



#### **Features**

### **General Description**

The MAX1748/MAX8726 triple-output DC-DC converters in a low-profile TSSOP package provide the regulated voltages required by active-matrix, thin-film transistor (TFT) liquid-crystal displays (LCDs). One high-power DC-DC converter and two low-power charge pumps convert the +3.3V to +5V input supply voltage into three independent output voltages.

The primary 1MHz DC-DC converter generates a boosted output voltage (VMAIN) up to 13V using ultra-small inductors and ceramic capacitors. The low-power BiCMOS control circuitry and the low on-resistance  $(0.35\Omega)$  of the integrated power MOSFET allows efficiency up to 93%.

The dual charge pumps independently regulate one positive output (VPOS) and one negative output (VNEG). These low-power outputs use external diode and capacitor stages (as many stages as required) to regulate output voltages up to +40V and down to -40V. A proprietary regulation algorithm minimizes output ripple, as well as capacitor sizes for both charge pumps.

For both the MAX1748 and MAX8726, the supply sequence is VMAIN first, VNEG next, and finally VPOS. The MAX1748 soft-starts each supply as soon as the previous supply finishes. The MAX8726 adds a delay between the startups of VMAIN and VNEG and also between VNFG and VPOS.

The MAX1748/MAX8726 are available in the ultra-thin TSSOP package (1.1mm max height).

- ♦ Three Integrated DC-DC Converters
- **♦ 1MHz Current-Mode PWM Boost Regulator** Up to +13V Main High-Power Output ±1% Accuracy High Efficiency (93%)
- **♦ Dual Charge-Pump Outputs** Up to +40V Positive Charge-Pump Output **Down to -40V Negative Charge-Pump Output**
- ♦ Internal Supply Sequencing
- **♦ Internal Power MOSFETs**
- ♦ +2.7V to +5.5V Input Supply
- ♦ 0.1µA Shutdown Current
- ♦ 0.6mA Quiescent Current
- ♦ Internal Soft-Start
- ♦ Power-Ready Output
- **♦ Ultra-Small External Components**
- ♦ Thin TSSOP Package (1.1mm max)

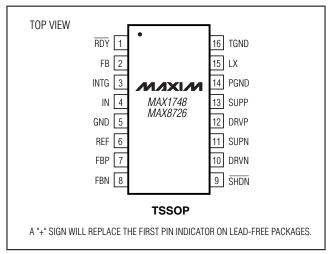
## **Ordering Information**

PART	TEMP RANGE	PIN-PACKAGE
MAX1748EUE	-40°C to +85°C	16 TSSOP
MAX8726EUE	-40°C to +85°C	16 TSSOP

## **Applications**

TFT Active-Matrix LCD Displays Passive-Matrix LCD Displays **PDAs** Digital Still Cameras Camcorders

## Pin Configuration



Typical Operating Circuit appears at end of data sheet.

Maxim Integrated Products 1

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#### **ABSOLUTE MAXIMUM RATINGS**

IN, SHDN, TGND to GND	0.3V to +6V
DRVN to GND	0.3V to (V <sub>SUPN</sub> + 0.3V)
DRVP to GND	-0.3V to (VSUPP + 0.3V)
PGND to GND	±0.3V
RDY to GND	0.3V to +14V
LX, SUPP, SUPN to PGND	0.3V to +14V
INTG, REF, FB, FBN, FBP to GND	0.3V to $(V_{IN} + 0.3V)$

Continuous Power Dissipation ( $T_A = +70^{\circ}$ C	C)
16-Pin TSSOP (derate 9.4mW/°C above	+70°C)755mW
Operating Temperature Range	
MAX1748EUE/MAX8726EUE	40°C to +85°C
Junction Temperature	+150°C
Storage Temperature Range	65°C to +150°C
Lead Temperature (soldering, 10s)	+300°C

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

#### **ELECTRICAL CHARACTERISTICS**

 $(V_{IN} = +3.0V, \overline{SHDN} = IN, V_{SUPP} = V_{SUPN} = 10V, TGND = PGND = GND, C_{REF} = 0.22 \mu F, C_{INTG} = 470 pF, T_A = 0°C to +85°C, unless otherwise noted. Typical values are at T_A = +25°C.)$ 

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
Input Supply Range	VIN		2.7		5.5	V
Input Undervoltage Threshold	V <sub>UVLO</sub>	V <sub>IN</sub> rising, 40mV hysteresis (typ)	2.2	2.4	2.6	V
IN Quiescent Supply Current	I <sub>IN</sub>	$V_{FB} = V_{FBP} = 1.5V$ , $V_{FBN} = -0.2V$		0.6	1	mA
SUPP Quiescent Current	ISUPP	V <sub>FBP</sub> = 1.5V		0.4	0.8	mA
SUPN Quiescent Current	ISUPN	$V_{FBN} = -0.1V$		0.4	0.8	mA
IN Shutdown Current		$V_{\overline{SHDN}} = 0$ , $V_{IN} = 5V$		0.1	10	μΑ
SUPP Shutdown Current		$V\overline{SHDN} = 0$ , $VSUPP = 13V$		0.1	10	μΑ
SUPN Shutdown Current		$V_{\overline{SHDN}} = 0$ , $V_{SUPN} = 13V$		0.1	10	μΑ
MAIN BOOST CONVERTER						
Output Voltage Range	V <sub>MAIN</sub>		VIN		13	V
FB Regulation Voltage	V <sub>FB</sub>	$T_A = 0$ °C to +85°C	1.235	1.248	1.261	V
FB Input Bias Current	I <sub>FB</sub>	V <sub>FB</sub> = 1.25V, INTG = GND	-50		+50	nA
Operating Frequency	fosc		0.85	1	1.15	MHz
Oscillator Maximum Duty Cycle			78	85	90	%
Load Regulation		I <sub>MAIN</sub> = 0 to 200mA, V <sub>MAIN</sub> = 10V		0.2		%
Line Regulation				0.1		%/V
Integrator Gm				320		μmho
LX Switch On-Resistance	R <sub>LX(ON)</sub>	$I_{LX} = 100mA$		0.35	0.7	Ω
LX Leakage Current	I <sub>L</sub> X	$V_{LX} = 13V$		0.01	20	μΑ
		Phase I = soft-start (1.0ms)	0.275	0.380	0.500	
LX Current Limit	livario	Phase II = soft-start (1.0ms)		0.75		^
LX Current Limit	I <sub>LX</sub> (MAX)	Phase III = soft-start (1.0ms)		1.12		А
		Phase IV = fully on (after 3.0ms)	1.1	1.5	2.0	
Maximum RMS LX Current				1		А
Soft-Start Period	tss	Power-up to the end of phase III		3072 / fosc		S
FB Fault Trip Level			1.07	1.1	1.14	V
POSITIVE CHARGE PUMP						
V <sub>SUPP</sub> Input Supply Range	VSUPP		2.7		13.0	V

## **ELECTRICAL CHARACTERISTICS (continued)**

 $(V_{IN} = +3.0V, \overline{SHDN} = IN, V_{SUPP} = V_{SUPN} = 10V, TGND = PGND = GND, C_{REF} = 0.22 \mu F, C_{INTG} = 470 pF, T_A = 0°C to +85°C, unless otherwise noted. Typical values are at T_A = +25°C.)$ 

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
Operating Frequency				0.5 x fosc		Hz
FBP Regulation Voltage	$V_{FBP}$		1.20	1.25	1.30	V
FBP Input Bias Current	I <sub>FBP</sub>	V <sub>FBP</sub> = 1.5V	-50		+50	nA
DRVP PCH On-Resistance				3	10	Ω
DRVP NCH On-Resistance		V <sub>FBP</sub> = 1.213V		1.5	4	Ω
DIVI NOITOII-Resistance		$V_{FBP} = 1.275V$	20			kΩ
FBP Power-Ready Trip Level		Rising edge	1.091	1.125	1.159	V
FBP Fault Trip Level		Falling edge		1.11		V
Maximum RMS DRVP Current				0.1		А
NEGATIVE CHARGE PUMP						
V <sub>SUPN</sub> Input Supply Range	VSUPN		2.7		13.0	V
Operating Frequency				0.5 x fosc		Hz
FBN Regulation Voltage	V <sub>FBN</sub>		-50	0	+50	mV
FBN Input Bias Current	I <sub>FBN</sub>	V <sub>FBN</sub> = -0.05V	-50		+50	nA
DRVN PCH On-Resistance				3	10	Ω
DDVALNOLLOs Decistoses		V <sub>FBN</sub> = 0.035V		1.5	4	Ω
DRVN NCH On-Resistance		$V_{FBN} = -0.025V$	20			kΩ
FBN Power-Ready Trip Level		Rising edge	80	110	165	mV
FBN Fault Trip Level		Falling edge		130		mV
Maximum RMS DRVN Current				0.1		А
REFERENCE						
Reference Voltage	V <sub>REF</sub>	-2μA < I <sub>REF</sub> < +50μA	1.231	1.25	1.269	V
Reference Undervoltage Threshold		V <sub>REF</sub> rising	0.9	1.05	1.2	V
LOGIC SIGNALS	_					
SHDN Input Low Voltage		0.4V hysteresis (typ)			0.9	V
SHDN Input High Voltage			2.1			V
SHDN Input Current	ISHDN			0.01	1	μΑ
RDY Output Low Voltage		I <sub>SINK</sub> = 2mA		0.25	0.5	V
RDY Output High Voltage		V <sub>RDY</sub> = 13V		0.01	1	μΑ



## **ELECTRICAL CHARACTERISTICS (continued)**

 $(V_{IN} = +3.0V, \overline{SHDN} = IN, V_{SUPP} = V_{SUPN} = 10V, TGND = PGND = GND, C_{REF} = 0.22 \mu F, C_{INTG} = 470 pF, T_A = -40 ^{\circ}C to +85 ^{\circ}C, unless otherwise noted.) (Note 1)$ 

PARAMETER	SYMBOL	CONDITIONS	MIN	MAX	UNITS
Input Supply Range	VIN		2.7	5.5	V
Input Undervoltage Threshold	V <sub>U</sub> VLO	V <sub>IN</sub> rising, 40mV hysteresis (typ)	2.2	2.6	V
IN Quiescent Supply Current	I <sub>IN</sub>	V <sub>FB</sub> = V <sub>FBP</sub> = 1.5V, V <sub>FBN</sub> = -0.2V		1	mA
SUPP Quiescent Current	ISUPP	V <sub>FBP</sub> = 1.5V		0.8	mA
SUPN Quiescent Current	ISUPN	V <sub>FBN</sub> = -0.1V		0.8	mA
IN Shutdown Current		$V_{\overline{SHDN}} = 0$ , $V_{IN} = 5V$		10	μΑ
SUPP Shutdown Current		VSHDN = 0, VSUPP = 13V		10	μΑ
SUPN Shutdown Current		VSHDN = 0, VSUPN = 13V		10	μΑ
MAIN BOOST CONVERTER					
Output Voltage Range	V <sub>MAIN</sub>		VIN	13.0	V
FB Regulation Voltage	V <sub>FB</sub>		1.222	1.271	V
FB Input Bias Current	I <sub>FB</sub>	V <sub>FB</sub> = 1.25V, INTG = GND	-50	+50	nA
Operating Frequency	Fosc		0.75	1.25	MHz
Oscillator Maximum Duty Cycle			78	90	%
LX Switch On-Resistance	R <sub>LX(ON)</sub>	I <sub>LX</sub> = 100mA		0.7	Ω
LX Leakage Current	ILχ	V <sub>L</sub> X = 13V		20	μΑ
17.0		Phase I = soft-start (1.0ms)	0.275	0.500	А
LX Current Limit	ILX(MAX)	Phase IV = fully on (after 3.0ms)	1.1	2.0	
FB Fault Trip Level			1.07	1.14	V
POSITIVE CHARGE PUMP			<u> </u>		
SUPP Input Supply Range	VSUPP		2.7	13.0	V
FBP Regulation Voltage	V <sub>FBP</sub>		1.20	1.30	V
FBP Input Bias Current	IFBP	V <sub>FBP</sub> = 1.5V	-50	+50	nA
DRVP PCH On-Resistance				10	Ω
DDVD NCH On Bosistanes		V <sub>FBP</sub> = 1.213V		4	Ω
DRVP NCH On-Resistance		V <sub>FBP</sub> = 1.275V	20		kΩ
FBP Power-Ready Trip Level		Rising edge	1.091	1.159	V
NEGATIVE CHARGE PUMP					
SUPN Input Supply Range	VSUPN		2.7	13.0	V
FBN Regulation Voltage	V <sub>FBN</sub>		-50	+50	mV
FBN Input Bias Current	I <sub>FBN</sub>	V <sub>FBN</sub> = -0.05V	-50	+50	nA
DRVN PCH On-Resistance				10	Ω
DD//N/N/CLL On D:-t		V <sub>FBN</sub> = 0.035V		4	Ω
DRVN NCH On-Resistance		V <sub>FBN</sub> = -0.025V	20		kΩ
FBN Power-Ready Trip Level		Rising edge	80	165	mV
REFERENCE					
Reference Voltage	V <sub>REF</sub>	-2μA < I <sub>REF</sub> < +50μA	1.223	1.269	V
Reference Undervoltage		V <sub>REF</sub> rising	0.9	1.2	V

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### **ELECTRICAL CHARACTERISTICS (continued)**

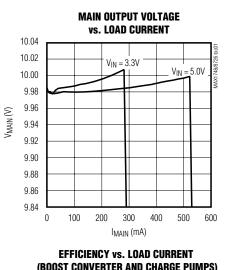
 $(V_{IN} = +3.0V, \overline{SHDN} = IN, V_{SUPP} = V_{SUPN} = 10V, TGND = PGND = GND, C_{REF} = 0.22\mu F, C_{INTG} = 470pF, T_A = -40^{\circ}C$  to +85°C, unless otherwise noted.) (Note 1)

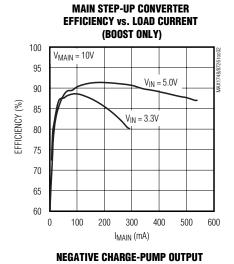
PARAMETER	SYMBOL	CONDITIONS	MIN	MAX	UNITS		
LOGIC SIGNALS							
SHDN Input Low Voltage		0.45V hysteresis (typ)		0.9	V		
SHDN Input High Voltage			2.1		V		
SHDN Input Current	ISHDN			1	μΑ		
RDY Output Low Voltage		I <sub>SINK</sub> = 2mA		0.5	V		
RDY Output High Leakage		$V_{\overline{RDY}} = 13V$		1	μΑ		

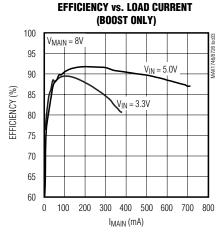
Note 1: Specifications from 0°C to -40°C are guaranteed by design, not production tested.

## **Typical Operating Characteristics**

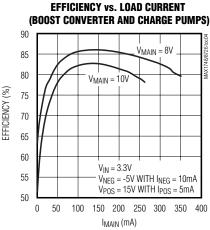
(Circuit of Figure 5,  $V_{IN} = 3.3V$ ,  $T_A = +25$ °C, unless otherwise noted.)

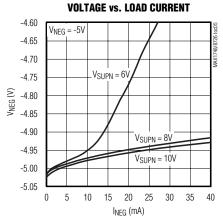


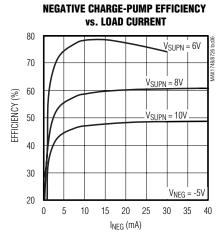




MAIN STEP-UP CONVERTER

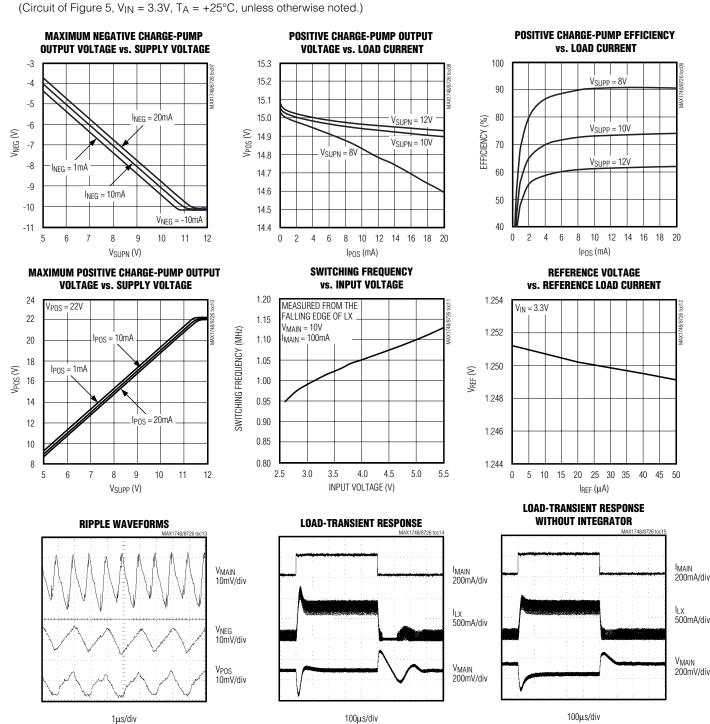






MIXIM

### Typical Operating Characteristics (continued)



 $V_{IN} = 3.3V$ ,  $V_{MAIN} = 10V$ ,

 $R_{MAIN} = 500\Omega \text{ TO } 50\Omega \text{ (20mA TO 200mA)}$ 

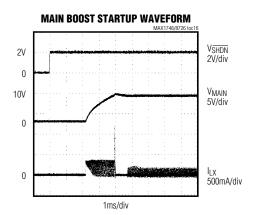
 $V_{IN} = 3.3V$ ,  $V_{MAIN} = 10V$ , INTG = REF,

 $R_{MAIN} = 500\Omega \text{ TO } 50\Omega \text{ (20mA TO 200mA)}$ 

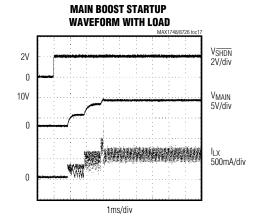
$$\begin{split} &V_{MAIN} = 10V, \ I_{MAIN} = 200 mA, \\ &V_{NEG} = -5V, \ I_{NEG} = 10 mA, \\ &V_{POS} = 15V, \ I_{POS} = 10 mA \end{split}$$

## Typical Operating Characteristics (continued)

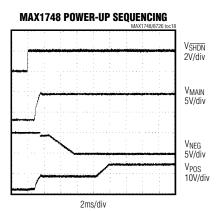
(Circuit of Figure 5,  $V_{IN}$  = 3.3V,  $T_A$  = +25°C, unless otherwise noted.)



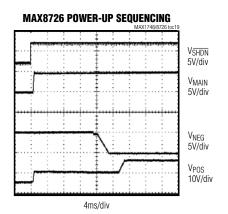
 $R_{MAIN}=1k\Omega,\,V_{MAIN}=10V$ 



 $V_{MAIN} = 10V$ ,  $R_{MAIN} = 50\Omega$  (200mA)



 $V_{MAIN} = 10V$ ,  $V_{NEG} = -5V$ ,  $V_{POS} = 15V$ 



 $V_{MAIN} = 10V$ ,  $V_{NEG} = -5V$ ,  $V_{POS} = 15V$ 

## **Pin Description**

PIN	NAME	FUNCTION
1	RDY	Active-Low, Open-Drain Output. Indicates all outputs are ready. The on-resistance is $125\Omega$ (typ).
2	FB	Main Boost Regulator Feedback Input. Regulates to 1.248V nominal. Connect feedback resistive divider to analog ground (GND).
3	INTG	Main Boost Integrator Output. If used, connect 470pF to analog ground (GND). To disable integrator, connect to REF.
4	IN	Supply Input. +2.7V to +5.5V input range. Bypass with a 0.1µF capacitor between IN and GND, as close to the pins as possible.
5	GND	Analog Ground. Connect to power ground (PGND) underneath the IC.
6	REF	Internal Reference Bypass Terminal. Connect a 0.22µF capacitor from this terminal to analog ground (GND). External load capability to 50µA.
7	FBP	Positive Charge-Pump Regulator Feedback Input. Regulates to 1.25V nominal. Connect feedback resistive divider to analog ground (GND).



### Pin Description (continued)

PIN	NAME	FUNCTION	
8	FBN	Negative Charge-Pump Regulator Feedback Input. Regulates to 0V nominal.	
9	SHDN	Active-Low Logic-Level Shutdown Input. Connect SHDN to IN for normal operation.	
10	DRVN	Negative Charge-Pump Driver Output. Output high level is V <sub>SUPN</sub> , and low level is PGND.	
11	SUPN	Negative Charge-Pump Driver Supply Voltage. Bypass to PGND with a 0.1µF capacitor.	
12	DRVP	Positive Charge-Pump Driver Output. Output high level is VSUPP, and low level is PGND.	
13	SUPP	Positive Charge-Pump Driver Supply Voltage. Bypass to PGND with a 0.1µF capacitor.	
14	PGND	Power Ground. Connect to GND underneath the IC.	
15	LX	Main Boost Regulator Power MOSFET n-Channel Drain. Connect output diode and output capacitor as close to PGND as possible.	
16	TGND	Must be connected to ground.	

### **Detailed Description**

The MAX1748/MAX8726 are highly efficient triple-output power supplies for TFT-LCD applications. These devices contain one high-power step-up converter and two low-power charge pumps. The primary boost converter uses an internal n-channel MOSFET to provide maximum efficiency and to minimize the number of external components. The output voltage of the main boost converter (VMAIN) can be set from VIN to 13V with external resistors.

The dual charge pumps independently regulate a positive output (VPOS) and a negative output (VNEG). These low-power outputs use external diode and capacitor stages (as many stages as required) to regulate output voltages up to +40V and down to -40V. A proprietary regulation algorithm minimizes output ripple as well as capacitor sizes for both charge pumps.

Also included in the MAX1748/MAX8726 is a precision 1.25V reference that sources up to  $50\mu\text{A}$ , logic shutdown, soft-start, power-up sequencing, fault detection, and an active-low open-drain ready output.

#### **Main Boost Converter**

The MAX1748/MAX8726 main step-up converter switches at a constant 1MHz internal oscillator frequency to allow the use of small inductors and output capacitors. The MOSFET switch pulse width is modulated to control the power transferred on each switching cycle and to regulate the output voltage.

During PWM operation, the internal clock's rising edge sets a flip-flop, which turns on the n-channel MOSFET (Figure 1). The switch turns off when the sum of the voltage-error, slope-compensation, and current-feedback signals trips the multi-input comparator and resets the flip-flop. The switch remains off for the rest of the clock cycle. Changes in the output-voltage error

signal shift the switch current trip level, consequently modulating the MOSFET duty cycle.

#### **Dual Charge-Pump Regulator**

The MAX1748/MAX8726 contain two individual low-power charge pumps. One charge pump inverts the supply voltage (SUPN) and provides a regulated negative output voltage. The second charge pump doubles the supply voltage (SUPP) and provides a regulated positive output voltage. The MAX1748/MAX8726 contain internal p-channel and n-channel MOSFETs to control the power transfer. The internal MOSFETs switch at a constant 500kHz (0.5 × fosc).

#### Negative Charge Pump

During the first half-cycle, the p-channel MOSFET turns on and the flying capacitor C5 charges to V<sub>SUPN</sub> minus a diode drop (Figure 2). During the second half-cycle, the p-channel MOSFET turns off, and the n-channel MOSFET turns on, level shifting C5. This connects C5 in parallel with the reservoir capacitor C6. If the voltage across C6 minus a diode drop is lower than the voltage across C5, charge flows from C5 to C6 until the diode (D5) turns off. The amount of charge transferred to the output is controlled by the variable n-channel on-resistance.

#### Positive Charge Pump

During the first half-cycle, the n-channel MOSFET turns on and charges the flying capacitor C3 (Figure 3). This initial charge is controlled by the variable n-channel on-resistance. During the second half-cycle, the n-channel MOSFET turns off and the p-channel MOSFET turns on, level shifting C3 by VSUPP volts. This connects C3 in parallel with the reservoir capacitor C4. If the voltage across C4 plus a diode drop (VPOS + VDIODE) is smaller than the level-shifted flying capacitor voltage (VC3 + VSUPP), charge flows from C3 to C4 until the diode (D3) turns off.

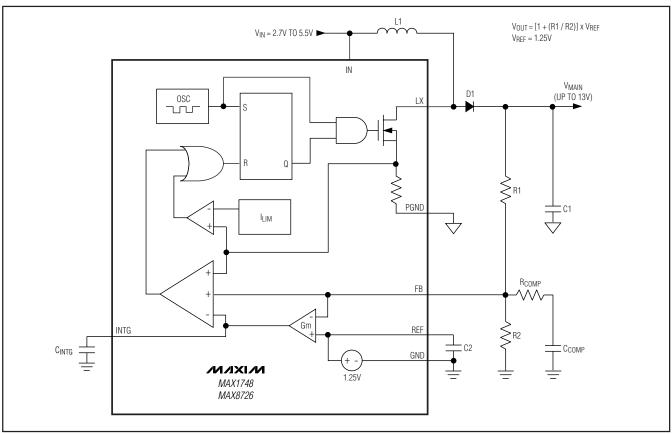


Figure 1. PWM Boost Converter Block Diagram

#### Soft-Start

For the main boost regulator, soft-start allows a gradual increase of the internal current-limit level during startup to reduce input surge currents. The MAX1748/MAX8726 divide the soft-start period into four phases. During phase 1, the MAX1748/MAX8726 limit the current limit to only 0.38A (see the *Electrical Characteristics* tables), approximately a quarter of the maximum current limit (ILX(MAX)). If the output does not reach regulation within 1ms, soft-start enters phase II and the current limit is increased by another 25%. This process is repeated for phase III. The maximum 1.5A (typ) current limit is reached at the end of phase III or when the output reaches regulation, whichever occurs first (see the startup waveforms in the *Typical Operating Characteristics*).

For the charge pumps, soft-start is achieved by controlling the rise rate of the output voltage. The output voltage regulates within 4ms, regardless of output capacitance and load, limited only by the regulator's output impedance.

#### Shutdown

A logic-low level on SHDN disables all three MAX1748/MAX8726 converters and the reference. When shut down, supply current drops to 0.1µA to maximize battery life and the reference is pulled to ground. The output capacitance and load current determine the rate at which each output voltage will decay. A logic-level high on SHDN power activates the MAX1748/MAX8726 (see the *Power-Up Sequencing* section). Do not leave SHDN floating. If unused, connect SHDN to IN.

#### **Power-Up Sequencing**

Upon power-up or exiting shutdown, the MAX1748 and MAX8726 start their respective power-up sequences.



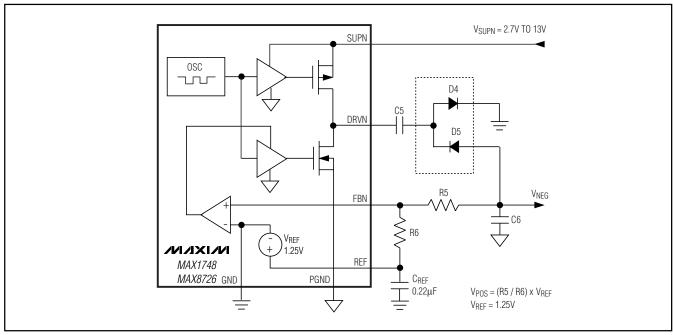


Figure 2. Negative Charge-Pump Block Diagram

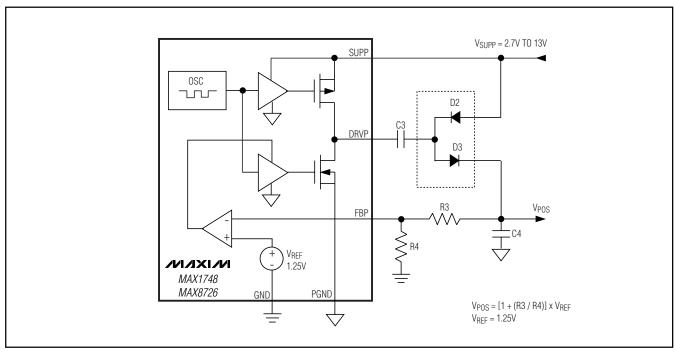


Figure 3. Positive Charge-Pump Block Diagram

In the MAX1748, the reference powers up first, then the main DC-DC step-up converter powers up with soft-start enabled. Once the main step-up converter reaches regulation, the negative charge pump turns on. When the negative output voltage reaches approximately 88% of its nominal value (VFBN < 110mV), the positive charge pump starts up. Finally, when the positive output voltage reaches 90% of its nominal value (VFBP > 1.125V), the active-low ready signal ( $\overline{\text{RDY}}$ ) goes low (see the *Power Ready* section).

In the MAX8726, the reference powers up first. After the reference is in regulation, the main DC-DC step-up converter powers up with soft-start enabled. The negative charge pump is enabled when the main step-up converter reaches regulation, and at least 16ms (typ) after the main step-up converter has been enabled. The positive charge pump is enabled when the negative output voltage reaches approximately 88% of its nominal value (VFBN < 110mV), and at least 4ms (typ) after the negative charge pump has been enabled. Finally, when the positive output voltage reaches 90% of its nominal value (VFBP > 1.125V), the active-low ready signal (RDY) goes low (see the *Power Ready* section).

#### **Power Ready**

Power ready is an open-drain output. When the power-up sequence is properly completed, the MOSFET turns on and pulls  $\overline{\text{RDY}}$  low with a typical 125 $\Omega$  on-resistance. If a fault is detected, the internal open-drain MOSFET appears as a high impedance. Connect a 100k $\Omega$  pullup resistor between  $\overline{\text{RDY}}$  and IN for a logic-level output.

#### Fault Detection

Once  $\overline{RDY}$  is low and if any output falls below its fault-detection threshold,  $\overline{RDY}$  goes high impedance.

For the reference, the fault threshold is 1.05V. For the main boost converter, the fault threshold is 88% of its nominal value ( $V_{FB} < 1.1V$ ). For the negative charge pump, the fault threshold is approximately 90% of its nominal value ( $V_{FBN} < 130 \text{mV}$ ). For the positive charge pump, the fault threshold is 88% of its nominal value ( $V_{FBP} < 1.11V$ ).

Once an output faults, all outputs later in the power sequence shut down until the faulted output rises above its power-up threshold. For example, if the negative charge-pump output voltage falls below the fault-detection threshold, the main boost converter remains active while the positive charge pump stops switching and its output voltage decays, depending on output capacitance and load. The positive charge-pump out-

put will not power up until the negative charge-pump output voltage rises above its power-up threshold (see the *Power-Up Sequencing* section).

#### **Voltage Reference**

The voltage at REF is nominally 1.25V. The reference can source up to 50µA with good load regulation (see the *Typical Operating Characteristics*). Connect a 0.22µF bypass capacitor between REF and GND.

### **Design Procedure**

### Main Boost Converter

#### Output Voltage Selection

Adjust the output voltage by connecting a voltage-divider from the output (V<sub>MAIN</sub>) to FB to GND (see the *Typical Operating Circuit*). Select R2 in the  $10k\Omega$  to  $20k\Omega$  range. Higher resistor values improve efficiency at low output current but increase output voltage error due to the feedback input bias current. Calculate R1 with the following equations:

$$R1 = R2 [(V_{MAIN} / V_{REF}) - 1]$$

where VREF = 1.25V. VMAIN can range from VIN to 13V.

#### Feedback Compensation

For stability, add a pole-zero pair from FB to GND in the form of a series resistor (R<sub>COMP</sub>) and capacitor (C<sub>COMP</sub>). The resistor should be half the value of the R2 feedback resistor.

#### **Inductor Selection**

Inductor selection depends on input voltage, output voltage, maximum current, switching frequency, size, and availability of inductor values. Other factors can include efficiency and ripple voltage. Inductors are specified by their inductance (L), peak current (IPEAK), and resistance (RL). The following boost-circuit equations are useful in choosing inductor values based on the application. They allow the trading of peak current and inductor value while allowing for consideration of component availability and cost.

The following equation includes a constant LIR, which is the ratio of the inductor peak-to-peak AC current to maximum average DC inductor current. A good compromise between the size of the inductor, loss, and output ripple is to choose an LIR of 0.3 to 0.5. The peak inductor current is then given by:

$$I_{PEAK} = \frac{I_{MAIN(MAX)} \times V_{MAIN}}{Efficiency \times V_{IN(MIN)}} \times [1 + (LIR/2)]$$



The inductance value is then given by:

$$L = \frac{{V_{IN(MIN)}}^2 \times Efficiency \times (V_{MAIN} - V_{IN(MIN)})}{{V_{(MAIN)}}^2 \times LIR \times I_{MAIN(MAX)} \times f_{OSC}}$$

Considering the typical operating circuit, the maximum DC load current (I<sub>MAIN(MAX)</sub>) is 200mA with a 10V output. A 6.8µH inductance value is then chosen, based on the above equations and using 85% efficiency and a 1MHz operating frequency. Smaller inductance values typically offer a smaller physical size for a given series resistance and current rating, allowing the smallest overall circuit dimensions. However, due to higher peak inductor currents, the output voltage ripple (I<sub>PEAK</sub> × output filter capacitor ESR) will be higher.

Use inductors with a ferrite core or equivalent; powder iron cores are not recommended for use with the MAX1748/MAX8726s' high switching frequencies. The inductor's maximum current rating should exceed IPEAK. Under fault conditions, inductor current may reach up to 2.0A. The MAX1748/MAX8726s' fast current-limit circuitry allows the use of soft-saturation inductors while still protecting the IC.

The inductor's DC resistance significantly affects efficiency. For best performance, select inductors with resistance less than the internal n-channel FET resistance. To minimize radiated noise in sensitive applications, use a shielded inductor.

The inductor should have as low a series resistance as possible. For continuous inductor current, the power loss in the inductor resistance, P<sub>LR</sub>, is approximated by:

$$P_{LR} \cong (I_{MAIN} \times V_{MAIN} / V_{IN})^2 \times R_L$$

where R<sub>L</sub> is the inductor series resistance.

#### **Output Capacitor**

A 10µF capacitor works well in most applications. The equivalent series resistance (ESR) of the output-filter capacitor affects efficiency and output ripple. Output voltage ripple is largely the product of the peak inductor current and the output capacitor ESR. Use low-ESR ceramic capacitors for best performance. Low-ESR, surface-mount tantalum capacitors with higher capacity may be used for load transients with high peak currents. Voltage ratings and temperature characteristics should be considered.

#### Input Capacitor

The input capacitor (C<sub>IN</sub>) in boost designs reduces the current peaks drawn from the input supply and reduces noise injection. The value of C<sub>IN</sub> is largely determined by the source impedance of the input supply. High source

impedance requires high input capacitance, particularly as the input voltage falls. Since step-up DC-DC converters act as "constant-power" loads to their input supply, input current rises as input voltage falls. A good starting point is to use the same capacitance value for  $C_{\text{IN}}$  as for  $C_{\text{OUT}}$ . Table 1 lists suggested component suppliers.

#### Integrator Capacitor

The MAX1748/MAX8726 contain an internal current integrator that improves the DC load regulation but increases the peak-to-peak transient voltage (see the load-transient waveforms in the *Typical Operating Characteristics*). For highly accurate DC load regulation, enable the current integrator by connecting a 470pF capacitor to INTG. To minimize the peak-to-peak transient voltage at the expense of DC regulation, disable the integrator by connecting INTG to REF and adding a 100k $\Omega$  resistor to GND.

#### Rectifier Diode

Use a Schottky diode with an average current rating equal to or greater than the peak inductor current, and a voltage rating at least 1.5 times the main output voltage (VMAIN).

**Table 1. Component Suppliers** 

SUPPLIER	PHONE	FAX				
INDUCTORS						
Coilcraft	847-639-6400	847-639-1469				
Coiltronics	561-241-7876	561-241-9339				
Sumida USA	847-956-0666	847-956-0702				
Toko	847-297-0070	847-699-1194				
CAPACITORS						
AVX	803-946-0690	803-626-3123				
Kemet	408-986-0424	408-986-1442				
Sanyo	619-661-6835	619-661-1055				
Taiyo Yuden	408-573-4150	408-573-4159				
DIODES	DIODES					
Central Semiconductor	516-435-1110	516-435-1824				
International Rectifier	310-322-3331	310-322-3332				
Motorola	602-303-5454	602-994-6430				
Nihon	847-843-7500	847-843-2798				
Zetex	516-543-7100	516-864-7630				

#### **Charge Pump**

#### **Efficiency Considerations**

The efficiency characteristics of the MAX1748/MAX8726 regulated charge pumps are similar to a linear regulator. They are dominated by quiescent current at low output currents and by the input voltage at higher output currents (see the *Typical Operating Characteristics*). So the maximum efficiency can be approximated by:

Efficiency  $\cong$  VNEG / [VIN  $\times$  N]; for the negative charge pump

Efficiency  $\cong$  VPOS / [VIN × (N + 1)]; for the positive charge pump

where N is the number of charge-pump stages.

#### **Output Voltage Selection**

Adjust the positive output voltage by connecting a voltage-divider from the output (VPOS) to FBP to GND (see the *Typical Operating Circuit*). Adjust the negative output voltage by connecting a voltage-divider from the output (VNEG) to FBN to REF. Select R4 and R6 in the  $50k\Omega$  to  $100k\Omega$  range. Higher resistor values improve efficiency at low output current but increase output-voltage error due to the feedback input bias current. Calculate the remaining resistors with the following equations:

R3 = R4 [(VPOS / VREF) - 1] R5 = R6 (VNEG / VREF)

where  $V_{REF} = 1.25V$ .  $V_{POS}$  can range from  $V_{SUPP}$  to 40V, and  $V_{NEG}$  can range from 0 to -40V.

#### Flying Capacitor

Increasing the flying capacitor's value reduces the output current capability. Above a certain point, increasing the capacitance has a negligible effect because the output current capability becomes dominated by the internal switch resistance and the diode impedance. Start with 0.1µF ceramic capacitors. Smaller values can be used for low-current applications.

### Charge-Pump Output Capacitor

Increasing the output capacitance or decreasing the ESR reduces the output ripple voltage and the peak-to-peak transient voltage. Use the following equation to approximate the required capacitor value:

Cout ≥ [lout / (500kHz × VRIPPLE)]

#### Charge-Pump Input Capacitor

Use a bypass capacitor with a value equal to or greater than the flying capacitor. Place the capacitor as close to the IC as possible. Connect directly to PGND.

#### Rectifier Diode

Use Schottky diodes with a current rating equal to or greater than 4 times the average output current, and a voltage rating at least 1.5 times V<sub>SUPP</sub> for the positive charge pump and V<sub>SUPN</sub> for the negative charge pump.

#### **PC Board Layout and Grounding**

Careful printed circuit layout is extremely important to minimize ground bounce and noise. First, place the main boost-converter output diode and output capacitor less than 0.2in (5mm) from the LX and PGND pins with wide traces and no vias. Then place 0.1µF ceramic bypass capacitors near the charge-pump input pins (SUPP and SUPN) to the PGND pin. Keep the chargepump circuitry as close to the IC as possible, using wide traces and avoiding vias when possible. Locate all feedback resistive dividers as close to their respective feedback pins as possible. The PC board should feature separate GND and PGND areas connected at only one point under the IC. To maximize output power and efficiency and to minimize output-power ripple voltage, use extra wide power ground traces and solder the IC's power ground pin directly to it. Avoid having sensitive traces near the switching nodes and high-current lines.

Refer to the MAX1748/MAX8726 evaluation kit for an example of proper board layout.

## \_Applications Information

#### Boost Converter Using a Cascoded MOSFET

For applications that require output voltages greater than 13V, cascode an external n-channel MOSFET (Figure 4). Place the MOSFET as close to the LX pin as possible. Connect the gate to the input voltage (VIN) and the source to LX.

#### **MOSFET Selection**

Choose a MOSFET with an on-resistance (RDS(ON)) lower than the internal n-channel MOSFET. Lower RDS(ON) will improve efficiency. The external n-channel MOSFET must have a drain-voltage rating higher than the main output voltage (VMAIN).

\_Chip Information

TRANSISTOR COUNT: 2846



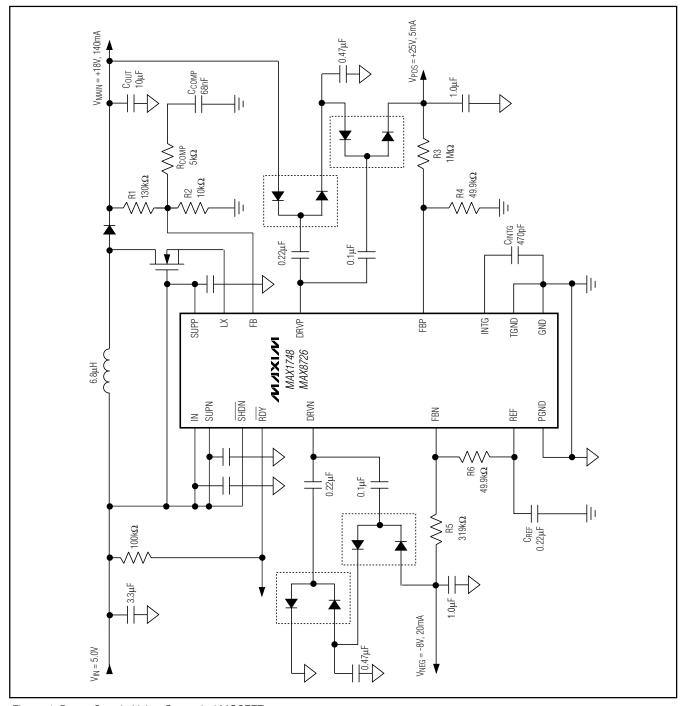
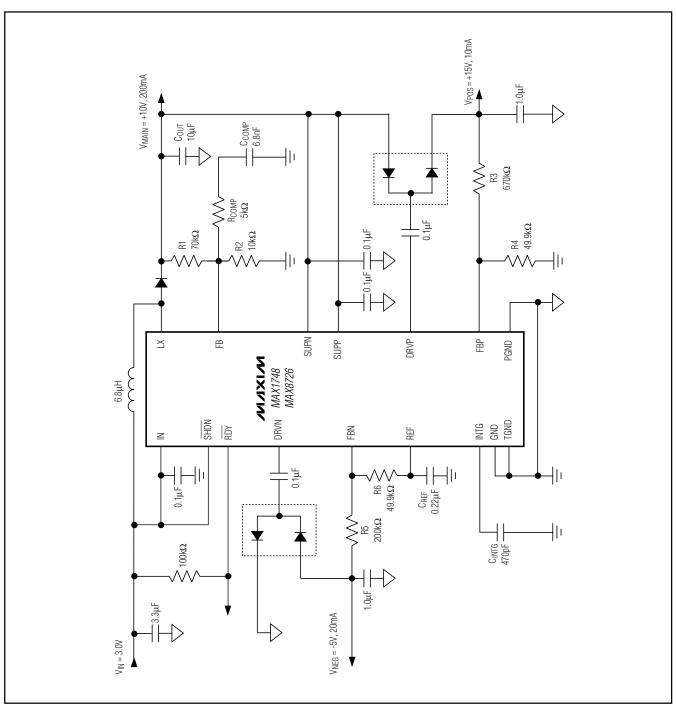


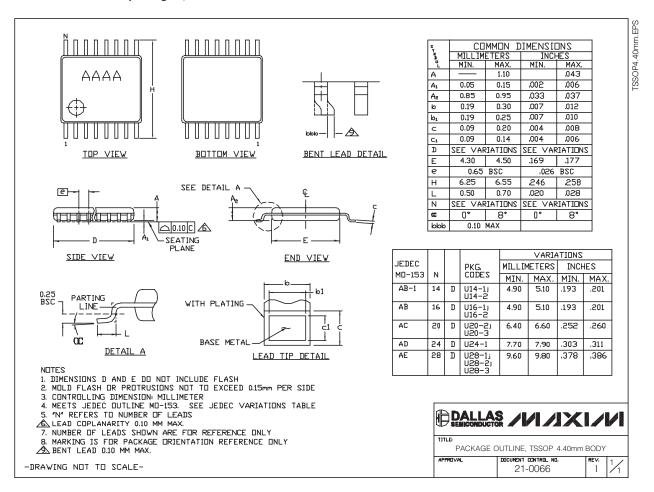
Figure 4. Power Supply Using Cascoded MOSFET

## **Typical Operating Circuit**



### **Package Information**

(The package drawing(s) in this data sheet may not reflect the most current specifications. For the latest package outline information, go to <a href="https://www.maxim-ic.com/packages">www.maxim-ic.com/packages</a>.)



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