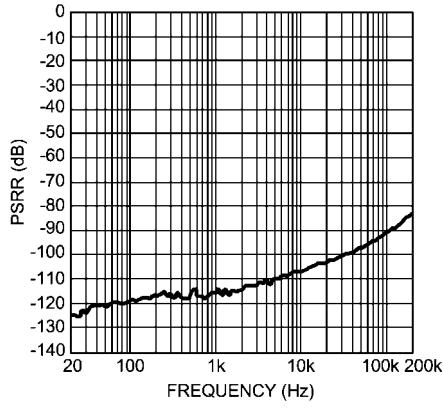
PSRR+ vs Frequency
 $V_{CC} = 17V, V_{EE} = -17V$
 $R_L = 10k\Omega, f = 200kHz, V_{RIPPLE} = 200mVpp$



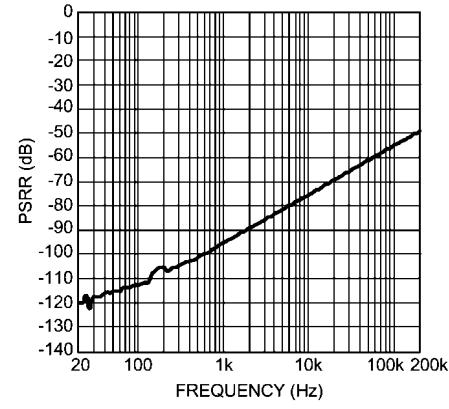
PSRR- vs Frequency
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 $R_L = 10k\Omega, f = 200kHz, V_{RIPPLE} = 200mVpp$



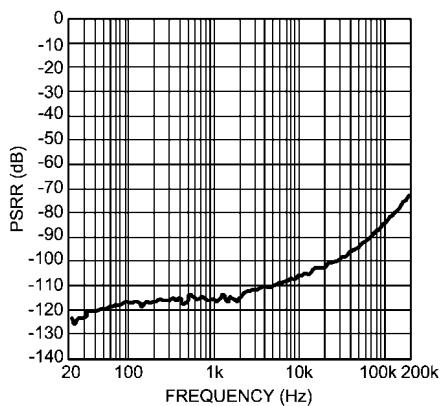
PSRR+ vs Frequency
 $V_{CC} = 17V, V_{EE} = -17V$
 $R_L = 2k\Omega, f = 200kHz, V_{RIPPLE} = 200mVpp$



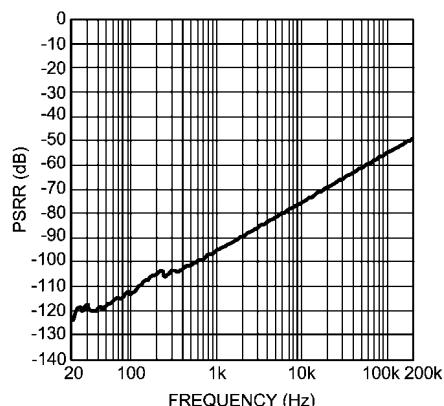
PSRR- vs Frequency
 $V_{CC} = 17V, V_{EE} = -17V$
 $R_L = 2k\Omega, f = 200kHz, V_{RIPPLE} = 200mVpp$



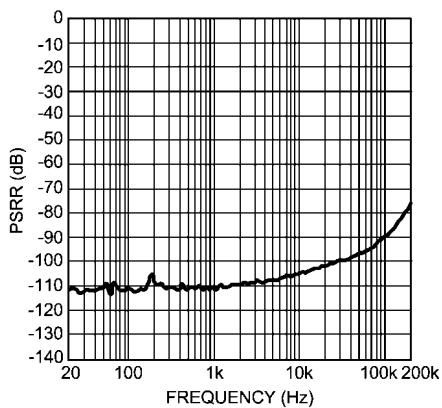
PSRR+ vs Frequency
 $V_{CC} = 17V, V_{EE} = -17V$
 $R_L = 600\Omega, f = 200kHz, V_{RIPPLE} = 200mVpp$



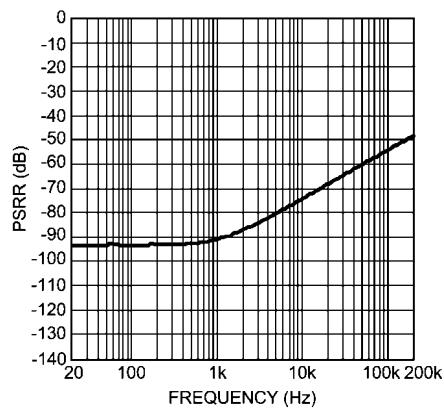
PSRR- vs Frequency
 $V_{CC} = 17V, V_{EE} = -17V$
 $R_L = 600\Omega, f = 200kHz, V_{RIPPLE} = 200mVpp$



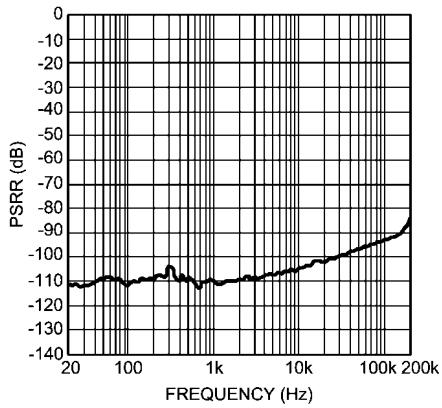
PSRR+ vs Frequency
 $V_{CC} = 2.5V, V_{EE} = -2.5V$
 $R_L = 10k\Omega, f = 200kHz, V_{RIPPLE} = 200mVpp$



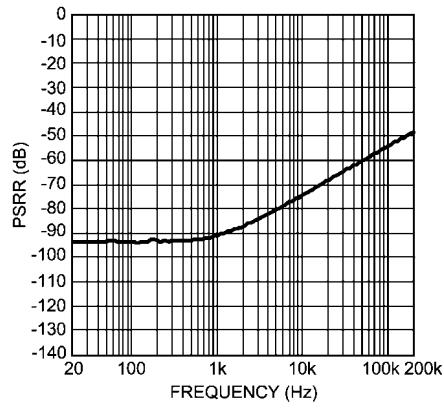
PSRR- vs Frequency
 $V_{CC} = 2.5V, V_{EE} = -2.5V$
 $R_L = 10k\Omega, f = 200kHz, V_{RIPPLE} = 200mVpp$



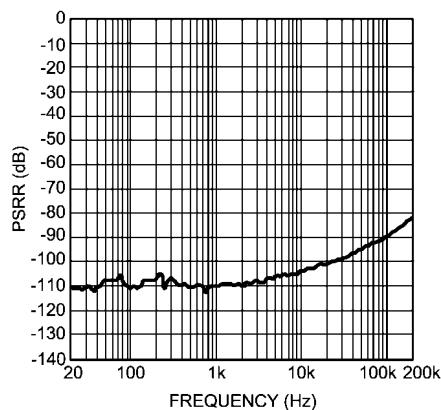
PSRR+ vs Frequency
 $V_{CC} = 2.5V, V_{EE} = -2.5V$
 $R_L = 2k\Omega, f = 200kHz, V_{RIPPLE} = 200mVpp$



PSRR- vs Frequency
 $V_{CC} = 2.5V, V_{EE} = -2.5V$
 $R_L = 2k\Omega, f = 200kHz, V_{RIPPLE} = 200mVpp$

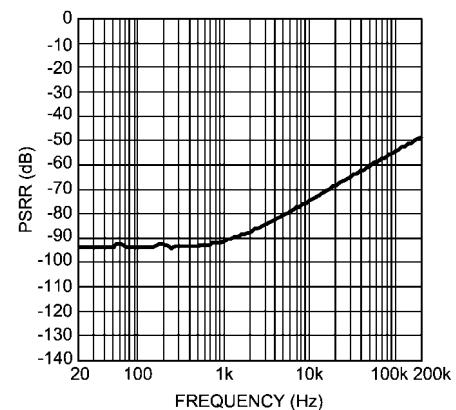


PSRR+ vs Frequency
 $V_{CC} = 2.5V$, $V_{EE} = -2.5V$
 $R_L = 600\Omega$, $f = 200kHz$, $V_{RIPPLE} = 200mVpp$



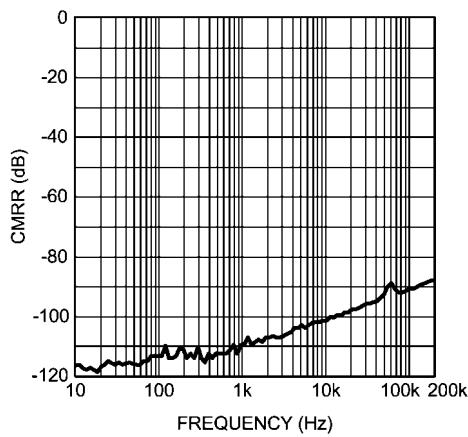
201572q2

PSRR- vs Frequency
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 $R_L = 600\Omega$, $f = 200kHz$, $V_{RIPPLE} = 200mVpp$



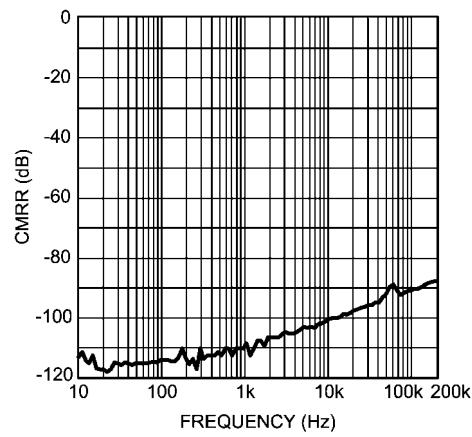
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CMRR vs Frequency
 $V_{CC} = 15V$, $V_{EE} = -15V$
 $R_L = 2k\Omega$



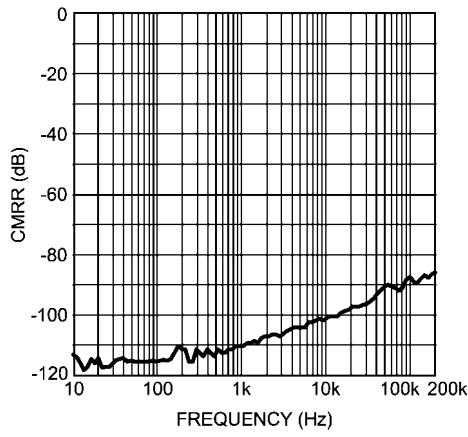
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CMRR vs Frequency
 $V_{CC} = 12V$, $V_{EE} = -12V$
 $R_L = 2k\Omega$



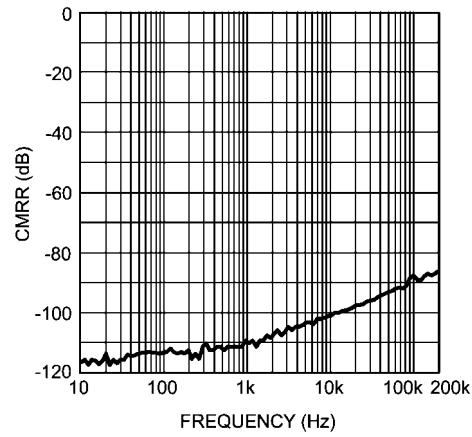
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CMRR vs Frequency
 $V_{CC} = 17V$, $V_{EE} = -17V$
 $R_L = 2k\Omega$

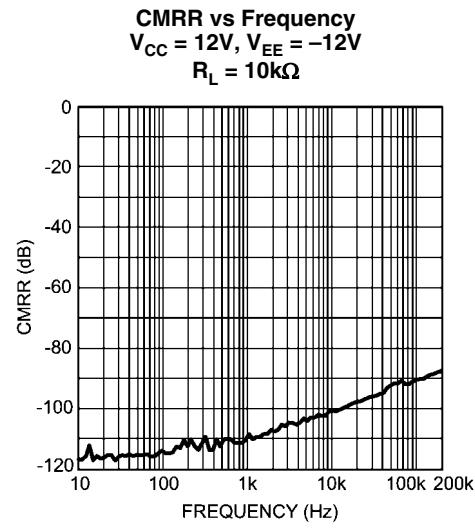
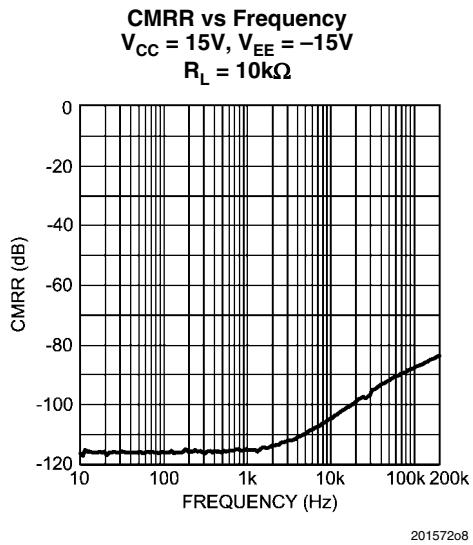
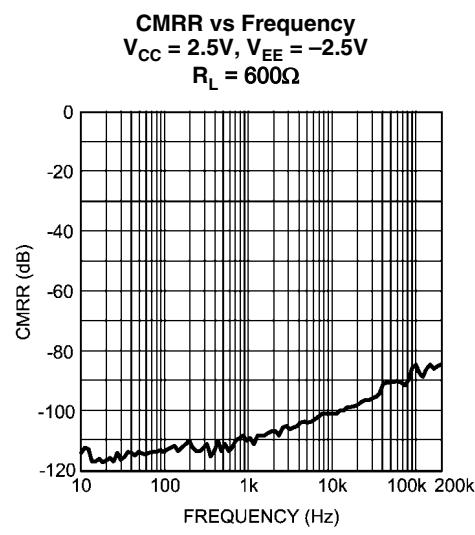
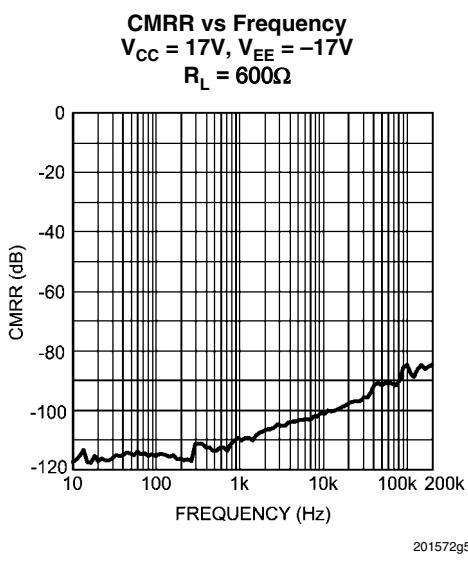
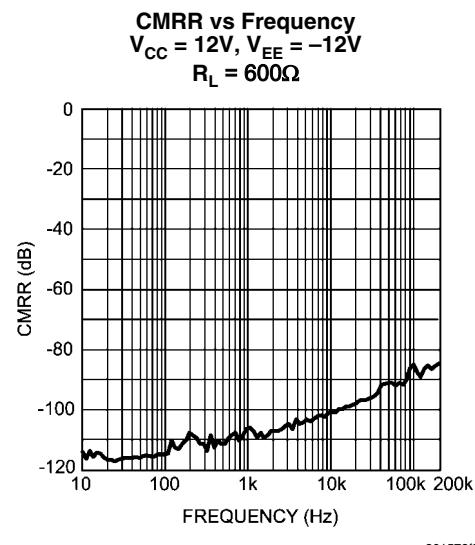
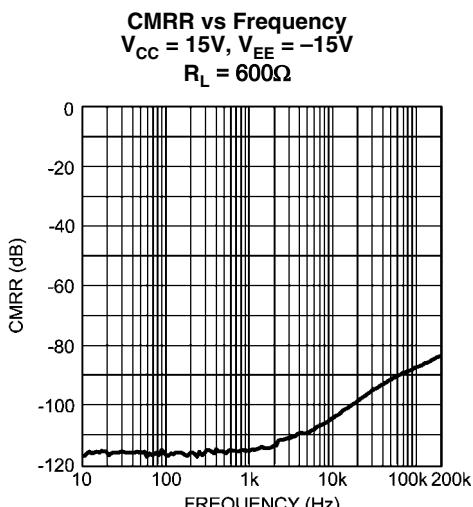


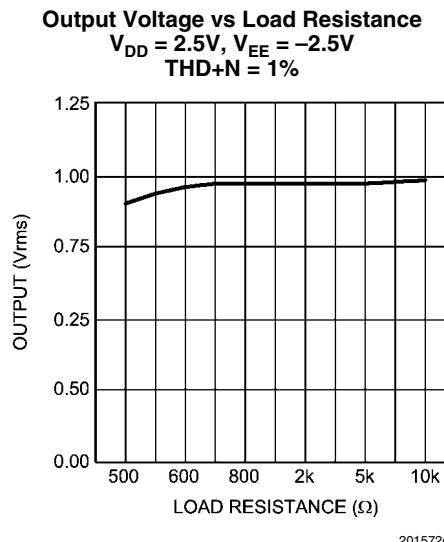
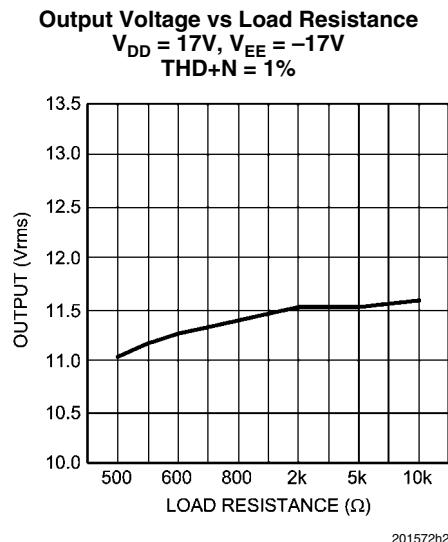
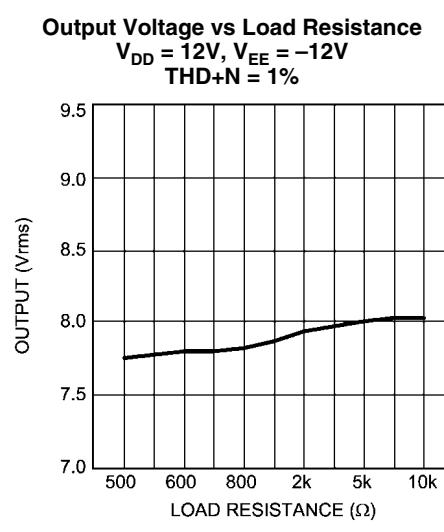
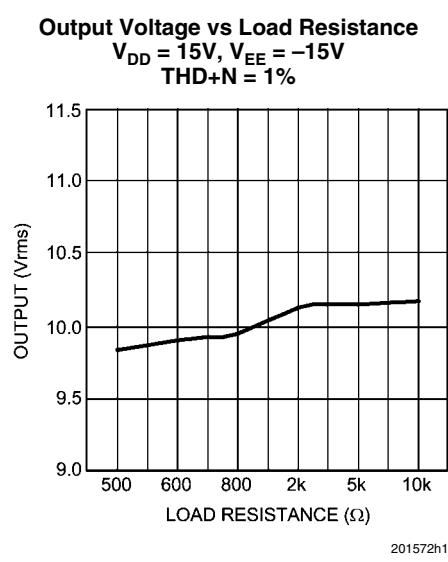
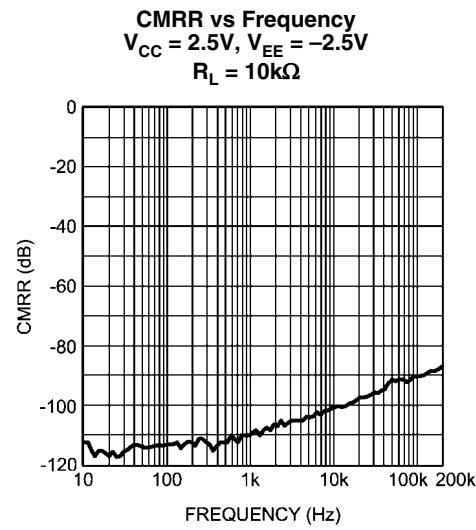
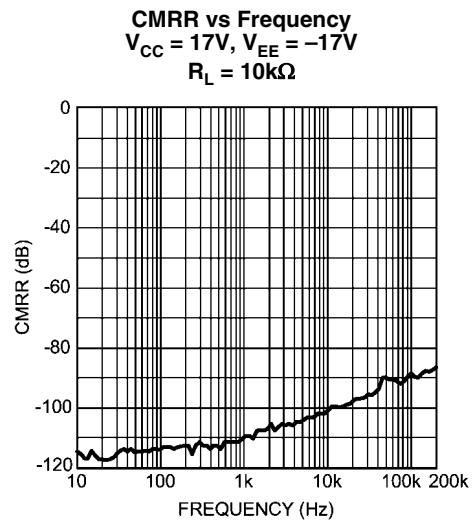
201572g3

CMRR vs Frequency
 $V_{CC} = 2.5V$, $V_{EE} = -2.5V$
 $R_L = 2k\Omega$

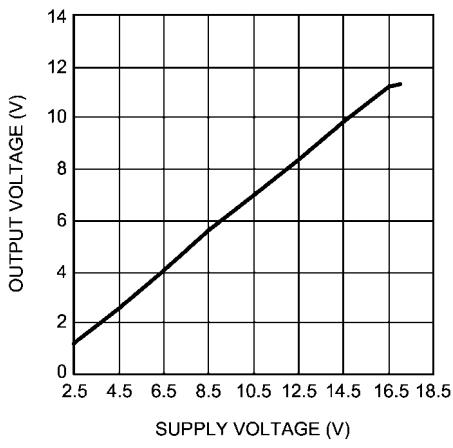


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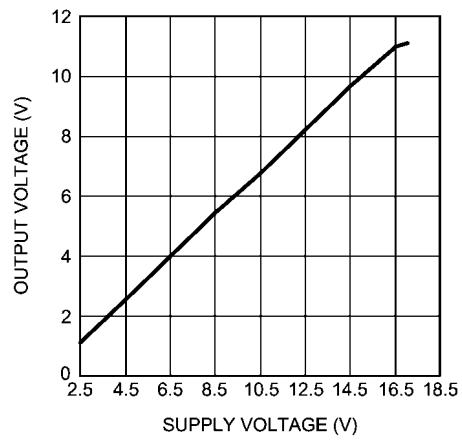




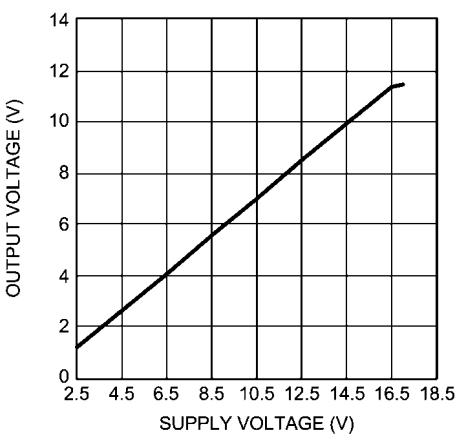
Output Voltage vs Supply Voltage
 $R_L = 2\text{k}\Omega$, THD+N = 1%



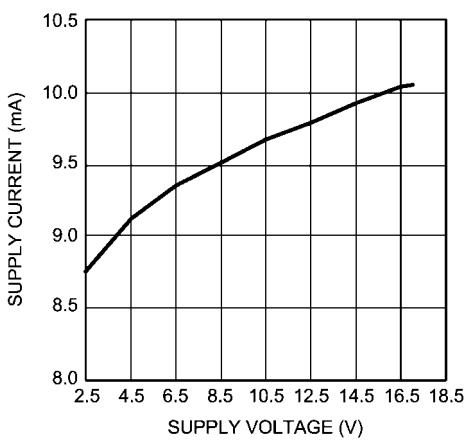
Output Voltage vs Supply Voltage
 $R_L = 600\Omega$, THD+N = 1%



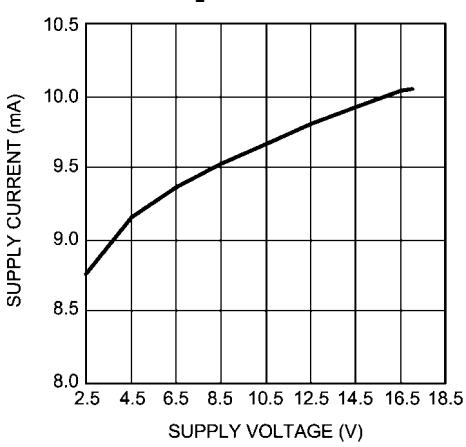
Output Voltage vs Supply Voltage
 $R_L = 10\text{k}\Omega$, THD+N = 1%



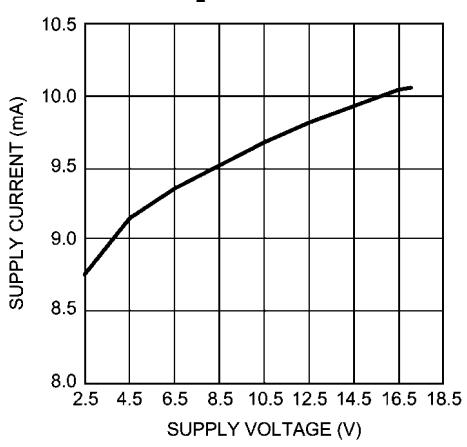
Supply Current vs Supply Voltage
 $R_L = 2\text{k}\Omega$

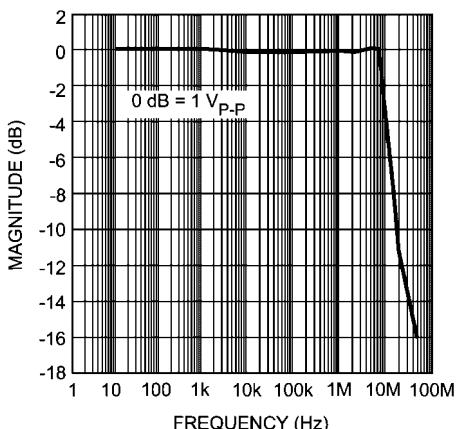


Supply Current vs Supply Voltage
 $R_L = 600\Omega$

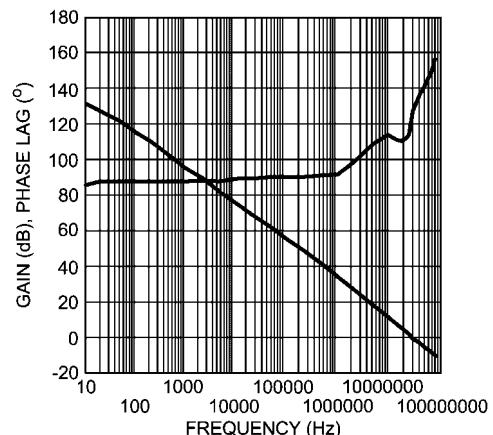


Supply Current vs Supply Voltage
 $R_L = 10\text{k}\Omega$

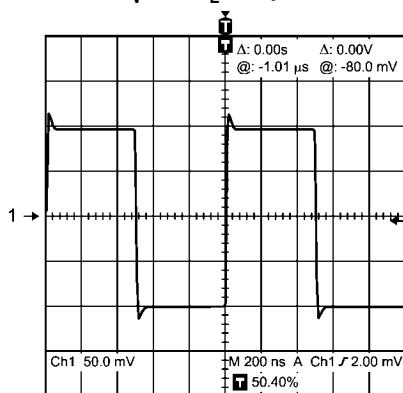


Full Power Bandwidth vs Frequency

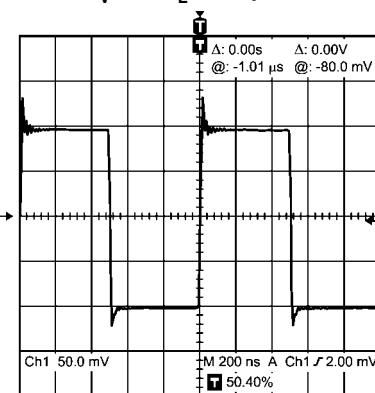
201572j0

Gain Phase vs Frequency

201572j1

Small-Signal Transient Response $A_V = 1, C_L = 10\text{pF}$ 

201572j7

Small-Signal Transient Response $A_V = 1, C_L = 100\text{pF}$ 

201572j8

Application Information

DISTORTION MEASUREMENTS

The vanishingly low residual distortion produced by LM4562 is below the capabilities of all commercially available equipment. This makes distortion measurements just slightly more difficult than simply connecting a distortion meter to the amplifier's inputs and outputs. The solution, however, is quite simple: an additional resistor. Adding this resistor extends the resolution of the distortion measurement equipment.

The LM4562's low residual distortion is an input referred internal error. As shown in Figure 1, adding the 10Ω resistor connected between the amplifier's inverting and non-inverting inputs changes the amplifier's noise gain. The result is that

the error signal (distortion) is amplified by a factor of 101. Although the amplifier's closed-loop gain is unaltered, the feedback available to correct distortion errors is reduced by 101, which means that measurement resolution increases by 101. To ensure minimum effects on distortion measurements, keep the value of R1 low as shown in Figure 1.

This technique is verified by duplicating the measurements with high closed loop gain and/or making the measurements at high frequencies. Doing so produces distortion components that are within the measurement equipment's capabilities. This datasheet's THD+N and IMD values were generated using the above described circuit connected to an Audio Precision System Two Cascade.

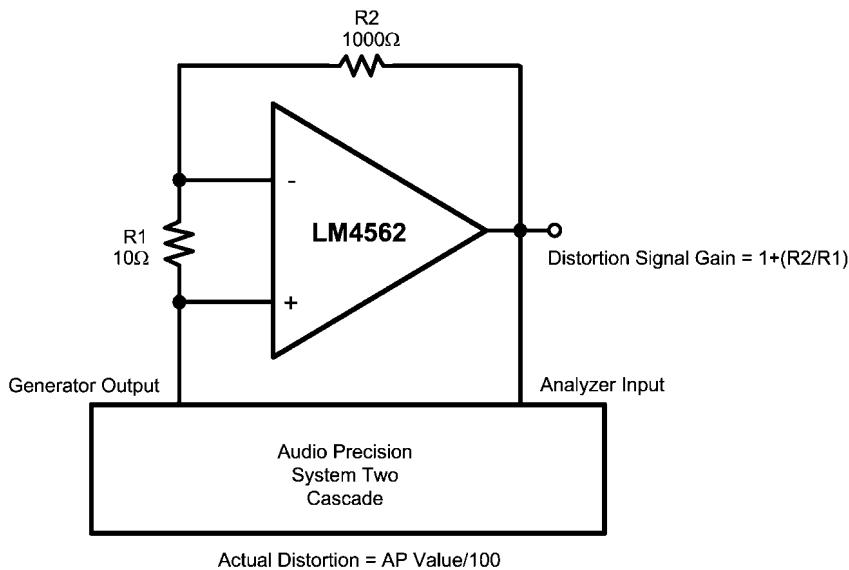
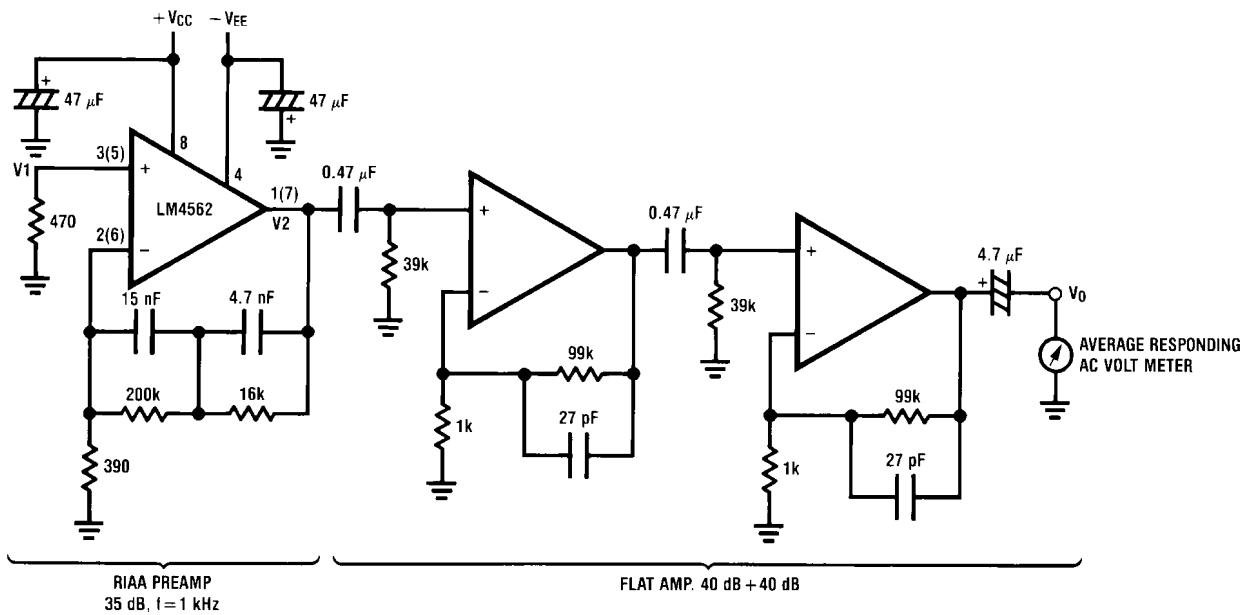


FIGURE 1. THD+N and IMD Distortion Test Circuit

The LM4562 is a high speed op amp with excellent phase margin and stability. Capacitive loads up to 100pF will cause little change in the phase characteristics of the amplifiers and are therefore allowable.

Capacitive loads greater than 100pF must be isolated from the output. The most straightforward way to do this is to put



Complete shielding is required to prevent induced pick up from external sources. Always check with oscilloscope for power line noise.

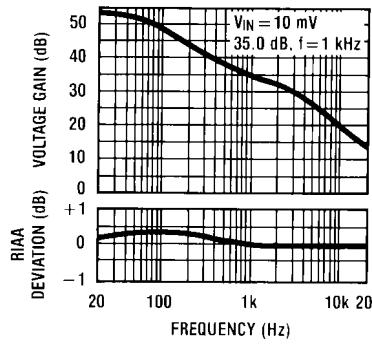
Noise Measurement Circuit

Total Gain: 115 dB @ $f = 1$ kHz

Input Referred Noise Voltage: $e_n = V_0/560,000$ (V)

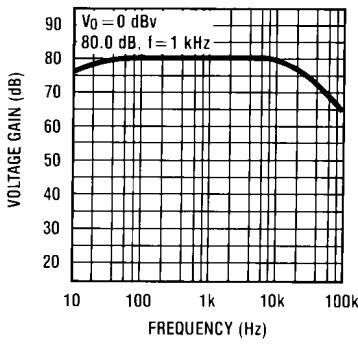
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RIAA Preamp Voltage Gain, RIAA Deviation vs Frequency



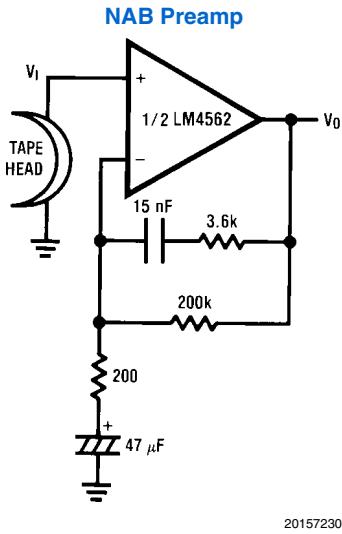
20157228

Flat Amp Voltage Gain vs Frequency



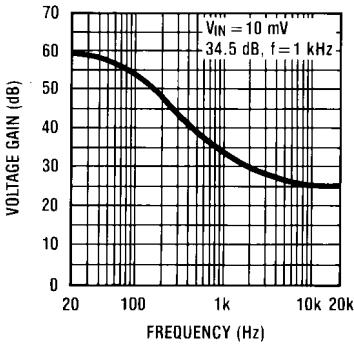
20157229

TYPICAL APPLICATIONS

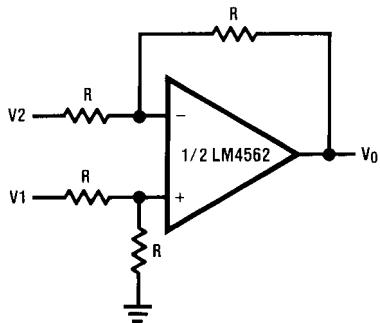


20157230

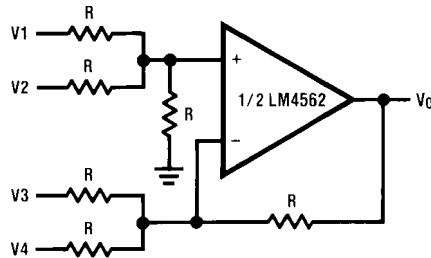
$A_V = 34.5$
 $F = 1 \text{ kHz}$
 $E_n = 0.38 \mu\text{V}$
A Weighted

NAB Preamp Voltage Gain vs Frequency

20157231

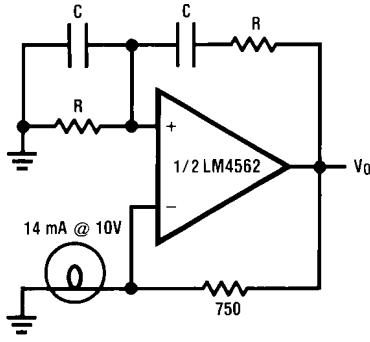
Balanced to Single Ended Converter

20157232

 $V_O = V1 - V2$ **Adder/Subtractor**

20157233

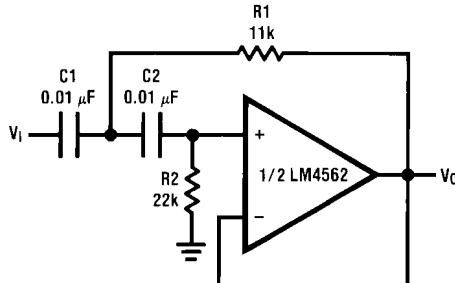
$$V_O = V1 + V2 - V3 - V4$$

Sine Wave Oscillator

20157234

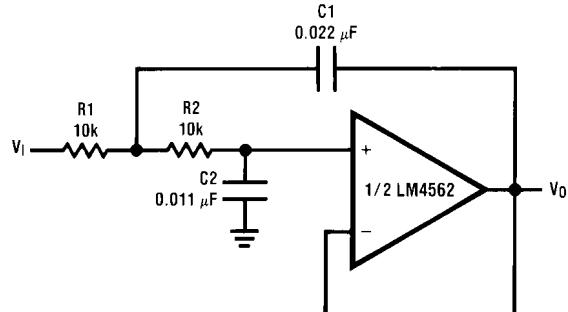
$$f_o = \frac{1}{2\pi RC}$$

Second Order High Pass Filter (Butterworth)



20157235

Second Order Low Pass Filter (Butterworth)



20157236

if $C_1 = C_2 = C$

$$R_1 = \frac{\sqrt{2}}{2\omega_o C}$$

$$R_2 = 2 \cdot R_1$$

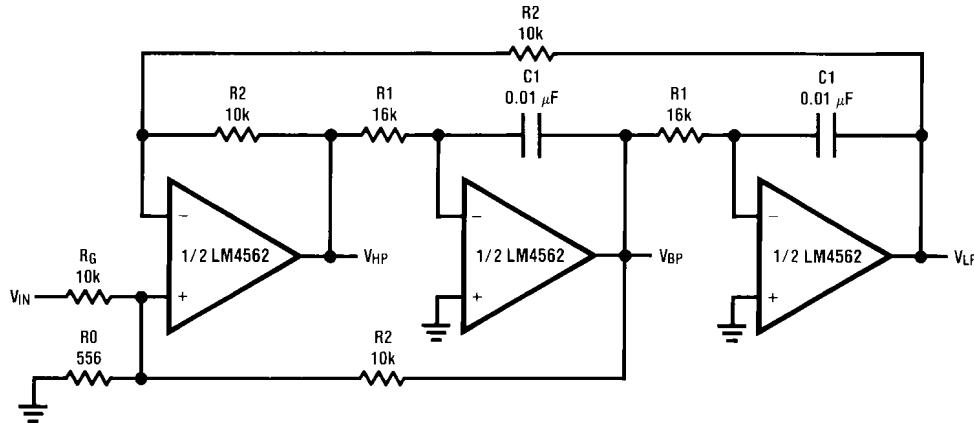
Illustration is $f_0 = 1$ kHzif $R_1 = R_2 = R$

$$C_1 = \frac{\sqrt{2}}{\omega_o R}$$

$$C_2 = \frac{C_1}{2}$$

Illustration is $f_0 = 1$ kHz

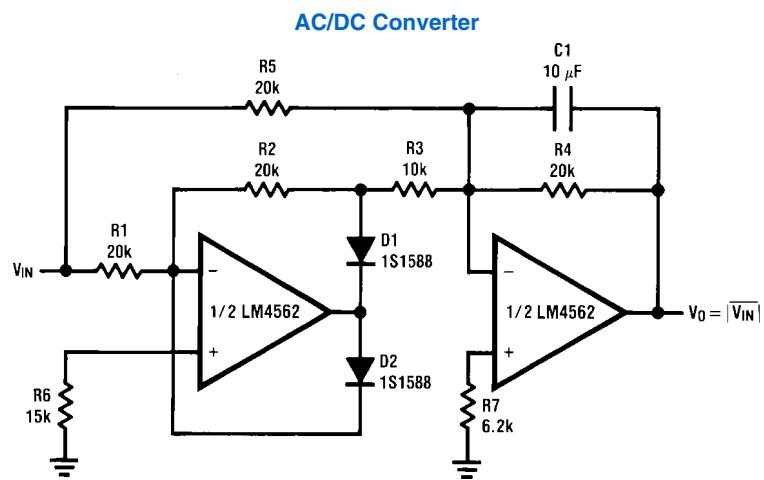
State Variable Filter



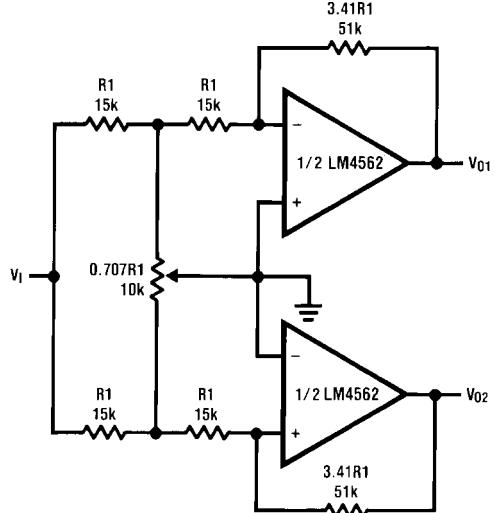
20157237

$$f_0 = \frac{1}{2\pi C_1 R_1}, Q = \frac{1}{2} \left(1 + \frac{R_2}{R_0} + \frac{R_2}{R_G} \right), A_{BP} = QA_{LP} = QA_{HP} = \frac{R_2}{R_G}$$

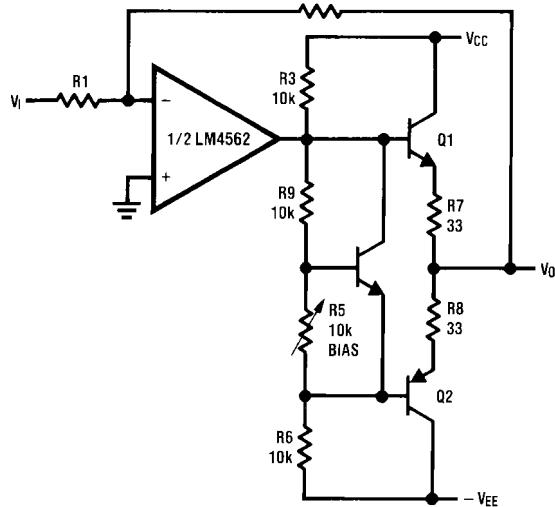
Illustration is $f_0 = 1$ kHz, $Q = 10$, $A_{BP} = 1$



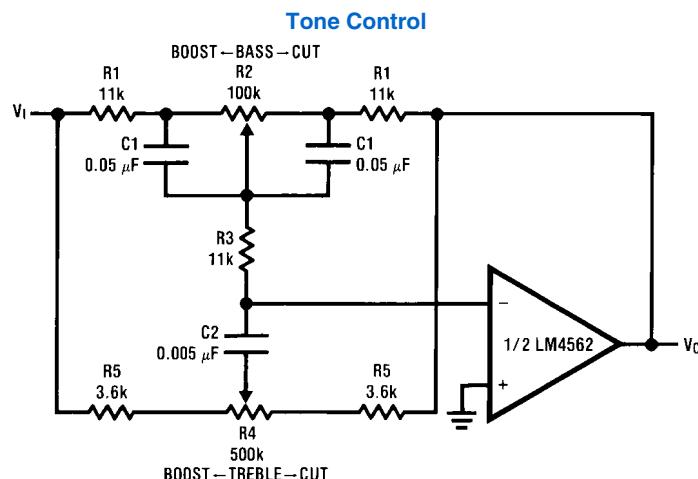
20157238

2 Channel Panning Circuit (Pan Pot)

20157239

Line Driver

20157240



20157241

$$f_L \approx \frac{1}{2\pi R_2 C_1}, f_{LB} \approx \frac{1}{2\pi R_1 C_1}$$

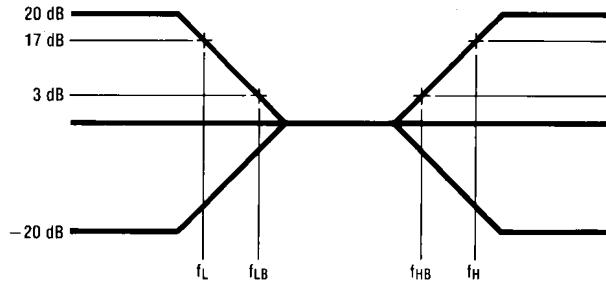
$$f_H \approx \frac{1}{2\pi R_5 C_2}, f_{HB} \approx \frac{1}{2\pi(R_1+R_5+2R_3)C_2}$$

Note: The equations started above are simplifications, providing guidance of general -3dB point values, when the potentiometers are at their null position.

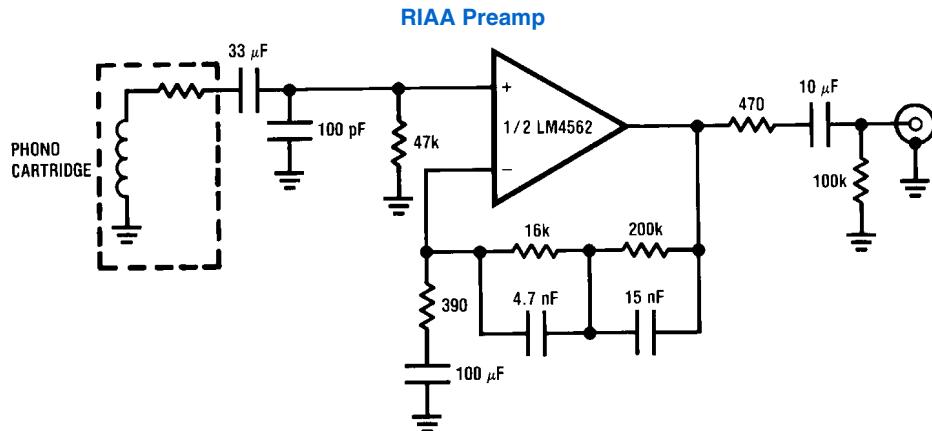
Illustration is:

$$f_L \approx 32 \text{ Hz}, f_{LB} \approx 320 \text{ Hz}$$

$$f_H \approx 11 \text{ kHz}, f_{HB} \approx 1.1 \text{ kHz}$$

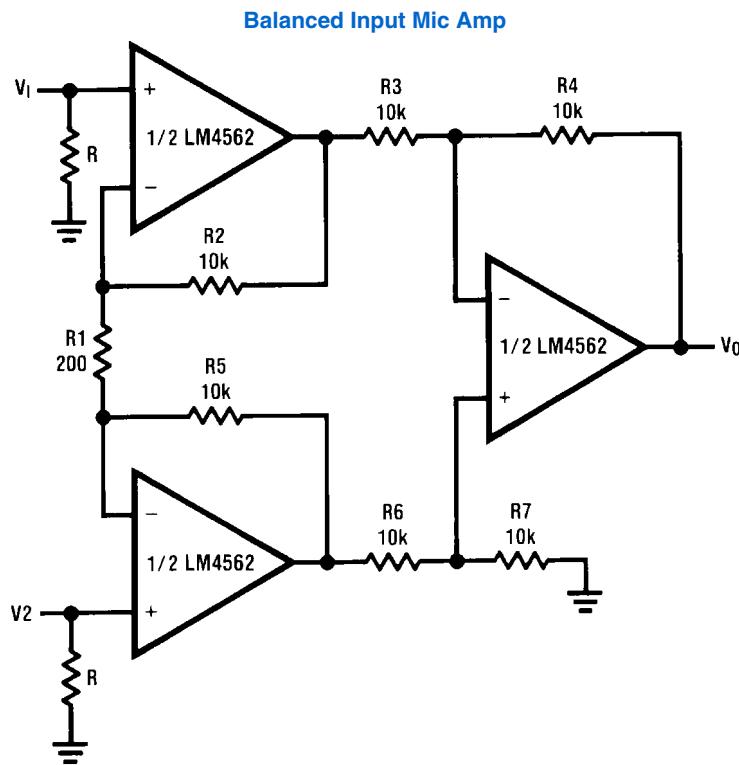


20157242



20157203

$A_v = 35 \text{ dB}$
 $E_n = 0.33 \mu\text{V}$
 $S/N = 90 \text{ dB}$
 $f = 1 \text{ kHz}$
 A Weighted
 A Weighted, $V_{IN} = 10 \text{ mV}$
 @ $f = 1 \text{ kHz}$



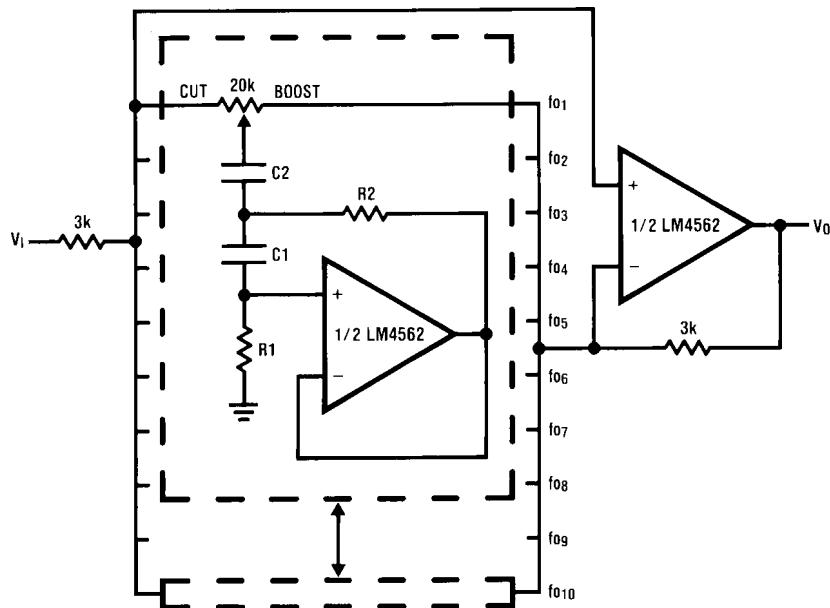
20157243

If $R_2 = R_5$, $R_3 = R_6$, $R_4 = R_7$

$$V_0 = \left(1 + \frac{2R_2}{R_1}\right) \frac{R_4}{R_3} (V_2 - V_1)$$

Illustration is:
 $V_0 = 101(V_2 - V_1)$

10 Band Graphic Equalizer



20157244

f_0 (Hz)	C_1	C_2	R_1	R_2
32	0.12μF	4.7μF	75kΩ	500Ω
64	0.056μF	3.3μF	68kΩ	510Ω
125	0.033μF	1.5μF	62kΩ	510Ω
250	0.015μF	0.82μF	68kΩ	470Ω
500	8200pF	0.39μF	62kΩ	470Ω
1k	3900pF	0.22μF	68kΩ	470Ω
2k	2000pF	0.1μF	68kΩ	470Ω
4k	1100pF	0.056μF	62kΩ	470Ω
8k	510pF	0.022μF	68kΩ	510Ω
16k	330pF	0.012μF	51kΩ	510Ω

Note 9: At volume of change = ± 12 dB $Q = 1.7$

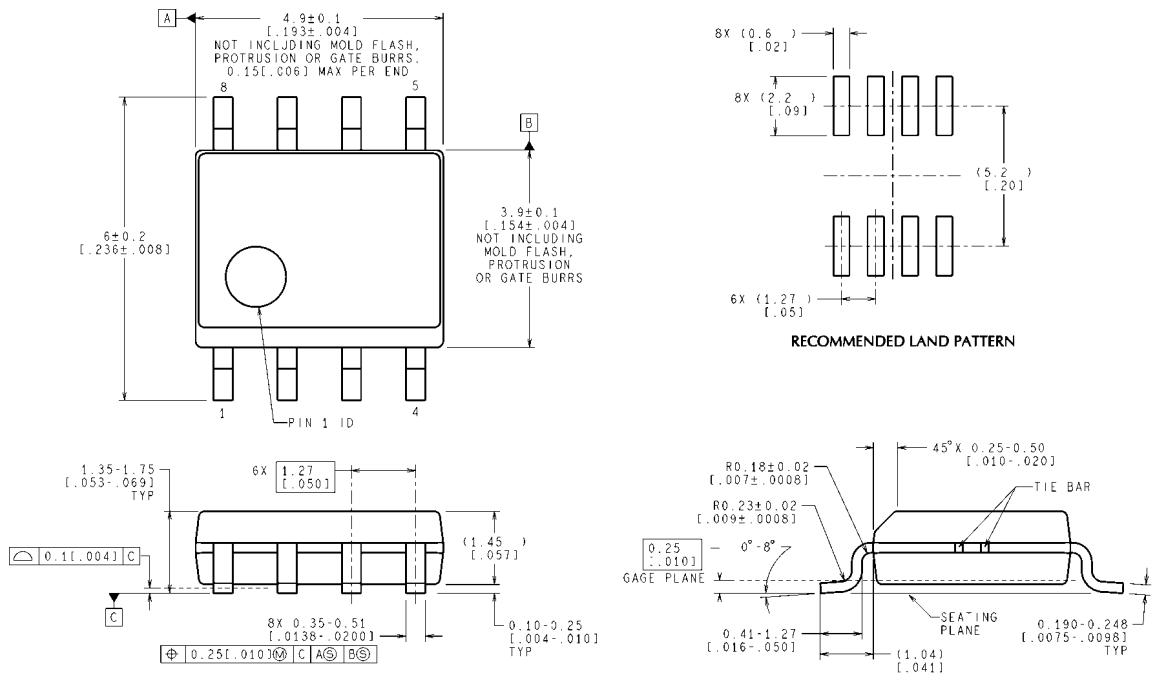
Reference: "AUDIO/RADIO HANDBOOK", National Semiconductor, 1980, Page 2-61

Revision History

Rev	Date	Description
1.0	08/16/06	Initial release.
1.1	08/22/06	Updated the Instantaneous Short Circuit Current specification.
1.2	09/12/06	Updated the three $\pm 15V$ CMRR Typical Performance Curves.
1.3	09/26/06	Updated interstage filter capacitor values on page 1 Typical Application schematic.
1.4	05/03/07	Added the "general note" under the EC table.
1.5	10/17/07	Replaced all the PSRR curves.
1.6	01/26/10	Edited the equations on page 28 (under Tone Control).

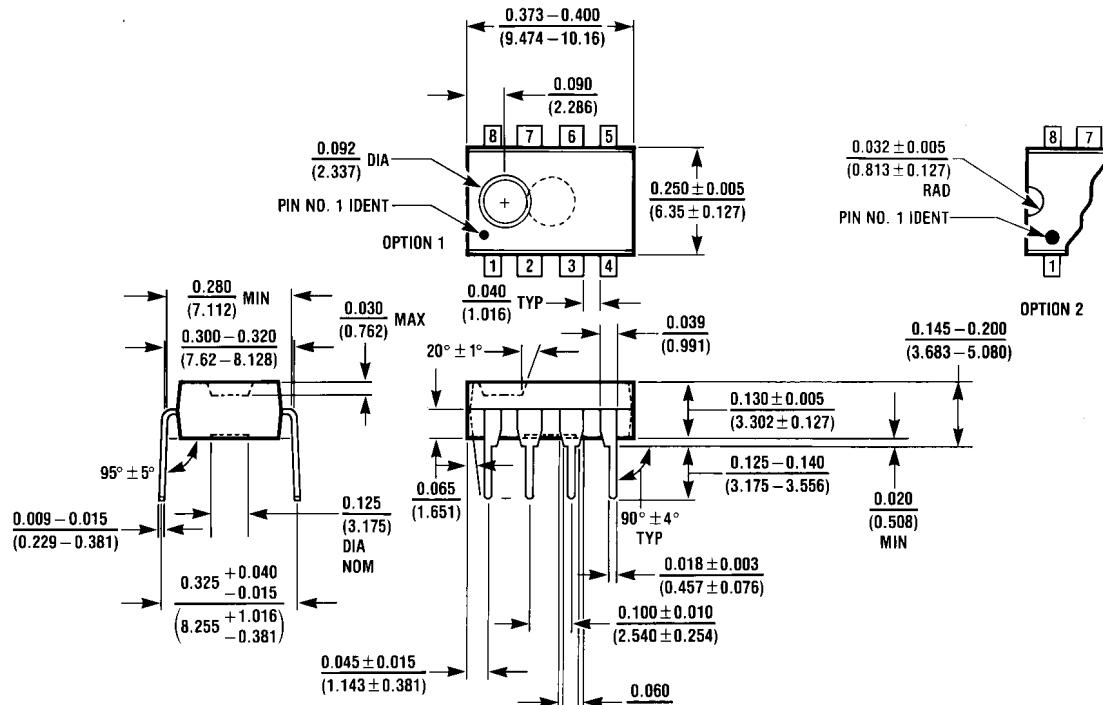
Physical Dimensions

inches (millimeters) unless otherwise noted

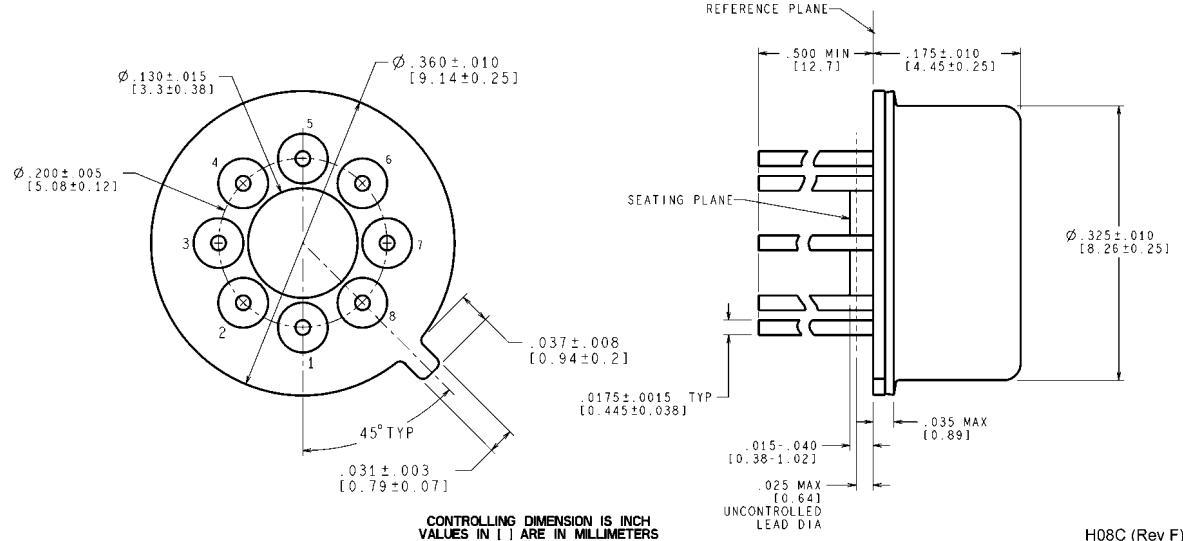


M08A (Rev M)

Narrow SOIC Package
Order Number LM4562MA
NS Package Number M08A



N08E (REV F)



H08C (Rev F)

TO-99 Metal Can Package
Order Number LM4562HA
NS Package Number H08C

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