## Low－Voltage，400mA Step－Down DC－DC Converters in SOT23

## General Description

The MAX1920／MAX1921 step－down converters deliver over 400 mA to outputs as low as 1.25 V ．These convert－ ers use a unique proprietary current－limited control scheme that achieves over 90\％efficiency．These devices maintain extremely low quiescent supply current $(50 \mu \mathrm{~A})$ ，and their high 1.2 MHz （max）operating frequency permits small，low－cost external components．This combi－ nation makes the MAX1920／MAX1921 excellent high－ efficiency alternatives to linear regulators in space－ constrained applications．
Internal synchronous rectification greatly improves effi－ ciency and eliminates the external Schottky diode required in conventional step－down converters．Both devices also include internal digital soft－start to limit input current upon startup and reduce input capacitor requirements．
The MAX1920 provides an adjustable output voltage （1．25V to 4V）．The MAX1921 provides factory－preset output voltages（see the Selector Guide）．Both are available in space－saving 6－pin SOT23 packages．The MAX1920 is also available in a 6－pin TDFN package．

## Applications

Next－Generation Wireless Handsets
PDAs，Palmtops，and Handy－Terminals
Battery－Powered Equipment
CDMA Power Amplifier Supply

Typical Operating Circuit

－ 400 mA Guaranteed Output Current
－Internal Synchronous Rectifier for＞90\％Efficiency
－Tiny 6－Pin SOT23 Package
－Available in 6－Pin TDFN Package（MAX1920）
－Up to 1.2 MHz Switching Frequency for Small External Components
－ $50 \mu \mathrm{~A}$ Quiescent Supply Current
－0．1 $\mu \mathrm{A}$ Logic－Controlled Shutdown
－2V to 5．5V Input Range
－Fixed 1．5V，1．8V，2．5V，3V，and 3．3V Output Voltages（MAX1921）
－Adjustable Output Voltage（MAX1920）
－$\pm 1.5 \%$ Initial Accuracy
－Soft－Start Limits Startup Current
Ordering Information

| PART | TEMP RANGE | PIN－PACKAGE |
| :--- | :--- | :--- |
| MAX1920EUT－T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 6 SOT23－6 |
| MAX1920EUT +T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 6 SOT23－ 6 |
| MAX1920ETT－T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 6 TDFN |
| MAX1920ETT +T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 6 TDFN |
| MAX1921EUT＿－-T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 6 SOT23－6 |
| MAX1921EUT＿+T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 6 SOT23－6 |

Note：The MAX1921 offers five preset output voltage options． See the Selector Guide，and then insert the proper designator into the blanks above to complete the part number． ＋Denotes lead－free package．

Pin Configuration

（）ARE FOR MAX1920 ONLY
A＂＋＂sign will replace the first pin indicator on lead－free packages．

## Low-Voltage, 400mA Step-Down DC-DC Converters in SOT23

## ABSOLUTE MAXIMUM RATINGS

| ND | V |
| :---: | :---: |
| OUT to AGND, LX to PGND . . . . . . . . . . . .-0.3 | to ( $\mathrm{IN}+0.3 \mathrm{~V}$ ) |
| AGND to PGND | -0.3V to +0.3V |
| OUT Short Circuit to GND | 10s |
| Continuous Power Dissipation ( $\mathrm{TA}=+70^{\circ} \mathrm{C}$ ) |  |
| 6-Pin SOT23-6 (derate $8.7 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $+70^{\circ} \mathrm{C}$ ) | 695mW |
|  |  |

Operating Temperature Range . . . . . . . . . . . . . . $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ Junction Temperature
$+150^{\circ} \mathrm{C}$
Storage Temperature . . . . . . . . . . . . . . . . . . . . $65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
Lead Temperature (soldering 10s) . . . . . . . . . . . . . . . . . $+300^{\circ} \mathrm{C}$

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## ELECTRICAL CHARACTERISTICS

$\left(\mathrm{V}\right.$ IN $=3.6 \mathrm{~V}, \overline{\mathrm{SHDN}}=\mathrm{IN}, \mathrm{T}_{\mathrm{A}}=0^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. Typical parameters are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted.) (Note 1)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Input Voltage Range | VIN | I(LX) < 400mA | 2.5 |  | 5.5 | V |
|  |  | $\begin{aligned} & I(L X)<200 \mathrm{~mA} \\ & (\text { MAX1921EUT15, MAX1921EUT18) } \end{aligned}$ | 2.0 |  | 2.5 |  |
| Startup Voltage |  |  |  |  | 2.0 | V |
| UVLO Threshold | UVLO | VIN rising |  | 1.85 | 1.95 | V |
|  |  | VIN falling | 1.50 | 1.65 |  |  |
| UVLO Hysteresis |  |  |  | 200 |  | mV |
| Quiescent Supply Current | IIN | No switching, no load |  | 50 | 70 | $\mu \mathrm{A}$ |
| Quiescent Supply Current Dropout | IIN | $\overline{\text { SHDN }}=1 \mathrm{~N}, \mathrm{OUT} / \mathrm{FB}=0$ |  | 220 | 300 | $\mu \mathrm{A}$ |
| Shutdown Supply Current | ISHDN | $\overline{\text { SHDN }}=$ GND |  | 0.1 | 4.0 | $\mu \mathrm{A}$ |
| Output Voltage Accuracy (MAX1921) |  | IOUT $=0, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | -1.5 |  | +1.5 | \% |
|  |  | Iout $=0$ to $400 \mathrm{~mA}, \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | -3 |  | +3 |  |
|  |  | Iout $=0$ to $200 \mathrm{~mA}, \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | -3 |  | +3 |  |
| OUT BIAS Current | IOUT | $\overline{\text { SHDN }}=0$ |  |  | 1 | $\mu \mathrm{A}$ |
|  |  | OUT at regulation voltage |  | 8 | 16 |  |
| Output Voltage Range (MAX1920) |  | Figure 4, $\mathrm{IN}=4.5 \mathrm{~V}$ | 1.25 |  | 4.00 | V |
| FB Feedback Threshold (MAX1920) | $V_{\text {FB }}$ | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 1.231 | 1.25 | 1.269 | V |
|  |  |  | 1.220 | 1.25 | 1.280 |  |
|  |  | $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 1.210 |  | 1.280 |  |
| FB Feedback Hysteresis (MAX1920) | VHYS |  |  | 5 |  | mV |
| FB Bias Current (MAX1920) | IfB | $\mathrm{FB}=1.5 \mathrm{~V}$ |  | 0.01 | 0.20 | $\mu \mathrm{A}$ |
| Load Regulation |  | Iout $=0$ to 400 mA |  | 0.005 |  | \%/mA |
| Line Regulation |  | $\mathrm{V} \mathrm{IN}=2.5 \mathrm{~V}$ to 5.5 V |  | 0.2 |  | \%/V |
| $\overline{\text { SHDN }}$ Input Voltage High | $\mathrm{V}_{\mathrm{IH}}$ |  | 1.6 |  |  | V |
| $\overline{\text { SHDN }}$ Input Voltage Low | VIL |  |  |  | 0.4 | V |
| $\overline{\text { SHDN Leakage Current }}$ | ISHDN | $\overline{\text { SHDN }}=$ GND or IN |  | 0.001 | 1.000 | $\mu \mathrm{A}$ |
| High-Side Current Limit | ILIMP |  | 525 | 730 | 950 | mA |

## Low-Voltage, 400mA Step-Down DC-DC Converters in SOT23

## ELECTRICAL CHARACTERISTICS (continued)

$\left(\mathrm{V} I \mathrm{~N}=3.6 \mathrm{~V}, \overline{\mathrm{SHDN}}=\mathrm{IN}, \mathrm{T}_{\mathrm{A}}=0^{\circ} \mathrm{C}\right.$ to $+85^{\circ} \mathrm{C}$. Typical parameters are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted.) (Note 1)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX |
| :--- | :---: | :--- | ---: | :---: | :---: | UNITS.

Note 1: All devices are $100 \%$ production tested at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$. Limits over the operating temperature range are guaranteed by design.

Typical Operating Characteristics
( $\mathrm{C}_{\mathrm{I}}=2.2 \mu \mathrm{~F}$ ceramic, Circuit of Figure 1, components of Table 1, unless otherwise noted.)


## Low-Voltage, 400mA Step-Down DC-DC Converters in SOT23

( $\mathrm{C}_{\mathrm{IN}}=2.2 \mu \mathrm{~F}$ ceramic, Circuit of Figure 1, components of Table 1, unless otherwise noted.)


MEDIUM-LOAD LINE-TRANSIENT RESPONSE


LIGHT-LOAD LINE-TRANSIENT RESPONSE


LOAD-TRANSIENT RESPONSE


# Low-Voltage, 400mA Step-Down DC-DC Converters in SOT23 

Pin Description

| PIN |  | NAME | FUNCTION |
| :---: | :---: | :---: | :---: |
| TDFN* | SO |  |  |
| 2 | 1 | IN | Supply voltage input for MAX1921EUT15 and MAX1921EUT18 is 2 V to 5.5 V . Supply voltage input for MAX1920 and other voltage versions of MAX1921 is 2.5 V to 5.5 V . Bypass IN to GND with a $2.2 \mu \mathrm{~F}$ ceramic capacitor as close to $I N$ as possible. |
| 6 | 2 | AGND | Analog Ground. Connect to PGND. |
| 1 | 3 | $\overline{\text { SHDN }}$ | Active-Low Shutdown Input. Connect $\overline{\text { SHDN }}$ to IN for normal operation. In shutdown, LX becomes high-impedance and quiescent current drops to $0.1 \mu \mathrm{~A}$. |
| - | 4 | OUT | MAX1921 Voltage Sense Input. OUT is connected to an internal voltage-divider. |
| 5 | 4 | FB | MAX1920 Voltage Feedback Input. FB regulates to 1.25 V nominal. Connect FB to an external resistive voltage-divider between the output voltage and GND. |
| 3 | 5 | PGND | Power Ground. Connect to AGND. |
| 4 | 6 | LX | Inductor Connection |

*MAX1920 only.

## Detailed Description

The MAX1920/MAX1921 step-down DC-DC converters deliver over 400 mA to outputs as low as 1.25 V . They use a unique proprietary current-limited control scheme that maintains extremely low quiescent supply current (50 A A), and their high 1.2 MHz (max) operating frequency permits small, low-cost external components.

## Control Scheme

The MAX1920/MAX1921 use a proprietary, current-limited control scheme to ensure high-efficiency, fast transient response, and physically small external components. This control scheme is simple: when the output voltage is out of regulation, the error comparator begins a switching cycle by turning on the high-side switch. This switch remains on until the minimum on-time of 400 ns expires and the output voltage regulates or the current-limit threshold is exceeded. Once off, the high-side switch remains off until the minimum off-time of 400ns expires and the output voltage falls out of regulation. During this period, the low-side synchronous rectifier turns on and


Figure 1. Typical Output Application Circuit (MAX1921)
remains on until either the high-side switch turns on again or the inductor current approaches zero. The internal synchronous rectifier eliminates the need for an external Schottky diode.
This control scheme allows the MAX1920/MAX1921 to provide excellent performance throughout the entire load-current range. When delivering light loads, the high-side switch turns off after the minimum on-time to reduce peak inductor current, resulting in increased efficiency and reduced output voltage ripple. When delivering medium and higher output currents, the MAX1920/MAX1921 extend either the on-time or the offtime, as necessary to maintain regulation, resulting in nearly constant frequency operation with high-efficiency and low-output voltage ripple.

Shutdown Mode
Connecting $\overline{\text { SHDN }}$ to GND places the MAX1920/ MAX1921 in shutdown mode and reduces supply current to $0.1 \mu \mathrm{~A}$. In shutdown, the control circuitry, internal switching MOSFET, and synchronous rectifier turn off and LX becomes high impedance. Connect $\overline{\text { SHDN }}$ to IN for normal operation.

Soft-Start
The MAX1920/MAX1921 have internal soft-start circuitry that limits current draw at startup, reducing transients on the input source. Soft-start is particularly useful for higher impedance input sources, such as Li+ and alkaline cells. Soft-start is implemented by starting with the current limit at $25 \%$ of its full current value and gradually increasing it in $25 \%$ steps until the full current limit is reached. See Soft-Start and Shutdown Response in the Typical Operating Characteristics.

# Low-Voltage, 400mA Step-Down DC-DC Converters in SOT23 

## Design Procedure

The MAX1920/MAX1921 are optimized for small external components and fast transient response. There are several application circuits (Figures 1 through 4) to allow the choice between ceramic or tantalum output capacitor and internally or externally set output voltages. The use of a small ceramic output capacitor is preferred for higher reliability, improved voltage-positioning transient response, reduced output ripple, and the smaller size and greater availability of ceramic versus tantalum capacitors.

Voltage Positioning
Figures 1 and 2 are the application circuits that utilize small ceramic output capacitors. For stability, the circuit obtains feedback from the LX node through R1, while load transients are fed-forward through CfF. Because there is no D.C. feedback from the output, the output voltage exhibits load regulation that is equal to the output load current multiplied by the inductor's series resistance. This small amount of load regulation is similar to voltage positioning as used by high-powered microprocessor supplies intended for personal computers. For the MAX1920/MAX1921, voltage positioning eliminates or greatly reduces undershoot and overshoot during load transients (see the Typical Operating Characteristics), which effectively halves the peak-to-peak output voltage excursions compared to traditional step-down converters.
For convenience, Table 1 lists the recommended external component values for use with the MAX1921 application circuit of Figure 1 with various input and output voltages.

Table 1. MAX1921 Suggested Components for Figure 1

| OUTPUT | INPUT SOURCE |  |  |
| :---: | :---: | :---: | :---: |
|  | 5 V | $3.3 \mathrm{~V}, 1 \mathrm{Li}+$, <br> $3 \times \mathrm{AA}$ | $2.5 \mathrm{~V}, 2 \times \mathrm{AA}$ |
|  |  |  |  |
| 3.0 V | $\mathrm{L}=10 \mu \mathrm{H}, \mathrm{COUT}=10 \mu \mathrm{~F}$, <br> $\mathrm{R} 1=8.25 \mathrm{k} \Omega, \mathrm{CFF}=3300 \mathrm{pF}$ | $\mathrm{N} / \mathrm{A}$ |  |
| 2.5 V | $\mathrm{L}=6.8 \mu \mathrm{H}, \mathrm{COUT}=6.8 \mu \mathrm{~F}$, <br> $\mathrm{R} 1=5.62 \mathrm{k} \Omega, \mathrm{CFF}=4700 \mathrm{pF}$ |  |  |
|  | $\mathrm{L}=10 \mu \mathrm{H}$, <br> 1.8 V <br> 1.5 V | $\mathrm{COUT}=10 \mathrm{FF}$, <br> $\mathrm{R} 1=8.25 \mathrm{k} \Omega$, <br> $\mathrm{CFF}=3300 \mathrm{pF}$ | $\mathrm{L}=4.7 \mu \mathrm{H}, \mathrm{COUT}=4.7 \mu \mathrm{~F}$, <br> $\mathrm{R} 1=4.75 \mathrm{k} \Omega, \mathrm{CFF}=5600 \mathrm{pF}$ |

## Inductor Selection

In order to calculate the smallest inductor, several calculations are needed. First, calculate the maximum duty cycle of the application as:

$$
\text { DutyCycle }(\mathrm{MAX})=\frac{\mathrm{V}_{\mathrm{OUT}}}{\mathrm{~V}_{\mathrm{IN}}(\mathrm{MIN})} \times 100 \%
$$

Second, calculate the critical voltage across the inductor as:

$$
\begin{aligned}
& \text { if DutyCycle }(\mathrm{MAX})<50 \% \text {, } \\
& \text { then } \mathrm{V}_{\text {CRITICAL }}=\left(\mathrm{VIN}(\mathrm{MIN})-\mathrm{VOUT}^{2}\right. \text {, } \\
& \text { else } \mathrm{V}_{\text {CRITICAL }}=\mathrm{V}_{\text {OUT }}
\end{aligned}
$$

Last, calculate the minimum inductor value as:

$$
\mathrm{L}(\mathrm{MIN})=2.5 \times 10^{-6} \times \mathrm{V}_{\mathrm{CRITICAL}}
$$

Select the next standard value larger than L(MIN). The $\mathrm{L}(\mathrm{MIN})$ calculation already includes a margin for inductance tolerance. Although values much larger than $\mathrm{L}(\mathrm{MIN})$ work, transient performance, efficiency, and inductor size suffer.
A 550 mA rated inductor is enough to prevent saturation for output currents up to 400 mA . Saturation occurs when the inductor's magnetic flux density reaches the maximum level the core can support and inductance falls. Choose a low DC-resistance inductor to improve efficiency. Tables 2 and 3 list some suggested inductors and suppliers.

Capacitor Selection
For nearly all applications, the input capacitor, CIN, may be as small as $2.2 \mu \mathrm{~F}$ ceramic with X 5 R or X7R
Table 2. Suggested Inductors

| PART NUMBER | $\underset{(\mu \mathrm{H})}{\mathrm{L}}$ | $\begin{gathered} R_{L} \\ \text { (ohms max) } \end{gathered}$ | Isat (A) | SIZE |
| :---: | :---: | :---: | :---: | :---: |
| Coilcraft <br> LPO1704 | 4.7 | 0.200 | 1.10 | $\begin{gathered} 6.6 \times 5.5 \times 1.0 \\ =36.3 \mathrm{~mm}^{3} \end{gathered}$ |
|  | 6.8 | 0.320 | 0.90 |  |
|  | 10 | 0.410 | 0.80 |  |
| $\begin{gathered} \text { Sumida } \\ \text { CDRH3D16 } \end{gathered}$ | 4.7 | 0.080 | 0.90 | $\begin{gathered} 3.8 \times 3.8 \times 1.8 \\ =26.0 \mathrm{~mm}^{3} \end{gathered}$ |
|  | 6.8 | 0.095 | 0.73 |  |
|  | 10 | 0.160 | 0.55 |  |
| Sumida CDRH2D18 | 4.7 | 0.081 | 0.63 | $\begin{gathered} 3.2 \times 3.2 \times 2.0 \\ =20.5 \mathrm{~mm}^{3} \end{gathered}$ |
|  | 6.8 | 0.108 | 0.57 |  |
| $\begin{aligned} & \text { Toko } \\ & \text { D312F } \end{aligned}$ | 4.7 | 0.38 | 0.74 | $\begin{gathered} 3.6 \times 3.6 \times 1.2 \\ =15.6 \mathrm{~mm}^{3} \end{gathered}$ |
|  | 10 | 0.79 | 0.50 |  |
| Toko D412F | 4.7 | 0.230 | 0.84 | $\begin{gathered} 4.6 \times 4.6 \times 1.2 \\ =25.4 \mathrm{~mm}^{3} \end{gathered}$ |
|  | 10 | 0.490 | 0.55 |  |
| TokoD52LC | 4.7 | 0.087 | 1.14 | $\begin{gathered} 5.0 \times 5.0 \times 2.0 \\ =50.0 \mathrm{~mm}^{3} \end{gathered}$ |
|  | 6.8 | 0.105 | 0.95 |  |
|  | 10 | 0.150 | 0.76 |  |

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dielectric．The input capacitor filters peak currents and noise at the voltage source and，therefore，must meet the input ripple requirements and voltage rating． Calculate the maximum RMS input current as：

$$
I_{I_{N}}(R M S)=I_{\text {OUT }}(M A X) \times \frac{\left.\sqrt{V_{\text {OUT }}\left(V_{\text {IN }}-V_{\text {OUT }}\right.}\right)}{V_{\text {IN }}}
$$

The output capacitor，COUT，may be either ceramic or tantalum depending upon the chosen application cir－ cuit（see Figures 1 through 4）．Table 3 lists some sug－ gested capacitor suppliers．

Ceramic Output Capacitor
For ceramic Cout，use the application circuit of Figure 1 or Figure 2．Calculate the minimum capacitor value as：

$$
\mathrm{C}_{\mathrm{OUT}}(\mathrm{MIN})=2.5 \times 10^{-6} \times \mathrm{V}_{\mathrm{CRITICAL}}
$$

Select the next standard value larger than Cout（MIN）． The Cout（MIN）calculation already includes a margin for capacitor tolerance．Values much larger than Cout（MIN）always improve transient performance and stability，but capacitor size and cost increase．


Figure 2．Typical Application Circuit（MAX1920）

Tantalum Output Capacitor
For tantalum COUT，use the application circuit of Figure 3 or Figure 4．With tantalum COUT，the equivalent series resistance（ESR）of Cout must be large enough for sta－ bility．Generally， 25 mV of ESR－ripple at the feedback node is sufficient．The simplified calculation is：

$$
\mathrm{ESR}_{\mathrm{COUT}}(\mathrm{MIN})=8.0 \times 10^{-2} \times \mathrm{V}_{\mathrm{OUT}}
$$

Because tantalum capacitors rarely specify minimum ESR，choose a capacitor with typical ESR that is about twice as much as ESRCOUT（MIN）．Although ESRs greater than this work，output ripple becomes larger．
For tantalum CoUT，calculate the minimum output capacitance as：

$$
\operatorname{CoUT}_{\text {OUI }}(\mathrm{MIN})=1.25 \times \frac{\mathrm{L} \times \mathrm{I}_{\mathrm{OUT}}(\mathrm{MAX})}{\mathrm{ESR}_{\text {COUT }}(\mathrm{MIN}) \times \mathrm{V}_{\text {CRITICAL }}}
$$

The 1.25 multiplier is for capacitor tolerance．Select any standard value larger than COUT（MIN）．

## Feedback and Compensation

The MAX1921 has factory preset output voltages of $1.5 \mathrm{~V}, 1.8 \mathrm{~V}, 2.5 \mathrm{~V}, 3 \mathrm{~V}$ ，and 3.3 V ，while the MAX1920 is externally adjusted by connecting FB to a resistive volt－ age－divider．When using a ceramic output capacitor， the feedback network must include a compensation feed－forward capacitor，CFF．


Figure 3．MAX1921 Application Circuit Using Tantalum Output Capacitor

# Low-Voltage, 400mA Step-Down DC-DC Converters in SOT23 

Table 3. Component Suppliers

| SUPPLIER |  | PHONE | WEBSITE |
| :--- | :--- | :---: | :---: |
| Coilcraft | $847-639-6400$ | www.coilcraft.com |  |
| Kemet | $408-986-0424$ | www.kemet.com |  |
| Murata | $814-237-1431$ | www.murata.com |  |
| Sumida | USA | $847-956-0666$ | www.sumida.com |
|  | Japan | $81-3-3607-5111$ |  |
| Taiyo <br> Yuden | USA | $408-573-4150$ | www.yuden.co.jp |
|  | Japan | $81-3-3833-5441$ |  |
| Toko | USA | $847-297-0070$ | www.toko.co.jp |
|  | Japan | $81-3-3727-1161$ |  |

MAX1921 Using Ceramic COUT
When using the application circuit of Figure 1, the inductor's series resistance causes a small amount of load regulation, as desired for a voltage-positioning load transient response. Choose R1 such that VOUT is high at no load by about half of this load regulation. The simplified calculation is:

$$
R 1=5 \times 10^{4} \times R_{L}(M A X)
$$

where $R_{L}(M A X)$ is the maximum series resistance of the inductor. Select a standard resistor value that is within $20 \%$ of this calculation.
Next, calculate CFF for 25 mV ripple at the internal feedback node. The simplified calculation is:

$$
C_{F F}=2.5 \times 10^{-5} / R 1
$$

where R1 is the standard resistor value that is used. Select a standard capacitor value that is within $20 \%$ of the calculated CFF.


Figure 4. MAX1920 Application Circuit Using Tantalum Output Capacitor

MAX1920 Using Ceramic Cout
When using the application circuit of Figure 2, the inductor's series resistance causes a small amount of load regulation, as desired for a voltage-positioning load transient response. Choose R1 and R2 such that VOUT is high at no load by about half of this load regulation:

$$
\mathrm{R} 1=\mathrm{R} 2 \times\left(\frac{\mathrm{V}_{\mathrm{OUT}}+\mathrm{R}_{\mathrm{L}} \times \mathrm{I}_{\mathrm{OUT}}(\mathrm{MAX}) / 2}{\mathrm{~V}_{\mathrm{REF}}}-1\right)
$$

where R 2 is chosen in the $50 \mathrm{k} \Omega$ to $500 \mathrm{k} \Omega$ range, $\mathrm{V}_{\mathrm{REF}}$ $=1.25 \mathrm{~V}$ and $R_{L}$ is the typical series resistance of the inductor. Use $1 \%$ or better resistors.
Next, calculate the equivalent resistance at the FB node as:

$$
R e q=R 1 \| R 2=\frac{R 1 \times R 2}{R 1+R 2}
$$

Then, calculate CFF for 25 mV ripple at FB. The simplified calculation is:

$$
\mathrm{C}_{\mathrm{FF}}=2.5 \times 10^{-5} / \mathrm{Req}
$$

Select a standard capacitor value that is within $20 \%$ of the calculated CFF.

MAX1920 Using Tantalum Cout
When using the application circuit of Figure 4, choose R1 and R2 such as to obtain the desired VOUT:

$$
\mathrm{R} 1=\mathrm{R} 2 \times\left(\frac{\mathrm{V}_{\mathrm{OUT}}}{\mathrm{~V}_{\mathrm{REF}}}-1\right)
$$

where R2 is chosen to be less than $50 \mathrm{k} \Omega$ and $\mathrm{V}_{\text {REF }}=$ 1.25V. Use $1 \%$ or better resistors.

## Layout Considerations

High switching frequencies make PC board layout a very important part of design. Good design minimizes excessive EMI on the feedback paths and voltage gradients in the ground plane, both of which can result in instability or regulation errors. Connect the inductor, input filter capacitor, and output filter capacitor as close to the device as possible, and keep their traces short, direct, and wide. Connect their ground pins at a single common node in a star ground configuration. The external voltage-feedback network should be very close to the FB pin, within 0.2in (5mm). Keep noisy traces, such as the LX trace, away from the voltagefeedback network; also keep them separate, using grounded copper. The MAX1920/MAX1921 evaluation kit data sheet includes a proper PC board layout and routing scheme.

# Low-Voltage, 400mA Step-Down DC-DC Converters in SOT23 

Selector Guide

| PART | Vout (V) | TOP MARK |
| :--- | :---: | :---: |
| MAX1920EUT | Adjustable | ABCO |
| MAX1920ETT | Adjustable | ADR |
| MAX1921EUT33 | 3.3 | ABCJ |
| MAX1921EUT30 | 3.0 | ABCK |
| MAX1921EUT25 | 2.5 | ABCL |
| MAX1921EUT18 | 1.8 | ABCM |
| MAX1921EUT15 | 1.5 | ABCN |

(The package drawing(s) in this data sheet may not reflect the most current specifications. For the latest package outline information, go to www.maxim-ic.com/packages.)


## Low-Voltage, 400mA Step-Down DC-DC Converters in SOT23

(The package drawing(s) in this data sheet may not reflect the most current specifications. For the latest package outline information, go to www.maxim-ic.com/packages.)

| COMMON DIMENSIONS |  |  |
| :---: | :---: | :---: |
| SYMBOL | MIN. | MAX. |
| A | 0.70 | 0.80 |
| D | 2.90 | 3.10 |
| E | 2.90 | 3.10 |
| A1 | 0.00 | 0.05 |
| L | 0.20 | 0.40 |
| k | 0.25 MIN. |  |
| A2 | 20 REF. |  |


| PACKAGE VARIATIONS |  |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PKG. CODE | N | D 2 | E 2 | e | JEDEC SPEC | b | $[(\mathrm{N} / 2)-1] \times \mathrm{e}$ | DOWNBONDS <br> ALLOWED |
| T633-1 | 6 | $1.50 \pm 0.10$ | $2.30 \pm 0.10$ | 0.95 BSC | MO229 / WEEA | $0.40 \pm 0.05$ | 1.90 REF | NO |
| T633-2 | 6 | $1.50 \pm 0.10$ | $2.30 \pm 0.10$ | 0.95 BSC | MO229 / WEEA | $0.40 \pm 0.05$ | 1.90 REF | NO |
| T833-1 | 8 | $1.50 \pm 0.10$ | $2.30 \pm 0.10$ | 0.65 BSC | MO229 / WEEC | $0.30 \pm 0.05$ | 1.95 REF | NO |
| T833-2 | 8 | $1.50 \pm 0.10$ | $2.30 \pm 0.10$ | 0.65 BSC | MO229 / WEEC | $0.30 \pm 0.05$ | 1.95 REF | NO |
| T833-3 | 8 | $1.50 \pm 0.10$ | $2.30 \pm 0.10$ | 0.65 BSC | MO229 / WEEC | $0.30 \pm 0.05$ | 1.95 REF | YES |
| T1033-1 | 10 | $1.50 \pm 0.10$ | $2.30 \pm 0.10$ | 0.50 BSC | MO229 / WEED -3 | $0.25 \pm 0.05$ | 2.00 REF | NO |
| T1433-1 | 14 | $1.70 \pm 0.10$ | $2.30 \pm 0.10$ | 0.40 BSC | --- | $0.20 \pm 0.05$ | 2.40 REF | YES |
| T1433-2 | 14 | $1.70 \pm 0.10$ | $2.30 \pm 0.10$ | 0.40 BSC | --- | $0.20 \pm 0.05$ | 2.40 REF | NO |

NOTES:

1. ALL DIMENSIONS ARE IN mm. ANGLES IN DEGREES.
2. COPLANARITY SHALL NOT EXCEED 0.08 mm .
3. WARPAGE SHALL NOT EXCEED 0.10 mm .
4. PACKAGE LENGTH/PACKAGE WIDTH ARE CONSIDERED AS SPECIAL CHARACTERISTIC(S).
5. DRAWING CONFORMS TO JEDEC MO229, EXCEPT DIMENSIONS "D2" AND "E2", AND T1433-1 \& T1433-2.
6. "N" IS THE TOTAL NUMBER OF LEADS.
7. NUMBER OF LEADS SHOWN ARE FOR REFERENCE ONLY.
-DRAWING NOT TO SCALE-


TILE PACKAGE OUTLINE, $6,8,10$ \& 14L, TDFN, EXPOSED PAD, $3 \times 3 \times 0$

| APROVN | DOCUMENTCONTROL No. $21-0137$ | $\stackrel{\stackrel{R}{\mathrm{ReV}} \mathrm{G}}{\mathrm{G}}$ | 2/2 |
| :---: | :---: | :---: | :---: |

## Low－Voltage，400mA Step－Down DC－DC Converters in SOT23

（The package drawing（s）in this data sheet may not reflect the most current specifications．For the latest package outline information， go to www．maxim－ic．com／packages．）


