

# 10A, 28V<sub>IN</sub> High Efficiency DC/DC µModule

### **FEATURES**

- Complete Switch Mode Power Supply
- Wide Input Voltage Range: 4.5V to 28V
- 10A DC, 12A Peak Output Current
- Parallel Two µModule™ DC/DC Converters for 20A Output Current
- 0.6V to 5V Output Voltage
- 1.5% Output Voltage Regulation
- Ultrafast Transient Response
- Current Mode Control
- -55°C to 125°C Operating Temperature Range (LTM4600HVMPV)
- Pb-Free (e4) RoHS Compliant Package Gold-Pad Finish
- Up to 92% Efficiency
- Programmable Soft-Start
- Output Overvoltage Protection
- Optional Short-Circuit Shutdown Timer
- Small Footprint, Low Profile (15mm × 15mm × 2.8mm) LGA Package

### **APPLICATIONS**

- Telecom and Networking Equipment
- Military and Avionics Systems
- Industrial Equipment
- Point of Load Regulation
- Servers

### DESCRIPTION

The LTM®4600HV is a complete 10A, DC/DC step down power supply with up to 28V input operation. Included in the package are the switching controller, power FETs, inductor, and all support components. Operating over an input voltage range of 4.5V to 28V, the LTM4600HV supports an output voltage range of 0.6V to 5V, set by a single resistor. This high efficiency design delivers 10A continuous current (12A peak), needing no heat sinks or airflow to meet power specifications. Only bulk input and output capacitors are needed to finish the design.

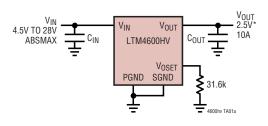
The low profile package (2.8mm) enables utilization of unused space on the bottom of PC boards for high density point of load regulation. High switching frequency and an adaptive on-time current mode architecture enables a very fast transient response to line and load changes without sacrificing stability. Fault protection features include integrated overvoltage and short circuit protection with a defeatable shutdown timer. A built-in soft-start timer is adjustable with a small capacitor.

The LTM4600HV is packaged in a thermally enhanced, compact ( $15 \text{mm} \times 15 \text{mm}$ ) and low profile (2.8 mm) overmolded Land Grid Array (LGA) package suitable for automated assembly by standard surface mount equipment. The LTM4600HV is Pb-free and RoHS compliant.

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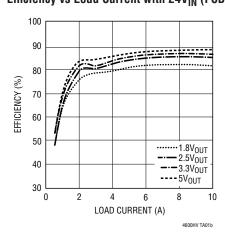
### TYPICAL APPLICATION

#### 10A µModule Power Supply with 4.5V to 28V Input



\*REVIEW DE-RATING CURVE AT THE HIGHER INPUT VOLTAGE

### Efficiency vs Load Current with 24V<sub>IN</sub> (FCB = 0)



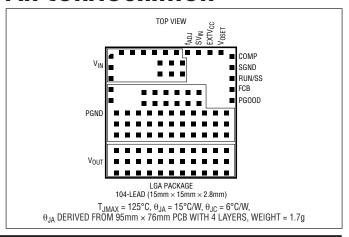


### **ABSOLUTE MAXIMUM RATINGS**

#### (Note 1)

\ /	
FCB, EXTV <sub>CC</sub> , PGOOD, RUN/SS, V <sub>OUT</sub>	0.3V to 6V
V <sub>IN</sub> , SV <sub>IN</sub> , f <sub>ADJ</sub>	0.3V to 28V
V <sub>OSET</sub> , COMP	0.3V to 2.7V
Operating Temperature Range (Note 2)	
E and I Grades	40°C to 85°C
MP Grade	55°C to 125°C
Junction Temperature	125°C
Storage Temperature Range	

### PIN CONFIGURATION



### ORDER INFORMATION

LEAD FREE FINISH TAPE AND REEL		PART MARKING	PACKAGE DESCRIPTION	TEMPERATURE RANGE
LTM4600HVEV#PBF	LTM4600HVEV#TRPBF	LTM4600HVEV	104-Lead (15mm × 15mm × 2.8mm)	-40°C to 85°C
LTM4600HVIV#PBF	LTM4600HVIV#TRPBF	LTM4600HVIV	104-Lead (15mm × 15mm × 2.8mm)	-40°C to 85°C
LTM4600HVMPV#PBF	LTM4600HVMPV#TRPBF	LTM4600HVMPV	104-Lead (15mm × 15mm × 2.8mm)	–55°C to 125°C

Consult LTC Marketing for parts specified with wider operating temperature ranges.

Consult LTC Marketing for information on non-standard lead based finish parts.

For more information on lead free part marking, go to: http://www.linear.com/leadfree/

For more information on tape and reel specifications, go to: http://www.linear.com/tapeandreel/

**ELECTRICAL CHARACTERISTICS** The  $\bullet$  denotes the specifications which apply over the full operating temperature range, otherwise specifications are at  $T_A = 25^{\circ}C$ ,  $V_{IN} = 12V$ . External  $C_{IN} = 120\mu F$ ,  $C_{OUT} = 200\mu F$ /Ceramic per typical application (front page) configuration.

TYP	MAX	UNITS
	28	V
1.50 1.50	1.522 1.530	V
3.4	4	V
0.6 0.7 0.8		A A A
1.2 42 1.8 36 35	75	mA mA mA mA
100		ns
400		ns
1.52 3.13 3.64 1.6		A A A A
	36 35 100 400 1.52 3.13 3.64	36 35 75 100 400 1.52 3.13 3.64



**ELECTRICAL CHARACTERISTICS** The • denotes the specifications which apply over the full operating temperature range, otherwise specifications are at  $T_A = 25$ °C,  $V_{IN} = 12V$ . External  $C_{IN} = 120\mu F$ ,  $C_{OUT} = 200\mu F$ /Ceramic per typical application (front page) configuration.

A
<b>I</b>
%
5 %
mV <sub>P-P</sub>
kHz
ms ms
mV
μs
A A A
9 V 6 V
V
μА
μА
mV
mA
kΩ
3 V
μА
5 %
5 %
%
V
.5

**Note 1:** Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.

**Note 2:** The LTM4600HVE is guaranteed to meet performance specifications from 0°C to 85°C. Specifications over the -40°C to 85°C

operating temperature range are assured by design, characterization and correlation with statistical process controls. The LTM46000HVMP is guaranteed and tested over the -55°C to 125°C temperature range. For output current derating at high temperature, please refer to Thermal Considerations and Output Current Derating discussion.

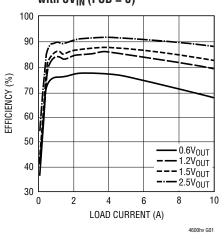
 $\textbf{Note 3:} \ \ \text{Refer to current de-rating curves and thermal application note}.$ 

Note 4: Test assumes current derating versus temperature.

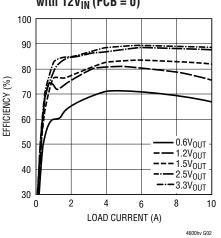


### TYPICAL PERFORMANCE CHARACTERISTICS (See Figure 21 for all curves)

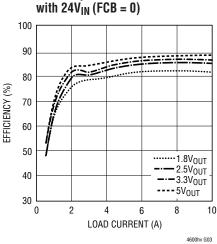




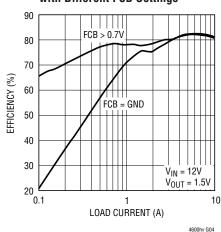
# Efficiency vs Load Current with 12V<sub>IN</sub> (FCB = 0)



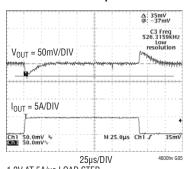
### Efficiency vs Load Current with 24V<sub>111</sub> (FCR = 0)



# Efficiency vs Load Current with Different FCB Settings

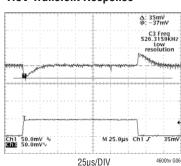


#### 1.2V Transient Response



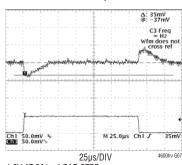
1.2V AT 5A/µs LOAD STEP C<sub>OUT</sub> = 3 • 22µF 6.3V CERAMICS 470µF 4V SANYO POSCAP C3 = 100pF

#### 1.5V Transient Response



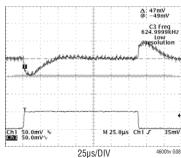
1.5V AT  $5A/\mu$ s LOAD STEP  $C_{OUT} = 3 \cdot 22\mu$ F 6.3V CERAMICS  $470\mu$ F 4V SANYO POSCAP C3 = 100pF

#### 1.8V Transient Response



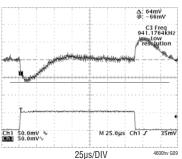
1.8V AT 5A/µs LOAD STEP C<sub>OUT</sub> = 3 • 22µF 6.3V CERAMICS 470µF 4V SANYO POSCAP C3 = 100pF

#### 2.5V Transient Response



2.5V AT 5A/µs LOAD STEP C<sub>OUT</sub> = 3 • 22µF 6.3V CERAMICS 470µF 4V SANYO POSCAP C3 = 100pF

#### 3.3V Transient Response



3.3V AT 5A/µs LOAD STEP

C<sub>OUT</sub> = 3 • 22µF 6.3V CERAMICS

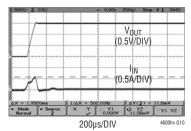
470µF 4V SANYO POSCAP

C3 = 100pF



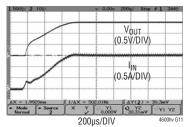
### TYPICAL PERFORMANCE CHARACTERISTICS (See Figure 21 for all curves)

Start-Up,  $I_{OUT} = 0A$ 



 $\begin{array}{l} V_{IN} = 12V \\ V_{OUT} = 1.5V \\ C_{OUT} = 200 \mu F \\ \text{NO EXTERNAL SOFT-START CAPACITOR} \end{array}$ 

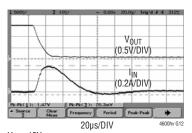
#### Start-Up, $I_{OUT} = 10A$ (Resistive Load)



 $V_{IN} = 12V$ 

V<sub>OUT</sub> = 1.5V C<sub>OUT</sub> = 200µF NO EXTERNAL SOFT-START CAPACITOR

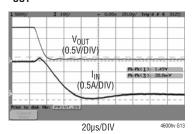
#### **Short-Circuit Protection**, $I_{OUT} = 0A$



 $V_{IN} = 12V$  $V_{OUT} = 1.5V$ 

C<sub>OUT</sub> = 2× 200µF/X5R NO EXTERNAL SOFT-START CAPACITOR

#### **Short-Circuit Protection,** $I_{OUT} = 10A$

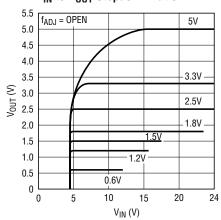


 $V_{IN} = 12V$  $V_{OUT} = 1.5V$ 

 $C_{OUT} = 2 \times 200 \mu F/X5R$ 

NO EXTERNAL SOFT-START CAPACITOR

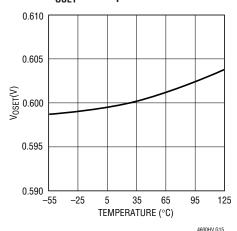
### V<sub>IN</sub> to V<sub>OUT</sub> Stepdown Ratio



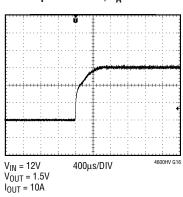
SEE FREQUENCY ADJUSTMENT DISCUSSION FOR 12V<sub>IN</sub> TO 5V<sub>OUT</sub> AND 5V<sub>IN</sub> TO 3.3V<sub>OUT</sub> CONVERSION

4600HV G14

### **V<sub>OSET</sub> vs Temperature**



#### Start-Up Waveform, $T_A = -55^{\circ}C$



### PIN FUNCTIONS (See Package Description for Pin Assignment)

 $V_{IN}$  (Bank 1): Power Input Pins. Apply input voltage between these pins and GND pins. Recommend placing input decoupling capacitance directly between  $V_{IN}$  pins and GND pins.

 $f_{ADJ}$  (Pin A15): A 110k resistor from  $V_{IN}$  to this pin sets the one-shot timer current, thereby setting the switching frequency. The LTM4600HV switching frequency is typically 850kHz. An external resistor to ground can be selected to reduce the one-shot timer current, thus lower the switching frequency to accommodate a higher duty cycle step down requirement. See the applications section.

**SV**<sub>IN</sub> (**Pin A17**): Supply Pinfor Internal PWM Controller. Leave this pin open or add additional decoupling capacitance.

**EXTV**<sub>CC</sub> (**Pin A19**): External 5V supply pin for controller. If left open or grounded, the internal 5V linear regulator will power the controller and MOSFET drivers. For high input voltage applications, connecting this pin to an external 5V will reduce the power loss in the power module. The EXTV<sub>CC</sub> voltage should never be higher than  $V_{IN}$ .

 $V_{OSET}$  (Pin A21): The Negative Input of The Error Amplifier. Internally, this pin is connected to  $V_{OUT}$  with a 100k precision resistor. Different output voltages can be programmed with additional resistors between the  $V_{OSET}$  and SGND pins.

**COMP (Pin B23):** Current Control Threshold and Error Amplifier Compensation Point. The current comparator threshold increases with this control voltage. The voltage ranges from 0V to 2.4V with 0.8V corresponding to zero sense voltage (zero current).

**SGND (Pin D23):** Signal Ground Pin. All small-signal components should connect to this ground, which in turn connects to PGND at one point.

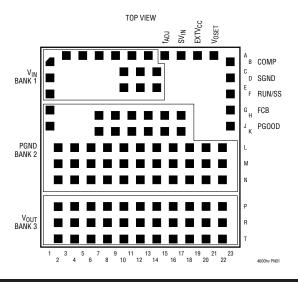
**RUN/SS (Pin F23):** Run and Soft-Start Control. Forcing this pin below 0.8V will shut down the power supply. Inside the power module, there is a 1000pF capacitor which provides approximately 0.7ms soft-start time with 200µF output capacitance. Additional soft-start time can be achieved by adding additional capacitance between the RUN/SS and SGND pins. The internal short-circuit latchoff can be disabled by adding a resistor between this pin and the  $V_{IN}$  pin. This resistor must supply a minimum 5µA pull up current.

**FCB (Pin G23):** Forced Continuous Input. Grounding this pin enables forced continuous mode operation regardless of load conditions. Tying this pin above 0.63V enables discontinuous conduction mode to achieve high efficiency operation at light loads. There is an internal 4.75K resistor between the FCB and SGND pins.

**PGOOD (Pin J23):** Output Voltage Power Good Indicator. When the output voltage is within 10% of the nominal voltage, the PGOOD is open drain output. Otherwise, this pin is pulled to ground.

**PGND (Bank 2):** Power ground pins for both input and output returns.

**V<sub>OUT</sub>** (**Bank 3**): Power Output Pins. Apply output load between these pins and GND pins. Recommend placing High Frequency output decoupling capacitance directly between these pins and GND pins.





### SIMPLIFIED BLOCK DIAGRAM

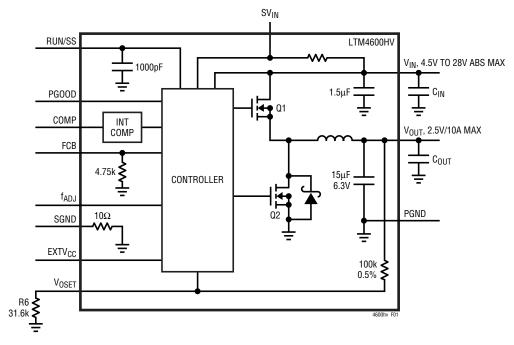


Figure 1. Simplified LTM4600HV Block Diagram

# **DECOUPLING REQUIREMENTS** $T_A = 25$ °C, $V_{IN} = 12$ V. Use Figure 1 configuration.

SYMBOL	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
C <sub>IN</sub>	External Input Capacitor Requirement (V <sub>IN</sub> = 4.5V to 28V, V <sub>OUT</sub> = 2.5V)	I <sub>OUT</sub> = 10A, 2x 10µF 35V Ceramic Taiyo Yuden GDK316BJ106ML	20			μF
C <sub>OUT</sub>	External Output Capacitor Requirement (V <sub>IN</sub> = 4.5V to 28V, V <sub>OUT</sub> = 2.5V)	I <sub>OUT</sub> = 10A, Refer to Table 2 in the Applications Information Section	100	200		μF

### **OPERATION**

#### µModule Description

The LTM4600HV is a standalone non-isolated synchronous switching DC/DC power supply. It can deliver up to 10A of DC output current with only bulk external input and output capacitors. This module provides a precisely regulated output voltage programmable via one external resistor from  $0.6V_{DC}$  to  $5.0V_{DC}.$  The input voltage range is 4.5V to 28V. A simplified block diagram is shown in Figure 1 and the typical application schematic is shown in Figure 21.

The LTM4600HV contains an integrated LTC constant on-time current-mode regulator, ultra-low  $R_{DS(ON)}$  FETs with fast switching speed and integrated Schottky diode. The typical switching frequency is 850kHz at full load. With current mode control and internal feedback loop compensation, the LTM4600HV module has sufficient stability margins and good transient performance under a wide range of operating conditions and with a wide range of output capacitors, even all ceramic output capacitors (X5R or X7R for extended temperature range).

Current mode control provides cycle-by-cycle fast current limit. In addition, foldback current limiting is provided in an over-current condition while  $V_{OSET}$  drops. Also, the LTM4600HV has defeatable short circuit latch off. Internal overvoltage and undervoltage comparators pull the open-drain PGOOD output low if the output feedback voltage exits a  $\pm 10\%$  window around the regulation point. Furthermore, in an overvoltage condition, internal top FET

Q1 is turned off and bottom FET Q2 is turned on and held on until the overvoltage condition clears.

Pulling the RUN/SS pin low forces the controller into its shutdown state, turning off both Q1 and Q2. Releasing the pin allows an internal 1.2 $\mu$ A current source to charge up the softstart capacitor. When this voltage reaches 1.5V, the controller turns on and begins switching.

At low load current the module works in continuous current mode by default to achieve minimum output voltage ripple. It can be programmed to operate in discontinuous current mode for improved light load efficiency when the FCB pin is pulled up above 0.8V and no higher than 6V. The FCB pin has a 4.75k resistor to ground, so a resistor to  $V_{\text{IN}}$  can set the voltage on the FCB pin.

When EXTV<sub>CC</sub> pin is grounded or open, an integrated 5V linear regulator powers the controller and MOSFET gate drivers. If a minimum 4.7V external bias supply is applied on the EXTV<sub>CC</sub> pin, the internal regulator is turned off, and an internal switch connects EXTV<sub>CC</sub> to the gate driver voltage. This eliminates the linear regulator power loss with high input voltage, reducing the thermal stress on the controller. The maximum voltage on EXTV<sub>CC</sub> pin is 6V. The EXTV<sub>CC</sub> voltage should never be higher than the V<sub>IN</sub> voltage. Also EXTV<sub>CC</sub> must be sequenced after V<sub>IN</sub>. Recommended for 24V operation to lower temperature in the  $\mu$ Module.

The typical LTM4600HV application circuit is shown in Figure 21. External component selection is primarily determined by the maximum load current and output voltage.

### **Output Voltage Programming and Margining**

The PWM controller of the LTM4600HV has an internal 0.6V $\pm$ 1% reference voltage. As shown in the block diagram, a 100k/0.5% internal feedback resistor connects V<sub>OUT</sub> and V<sub>OSET</sub> pins. Adding a resistor R<sub>SET</sub> from V<sub>OSET</sub> pin to SGND pin programs the output voltage:

$$V_0 = 0.6V \bullet \frac{100k + R_{SET}}{R_{SET}}$$

Table 1 shows the standard values of 1% R<sub>SET</sub> resistor for typical output voltages:

Table 1.

$R_{SET}$ (k $\Omega$ )	Open	100	66.5	49.9	43.2	31.6	22.1	13.7
V <sub>0</sub> (V)	0.6	1.2	1.5	1.8	2	2.5	3.3	5

Voltage margining is the dynamic adjustment of the output voltage to its worst case operating range in production testing to stress the load circuitry, verify control/protection functionality of the board and improve the system reliability. Figure 2 shows how to implement margining function with the LTM4600HV. In addition to the feedback resistor  $R_{SET}$ , several external components are added. Turn off both transistor  $Q_{UP}$  and  $Q_{DOWN}$  to disable the margining. When  $Q_{UP}$  is on and  $Q_{DOWN}$  is off, the output

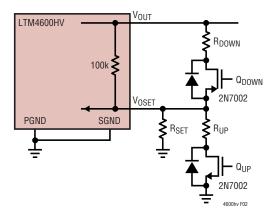


Figure 2. LTM4600HV Margining Implementation

voltage is margined up. The output voltage is margined down when  $Q_{DOWN}$  is on and  $Q_{UP}$  is off. If the output voltage  $V_0$  needs to be margined up/down by  $\pm M\%$ , the resistor values of  $R_{UP}$  and  $R_{DOWN}$  can be calculated from the following equations:

$$\frac{(R_{SET} \| R_{UP}) \bullet V_0 \bullet (1 + M\%)}{(R_{SET} \| R_{UP}) + 100 k\Omega} = 0.6V$$

$$\frac{R_{SET} \bullet V_0 \bullet (1-M\%)}{R_{SET} + (100k\Omega \|R_{DOWN})} = 0.6V$$

### **Input Capacitors**

The LTM4600HV  $\mu$ Module should be connected to a low ac-impedance DC source. High frequency, low ESR input capacitors are required to be placed adjacent to the module. In Figure 21, the bulk input capacitor  $C_{IN}$  is selected for its ability to handle the large RMS current into the converter. For a buck converter, the switching duty-cycle can be estimated as:

$$D = \frac{V_0}{V_{IN}}$$

Without considering the inductor current ripple, the RMS current of the input capacitor can be estimated as:

$$I_{CIN(RMS)} = \frac{I_{O(MAX)}}{n\%} \bullet \sqrt{D \bullet (1-D)}$$

In the above equation,  $\eta\%$  is the estimated efficiency of the power module. C1 can be a switcher-rated electrolytic aluminum capacitor, OS-CON capacitor or high volume ceramic capacitors. Note the capacitor ripple current ratings are often based on only 2000 hours of life. This makes it advisable to properly derate the input capacitor, or choose a capacitor rated at a higher temperature than required. Always contact the capacitor manufacturer for derating requirements over temperature.

In Figure 21, the input capacitors are used as high frequency input decoupling capacitors. In a typical 10A output application, 1-2 pieces of very low ESR X5R or X7R (for extended temperature range), 10µF ceramic capacitors are recommended. This decoupling capacitor



should be placed directly adjacent the module input pins in the PCB layout to minimize the trace inductance and high frequency AC noise.

### **Output Capacitors**

The LTM4600HV is designed for low output voltage ripple. The bulk output capacitors  $C_{OUT}$  is chosen with low enough effective series resistance (ESR) to meet the output voltage ripple and transient requirements.  $C_{OUT}$  can be low ESR tantalum capacitor, low ESR polymer capacitor or ceramic capacitor (X5R or X7R). The typical capacitance is 200µF if all ceramic output capacitors are used. The internally optimized loop compensation provides sufficient stability margin for all ceramic capacitors applications. Additional output filtering may be required by the system designer, if further reduction of output ripple or dynamic transient spike is required. Refer to Table 2 for an output capacitance matrix for each output voltage Droop, peak to peak deviation and recovery time during a  $5A/\mu s$  transient with a specific output capacitance.

# Fault Conditions: Current Limit and Over current Foldback

The LTM4600HV has a current mode controller, which inherently limits the cycle-by-cycle inductor current not only in steady state operation, but also in transient.

To further limit current in the event of an over load condition, the LTM4600HV provides foldback current limiting. If the output voltage falls by more than 50%, then the maximum output current is progressively lowered to about one sixth of its full current limit value.

#### Soft-Start and Latchoff with the RUN/SS pin

The RUN/SS pin provides a means to shut down the LTM4600HV as well as a timer for soft-start and overcurrent latchoff. Pulling the RUN/SS pin below 0.8V puts the LTM4600HV into a low quiescent current shutdown (IQ  $\leq$  75µA). Releasing the pin allows an internal 1.2µA current source to charge up the timing capacitor  $C_{SS}$ . Inside LTM4600HV, there is an internal 1000pF capacitor from RUN/SS pin to ground. If RUN/SS pin has an external capacitor  $C_{SS\_EXT}$  to ground, the delay before starting is about:

$$t_{DELAY} = \frac{1.5V}{1.2\mu A} \bullet (C_{SS\_EXT} + 1000pF)$$

When the voltage on RUN/SS pin reaches 1.5V, the LTM4600HV internal switches are operating with a clamping of the maximum output inductor current limited by the RUN/SS pin total soft-start capacitance. As the RUN/SS pin voltage rises to 3V, the soft-start clamping of the inductor current is released.

### VIN to Vout Stepdown Ratios

There are restrictions in the maximum  $V_{IN}$  to  $V_{OUT}$  step down ratio that can be achieved for a given input voltage. These contraints are shown in the Typical Performance Characteristics curves labeled " $V_{IN}$  to  $V_{OUT}$  Stepdown Ratio". Note that additional thermal de-rating may apply. See the Thermal Considerations and Output Current De-Rating sections of this data sheet.

LINEAR

Table 2. Output Voltage Response Versus Component Matrix \*(Refer to Figure 21)

#### TYPICAL MEASURED VALUES

C <sub>OUT1</sub> VENDORS	PART NUMBER	C <sub>OUT2</sub> VENDORS	PART NUMBER
TDK	C4532X5R0J107MZ (100µF,6.3V)	SANYO POSCAP	6TPE330MIL (330μF, 6.3V)
TAIYO YUDEN	JMK432BJ107MU-T ( 100μF, 6.3V)	SANYO POSCAP	2R5TPE470M9 (470μF, 2.5V)
TAIYO YUDEN	JMK316BJ226ML-T501 ( 22μF, 6.3V)	SANYO POSCAP	4TPE470MCL (470μF, 4V)
TAIYO YUDEN	JMK316BJ226ML-T501 ( 22μF, 6.3V)	SANYO POSCAP	6TPD470M (470μF, 6.3V)

V <sub>OUT</sub> (V)	C <sub>IN</sub> (CERAMIC)	C <sub>IN</sub> (BULK)	C <sub>OUT1</sub> (CERAMIC)	C <sub>OUT2</sub> (BULK)	C <sub>COMP</sub>	C3	V <sub>IN</sub> (V)	DROOP (mV)	PEAK TO PEAK (mV)	RECOVERY TIME (µs)	LOAD STEP (A/µs)
1.2	2 × 10μF 35V	150µF 35V	3 × 22μF 6.3V	470µF 4V	NONE	100pF	5	35	68	25	5
1.2	2 × 10µF 35V	150µF 35V	1 × 100µF 6.3V	470μF 2.5V	NONE	100pF	5	35	70	20	5
1.2	2 × 10µF 35V	150µF 35V	2 × 100µF 6.3V	330µF 6.3V	NONE	100pF	5	40	80	20	5
1.2	2 × 10µF 35V	150µF 35V	4 × 100μF 6.3V	NONE	NONE	100pF	5	49	98	20	5
1.2	2 × 10µF 35V	150µF 35V	3 × 22μF 6.3V	470µF 4V	NONE	100pF	12	35	68	25	5
1.2	2 × 10µF 35V	150µF 35V	1 × 100µF 6.3V	470μF 2.5V	NONE	100pF	12	35	70	20	5
1.2	2 × 10μF 35V	150µF 35V	2 × 100µF 6.3V	330µF 6.3V	NONE	100pF	12	40	80	20	5
1.2	2 × 10μF 35V	150µF 35V	4 × 100μF 6.3V	NONE	NONE	100pF	12	49	98	20	5
1.5	2 × 10μF 35V	150μF 35V	3 × 22μF 6.3V	470μF 4V	NONE	100pF	5	36	75	25	5
1.5	2 × 10μF 35V	150µF 35V	1 × 100µF 6.3V	470μF 2.5V	NONE	100pF	5	37	79	20	5
1.5	2 × 10μF 35V	150μF 35V	2 × 100µF 6.3V	330µF 6.3V	NONE	100pF	5	44	84	20	5
1.5	2 × 10μF 35V	150µF 35V	4 × 100μF 6.3V	NONE	NONE	100pF	5	61	118	20	5
1.5	2 × 10μF 35V	150μF 35V	3 × 22μF 6.3V	470μF 4V	NONE	100pF	12	36	75	25	5
1.5	2 × 10μF 35V	150µF 35V	1 × 100μF 6.3V	470μF 2.5V	NONE	100pF	12	37	79	20	5
1.5	2 × 10μF 35V	150μF 35V	2 × 100µF 6.3V	330µF 6.3V	NONE	100pF	12	44	89	20	5
1.5	2 × 10μF 35V	150μF 35V	4 × 100μF 6.3V	NONE	NONE	100pF	12	54	108	20	5
1.8	2 × 10μF 35V	150μF 35V	3 × 22μF 6.3V	470μF 4V	NONE	100pF	5	40	81	30	5
1.8	2 × 10μF 35V	150µF 35V	1 × 100µF 6.3V	470μF 2.5V	NONE	100pF	5	44	88	20	5
1.8	2 × 10μF 35V	150μF 35V	2 × 100μF 6.3V	330µF 6.3V	NONE	100pF	5	46	91	20	5
1.8	2 × 10μF 35V	150µF 35V	4 × 100μF 6.3V	NONE	NONE	100pF	5	62	128	20	5
1.8	2 × 10μF 35V	150μF 35V	3 × 22μF 6.3V	470μF 4V	NONE	100pF	12	40	81	30	5
1.8	2 × 10μF 35V	150µF 35V	1 × 100μF 6.3V	470μF 2.5V	NONE	100pF	12	44	85	20	5
1.8	2 × 10µF 35V	150μF 35V	2 × 100µF 6.3V	330µF 6.3V	NONE	100pF	12	44	91	20	5
1.8	2 × 10µF 35V	150μF 35V	4 × 100μF 6.3V	NONE	NONE	100pF	12	62	125	20	5
2.5	2 × 10μF 35V	150μF 35V	1 × 100μF 6.3V	470μF 4V	NONE	100pF	5	48	103	30	5
2.5	2 × 10µF 35V	150µF 35V	2 × 100µF 6.3V	330µF 6.3V	NONE	100pF	5	56	113	30	5
2.5	2 × 10μF 35V	150μF 35V	3 × 22μF 6.3V	470μF 4V	NONE	100pF	5	57	116	30	5
2.5	2 × 10μF 35V	150μF 35V	4 × 100μF 6.3V	NONE	NONE	100pF	5	60	115	25	5
2.5	2 × 10μF 35V	150μF 35V	1 × 100μF 6.3V	470μF 4V	NONE	100pF	12	48	103	30	5
2.5	2 × 10μF 35V	150μF 35V	3 × 22μF 6.3V	470μF 4V	NONE	100pF	12	51	102	30	5
2.5	2 × 10μF 35V	150µF 35V	2 × 100µF 6.3V	330µF 6.3V	NONE	100pF	12	56	113	30	5
2.5	2 × 10μF 35V	150μF 35V	4 × 100μF 6.3V	NONE	NONE	100pF	12	70	159	25	5
2.5	2 × 10μF 35V	150µF 35V	3 × 22μF 6.3V	470μF 6.3V	NONE	100pF	24	56	112	30	5
2.8	2 × 10μF 35V	150µF 35V	3 × 22μF 6.3V	470μF 6.3V	NONE	100pF	24	50	100	30	5
3.3	2 × 10μF 35V	150µF 35V	2 × 100µF 6.3V	330µF 6.3V	NONE	100pF	7	64	126	30	5
3.3	2 × 10μF 35V	150µF 35V	1 × 100μF 6.3V	470μF 4V	NONE	100pF	7	66	132	30	5
3.3	2 × 10μF 35V	150µF 35V	3 × 22μF 6.3V	470μF 4V	NONE	100pF	7	82	166	35	5
3.3	2 × 10μF 35V	150µF 35V	4 × 100μF 6.3V	NONE	NONE	100pF	7	100	200	25	5
3.3	2 × 10µF 35V	150µF 35V	1 × 100µF 6.3V	470µF 4V	NONE	_		52	106	30	5
3.3	2 × 10μF 35V	150µF 35V	3 × 22μF 6.3V	470μF 4V	NONE	100pF	12	64	129	35	5
3.3	2 × 10µF 35V	150µF 35V	2 × 100µF 6.3V	330µF 6.3V	NONE	100pF	12	64	126	30	5
3.3	2 × 10µF 35V	150µF 35V	4 × 100μF 6.3V	NONE	NONE	100pF	12	76	144	25	5
3.3	2 × 10μF 35V	150µF 35V	3 × 22µF 6.3V	470µF 6.3V	NONE	100pF	24	74	149	30	5
	2 × 10µF 35V	150µF 35V	4 × 100μF 6.3V	NONE	NONE	100pF	15	188	375	25	5
5	2 × 10µF 35V	150µF 35V	4 × 100μF 6.3V	NONE	NONE	100pF	20	159	320	25	5

<sup>\*</sup>X7R is recommended for extended temperature range.



After the controller has been started and given adequate time to charge up the output capacitor,  $C_{SS}$  is used as a short-circuit timer. After the RUN/SS pin charges above 4V, if the output voltage falls below 75% of its regulated value, then a short-circuit fault is assumed. A 1.8 $\mu$ A current then begins discharging  $C_{SS}$ . If the fault condition persists until the RUN/SS pin drops to 3.5V, then the controller turns off both power MOSFETs, shuting down the converter permanently. The RUN/SS pin must be actively pulled down to ground in order to restart operation.

The over-current protection timer requires the soft-start timing capacitor  $C_{SS}$  be made large enough to guarantee that the output is in regulation by the time  $C_{SS}$  has reached the 4V threshold. In general, this will depend upon the size of the output capacitance, output voltage and load current characteristic. A minimum external soft-start capacitor can be estimated from:

$$C_{SS\_EXT} + 1000 pF > C_{OUT} \bullet V_{OUT} (10^{-3} [F/V_S])$$

Generally 0.1µF is more than sufficient.

Since the load current is already limited by the current mode control and current foldback circuitry during a shortcircuit, over-current latchoff operation is NOT always needed or desired, especially the output has large amount of capacitance or the load draw huge current during start up. The latchoff feature can be overridden by a pull-up current greater than  $5\mu A$  but less than  $80\mu A$  to the RUN/SS pin. The additional current prevents the discharge of  $C_{SS}$  during a fault and also shortens the soft-start period. Using a resistor from RUN/SS pin to  $V_{IN}$  is a simple solution

to defeat latchoff. Any pull-up network must be able to maintain RUN/SS above 4V maximum latchoff threshold and overcome the  $4\mu A$  maximum discharge current. Figure 3 shows a conceptual drawing of  $V_{RUN}$  during startup and short circuit.

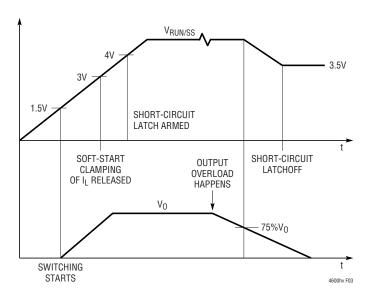


Figure 3. RUN/SS Pin Voltage During Startup and Short-Circuit Protection

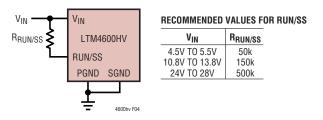


Figure 4. Defeat Short-Circuit Latchoff with a Pull-Up Resistor to  $\mbox{\sc V}_{\mbox{\scriptsize IN}}$ 

LINEAR TECHNOLOGY

#### Enable

The RUN/SS pin can be driven from logic as shown in Figure 5. This function allows the LTM4600HV to be turned on or off remotely. The  $\overline{ON}$  signal can also control the sequence of the output voltage.

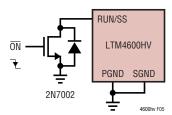


Figure 5. Enable Circuit with External Logic

#### Output Voltage Tracking

For the applications that require output voltage tracking, several LTM4600HV modules can be programmed by the power supply tracking controller such as the LTC2923. Figure 6 shows a typical schematic with LTC2923. Coincident, ratiometric and offset tracking for  $V_0$  rising and falling can be implemented with different sets of resistor values. See the LTC2923 data sheet for more details.

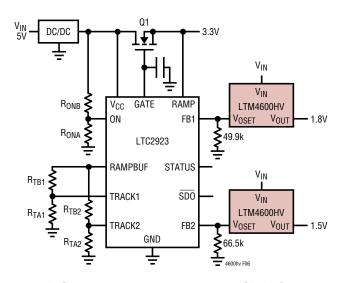


Figure 6. Output Voltage Tracking with the LTC2923 Controller

### **EXTV<sub>CC</sub> Connection**

An internal low dropout regulator produces an internal 5V supply that powers the control circuitry and FET drivers. Therefore, if the system does not have a 5V power rail, the LTM4600HV can be directly powered by  $V_{\text{IN}}$ . The gate driver current through LDO is about 18mA. The internal LDO power dissipation can be calculated as:

$$P_{LDO\ LOSS} = 18mA \cdot (V_{IN} - 5V)$$

The LTM4600HV also provides an external gate driver voltage pin EXTV $_{CC}$ . If there is a 5V rail in the system, it is recommended to connect EXTV $_{CC}$  pin to the external 5V rail. Whenever the EXTV $_{CC}$  pin is above 4.7V, the internal 5V LDO is shut off and an internal 50mA P-channel switch connects the EXTV $_{CC}$  to internal 5V. Internal 5V is supplied from EXTV $_{CC}$  until this pin drops below 4.5V. Do not apply more than 6V to the EXTV $_{CC}$  pin and ensure that EXTV $_{CC}$  < V $_{IN}$ . The following list summaries the possible connections for EXTV $_{CC}$ :

- 1. EXTV $_{\text{CC}}$  grounded. Internal 5V LDO is always powered from the internal 5V regulator.
- 2. EXTV<sub>CC</sub> connected to an external supply. Internal LDO is shut off. A high efficiency supply compatible with the MOSFET gate drive requirements (typically 5V) can improve overall efficiency. With this connection, it is always required that the EXTV<sub>CC</sub> voltage can not be higher than  $V_{IN}$  pin voltage.
- 3. EXTV<sub>CC</sub> is recommended for  $V_{IN} > 20V$

### **Discontinuous Operation and FCB Pin**

The FCB pin determines whether the internal bottom MOSFET remains on when the current reverses. There is an internal 4.75k pull-down resistor connecting this pin to ground. The default light load operation mode is forced continuous (PWM) current mode. This mode provides minimum output voltage ripple.

In the application where the light load efficiency is important, tying the FCB pin above 0.6V threshold enables discontinuous operation where the bottom MOSFET turns off when inductor current reverses. Therefore, the conduction loss is minimized and light load efficiency is improved. The penalty is that the controller may skip cycle and the output voltage ripple increases at light load.

#### Paralleling Operation with Load Sharing

Two or more LTM4600HV modules can be paralleled to provide higher than 10A output current. Figure 7 shows the necessary interconnection between two paralleled modules. The OPTI-LOOP™ current mode control ensures good current sharing among modules to balance the thermal stress. The new feedback equation for two or more LTM4600HVs in parallel is:

$$V_{OUT} = 0.6V \bullet \frac{\frac{100k}{N} + R_{SET}}{R_{SET}}$$

where N is the number of LTM4600HVs in parallel.

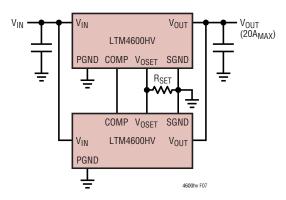


Figure 7. Parallel Two µModules with Load Sharing

### **Thermal Considerations and Output Current Derating**

The power loss curves in Figures 8 and 15 can be used in coordination with the load current derating curves in Figures 9 to 14, and Figures 16 to 19 for calculating an approximate  $\theta_{JA}$  for the module with various heatsinking methods. Thermal models are derived from several temperature measurements at the bench, and thermal modeling analysis. Application Note 103 provides a detailed

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explanation of the analysis for the thermal models, and the derating curves. Tables 3 and 4 provide a summary of the equivalent  $\theta_{JA}$  for the noted conditions. These equivalent  $\theta_{JA}$  parameters are correlated to the measure values, and improved with air-flow. The case temperature is maintained at 100°C or below for the derating curves. This allows for 4W maximum power dissipation in the total module with top and bottom heatsinking, and 2W power dissipation through the top of the module with an approximate  $\theta_{JC}$  between 6°C/W to 9°C/W. This equates to a total of 124°C at the junction of the device.

#### **Safety Considerations**

The LTM4600HV modules do not provide isolation from  $V_{\text{IN}}$  to  $V_{\text{OUT}}$ . There is no internal fuse. If required, a slow blow fuse with a rating twice the maximum input current should be provided to protect each unit from catastrophic failure.

### Layout Checklist/Example

The high integration of the LTM4600HV makes the PCB board layout very simple and easy. However, to optimize its electrical and thermal performance, some layout considerations are still necessary.

- Use large PCB copper areas for high current path, including  $V_{IN}$ , PGND and  $V_{OUT}$ . It helps to minimize the PCB conduction loss and thermal stress
- Place high frequency ceramic input and output capacitors next to the V<sub>IN</sub>, PGND and V<sub>OUT</sub> pins to minimize high frequency noise
- Place a dedicated power ground layer underneath the unit
- To minimize the via conduction loss and reduce module thermal stress, use multiple vias for interconnection between top layer and other power layers
- Do not put vias directly on pad unless they are capped.
- Use a separated SGND ground copper area for components connected to signal pins. Connect the SGND to PGND underneath the unit

Figure 20 gives a good example of the recommended layout.



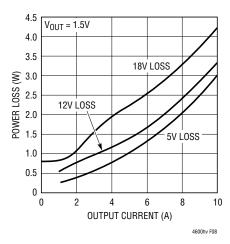


Figure 8. 1.5V Power Loss Curves vs Load Current

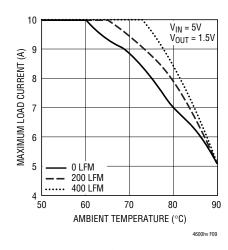


Figure 9. No Heatsink

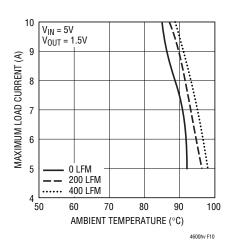


Figure 10. BGA Heatsink

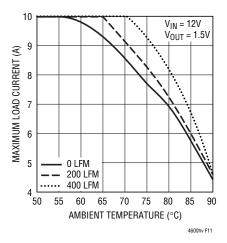


Figure 11. No Heatsink

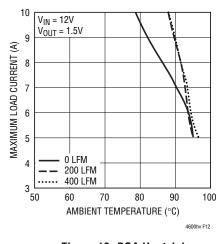


Figure 12. BGA Heatsink

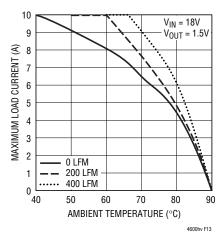


Figure 13. No Heatsink

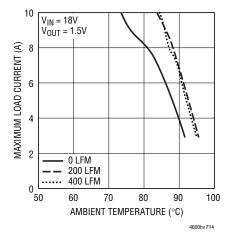


Figure 14. BGA Heatsink

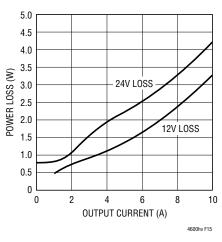


Figure 15. 3.3V Power Loss Curves vs Load Current

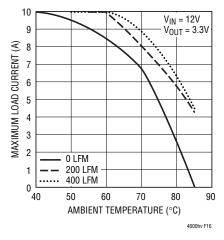


Figure 16. No Heatsink



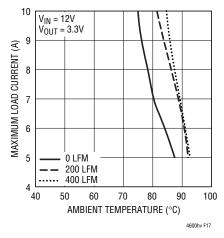


Figure 17. BGA Heatsink

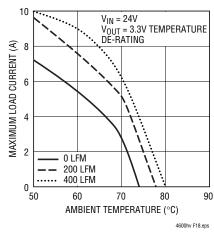


Figure 18. No Heatsink

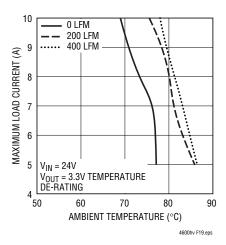


Figure 19. BGA Heatsink

Table 3. 1.5V Output

DERATING CURVE	V <sub>IN</sub> (V)	POWER LOSS CURVE	AIR FLOW (LFM)	HEATSINK	θ <sub>JA</sub> (°C/W)
Figures 9, 11, 13	5, 12, 18	Figure 8	0	None	15.2
Figures 9, 11, 13	5, 12, 18	Figure 8	200	None	14
Figures 9, 11, 13	5, 12, 18	Figure 8	400	None	12
Figures 10, 12, 14	5, 12, 18	Figure 8	0	BGA Heatsink	13.9
Figures 10, 12, 14	5, 12, 18	Figure 8	200	BGA Heatsink	11.3
Figures 10, 12, 14	5, 12, 18	Figure 8	400	BGA Heatsink	10.25

Table 4. 3.3V Output

DERATING CURVE	V <sub>IN</sub> (V)	POWER LOSS CURVE	AIR FLOW (LFM)	HEATSINK	θ <sub>JA</sub> (°C/W)
Figures 16, 18	12, 24	Figure 15	0	None	15.2
Figures 16, 18	12, 24	Figure 15	200	None	14.6
Figures 16, 18	12, 24	Figure 15	400	None	13.4
Figures 17, 19	12, 24	Figure 15	0	BGA Heatsink	13.9
Figures 17, 19	12, 24	Figure 15	200	BGA Heatsink	11.1
Figures 17, 19	12, 24	Figure 15	400	BGA Heatsink	10.5

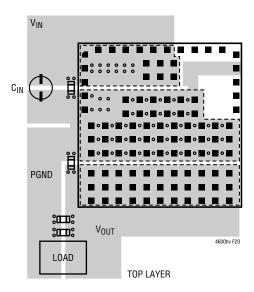
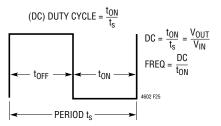


Figure 20. Recommended PCB Layout

#### LTM4600HV Frequency Adjustment

The LTM4600HV is designed to typically operate at 850kHz across most input and output conditions. The control architecture is constant on time valley mode current control. The f<sub>ADJ</sub> pin is typically left open or decoupled with an optional 1000pF capacitor. The switching frequency has been optimized to maintain constant output ripple over the operating conditions. The equations for setting the operating frequency are set around a programmable constant on time. This on time is developed by a programmable current into an on board 10pF capacitor that establishes a ramp that is compared to a voltage threshold equal to the output voltage up to a 2.4V clamp. This I<sub>ON</sub> current is equal to:  $I_{ON} = (V_{IN} - 0.7V)/110k$ , with the 110k onboard resistor from  $V_{IN}$  to  $f_{ADJ}$ . The on time is equal to  $t_{ON} = (V_{OUT}/I_{ON})$ • 10pF and  $t_{OFF} = t_s - t_{ON}$ . The frequency is equal to: Freq. = DC/ $t_{ON}$ . The  $l_{ON}$  current is proportional to  $V_{IN}$ , and the regulator duty cycle is inversely proportional to V<sub>IN</sub>, therefore the step-down regulator will remain relatively constant frequency as the duty cycle adjustment takes place with lowering  $V_{IN}$ . The on time is proportional to  $V_{OUT}$  up to a 2.4V clamp. This will hold frequency relatively constant with different output voltages up to 2.4V. The regulator switching period is comprised of the on time and off time as depicted in the following waveform. The on time is equal to  $t_{ON} = (V_{OUT}/I_{ON}) \cdot 10pF$  and  $t_{OFF} = t_s - t_{ON}$ . The frequency is equal to: Frequency =  $DC/t_{ON}$ ).



The LTM4600HV has a minimum ( $t_{ON}$ ) on time of 100 nanoseconds and a minimum ( $t_{OFF}$ ) off time of 400 nanoseconds. The 2.4V clamp on the ramp threshold as a function of V<sub>OUT</sub> will cause the switching frequency to increase by the ratio of  $V_{OUT}/2.4V$  for 3.3V and 5V outputs. This is due to the fact the on time will not increase as  $V_{OUT}$ increases past 2.4V. Therefore, if the nominal switching frequency is 850kHz, then the switching frequency will increase to ~1.2MHz for 3.3V, and ~1.7MHz for 5V outputs due to Frequency =  $(DC/t_{ON})$  When the switching frequency increases to 1.2MHz, then the time period  $t_s$  is reduced to ~833 nanoseconds and at 1.7MHz the switching period reduces to ~588 nanoseconds. When higher duty cycle conversions like 5V to 3.3V and 12V to 5V need to be accommodated, then the switching frequency can be lowered to alleviate the violation of the 400ns minimum off time. Since the total switching period is  $t_S = t_{ON} + t_{OFF}$  $t_{OFF}$  will be below the 400ns minimum off time. A resistor from the f<sub>AD,I</sub> pin to ground can shunt current away from the on time generator, thus allowing for a longer on time and a lower switching frequency. 12V to 5V and 5V to 3.3V derivations are explained in the data sheet to lower switching frequency and accommodate these step-down conversions.

Equations for setting frequency for 12V to 5V:

$$I_{ON} = (V_{IN} - 0.7V)/110k; I_{ON} = 103\mu A$$

frequency = 
$$(I_{ON}/[2.4V \cdot 10pF]) \cdot DC = 1.79MHz$$
; DC = duty cycle, duty cycle is  $(V_{OUT}/V_{IN})$ 

$$t_S$$
 =  $t_{ON}$  +  $t_{OFF}$ ,  $t_{ON}$  = on-time,  $t_{OFF}$  = off-time of the switching period;  $t_S$  = 1/frequency

 $t_{OFF}$  must be greater than 400ns, or  $t_S - t_{ON} > 400$ ns.

$$t_{ON} = DC \cdot t_S$$

1MHz frequency or 1µs period is chosen for 12V to 5V.



 $t_{ON} = 0.41 \cdot 1 \mu s \approx 410 ns$ 

 $t_{OFF} = 1\mu s - 410ns \approx 590ns$ 

 $t_{\mbox{\scriptsize ON}}$  and  $t_{\mbox{\scriptsize OFF}}$  are above the minimums with adequate guard band.

Using the frequency =  $(I_{ON}/[2.4V \cdot 10pF]) \cdot DC$ , solve for  $I_{ON} = (1MHz \cdot 2.4V \cdot 10pF) \cdot (1/0.41) \approx 58\mu A$ .  $I_{ON}$  current calculated from 12V input was  $103\mu A$ , so a resistor from  $f_{ADJ}$  to ground =  $(0.7V/15k) = 46\mu A$ .  $103\mu A - 46\mu A = 57\mu A$ , sets the adequate  $I_{ON}$  current for proper frequency range for the higher duty cycle conversion of 12V to 5V. Input voltage range is limited to 9V to 16V. Higher input voltages can be used without the 15k on  $f_{ADJ}$ . The inductor ripple current gets too high above 16V, and the 400ns minimum off-time is limited below 9V.

Equations for setting frequency for 5V to 3.3V:

 $I_{ON} = (V_{IN} - 0.7V)/110k; I_{ON} = 39\mu A$ 

frequency =  $(I_{ON}/[2.4V \cdot 10pF]) \cdot DC = 1.07MHz$ ; DC = duty cycle, duty cycle is  $(V_{OUT}/V_{IN})$ 

 $t_S = t_{ON} + t_{OFF}$   $t_{ON} = on-time$ ,  $t_{OFF} = off-time$  of the switching period;  $t_S = 1/f$ requency

 $t_{OFF}$  must be greater than 400ns, or  $t_S - t_{ON} > 400$ ns.

$$t_{ON} = DC \cdot t_S$$

~450kHz frequency or 2.22µs period is chosen for 5V to 3.3V. Frequency range is about 450kHz to 650kHz from 4.5V to 7V input.

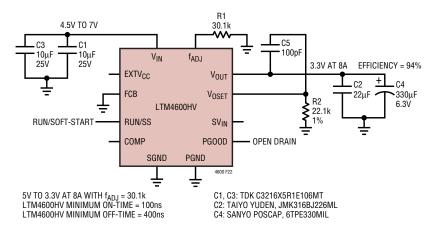
$$t_{ON} = 0.66 \cdot 2.22 \mu s \approx 1.46 \mu s$$

$$t_{OFF} = 2.22 \mu s - 1.46 \mu s \approx 760 ns$$

 $t_{\mbox{\scriptsize ON}}$  and  $t_{\mbox{\scriptsize OFF}}$  are above the minimums with adequate guard band.

Using the frequency =  $(I_{ON}/[2.4V \cdot 10pF]) \cdot DC$ , solve for  $I_{ON} = (450 \text{kHz} \cdot 2.4V \cdot 10pF) \cdot (1/0.66) \cong 16 \mu A$ .  $I_{ON}$  current calculated from 5V input was  $39 \mu A$ , so a resistor from  $f_{ADJ}$  to ground =  $(0.7V/30.1k) = 23 \mu A$ .  $39 \mu A - 23 \mu A = 16 \mu A$ , sets the adequate  $I_{ON}$  current for proper frequency range for the higher duty cycle conversion of 5V to 3.3V. Input voltage range is limited to 4.5V to 7V. Higher input voltages can be used without the 30.1k on  $f_{ADJ}$ . The inductor ripple current gets too high above 7V, and the 400ns minimum off-time is limited below 4.5V.

#### 5V to 3.3V at 8A

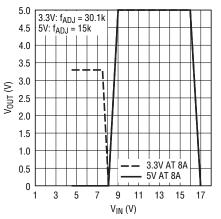


LINEAR

#### 12V to 5V at 8A R1 15k 9V TO 16V L C5 **-** C3 100pF **-** 10μF 25V $V_{IN}$ f<sub>ADJ</sub> EFFICIENCY = 94% 25V **5V AT 8A** EXTV<sub>CC</sub> $V_{OUT}$ FCB VOSET •330μF R2 LTM4600HV <u></u> 13.7k 1% 6.3Ÿ RUN/SOFT-START RUN/SS $SV_{IN}$ OPEN DRAIN COMP PG00D SGND **PGND** 12V TO 5V AT 8A WITH f<sub>ADJ</sub> = 15k LTM4600HV MINIMUM ON-TIME = 100ns C1, C3: TDK C3216X5R1E106MT C2: TAIYO YUDEN, JMK316BJ226ML

C4: SANYO POSCAP, 6TPE330MIL

# V<sub>IN</sub> to V<sub>OUT</sub> Stepdown Ratio for 12V to 5V and 5V to 3.3V



4600 F24

### TYPICAL APPLICATION

LTM4600HV MINIMUM OFF-TIME = 400ns

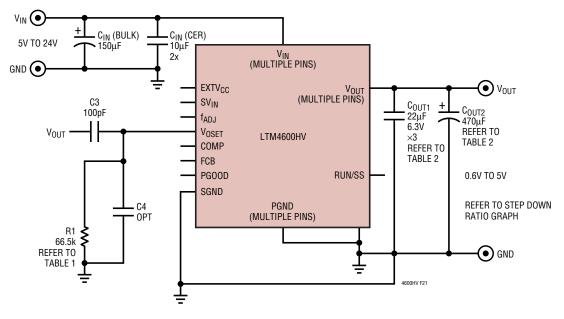
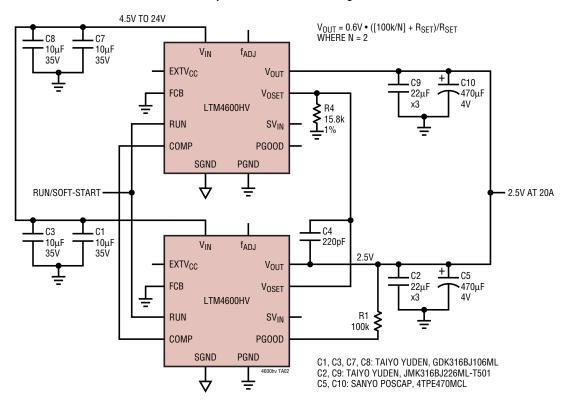


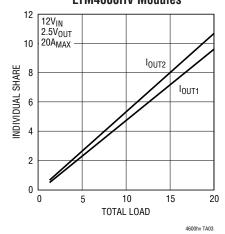
Figure 21. Typical Application, 5V to 24V Input, 0.6V to 5V Output, 10A Max

### TYPICAL APPLICATION

#### **Parallel Operation and Load Sharing**

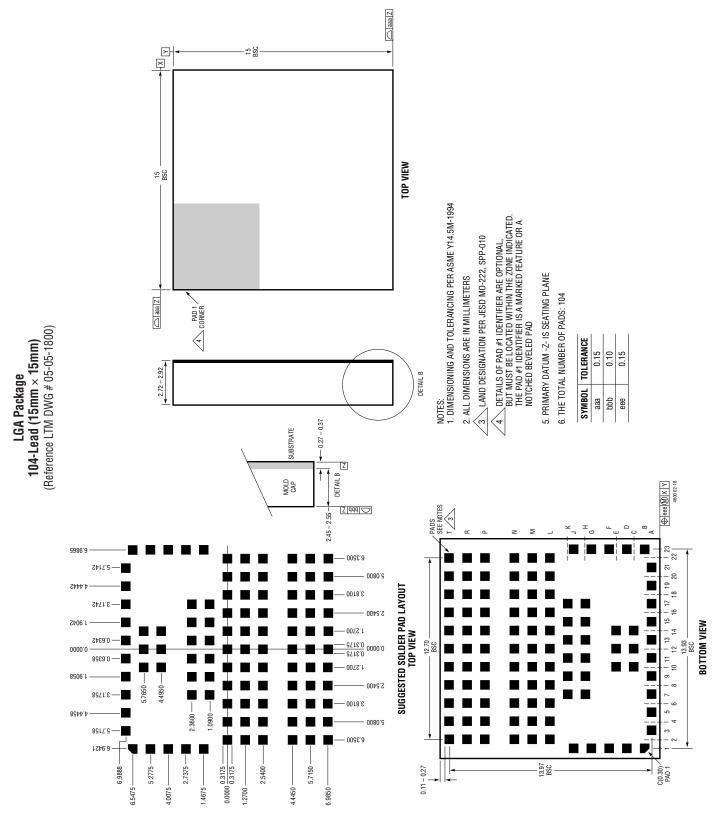


## Current Sharing Between Two LTM4600HV Modules





### PACKAGE DESCRIPTION



### PACKAGE DESCRIPTION

### Pin Assignment Tables (Arranged by Pin Number)

PIN NAME	PIN NAME	PIN NAME	PIN NAME	PIN NAME	PIN NAME	PIN NAME	PIN NAME
A1 -	B1 V <sub>IN</sub>	C1 -	D1 V <sub>IN</sub>	E1 -	F1 V <sub>IN</sub>	G1 PGND	H1 -
A2 -	B2 -	C2 -	D2 -	E2 -	F2 -	G2 -	H2 -
A3 V <sub>IN</sub>	B3 -	C3 -	D3 -	E3 -	F3 -	G3 -	H3 -
A4 -	B4 -	C4 -	D4 -	E4 -	F4 -	G4 -	H4 -
A5 V <sub>IN</sub>	B5 -	C5 -	D5 -	E5 -	F5 -	G5 -	H5 -
A6 -	B6 -	C6 -	D6 -	E6 -	F6 -	G6 -	H6 -
A7 V <sub>IN</sub>	B7 -	C7 -	D7 -	E7 -	F7 -	G7 -	H7 PGND
A8 -	B8 -	C8 -	D8 -	E8 -	F8 -	G8 -	Н8 -
A9 V <sub>IN</sub>	В9 -	C9 -	D9 -	E9 -	F9 -	G9 -	H9 PGND
A10 -	B10 -	C10 V <sub>IN</sub>	D10 -	E10 V <sub>IN</sub>	F10 -	G10 -	H10 -
A11 V <sub>IN</sub>	B11 -	C11 -	D11 -	E11 -	F11 -	G11 -	H11 PGND
A12 -	B12 -	C12 V <sub>IN</sub>	D12 -	E12 V <sub>IN</sub>	F12 -	G12 -	H12 -
A13 V <sub>IN</sub>	B13 -	C13 -	D13 -	E13 -	F13 -	G13 -	H13 PGND
A14 -	B14 -	C14 V <sub>IN</sub>	D14 -	E14 V <sub>IN</sub>	F14 -	G14 -	H14 -
A15 f <sub>ADJ</sub>	B15 -	C15 -	D15 -	E15 -	F15 -	G15 -	H15 PGND
A16 -	B16 -	C16 -	D16 -	E16 -	F16 -	G16 -	H16 -
A17 SV <sub>IN</sub>	B17 -	C17 -	D17 -	E17 -	F17 -	G17 -	H17 PGND
A18 -	B18 -	C18 -	D18 -	E18 -	F18 -	G18 -	H18 -
A19 EXTV <sub>CC</sub>	B19 -	C19 -	D19 -	E19 -	F19 -	G19 -	H19 -
A20 -	B20 -	C20 -	D20 -	E20 -	F20 -	G20 -	H20 -
A21 V <sub>OSET</sub>	B21 -	C21 -	D21 -	E21 -	F21 -	G21 -	H21 -
A22 -	B22 -	C22 -	D22 -	E22 -	F22 -	G22 -	H22 -
A23 -	B23 COMP	C23 -	D23 SGND	E23 -	F23 RUN/SS	G23 FCB	H23 -

PI	N NAME	PIN NA	VIE P	IN NAME	PIN	NAME	PII	NAME	PII	N NAME	PII	NAME	PIN NAME	
J1	PGND	K1 -	L1	-	M1	-	N1	-	P1	-	R1	-	T1	-
J2	-	K2 -	L2	PGND	M2	PGND	N2	PGND	P2	V <sub>OUT</sub>	R2	V <sub>OUT</sub>	T2	V <sub>OUT</sub>
J3	-	K3 -	L3	-	M3	-	N3	-	P3	-	R3	-	T3	-
J4	-	K4 -	L4	PGND	M4	PGND	N4	PGND	P4	V <sub>OUT</sub>	R4	V <sub>OUT</sub>	T4	V <sub>OUT</sub>
J5	-	K5 -	L5	-	M5	-	N5	-	P5	-	R5	-	T5	-
J6	-	K6 -	L6	PGND	M6	PGND	N6	PGND	P6	V <sub>OUT</sub>	R6	V <sub>OUT</sub>	T6	V <sub>OUT</sub>
J7	-	K7 PGN	D L7	-	M7	-	N7	-	P7	-	R7	-	T7	-
J8	-	K8	L8	PGND	M8	PGND	N8	PGND	P8	V <sub>OUT</sub>	R8	V <sub>OUT</sub>	T8	V <sub>OUT</sub>
J9	-	K9 PGN	D L9	-	M9	-	N9	-	P9	-	R9	-	T9	-
J10	-	K10	L10	PGND	M10	PGND	N10	PGND	P10	V <sub>OUT</sub>	R10	V <sub>OUT</sub>	T10	V <sub>OUT</sub>
J11	-	K11 PGN	D L11	-	M11	-	N11	-	P11	-	R11	-	T11	-
J12	-	K12 -	L12	PGND	M12	PGND	N12	PGND	P12	V <sub>OUT</sub>	R12	V <sub>OUT</sub>	T12	V <sub>OUT</sub>
J13	-	K13 PGN	D L13	-	M13	-	N13	-	P13	-	R13	-	T13	-
J14	-	K14 -	L14	PGND	M14	PGND	N14	PGND	P14	$V_{OUT}$	R14	$V_{OUT}$	T14	$V_{OUT}$
J15	-	K15 PGN	D L15	-	M15	-	N15	-	P15	-	R15	-	T15	-
J16	-	K16 -	L16	PGND	M16	PGND	N16	PGND	P16	$V_{OUT}$	R16	$V_{OUT}$	T16	$V_{OUT}$
J17	-	K17 PGN	D L17	-	M17	-	N17	-	P17	-	R17	-	T17	-
J18	-	K18 -	L18	PGND	M18	PGND	N18	PGND	P18	$V_{OUT}$	R18	$V_{OUT}$	T18	$V_{OUT}$
J19	-	K19 -	L19	-	M19	-	N19	-	P19	-	R19	-	T19	-
J20	-	K20 -	L20	PGND	M20	PGND	N20	PGND	P20	V <sub>OUT</sub>	R20	V <sub>OUT</sub>	T20	V <sub>OUT</sub>
J21	-	K21 -	L21	-	M21	-	N21	-	P21	-	R21	-	T21	-
J22	-	K22 -	L22	PGND	M22	PGND	N22	PGND	P22	V <sub>OUT</sub>	R22	V <sub>OUT</sub>	T22	V <sub>OUT</sub>
J23	PG00D	K23 -	L23	-	M23	-	N23	-	P23	-	R23	-	T23	-

LINEAR TECHNOLOGY

### PACKAGE DESCRIPTION

### Pin Assignment Tables (Arranged by Pin Number)

PIN NAME		
G1	PGND	
H7 H9 H11 H13 H15 H17	PGND PGND PGND PGND PGND PGND	
J1	PGND	
K7 K9 K11 K13 K15 K17	PGND PGND PGND PGND PGND PGND	
L2 L4 L6 L8 L10 L12 L14 L16 L18 L20 L22	PGND PGND PGND PGND PGND PGND PGND PGND	
M2 M4 M6 M8 M10 M12 M14 M16 M18 M20 M22	PGND PGND PGND PGND PGND PGND PGND PGND	
N2 N4 N6 N8 N10 N12 N14 N16 N18 N20 N22	PGND PGND PGND PGND PGND PGND PGND PGND	

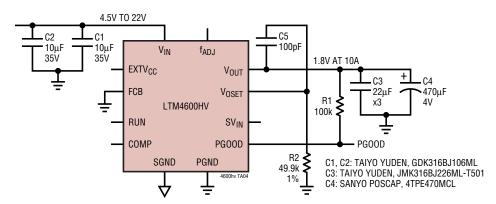
PIN NAME		
P2	V <sub>OUT</sub>	
P4	V <sub>OUT</sub>	
P6	l V <sub>OUT</sub>	
P8	l V <sub>OUT</sub>	
P10	l V <sub>OUT</sub>	
P12	l V <sub>OUT</sub>	
P14	l V <sub>OUT</sub>	
P16	l V <sub>OUT</sub>	
P18	V <sub>OUT</sub>	
P20	V <sub>OUT</sub>	
P22	V <sub>OUT</sub>	
R2	V <sub>OUT</sub>	
R4	V <sub>OUT</sub>	
R6	V <sub>OUT</sub>	
R8	V <sub>OUT</sub>	
R10	V <sub>OUT</sub>	
R12	V <sub>OUT</sub>	
R14 R16	V <sub>OUT</sub>	
R18	V <sub>OUT</sub>	
R20	Vout	
R22	V <sub>OUT</sub>	
T2	V <sub>OUT</sub>	
T4	V <sub>OUT</sub>	
T6 T8	V <sub>OUT</sub>	
T10	Vout	
T12	V <sub>OUT</sub>	
T14	V <sub>OUT</sub> V <sub>OUT</sub>	
T16	Vout	
T18	Vout	
T20	Vout	
T22	V <sub>OUT</sub>	
	1 001	

PIN NAME	
A3 A5 A7 A9 A11 A13	VIN VIN VIN VIN VIN VIN
B1	V <sub>IN</sub>
C10 C12 C14	V <sub>IN</sub> V <sub>IN</sub> V <sub>IN</sub>
D1	V <sub>IN</sub>
E10 E12 E14	V <sub>IN</sub> V <sub>IN</sub> V <sub>IN</sub>
F1	V <sub>IN</sub>

PIN NAME		
A15	$f_{ADJ}$	
A17	SV <sub>IN</sub>	
A19	$EXTV_CC$	
A21	V <sub>OSET</sub>	
B23	COMP	
D23	SGND	
F23	RUN/SS	
G23	FCB	
J23	PG00D	

### TYPICAL APPLICATION

#### 1.8V, 10A Regulator



### **RELATED PARTS**

PART NUMBER	DESCRIPTION	COMMENTS
LTC2900	Quad Supply Monitor with Adjustable Reset Timer	Monitors Four Supplies; Adjustable Reset Timer
LTC2923	Power Supply Tracking Controller	Tracks Both Up and Down; Power Supply Sequencing
LT3825/LT3837	Synchronous Isolated Flyback Controllers	No Optocoupler Required; 3.3V, 12A Output; Simple Design
LTM4600	10A DC/DC μModule	Basic 10A DC/DC μModule
LTM4601	12A DC/DC µModule with PLL, Output Tracking/ Margining and Remote Sensing	Synchronizable, PolyPhase Operation to 48A, LTM4601-1 Version has no Remote Sensing
LTM4602	6A DC/DC μModule	Pin Compatible with the LTM4600
LTM4603	6A DC/DC μModule with PLL and Outpupt Tracking/ Margining and Remote Sensing	Synchronizable, PolyPhase Operation to 48A, LTM4601-1 Version has no Remote Sensing, Pin Compatible with the LTM4601