# FODM3062，FODM3063，FODM3082，FODM3083 4－Pin Full Pitch Mini－Flat Package Zero－Cross Triac Driver Output Optocouplers 

## Features

■ dv／dt of $600 \mathrm{~V} / \mu \mathrm{s}$ guaranteed
■ Compact 4－pin surface mount package （ 2.4 mm maximum standoff height）
■ Zero voltage crossing
■ Peak blocking voltage：600V（FODM306X）
800V（FODM308X）
■ Available in tape and reel quantities of 2500
■ C－UL，UL and VDE certifications pending

## Applications

■ Solenoid／valve controls
－Lighting controls
－Static power switches
－AC motor drives
－Temperature controls
■ E．M．contactors
－AC motor starters
－Solid state relays

## Description

The FODM306X and FODM308X series consist of an infrared emitting diode optically coupled to a monolithic silicon detector performing the function of a zero voltage crossing bilateral triac driver，and is housed in a compact 4 －pin mini－flat package．The lead pitch is 2.54 mm ．They are designed for use with a triac in the interface of logic systems to equipment powered from 115／240 VAC lines， such as solid state relays，industrial controls，motors， solenoids and consumer appliances．

## Package Dimensions



## Note：

All dimensions are in millimeters．

Absolute Maximum Ratings ( $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless otherwise specified)
Stresses exceeding the absolute maximum ratings may damage the device. The device may not function or be operable above the recommended operating conditions and stressing the parts to these levels is not recommended. In addition, extended exposure to stresses above the recommended operating conditions may affect device reliability. The absolute maximum ratings are stress ratings only.

| Symbol | Parameter |  | Rating | Units |
| :---: | :---: | :---: | :---: | :---: |
| TOTAL PACKAGE |  |  |  |  |
| $\mathrm{T}_{\text {STG }}$ | Storage Temperature |  | -55 to +150 | ${ }^{\circ} \mathrm{C}$ |
| ToPR | Operating Temperature |  | -40 to +100 | ${ }^{\circ} \mathrm{C}$ |
| EMITTER |  |  |  |  |
| $\mathrm{I}_{\mathrm{F} \text { (avg) }}$ | Continuous Forward Current |  | 60 | mA |
| $\mathrm{I}_{\mathrm{F} \text { (pk) }}$ | Peak Forward Current (1 $\mu \mathrm{s}$ pulse, 300pps.) |  | 1 | A |
| $\mathrm{V}_{\mathrm{R}}$ | Reverse Input Voltage |  | 6 | V |
| $\mathrm{P}_{\mathrm{D}}$ | Power Dissipation (No derating required over operating temp. range) |  | 100 | mW |
| DETECTOR |  |  |  |  |
| $\mathrm{I}_{\mathrm{T} \text { (RMS) }}$ | On-State RMS Current |  | 70 | mA (RMS) |
| $\mathrm{V}_{\mathrm{DRM}}$ | Off-State Output Terminal Voltage | FODM3062/FODM3063 | 600 | V |
|  |  | FODM3082/FODM3083 | 800 |  |
| $\mathrm{P}_{\mathrm{D}}$ | Power Dissipation (No derating required over operating temp. range) |  | 300 | mW |

Electrical Characteristics ( $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ )
Individual Component Characteristics

| Symbol | Parameter | Test Conditions | Min. | Typ.* | Max. | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EMITTER |  |  |  |  |  |  |
| $V_{F}$ | Input Forward Voltage | $\mathrm{I}_{\mathrm{F}}=30 \mathrm{~mA}$ |  |  | 1.5 | V |
| $\mathrm{I}_{\mathrm{R}}$ | Reverse Leakage Current | $\mathrm{V}_{\mathrm{R}}=6 \mathrm{~V}$ |  |  | 100 | $\mu \mathrm{A}$ |
| DETECTOR |  |  |  |  |  |  |
| IDRM1 | Peak Blocking Current, Either Direction | Rated $\mathrm{V}_{\text {DRM }}, \mathrm{I}_{\mathrm{F}}=0^{(1)}$ |  |  | 500 | nA |
| dV/dt | Critical Rate of Rise of Off-State Voltage | $\mathrm{I}_{\mathrm{F}}=0\left(\right.$ Figure 1) ${ }^{(2)}$ | 600 |  |  | V/us |

Transfer Characteristics

| Symbol | DC Characteristics | Test Conditions | Device | Min. | Typ.* | Max. | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{I}_{\mathrm{FT}}$ | LED Trigger Current | Main Terminal Voltage $=3 V^{(3)}$ | FODM3062 |  |  | 10 | mA |
|  |  |  | FODM3082 |  |  |  |  |
|  |  |  | FODM3063 |  |  | 5 |  |
|  |  |  | FODM3083 |  |  |  |  |
| $\mathrm{I}_{\mathrm{H}}$ | Holding Current, Either Direction |  | All |  | 300 |  | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\text {TM }}$ | Peak On-State Voltage, Either Direction | $\begin{aligned} & I_{\mathrm{F}}=\text { Rated } \mathrm{I}_{\mathrm{FT}}, \\ & \mathrm{I}_{\mathrm{TM}}=100 \mathrm{~mA} \text { peak } \end{aligned}$ | All |  |  | 3 | V |

Zero Crossing Characteristics

| Symbol | Characteristics | Test Conditions | Device | Min. | Typ.* | Max. | Units |
| :---: | :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\mathrm{IH}}$ | Inhibit Voltage, <br> MT1-MT2 Voltage <br> above which device <br> will not trigger | $\mathrm{I}_{\mathrm{F}}=$ Rated I $\mathrm{I}_{\mathrm{FT}}$ | All |  |  | 20 | V |
| IDRM2 | Leakage in Inhibit <br> State | $\mathrm{I}_{\mathrm{F}}=$ Rated I <br> Rated VDRM, <br> Off-State | All |  |  | 2 | mA |

## Isolation Characteristics

| Characteristics | Test Conditions | Symbol | Device | Min. | Typ.* | Max. | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Steady State Isolation Voltage ${ }^{(4)}$ | (1 Minute) $\text { R.H. }=40 \% \text { to } 60 \%$ | $\mathrm{V}_{\text {ISO }}$ | All | 3750 |  |  | VRMS |

*All typicals at $25^{\circ} \mathrm{C}$.

## Notes:

1. Test voltage must be applied within dv/dt rating.
2. This is static $d v / d t$. See Figure 1 for test circuit. Commutating $d v / d t$ is function of the load-driving thyristor(s) only.
3. All devices are guaranteed to trigger at an $I_{\mathrm{F}}$ value less than or equal to $\max \mathrm{I}_{\mathrm{FT}}$. Therefore, recommended operating $I_{F}$ lies between max $I_{F T}\left(10 \mathrm{~mA}\right.$ for FODM3062/82, 5 mA for $\mathrm{FODM}^{2} 3063 / 83$ ) and absolute max $\mathrm{I}_{\mathrm{F}}(60 \mathrm{~mA})$.
4. Steady state isolation voltage, $\mathrm{V}_{\text {ISO }}$, is an internal device dielectric breakdown rating. For this test, pins $1 \& 2$ are common, and pins $3 \& 4$ are common.

## Typical Performance Curves



Fig. 3 Holding Current vs. Ambient Temperature


Fig. 2 Leakage Current vs. Ambient Temperature


Fig. 4 Trigger Current vs. Ambient Temperature


## Typical Performance Curves (Continued)

Fig. 5 LED Current Required to Trigger vs. LED Pulse Width


PW ${ }_{\text {IN }}$ - LED TRIGGER PULSE WIDTH $\left({ }^{\circ} \mathrm{C}\right.$ )

Fig. 6 Off-State Output Terminal Voltage vs. Ambient Temperature


Fig. 7 On-State Characteristics



## Determining the Power Rating of the Series Resistors Used in a Zero-Cross Opto-TRIAC Driver Application

The following will present the calculations for determining the power dissipation of the current limiting resistors found in an opto-TRIAC driver interface.

Figure 10 shows a typical circuit to drive a sensitive gate four quadrant power TRIAC. This figure provides typical resistor values for a zero line cross detecting opto-TRIAC when operated from a mains voltage of 20 V to 240 V . The wattage rating for each resistor is not given because their dissipation is dependent upon characteristics of the power TRIAC being driven.
Recall that the opto-TRIAC is used to trigger a four quadrant power TRIAC. Please note that these optoTRIACs are not recommended for driving "snubberless" three quadrant power TRIACs.
Under normal operation, the opto-TRIAC will fire when the mains voltage is lower than the minimum inhibit trigger voltage, and the LED is driven at a current greater than the maximum LED trigger current. As an example for the FODM3063, the LED trigger current should be greater than 5 mA , and the mains voltage is less than 10 V peak. The inhibit voltage has a typical range of 10 V minimum and 20 V maximum. This means that if a sufficient LED current is flowing when the mains voltage is less than 10 V , the device will fire. If a trigger appears between 10 V and 20 V , the device may fire. If the trigger occurs after the mains voltage has reached 20Vpeak, the device will not fire.

The power dissipated from resistors placed in series with the opto-TRIAC and the gate of the power TRIAC is much smaller than one would expect. These current handling components only conduct current when the mains voltage is less than the maximum inhibit voltage. If the opto-TRIAC is triggered when the mains voltage is greater than the inhibit voltage, only the TRIAC leakage current will flow. The power dissipation in a $360 \Omega$ resistor shown in Figure 10 is the product of the resistance ( $360 \Omega$ ) times the square of the current sum of main TRIAC's gate current plus the current flowing gate to the MT2 resistor connection (330 ). This power calculation is further modified by the duty factor of the duration for this current flow. The duty factor is the ratio of the turn-on time of the main TRIAC to the sine of the single cycle time. Assuming a main TRIAC turn-on time of $50 \mu \mathrm{~s}$ and a 60 Hz mains voltage, the duty cycle is approximately $0.6 \%$. The opto-TRIAC only conducts current while triggering the main TRIAC. Once the main TRIAC fires, its onstate voltage is typically lower than the on-state sustaining voltage of the opto-TRIAC. Thus, once the main TRIAC fires, the opto-TRIAC is often shunted off. This situation results in very low power dissipation for both the $360 \Omega$ and $330 \Omega$ resistors, when driving a traditional four quadrant power TRIAC.

If a three quadrant "snubberless" TRIAC is driven by the opto-TRIAC, the calculations are different. When the main power TRIAC is driving a high power factor (resistive) load, it shuts off during the fourth quadrant.


Typical circuit for use when hot line switching of 240VAC s required. In this circuit the "hot" side of the line is switched and the load connected to the cold or neutral side. The load may be connected to either the neutral or hot line.
$R_{\text {in }}$ is calculated so that $I_{F}$ is equal to the rated $I_{F T}$ of the part, 5 mA for the FODM3063/83 and 10 mA for the
240 VAC FODM3062/82. The $39 \Omega$ resistor and $0.01 \mu \mathrm{~F}$ capacitor are FODM3062/82. The $39 \Omega$ resistor and $0.01 \mu \mathrm{~F}$ capacitor are
for snubbing of the triac and may or may not be necessary depending upon the particular triac and load used.

Figure 10. Hot-Line Switching Application Circuit

If sufficient holding current is still flowing through the opto-TRIAC, the opto-TRIAC will turn-on and attempt to carry the power TRIACs load. This situation typically causes the opto-TRIAC to operate beyond its maximum current rating, and product and resistor failures typically result. For this reason, using an optoTRIAC to drive a three quadrant "snubberless" power TRIAC is not recommended.

Power in the $360 \Omega$ resistor, when driving a sensitive gate 4 quadrant power TRIAC:

$$
\begin{aligned}
& \mathrm{I}_{\mathrm{GT}}=20 \mathrm{~mA} \\
& \mathrm{~V}_{\mathrm{GT}}=1.5 \mathrm{~V} \\
& \mathrm{DF}=0.6 \% \\
\mathrm{P}= & \left(\mathrm{I}_{\mathrm{GT}}+\mathrm{V}_{\mathrm{GT}} / 330 \Omega\right)^{2} \times 360 \Omega \times \mathrm{DF} \\
\mathrm{P}= & (20 \mathrm{~mA}+1.5 / 330 \Omega)^{2 *} \times 360 \Omega \times 0.6 \%=1.3 \mathrm{~mW}
\end{aligned}
$$

A $1 / 4$ watt resistor is more than adequate for both the $360 \Omega$ and $330 \Omega$ resistors.

The real power in the snubber resistor is based upon the integral of the power transient present when the load commutes. A fast commuting transient may allow a peak current of 4 A to 8 A in the snubbing filter. For best results, the capacitor should be a nonpolarized AC unit with a low ESR. The $39 \Omega$ series resistor sets a time constant and limits the peak current. For a resistive load with a power factor near unity, the commutating transients will be small. This results in a very small peak current given the $0.01 \mu \mathrm{~F}$ capacitor's reactance. Normally, for factional horsepower reactive loads, the resistor found in the snubber circuit will have a power rating from $1 / 2 \mathrm{~W}$ to 2 W . The resistor should be a low inductance type to adequately filter the high frequency transients.


## Tape and Reel Information



| Description |  | Symbol |
| :--- | :---: | :---: |
|  | 2.54 Pitch |  |
| Tape Width | W | Dimensions |
| Tape Thickness | t | $12.00 \pm 0.4$ |
| Sprocket Hole Pitch | $\mathrm{P}_{0}$ | $0.35 \pm 0.02$ |
| Sprocket Hole Dia. | $\mathrm{D}_{0}$ | $4.00 \pm 0.20$ |
| Sprocket Hole Location | E | $1.55 \pm 0.20$ |
| Pocket Location | F | $1.75 \pm 0.20$ |
|  | $\mathrm{P}_{2}$ | $5.50 \pm 0.20$ |
| Pocket Pitch | P | $2.00 \pm 0.20$ |
| Pocket Dimension | $\mathrm{A}_{0}$ | $8.00 \pm 0.20$ |
|  | $\mathrm{~B}_{0}$ | $4.75 \pm 0.20$ |
|  | $\mathrm{~K}_{0}$ | $7.30 \pm 0.20$ |
| Pocket Hole Dia. | $\mathrm{D}_{1}$ | $2.30 \pm 0.20$ |
| Cover Tape Width | $\mathrm{W}_{1}$ | $1.55 \pm 0.20$ |
| Cover Tape Thickness | d | 9.20 |
| Max. Component Rotation or Tilt |  | $0.065 \pm 0.02$ |
| Devices Per Reel |  | $20^{\circ} \mathrm{max}$ |
| Reel Diameter | 2500 |  |



## Reflow Profile



| Profile Feature | Pb-Free Assembly Profile |
| :--- | :---: |
| Temperature Min. (Tsmin) | $150^{\circ} \mathrm{C}$ |
| Temperature Max. (Tsmax) | $200^{\circ} \mathrm{C}$ |
| Time ( $\mathrm{t}_{\mathrm{S}}$ ) from (Tsmin to Tsmax) | $60-120$ seconds |
| Ramp-up Rate ( $\mathrm{t}_{\mathrm{L}}$ to $\mathrm{t}_{\mathrm{P}}$ ) | $3^{\circ} \mathrm{C} /$ second max. |
| Liquidous Temperature $\left(\mathrm{T}_{\mathrm{L}}\right)$ | $217^{\circ} \mathrm{C}$ |
| Time ( $\mathrm{t}_{\mathrm{L}}$ ) Maintained Above ( $\mathrm{T}_{\mathrm{L}}$ ) | $60-150$ seconds |
| Peak Body Package Temperature | $260^{\circ} \mathrm{C}+0^{\circ} \mathrm{C} /-5^{\circ} \mathrm{C}$ |
| Time ( $\mathrm{t}_{\mathrm{P}}$ ) within $5^{\circ} \mathrm{C}$ of $260^{\circ} \mathrm{C}$ | 30 seconds |
| Ramp-down Rate $\left(\mathrm{T}_{\mathrm{P}}\right.$ to $\mathrm{T}_{\mathrm{L}}$ ) | $6^{\circ} \mathrm{C} /$ second max. |
| Time $25^{\circ} \mathrm{C}$ to Peak Temperature | 8 minutes max. |

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