## High Efficiency White LED Driver with Programmable Ambient Light Sensing Capability and I ${ }^{2}$ C-Compatible Interface

## General Description

The LM3530 current mode boost converter supplies the power and controls the current in up to 11 series white LED's. The 839 mA current limit and 2.7 V to 5.5 V input voltage range make the device a versatile backlight power source ideal for operation in portable applications.
The LED current is adjustable from 0 to 29.5 mA via an I2Ccompatible interface. The 127 different current steps and 8 different maximum LED current levels give over 1000 programmable LED current levels. Additionally, PWM brightness control is possible through an external logic level input.
The device also features two Ambient Light Sensor inputs. These are designed to monitor analog output ambient light sensors and provide programmable adjustment of the LED current with changes in ambient light. Each ambient light sensor input has independently programmable internal voltage setting resistors which can be made high impedance to reduce power during shutdown. The LM3530's 500 kHz switching frequency allows for high converter efficiency over a wide output voltage range accommodating from 2 to 11 series LEDs. Finally, the support of Content Adjusted Backlighting maximizes battery life while maintaining display image quality.
The LM3530 is available in a tiny 12 -bump ( $1.6 \mathrm{~mm} \times 1.2 \mathrm{~mm}$ $\times 0.425 \mathrm{~mm}$ ) micro SMD package and operates over the $-40^{\circ}$ C to $+85^{\circ} \mathrm{C}$ temperature range.

## Features

- Drives up to 11 LED's in series
- 1000:1 Dimming Ratio
- $90 \%$ Efficient
- Programmable Dual Ambient Light Sensor Inputs with internal ALS Voltage Setting Resistors
- I2C Programmable Logarithmic or Linear Brightness Control
- External PWM Input for Simple Brightness Adjustment
- True Shutdown Isolation for LED's and Ambient Light Sensors
- Internal Soft-Start Limits Inrush Current
- Wide 2.7V to 5.5V Input Voltage Range
- 40 V and 25 V Over-Voltage Protection Options
- 500 kHz Fixed Frequency Operation
- 839mA Peak Current Limit
- Low-Profile 12-bump micro SMD Package


## Applications

- Smartphone LCD Backlighting
- Personal Navigation LCD Backlighting
- 2 to 11 series White LED Backlit Display Power Source


## Typical Application Circuit



## LM3530 Layout Example



30086683

## Connection Diagram

Top View


## Ordering Information

| Order Number | Package Type | Supplied As | Lead Free? | Top Mark (2 lines: first line (XX) is date code and die run code, second line is voltage option) | Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| LM3530UME-25A NOPB | 12-Bump micro SMD | 250 units, Tape-andReel, No Lead | Yes | $\begin{aligned} & \hline \mathrm{XX} \\ & \mathrm{DS} \end{aligned}$ | 25V OVP, ${ }^{12}$ C Address 0x36 |
| LM3530UMX-25A NOPB | 12-Bump micro SMD | 3000 units, Tape-andReel, No Lead | Yes | $\begin{aligned} & \hline \mathrm{XX} \\ & \mathrm{DS} \end{aligned}$ | 25V OVP <br> ${ }^{12} \mathrm{C}$ Address 0x36 |
| LM3530UME-40 NOPB | 12-Bump micro SMD | 250 units, Tape-andReel, No Lead | Yes | $\begin{aligned} & \mathrm{XX} \\ & 40 \end{aligned}$ | 40V OVP <br> I2C Address. 0x38 |
| LM3530UMX-40 NOPB | 12-Bump micro SMD | 3000 units, Tape-andReel, No Lead | Yes | $\begin{aligned} & \hline X X \\ & 40 \end{aligned}$ | 40V OVP I2C Address 0x38 |
| LM3530UME-40B NOPB | 12-Bump micro SMD | 250 units, Tape-and- <br> Reel, No Lead | Yes | $\begin{aligned} & \hline \text { XX } \\ & \text { DT } \end{aligned}$ | 40V OVP I2C Address 0x39 |
| LM3530UMX-40B NOPB | 12-Bump micro SMD | 3000 units, Tape-andReel, No Lead | Yes | $\begin{aligned} & \hline \text { XX } \\ & \text { DT } \end{aligned}$ | 40V OVP <br> I2C Address 0x39 |

## Pin Descriptions/Functions

| Pin | Name | Description |
| :---: | :--- | :--- |
| C3 | IN | Input Voltage Connection. Connect a 2.7 V to 5.5 V supply to IN and bypass to GND with a $2.2 \mu \mathrm{~F}$ <br> or greater ceramic capacitor. |
| D2 | OVP | Output Voltage Sense Connection for Over-Voltage Sensing. Connect OVP to the positive <br> terminal of the output capacitor. |
| A3 | SW | Inductor Connection, Diode Anode Connection, and Drain Connection for Internal NFET. <br> Connect the inductor and diode as close as possible to SW to reduce parasitic inductance and <br> capacitive coupling to nearby traces. |
| D3 | ILED | Input Terminal to Internal Current Sink. The boost converter regulates ILED to 0.4V. |
| D1 | ALS1 | Ambient Light Sensor Input \#1 with Programmable Internal Pull-down Resistor. |
| A1 | SDA | Serial Data Connection for I²C-Compatible Interface. |
| A2 | SCL | Serial Clock Connection for IC-Compatible Interface. |
| B3 | GND | Ground |
| C1 | ALS2 | Ambient Light Sensor Input \#2 with Programmable Internal Pull-down Resistor. |
| B1 | PWM | External PWM Brightness Control Input and Simple Enable Input. |
| B2 | INT | Logic Interrupt Output Signaling the ALS Zone Has Changed. |
| C2 | HWEN | Active High Hardware Enable (Active Low Reset). Pull this pin high to enable the LM3530. |

## Absolute Maximum Ratings <br> (Note 1, Note <br> 2) <br> If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/ Distributors for availability and specifications.

| $\mathrm{V}_{\text {IN }}$ to GND | -0.3 V to +6 V |
| :---: | :---: |
| $\mathrm{V}_{\text {SW }}, \mathrm{V}_{\text {OVP }}, \mathrm{V}_{\text {ILED }}$ to GND | -0.3V to 45V |
| $\begin{aligned} & \mathrm{V}_{\mathrm{SCL}}, \mathrm{~V}_{\mathrm{SDA}}, \mathrm{~V}_{\mathrm{ALS} 1}, \mathrm{~V}_{\mathrm{PWM}}, \mathrm{~V}_{\mathrm{INT}}, \\ & \mathrm{~V}_{\text {HWEN }} \text { to } G N D \end{aligned}$ | -0.3 V to +6 V |
| $\mathrm{V}_{\text {ALS } 2}$ to GND | -0.3V to $\mathrm{V}_{\text {IN }}+0.3 \mathrm{~V}$ |
| Continuous Power Dissipation | Internally Limited |
| Junction Temperature ( $\mathrm{J}_{\mathrm{J} \text {-max }}$ ) | $+150^{\circ} \mathrm{C}$ |
| Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Maximum Lead Temperature (Soldering, 10s) | (Note 3) |
| ESD Rating (Note 9) Human |  |
| Body Model | 2.0kV |

Operating Ratings (Note 1, Note 2)

| V $_{\text {IN }}$ to GND | 2.7 V to 5.5 V |
| :--- | ---: |
| $\mathrm{~V}_{\text {SW }}, \mathrm{V}_{\text {OVP }}, \mathrm{V}_{\text {ILED }}$, to GND | 0 to +40 V |
| Junction Temperature Range | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| $\left(\mathrm{T}_{\mathrm{J}}\right)($ Note 4) |  |
| Ambient Temperature Range | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| $\left(\mathrm{T}_{\mathrm{A}}\right)$ (Note 5) |  |

## Thermal Properties

Junction to Ambient Thermal
$61.7^{\circ} \mathrm{C} / \mathrm{W}$
Resistance ( $\mathrm{T}_{\text {JA }}$ )(Note 6)

## ESD Caution Notice

National Semiconductor recommends that all integrated circuits be handled with appropriate ESD precautions. Failure to observe proper ESD handling techniques can result in damage to the device.

## Electrical Characteristics (Note 2, Note 7)

Limits in standard type face are for $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ and those in boldface type apply over the full operating ambient temperature range $\left(-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C}\right)$. Unless otherwise specified $\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}$.

| Symbol | Parameter | Conditions |  | Min | Typ | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| lied | Output Current Regulation | $2.7 \mathrm{~V} \geq \mathrm{V}_{\mathrm{IN}} \geq 5.5 \mathrm{~V}$, Full-Scale Current $=19 \mathrm{~mA}$, BRT Code $=$ 0x7F, ALS Select Bit = 0, I2C Enable = 1 |  | 17.11 | 18.6 | 20.08 | mA |
| $\mathrm{V}_{\text {REG_CS }}$ | Regulated Current Sink Headroom Voltage |  |  |  | 400 |  | mV |
| $\mathrm{V}_{\mathrm{HR}}$ | Current Sink Minimum Headroom Voltage | ${ }^{\text {LED }}$ = 95\% of nominal |  |  | 200 |  | mV |
| $\mathrm{R}_{\text {DSON }}$ | NMOS Switch On Resistance | $\mathrm{I}_{\mathrm{sw}}=100 \mathrm{~mA}$ |  |  | 0.25 |  | $\Omega$ |
| $\mathrm{I}_{\mathrm{CL}}$ | NMOS Switch Current Limit | $2.7 \mathrm{~V} \leq \mathrm{V}_{\mathrm{IN}} \leq 5.5 \mathrm{~V}$ <br> Note: (Note 10) |  | 739 | 839 | 936 | mA |
| $\mathrm{V}_{\text {ovp }}$ | Output Over-Voltage <br> Protection | ON Threshold,$\begin{aligned} & 2.7 \mathrm{~V} \leq \mathrm{V}_{\text {IN }} \leq \\ & 5.5 \mathrm{~V} \end{aligned}$ | 40 V version | 40 | 41 | 42 |  |
|  |  |  | 25 V version | 23.6 | 24 | 24.6 | V |
|  |  | Hysteresis |  |  | 1 |  |  |
| $\mathrm{f}_{\text {Sw }}$ | Switching Frequency | $2.7 \mathrm{~V} \leq \mathrm{V}_{\mathrm{IN}} \leq 5.5 \mathrm{~V}$ |  | 450 | 500 | 550 | kHz |
| $\mathrm{D}_{\text {MAX }}$ | Maximum Duty Cycle |  |  |  | 94 |  | \% |
| $\mathrm{D}_{\text {MIN }}$ | Minimum Duty Cycle |  |  |  | 10 |  | \% |
| $\mathrm{I}_{\mathrm{Q}}$ | Quiescent Current, Device Not Switching | $\mathrm{V}_{\text {HWEN }}=\mathrm{V}_{\text {IN }}$ |  |  | 490 | 600 | $\mu \mathrm{A}$ |
| $\underline{\mathrm{I}_{\text {Q_S }}}$ | Switching Supply Current | $\mathrm{I}_{\text {LED }}=19 \mathrm{~mA}, \mathrm{~V}_{\text {OUT }}=36 \mathrm{~V}$ |  |  | 1.35 |  | mA |
| $\mathrm{I}_{\text {SHDN }}$ | Shutdown Current | $\begin{aligned} & \mathrm{V}_{\text {HWEN }}=\mathrm{GND}, 2.7 \mathrm{~V} \geq \mathrm{V}_{\mathrm{IN}} \geq \\ & 5.5 \mathrm{~V} \end{aligned}$ |  |  | 1 | 2 | $\mu \mathrm{A}$ |
| $\mathrm{I}_{\text {LED_MIN }}$ | Minimum LED Current | $\begin{aligned} & \hline \begin{array}{l} \text { Full-Scale Current }=19 \mathrm{~mA} \\ \text { setting } \\ \text { BRT }=0 \times 01 \\ \hline \end{array}{ }^{2} \\ & \hline \end{aligned}$ |  |  | 9.5 |  | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\text {ALS }}$ | Ambient Light Sensor Reference Voltage | $2.7 \mathrm{~V} \geq \mathrm{V}_{\text {IN }} \geq 5.5 \mathrm{~V}$ ( Note 11) |  | 0.97 | 1 | 1.03 | V |


| Symbol | Parameter | Conditions | Min | Typ | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {HWEN }}$ | Logic Thresholds - Logic Low |  | 0 |  | 0.4 | V |
|  | Logic Thresholds - Logic High |  | 1.2 |  | $\mathrm{V}_{\mathrm{IN}}$ |  |
| $\overline{T_{S D}}$ | Thermal Shutdown |  |  | +140 |  | ${ }^{\circ} \mathrm{C}$ |
|  | Hysteresis |  |  | 15 |  |  |
| RALS1, RALS2 | ALS Input Internal Pull-down Resistors | $2.7 \mathrm{~V} \geq \mathrm{V}_{\text {IN }} \geq 5.5 \mathrm{~V}$ | 12.77 | 13.531 | 14.29 | $\mathrm{k} \Omega$ |
|  |  |  | 8.504 | 9.011 | 9.518 |  |
|  |  |  | 5.107 | 5.411 | 5.715 |  |
|  |  |  | 2.143 | 2.271 | 2.399 |  |
|  |  |  | 1.836 | 1.946 | 2.055 |  |
|  |  |  | 1.713 | 1.815 | 1.917 |  |
|  |  |  | 1.510 | 1.6 | 1.69 |  |
|  |  |  | 1.074 | 1.138 | 1.202 |  |
|  |  |  | 0.991 | 1.050 | 1.109 |  |
|  |  |  | 0.954 | 1.011 | 1.068 |  |
|  |  |  | 0.888 | 0.941 | 0.994 |  |
|  |  |  | 0.717 | 0.759 | 0.802 |  |
|  |  |  | 0.679 | 0.719 | 0.760 |  |
|  |  |  | 0.661 | 0.700 | 0.740 |  |
|  |  |  | 0.629 | 0.666 | 0.704 |  |
| Logic Voltage Specifications (SCL, SDA, PWM, INT) |  |  |  |  |  |  |
| $\mathrm{V}_{\text {IL }}$ | Input Logic Low | $2.7 \mathrm{~V} \leq \mathrm{V}_{\text {IN }} \leq 5.5 \mathrm{~V}$ | 0 |  | 0.54 | V |
| $\mathrm{V}_{\mathrm{IH}}$ | Input Logic High | $2.7 \mathrm{~V} \leq \mathrm{V}_{\text {IN }} \leq 5.5 \mathrm{~V}$ | 1.26 |  | $\mathrm{V}_{\mathrm{IN}}$ | V |
| $\mathrm{V}_{\mathrm{OL}}$ | Output Logic Low (SDA, INT) | $\mathrm{I}_{\text {LOAD }}=3 \mathrm{~mA}$ |  |  | 400 | mV |
| 12C-Compatible Timing Specifications (SCL, SDA) (Note 8) |  |  |  |  |  |  |
| $\mathrm{t}_{1}$ | SCL (Clock Period) |  | 2.5 |  |  | $\mu \mathrm{s}$ |
| $\mathrm{t}_{2}$ | Data In Setup Time to SCL High |  | 100 |  |  | ns |
| $\mathrm{t}_{3}$ | Data Out Stable After SCL Low |  | 0 |  |  | ns |
| $\mathrm{t}_{4}$ | SDA Low Setup Time to SCL <br> Low (Start) |  | 100 |  |  | ns |
| $\mathrm{t}_{5}$ | SDA High Hold Time After SCL High (Stop) |  | 100 |  |  | ns |
| Simple Interface (PWM pin) |  |  |  |  |  |  |
| $\mathrm{t}_{\text {PWM_HIGH }}$ | Enable time, PWM pin must be held high |  | 1.5 | 2 | 2.6 | ms |
| tewm_Low | Disable time, PWM pin must be held low |  | 1.48 | 2 | 2.69 |  |

Note 1: Absolute Maximum Ratings are limits beyond which damage to the device may occur. Operating Ratings are conditions for which the device is intended to be functional, but device parameter specifications may not be guaranteed. For guaranteed specifications and test conditions, see the Electrical Characteristics table.
Note 2: All voltages are with respect to the potential at the GND pin.
Note 3: For detailed soldering specifications and information, please refer to National Semiconductor Application Note 1112: Micro SMD Wafer Level Chip Scale Package (AN-1112), available at www.national.com.
Note 4: Internal thermal shutdown circuitry protects the device from permanent damage. Thermal shutdown engages at $\mathrm{T}_{\mathrm{J}}=+140^{\circ} \mathrm{C}$ (typ.) and disengages at $\mathrm{T}_{\mathrm{J}}=+125^{\circ} \mathrm{C}$ (typ.).
Note 5: In applications where high power dissipation and/or poor package thermal resistance is present, the maximum ambient temperature may have to be derated. Maximum ambient temperature $\left(\mathrm{T}_{\mathrm{A}-\mathrm{MAX}}\right)$ is dependent on the maximum operating junction temperature $\left(\mathrm{T}_{\mathrm{J}} \mathrm{MAX}\right.$-OP $=+125^{\circ} \mathrm{C}$ ), the maximum power dissipation of the device in the application ( $\mathrm{P}_{\mathrm{D}-\mathrm{MAX}}$ ), and the junction-to ambient thermal resistance of the part/package in the application ( $\theta_{\mathrm{JA}}$ ), as given by the following equation: $T_{A-M A X}=T_{J-M A X-O P}-\left(\theta_{J A} \times P_{D-M A X}\right)$.
Note 6: Junction-to-ambient thermal resistance $\left(\theta_{\mathrm{JA}}\right)$ is taken from a thermal modeling result, performed under the conditions and guidelines set forth in the JEDEC standard JESD51-7. The test board is a 4-layer FR-4 board measuring $102 \mathrm{~mm} \times 76 \mathrm{~mm} \times 1.6 \mathrm{~mm}$ with a $2 \times 1$ array of thermal vias. The ground plane on the board is $50 \mathrm{~mm} \times 50 \mathrm{~mm}$. Thickness of copper layers are $36 \mu \mathrm{~m} / 18 \mu \mathrm{~m} / 18 \mu \mathrm{~m} / 36 \mu \mathrm{~m}(1.5 \mathrm{oz} / 1 \mathrm{oz} / 1 \mathrm{oz} / 1.5 \mathrm{oz})$. Ambient temperature in simulation is $22^{\circ} \mathrm{C}$ in still air. Power dissipation is 1 W . The value of $\theta_{\mathrm{JA}}$ of this product in the micro SMD package could fall in a range as wide as $60^{\circ} \mathrm{C} / \mathrm{W}$ to $110^{\circ} \mathrm{C} / \mathrm{W}$ (if not wider), depending on PCB material, layout, and environmental conditions. In applications where high maximum power dissipation exists special care must be paid to thermal dissipation issues.
Note 7: Min and Max limits are guaranteed by design, test, or statistical analysis. Typical (typ.) numbers are not guaranteed, but represent the most likely norm. Note 8: SCL and SDA must be glitch-free in order for proper brightness control to be realized.
Note 9: The human body model is a 100 pF capacitor discharged through $1.5 \mathrm{k} \Omega$ resistor into each pin. (MIL-STD-883 3015.7).
Note 10: The value for current limit given in the Electrical Table is measured in an open loop test by forcing current into SW until the current limit comparator threshold is reached. The typical curve for current limit is measured in closed loop using the typical application circuit by increasing IOUT until the peak inductor current stops increasing. Closed loop data appears higher due to the delay between the comparator trip point and the NFET turning off. This delay allows the closed loop inductor current to ramp higher after the trip point by approximately $100 \mathrm{~ns} \times$ VIN/L
Note 11: The ALS voltage specification is the maximum trip threshold for the ALS zone boundary (Code 0xFF). Due to random offsets and the mechanism for which the hysteresis voltage varies, it is recommended that only Codes $0 \times 04$ and above be used for Zone Boundary Thresholds. See Zone Boundary Trip Points and Hysteresis and Minimum Zone Boundary Settings sections.

## Timing Diagrams



FIGURE 1. ${ }^{2} \mathrm{C}$-Compatible Timing


FIGURE 2. Simple Enable/Disable Timing

Typical Performance Characteristics $\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}$, LEDs are OVSRWAC1R6 from OPTEK Technology, $C_{\text {OUT }}=1 \mu \mathrm{~F}, \mathrm{C}_{\text {IN }}=1 \mu \mathrm{~F}, \mathrm{~L}=$ TDK VLF5012ST-100M1R0, $\left(\mathrm{R}_{\mathrm{L}}=0.24 \Omega\right)$, $\mathrm{L}_{\mathrm{LED}}=19 \mathrm{~mA}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ unless otherwise specified.


30086651


30086653

Efficiency vs $\mathrm{I}_{\text {LED }}\left(\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}\right)$


30086654


30086652


Efficiency vs $\mathrm{ILED}\left(\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}\right)$


## LED Current vs $\mathrm{V}_{\mathrm{IN}}$ (19mA Full-Scale Setting)



30086675


30086657

Internal ALS Resistor vs $\mathrm{V}_{\mathrm{IN}}\left(\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}\right)$ ALS Resistor Select Register $=0 \times 44$


Shutdown Current vs $\mathrm{V}_{\mathrm{IN}}$



30086658

## Current Limit vs $\mathrm{V}_{\mathrm{IN}}($ Closed Loop, $\mathbf{L}=\mathbf{2 2 \mu} \mathbf{H}$ (Note 10))



30086673

Over Voltage Protection vs $\mathrm{V}_{\text {IN }}\left(\mathrm{V}_{\text {OUT }}\right.$ Rising)


30086660


30086678


30086680


Switching Frequency vs $\mathbf{V}_{\mathbf{I N}}$


30086677


30086699

## Ramp Rate (Exponential) (2.048ms/step up and down)



Channel 2: SDA (5V/div)
Channel 3: ILED (10mA/div)
Time Base ( $100 \mathrm{~ms} / \mathrm{div}$ )

## Ramp Rate (Exponential)

 ( $8.192 \mathrm{~ms} / \mathrm{step}$ up and down)

30086692
Channel 2: SDA (5V/div)
Channel 3: ILED (10mA/div)
Time Base ( $400 \mathrm{~ms} / \mathrm{div}$ )


30086689
Channel 2: SDA (5V/div)
Channel 3: ILED (10mA/div)
Time Base ( $40 \mathrm{~ms} / \mathrm{div}$ )


Channel 2: SDA (5V/div)
Channel 3: ILED ( $10 \mathrm{~mA} / \mathrm{div}$ )
Time Base ( $200 \mathrm{~ms} /$ div)

## Ramp Rate (Exponential)

 ( $16.384 \mathrm{~ms} /$ step up and down)

30086693
Channel 2: SDA (5V/div)
Channel 3: ILED (10mA/div)
Time Base (1s/div)

## Ramp Rate (Exponential)

 ( $32.768 \mathrm{~ms} / \mathrm{step}$ up and down)

30086694
Channel 2: SDA (5V/div)
Channel 3: ILED (10mA/div)
Time Base (2s/div)

## Startup Plot <br> $\left(\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}\right.$, ILED $=19 \mathrm{~mA}, \mathrm{~L}=22 \mu \mathrm{H}$, Ramp Rate $\left.=8 \mu \mathrm{~s} / \mathrm{step}\right)$ <br>  <br> 30086696

Channel 1: IIN (200mA/div)
Channel 3: VOUT (20V/div)
Channel 4 (10mA/div)
Time Base ( $2 \mathrm{~ms} / \mathrm{div}$ )

Ramp Rate (Exponential) ( $65.538 \mathrm{~ms} / \mathrm{step}$ up and down)


30086695
Channel 2: SDA (5V/div)
Channel 3: ILED (10mA/div)
Time Base ( $4 \mathrm{~s} / \mathrm{div}$ )

$I_{\text {LED }}$ Response to Step Change in PWM Duty Cycle
$\left(\mathrm{D}_{\mathrm{PWM}}\right.$ from $30 \%$ to $70 \%$, $\mathrm{I}_{\text {LED }}$ Full Scale $\left.=19 \mathrm{~mA}, \mathrm{f}_{\mathrm{PWM}}=5 \mathrm{kHz}\right)$


Channel 4: ILED (5mA/div)
Channel 2: PWM (5V/div)
Time Base ( $2 \mathrm{~ms} / \mathrm{div}$ )

## Operational Description

The LM3530 utilizes an asynchronous step-up, current mode, PWM controller and regulated current sink to provide an efficient and accurate LED current for white LED bias. The device powers a single series string of LEDs with output voltages of up to 40 V and a peak inductor current of typically 839 mA . The input active voltage range is from 2.7 V to 5.5 V .

## STARTUP

An internal soft-start prevents large inrush currents during startup that can cause excessive current spikes at the input. For the typical application circuit (using a $10 \mu \mathrm{H}$ inductor, a $2.2 \mu \mathrm{~F}$ input capacitor, and a $1 \mu \mathrm{~F}$ output capacitor) the average input current during startup ramps from 0 to 300 mA in 3ms. See Start Up Plots in the Typical Performance Characteristics.

## LIGHT LOAD OPERATION

The LM3530's boost converter operates in three modes: continuous conduction, discontinuous conduction, and skip mode. Under heavy loads when the inductor current does not reach zero before the end of the switching period, the device switches at a constant frequency ( 500 kHz typical). As the output current decreases and the inductor current reaches zero before the end of the switching period, the device operates in discontinuous conduction. At very light loads the LM3530 will enter skip mode operation causing the switching period to lengthen and the device to only switch as required
to maintain regulation at the output. Light load operation provides for improved efficiency at lighter LED currents compared to continuous and discontinuous conduction. This is due to the pulsed frequency operation resulting in decreased switching losses in the boost converter.

## AMBIENT LIGHT SENSOR

The LM3530 incorporates a dual input Ambient Light Sensing interface (ALS1 and ALS2) which translates an analog output ambient light sensor to a user-specified brightness level. The ambient light sensing circuit has 4 programmable boundaries (ZB0 - ZB3) which define 5 ambient brightness zones. Each ambient brightness zone corresponds to a programmable brightness threshold (ZOT - Z4T). The ALS interface is programmable to accept the ambient light information from either the highest voltage of ALS1 or ALS2, the average voltage of ALS1 or ALS2, or selectable from either ALS1 or ALS2.
Furthermore, each ambient light sensing input (ALS1 or ALS2) features 15 internal software selectable voltage setting resistors. This allows the LM3530 the capability of interfacing with a wide selection of ambient light sensors. Additionally, the ALS inputs can be configured as high impedance, thus providing for a true shutdown during low power modes. The ALS resistors are selectable through the ALS Resistor Select Register (see Table 9). Figure 3 shows a functional block diagram of the ambient light sensor input. VSNS represents the active input as described in Table 6 bits [6:5].

## FIGURE 3. Ambient Light Sensor Functional Block Diagram

## ALS OPERATION

The ambient light sensor input has a 0 to 1 V operational input voltage range. The Typical Application Circuit shows the LM3530 with dual ambient light sensors (AVAGO, APDS-9005) and the internal ALS Resistor Select Register set to $0 \times 44(2.27 \mathrm{k} \Omega)$. This circuit converts 0 to 1000 LUX light into approximately a 0 to 850 mV linear output voltage. The voltage at the active ambient light sensor input (ALS1 or ALS2) is compared against the 8 bit values programmed into the Zone Boundary Registers (ZB0-ZB3). When the ambient light sensor output crosses one of the ZBO - ZB3 programmed thresholds the internal ALS circuitry will smoothly transition
the LED current to the new 7 bit brightness level as programmed into the appropriate Zone Target Register (ZOT Z4T) (see Figure 4).
The ALS Configuration Register bits [6:5] programs which input is the active input, bits [4:3] control the on/off state of the ALS circuitry, and bits [2:0] control the ALS input averaging time. Additionally, the ALS Information Register is a read-only register which contains a flag (bit 3) which is set each time the active ALS input changes to a new zone. This flag is reset when the register is read back. Bits [2:0] of this register contain the current active zone information.



30086608

## FIGURE 4. Ambient Light Input to Backlight Mapping

## ALS AVERAGING TIME

The ALS Averaging Time is the time over which the Averager block collects samples from the A/D converter and then averages them to pass to the discriminator block (see Figure 3). Ambient light sensor samples are averaged and then further processed by the discriminator block to provide rejection of noise and transient signals. The averager is configurable with 8 different averaging times to provide varying amounts of noise and transient rejection (see Table 5). The discriminator block algorithm has a maximum latency of two averaging cycles; therefore, the averaging time selection determines the amount of delay that will exist between a steady-state change in the ambient light conditions and the associated change of the backlight illumination. For example, the A/D converter samples the ALS inputs at 16 kHz . If the averaging time is set to 1024 ms then the Averager will send the updated zone information to the discriminator every 1024 ms . This zone information contains the average of 16384 samples ( $1024 \mathrm{~ms} \times 16 \mathrm{kHz}$ ). Due to the latency of 2 averaging cycles, the LED current will not change until there has been a steadystate change in the ambient light for at least 2 averaging periods.

## Averager Operation

The magnitude and direction (either increasing or decreasing) of the Averager output is used to determine whether the LM3530 should change brightness zones. The Averager block functions as follows:

1. First, the Averager always begins with a Zone 0 reading stored at startup. If the main display LEDs are active before the ALS block is enabled, it is recommended that the ALS Enable 1 bit is set to ' 1 ' at least 3 averaging periods before the ALS Enable 2 bit is set.
2. The Averager will always round down to the lower zone in the event of a non-integer zone average. For example,
if during an averaging period the ALS input transitions between zone's 1 and 2 resulting in an averager output of 1.75 , then the averager output will round down to 1 (see Figure 5).
3. The two most current averaging samples are used to make zone change decisions.
4. To make a zone change, data from three averaging cycles are needed. (Starting Value, First Transition, Second Transition or Rest).
5. To Increase the brightness zone, the Averager output must have increased for at least 2 averaging periods or increased and remained at the new level for at least two averaging periods (' + ' to ' + ' or ' + ' to 'Rest' in Figure 6).
6. To decrease the brightness zone, the Averager output must have decreased for at least 2 averaging periods or decreased and remained at the new level for at least two averaging periods ('-' to '-' or '-' to 'Rest' in Figure 6).
In the case of two consecutive increases or decreases in the Averager output, the LM3530 will transition to zone equal to the last averager output (Figure 6).
Using the diagram for the ALS block (Figure 3), the flow of information is shown in (Figure 7). This starts with the ALS input into the $A / D$, into the Averager, and then into the Discriminator. Each state filters the previous output to help prevent unwanted zone to zone transitions.
When using the ALS averaging function, it is important to remember that the averaging cycle is free running and is not synchronized with changing ambient lighting conditions. Due to the nature of the averager round down, an increase in brightness can take between 2 and 3 averaging cycles to change zones, while a decrease in brightness can take between 1 and 2 averaging cycles. See Table 6 for a list of possible Averager periods. Figure 8 shows an example of how the perceived brightness change time can vary.


FIGURE 5. Averager Calculation


FIGURE 6. Brightness Zone Change Examples


FIGURE 7. Ambient Light Input to Backlight Transition


FIGURE 8. Perceived Brightness Change Time

## ZONE BOUNDARY SETTINGS

Registers $0 \times 60,0 \times 61,0 \times 62$, and $0 \times 63$ set the 4 zone boundaries (thresholds) for the ALS inputs. These 4 zone boundaries create 5 brightness zones which map over to 5 separate brightness zone targets (see Figure 4). Each 8-bit zone boundary register can set a threshold from typically 0 to 1V with linear step sizes of approximately $1 / 255=3.92 \mathrm{mV}$. Additionally, each zone boundary has built in hysteresis which can be either lower or higher then the programmed Zone Boundary depending on the last direction (either up or down) of the ALS input voltage.

## ZONE BOUNDARY TRIP POINTS AND HYSTERESIS

For each zone boundary setting, the trip point will vary above or below the nominal set point depending on the direction (either up or down) of the ALS input voltage. This is designed to keep the ALS input from oscillating back and forth between zones in the event that the ALS voltage is residing near to the programmed zone boundary threshold. The Zone Boundary Hysteresis will follow these 2 rules:

1. If the last zone transition was from low to high, then the trip point $\left(\mathrm{V}_{\text {TRIP }}\right)$ will be $\mathrm{V}_{\text {ZONE_BOUNDARY }}-\mathrm{V}_{\text {HYST }} / 2$, where $V_{\text {ZONE_BOUNDARY }}$ is the zone boundary set point as
programmed into the Zone Boundary registers, and $\mathrm{V}_{\text {HYST }}$ is typically 7 mV .
2. If the last zone transition was from high to low then the trip point ( $\mathrm{V}_{\text {TRIP }}$ ) will be $\mathrm{V}_{\text {ZONE_BOUNDARY }}+\mathrm{V}_{\mathrm{HYST}} / 2$.
Figure 9 details how the LM3530's ALS Input Zone Boundary Thresholds vary depending on the direction of the ALS input voltage.


FIGURE 9. Zone Boundaries With Hysteresis

## MINIMUM ZONE BOUNDARY SETTINGS

The actual minimum zone boundary setting is code $0 \times 03$. Codes of $0 \times 00,0 \times 01$, and $0 \times 02$ are all mapped to code $0 \times 03$. Table 1 shows the: Zone Boundary codes $0 \times 00$ through 0x04, the typical thresholds, and the high and low hysteresis values. The remapping of codes $0 \times 00-0 \times 02$ plus the additional 4 mV

Referring to Figure 9, each numbered trip point shown is determined from the direction of the previous ALS zone transition.
of offset voltage is necessary to prevent random offsets and noise on the ALS inputs from creating threshold levels that are below GND. This essentially guarantees that any Zone Boundary threshold selected is achievable with positive ALS voltages.

TABLE 1. Ideal Zone Boundary Settings with Hysteresis (Lower 5 Codes)

| Zone Boundary Code | Typical Zone Boundary <br> Threshold | Typical Threshold + <br> Hysteresis | Typical Threshold - <br> Hysteresis |
| :---: | :---: | :---: | :---: |
| $0 \times 00$ | 15.8 mV | 19.3 mV | 12.3 mV |
| $0 \times 01$ | 15.8 mV | 19.3 mV | 12.3 mV |
| $0 \times 02$ | 15.8 mV | 19.3 mV | 12.3 mV |
| $0 \times 03$ | 15.8 mV | 19.3 mV | 12.3 mV |
| $0 \times 04$ | 19.7 mV | 23.2 mV | 16.2 mV |

## LED CURRENT CONTROL

The LED current is is a function of the Full Scale Current, the Brightness Code, and the PWM input duty cycle. The Bright-
ness Code can either come from the BRT Register (0xA0) in I2C Compatible Current Control, or from the ALS Zone Target Registers (Address 0x70-0x74) in Ambient Light Current Control. Figure 10 shows the current control block diagram.


Note 1: Acode is a Scaler between 0 and 1 based on the Brightness Data or Zone Target Data Depending on the ALS Select Bit
Note 2: $\mathrm{D}_{\mathrm{PWM}}$ Is a Scaler between 0 and 1 and corresponds to the duty cycle of the PWM input signal
Note 3: For EN_PWM bit $=1$
$I_{\text {LED }}=I_{\text {FS }} \times A_{\text {CODE }} \times D_{\text {PWM }}$
For EN_PWM bit $=0$
$I_{\text {LED }}=I_{\text {FS }} \times A_{\text {CODE }}$

FIGURE 10. Current Control Block Diagram

The following sections describe each of these LED current control methods.

## PWM + I2C-COMPATIBLE CURRENT CONTROL

$\mathrm{PWM}+{ }^{2} \mathrm{C}$-compatible current control is enabled by writing a ' 1 ' to the Enable PWM bit (General Configuration Register bit [5]) and writing a ' 1 ' to the $1^{2} \mathrm{C}$ Device Enable bit (General Configuration Register bit 0). This makes the LED current a function of the PWM input duty cycle (D), the Full-Scale LED current ( $\mathrm{l}_{\text {LED_FS }}$ ), and the \% of full-scale LED current. The \% of Full-Scale LED current is set by the code in the Brightness

Control Register. The LED current using PWM $+\mathrm{I}^{2} \mathrm{C}$-Compatible Control is given by the following equation:

$$
I_{\text {LED }}=I_{\text {LED_FS }} \times B R T \times D
$$

BRT is the percentage of Full Scale Current as set in the Brightness Control Register. The Brightness Control Register can have either exponential or linear brightness mapping depending on the setting of the BMM bit (bit [1] in General Configuration Register).

## EXPONENTIAL OR LINEAR BRIGHTNESS MAPPING MODES

With bit [1] of the General Configuration Register set to 0 (default) exponential mapping is selected and the code in the Brightness Control Register corresponds to the Full-Scale LED current percentages in Table 1 and Figure 11. With bit [1] set to 1 linear mapping is selected and the code in the Brightness Control Register corresponds to the Full-Scale LED current percentages in Table 2 and Figure 12.

## PWM INPUT POLARITY

Bit [6] of the General Configuration Register controls the PWM input polarity. Setting this bit to 0 (default) selects positive polarity and makes the LED current (with PWM mode enabled) a function of the positive duty cycle at PWM. With this bit set to ' 0 ' the LED current (with PWM mode enabled) becomes a function of the negative duty cycle at PWM.
The PWM input is a logic level input with a frequency range of 400 Hz to 50 kHz . Internal filtering of the PWM input signal converts the duty cycle information to an average (analog) control signal which directly controls the LED current.

## Example: PWM + ${ }^{2} \mathbf{C}$-Compatible Current Control

As an example, assume the the General Configuration Register is loaded with (0x2D). From Table 4, this sets up the LM3530 with:
Simple Enable OFF (bit $7=0$ )
Positive PWM Polarity (bit $6=0$ )
PWM Enabled (bit $5=1$ )
Full-Scale Current set at 15.5 mA (bits [4:2] = 100)
Brightness Mapping set for Exponential (bit $1=0$ )
Device Enabled via ${ }^{2} \mathrm{C}$ (bit $0=1$ )
Next, the Brightness Control Register is loaded with 0x73. This sets the LED current to $51.406 \%$ of full scale (see ). Finally, the PWM input is driven with a 0 to 2 V pulse waveform at $70 \%$ duty cycle. The LED current under these conditions will be:
Where BRT is the percentage of $\mathrm{I}_{\text {LED_FS }}$ as set in the Brightness Control Register,

$$
I_{\text {LED }}=I_{\text {LED_FS }} \times \text { BRT } \times D=15.5 \mathrm{~mA} \times 51.4 \% \times 70 \% \approx 5.58 \mathrm{~mA} .
$$

## ${ }^{12} \mathrm{C}-\mathrm{COMPATIBLE}$ CURRENT CONTROL ONLY

${ }^{12} \mathrm{C}$-Compatible Control is enabled by writing a ' 1 ' to the $\mathrm{I}^{2} \mathrm{C}$ Device Enable bit (bit [0] of the General Configuration Regis-
ter), a ' 0 ' to the Simple Enable bit (bit 7), and a ' 0 ' to the PWM Enable bit (bit 5). With bit $5=0$, the duty cycle information at the PWM input is not used in setting the LED current.
In this mode the LED current is a function of the Full-Scale LED current bits (bits [4:2] of the General Configuration Register) and the code in the Brightness Control Register. The LED current mapping for the Brightness Control Register can be linear or exponential depending on bit [1] in the General Configuration Register (see Exponential or Linear Brightness Mapping Modes section). Using I2C-Compatible Control Only, the Full-Scale LED Current bits and the Brightness Control Register code provides nearly 1016 possible current levels selectable over the $\mathrm{I}^{2} \mathrm{C}$-compatible interface.

## Example: ${ }^{2} \mathrm{C}$-Compatible Current Control Only

As an example, assume the General Configuration Register is loaded with $0 \times 15$. From this sets up the LM3530 with:
Simple Enable OFF (bit $7=0$ )
Positive PWM Polarity (bit $6=0$ )
PWM Disabled (bit $5=0$ )
Full-Scale Current set at 22.5 mA (bits [4:2] = 101)
Brightness Mapping set for Exponential (bit $1=0$ )
Device Enabled via I2C (bit $0=1$ )
The Brightness Control Register is then loaded with $0 \times 72$ ( $48.438 \%$ of full-scale current from ). The LED current with this configuration becomes:
$I_{\text {LED }}=I_{\text {LED_FS }} \times B R T=22.5 \mathrm{~mA} \times 0.48438 \approx 10.9 \mathrm{~mA}$.
Where BRT is the \% of $I_{\text {LED_FS }}$ as set in the Brightness Control Register.
Next, the brightness mapping is set to linear mapping mode (bit [1] in General Configuration Register set to 1). Using the same Full-Scale current settings and Brightness Control Register settings as before, the LED current becomes:

$$
I_{\text {LED }}=I_{\text {LED_FS }} \times B R T=22.5 \mathrm{~mA} \times 0.8976 \approx 20.2 \mathrm{~mA} .
$$

Which is higher now since the code in the Brightness Control Register (0x72) corresponds to $89.76 \%$ of Full-Scale LED Current due to the different mapping mode given in .


FIGURE 11. Exponential Brightness Mapping

TABLE 2. ILED vs. Brightness Register Data (Exponential Mapping)

| $\begin{aligned} & \text { BRT Data } \\ & \text { (Hex) } \end{aligned}$ | \% Full-Scale Current | $\begin{aligned} & \text { BRT Data } \\ & \text { (Hex) } \end{aligned}$ | \% of FullScale Current | BRT Data (Hex) | \% of Full-Scale Current | $\begin{aligned} & \text { BRT Data } \\ & \text { (Hex) } \end{aligned}$ | \% of Full-Scale Current |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0 \times 00$ | 0.00\% | $0 \times 20$ | 0.500\% | $0 \times 40$ | 2.953\% | $0 \times 60$ | 17.813\% |
| $0 \times 01$ | 0.080\% | $0 \times 21$ | 0.523\% | $0 \times 41$ | 3.125\% | $0 \times 61$ | 18.750\% |
| $0 \times 02$ | 0.086\% | $0 \times 22$ | 0.555\% | 0x42 | 3.336\% | $0 \times 62$ | 19.922\% |
| $0 \times 03$ | 0.094\% | $0 \times 23$ | 0.586\% | 0x43 | 3.500\% | $0 \times 63$ | 20.859\% |
| $0 \times 04$ | 0.102\% | $0 \times 24$ | 0.617\% | 0x44 | 3.719\% | $0 \times 64$ | 22.266\% |
| $0 \times 05$ | 0.109\% | $0 \times 25$ | 0.656\% | $0 \times 45$ | 3.906\% | $0 \times 65$ | 23.438\% |
| $0 \times 06$ | 0.117\% | $0 \times 26$ | 0.695\% | $0 \times 46$ | 4.141\% | $0 \times 66$ | 24.844\% |
| $0 \times 07$ | 0.125\% | $0 \times 27$ | 0.734\% | 0x47 | 4.375\% | $0 \times 67$ | 26.250\% |
| $0 \times 08$ | 0.133\% | $0 \times 28$ | 0.773\% | 0x48 | 4.648\% | 0x68 | 27.656\% |
| $0 \times 09$ | 0.141\% | $0 \times 29$ | 0.820\% | 0x49 | 4.922\% | $0 \times 69$ | 29.297\% |
| 0x0A | 0.148\% | 0x2A | 0.867\% | 0x4A | 5.195\% | $0 \times 6 \mathrm{~A}$ | 31.172\% |
| $0 \times 0 \mathrm{~B}$ | 0.156\% | $0 \times 2 \mathrm{~B}$ | 0.914\% | 0x4B | 5.469\% | $0 \times 6 \mathrm{~B}$ | 32.813\% |
| $0 \times 0 \mathrm{C}$ | 0.164\% | 0x2C | 0.969\% | 0x4C | 5.781\% | 0x6C | 34.453\% |
| 0x0D | 0.172\% | 0x2D | 1.031\% | 0x4D | 6.125\% | 0x6D | 35.547\% |
| $0 \times 0 \mathrm{E}$ | 0.180\% | $0 \times 2 \mathrm{E}$ | 1.078\% | $0 \times 4 \mathrm{E}$ | 6.484\% | $0 \times 6 \mathrm{E}$ | 38.828\% |
| $0 \times 0 \mathrm{~F}$ | 0.188\% | 0x2F | 1.148\% | 0x4F | 6.875\% | $0 \times 6 \mathrm{~F}$ | 41.016\% |
| $0 \times 10$ | 0.203\% | $0 \times 30$ | 1.219\% | 0x50 | 7.266\% | 0x70 | 43.203\% |
| $0 \times 11$ | 0.211\% | $0 \times 31$ | 1.281\% | $0 \times 51$ | 7.656\% | 0x71 | 45.938\% |
| $0 \times 12$ | 0.227\% | $0 \times 32$ | 1.359\% | $0 \times 52$ | 8.047\% | $0 \times 72$ | 48.438\% |
| $0 \times 13$ | 0.242\% | $0 \times 33$ | 1.430\% | $0 \times 53$ | 8.594\% | $0 \times 73$ | 51.406\% |
| $0 \times 14$ | 0.250\% | $0 \times 34$ | 1.523\% | $0 \times 54$ | 9.063\% | 0x74 | 54.141\% |
| $0 \times 15$ | 0.266\% | $0 \times 35$ | 1.594\% | $0 \times 55$ | 9.609\% | $0 \times 75$ | 57.031\% |
| $0 \times 16$ | 0.281\% | $0 \times 36$ | 1.688\% | $0 \times 56$ | 10.078\% | $0 \times 76$ | 60.703\% |
| $0 \times 17$ | 0.297\% | $0 \times 37$ | 1.781\% | $0 \times 57$ | 10.781\% | $0 \times 77$ | 63.984\% |
| $0 \times 18$ | 0.320\% | $0 \times 38$ | 1.898\% | $0 \times 58$ | 11.250\% | 0x78 | 67.813\% |
| 0x19 | 0.336\% | $0 \times 39$ | 2.016\% | $0 \times 59$ | 11.953\% | 0x79 | 71.875\% |
| 0x1A | 0.352\% | 0x3A | 2.109\% | 0x5A | 12.656\% | 0x7A | 75.781\% |
| $0 \times 1 \mathrm{~B}$ | 0.375\% | $0 \times 3 \mathrm{~B}$ | 2.250\% | 0x5B | 13.359\% | 0x7B | 79.688\% |
| $0 \times 1 \mathrm{C}$ | 0.398\% | 0x3C | 2.367\% | 0x5C | 14.219\% | 0x7C | 84.375\% |


| BRT Data <br> (Hex) | \% Full-Scale <br> Current | BRT Data <br> (Hex) | \% of Full- <br> Scale <br> Current | BRT Data <br> (Hex) | \% of Full-Scale <br> Current | BRT Data <br> (Hex) | \% of Full-Scale <br> Current |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0 \times 1 \mathrm{D}$ | $0.422 \%$ | $0 \times 3 \mathrm{D}$ | $2.508 \%$ | $0 \times 5 \mathrm{D}$ | $15.000 \%$ | $0 \times 7 \mathrm{D}$ | $89.844 \%$ |
| $0 \times 1 \mathrm{E}$ | $0.445 \%$ | $0 \times 3 \mathrm{E}$ | $2.648 \%$ | $0 \times 5 \mathrm{E}$ | $15.859 \%$ | $0 \times 7 \mathrm{E}$ | $94.531 \%$ |
| $0 \times 1 \mathrm{~F}$ | $0.469 \%$ | $0 \times 3 \mathrm{~F}$ | $2.789 \%$ | $0 \times 5 \mathrm{~F}$ | $16.875 \%$ | $0 \times 7 \mathrm{~F}$ | $100.00 \%$ |



FIGURE 12. Linear Brightness Mapping

TABLE 3. I LED vs. Brightness Register Data (Linear Mapping)

| BRT Data (Hex) | \% Full-Scale Current (Linear) | BRT Data (Hex) | \% of Full- <br> Scale <br> Current <br> (Linear) | BRT Data (Hex) | \% of Full-Scale Current (Linear) | BRT Data (Hex) | \% of FullScale Current (Linear) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0 \times 00$ | 0.00\% | 0x20 | 25.20\% | 0x40 | 50.39\% | 0x60 | 75.59\% |
| $0 \times 01$ | 0.79\% | $0 \times 21$ | 25.98\% | $0 \times 41$ | 51.18\% | $0 \times 61$ | 76.38\% |
| $0 \times 02$ | 1.57\% | $0 \times 22$ | 26.77\% | 0x42 | 51.97\% | 0x62 | 77.17\% |
| $0 \times 03$ | 2.36\% | $0 \times 23$ | 27.56\% | $0 \times 43$ | 52.76\% | $0 \times 63$ | 77.95\% |
| $0 \times 04$ | 3.15\% | $0 \times 24$ | 28.35\% | $0 \times 44$ | 53.54\% | 0x64 | 78.74\% |
| 0x05 | 3.94\% | 0x25 | 29.13\% | 0x45 | 54.33\% | 0x65 | 79.53\% |
| $0 \times 06$ | 4.72\% | 0x26 | 29.92\% | 0x46 | 55.12\% | $0 \times 66$ | 80.31\% |
| $0 \times 07$ | 5.51\% | $0 \times 27$ | 30.71\% | $0 \times 47$ | 55.91\% | $0 \times 67$ | 81.10\% |
| $0 \times 08$ | 6.30\% | $0 \times 28$ | 31.50\% | $0 \times 48$ | 56.69\% | 0x68 | 81.89\% |
| 0x09 | 7.09\% | 0x29 | 32.28\% | 0x49 | 57.48\% | 0x69 | 82.68\% |
| $0 \times 0 \mathrm{~A}$ | 7.87\% | 0x2A | 33.07\% | 0x4A | 58.27\% | $0 \times 6 \mathrm{~A}$ | 83.46\% |
| 0x0B | 8.66\% | 0x2B | 33.86\% | 0x4B | 59.06\% | 0x6B | 84.25\% |
| 0x0C | 9.45\% | 0x2C | 34.65\% | 0x4C | 59.84\% | 0x6C | 85.04\% |
| 0x0D | 10.24\% | $0 \times 2 \mathrm{D}$ | 35.43\% | 0x4D | 60.63\% | 0x6D | 85.83\% |
| 0x0E | 11.02\% | 0x2E | 36.22\% | 0x4E | 61.42\% | 0x6E | 86.61\% |
| 0x0F | 11.81\% | 0x2F | 37.01\% | 0x4F | 62.20\% | 0x6F | 87.40\% |
| $0 \times 10$ | 12.60\% | 0x30 | 37.80\% | $0 \times 50$ | 62.99\% | 0x70 | 88.19\% |
| $0 \times 11$ | 13.39\% | $0 \times 31$ | 38.58\% | $0 \times 51$ | 63.78\% | 0x71 | 88.98\% |
| $0 \times 12$ | 14.17\% | $0 \times 32$ | 39.37\% | 0x52 | 64.57\% | 0x72 | 89.76\% |
| $0 \times 13$ | 14.96\% | 0x33 | 40.16\% | $0 \times 53$ | 65.35\% | 0x73 | 90.55\% |
| $0 \times 14$ | 15.75\% | $0 \times 34$ | 40.94\% | $0 \times 54$ | 66.14\% | $0 \times 74$ | 91.34\% |
| $0 \times 15$ | 16.54\% | 0x35 | 41.73\% | 0x55 | 66.93\% | 0x75 | 92.13\% |


| BRT Data (Hex) | \% Full-Scale Current (Linear) | BRT Data (Hex) | \% of Full- <br> Scale Current (Linear) | BRT Data (Hex) | \% of Full-Scale Current (Linear) | BRT Data (Hex) | \% of FullScale Current (Linear) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0 \times 16$ | 17.32\% | $0 \times 36$ | 42.52\% | $0 \times 56$ | 67.72\% | 0x76 | 92.91\% |
| $0 \times 17$ | 18.11\% | $0 \times 37$ | 43.31\% | $0 \times 57$ | 68.50\% | $0 \times 77$ | 93.70\% |
| $0 \times 18$ | 18.90\% | $0 \times 38$ | 44.09\% | $0 \times 58$ | 69.29\% | 0x78 | 94.49\% |
| $0 \times 19$ | 19.69\% | $0 \times 39$ | 44.88\% | $0 \times 59$ | 70.08\% | $0 \times 79$ | 95.28\% |
| $0 \times 1 \mathrm{~A}$ | 20.47\% | 0x3A | 45.67\% | 0x5A | 70.87\% | 0x7A | 96.06\% |
| 0x1B | 21.26\% | $0 \times 3 \mathrm{~B}$ | 46.46\% | 0x5B | 71.65\% | 0x7B | 96.85\% |
| 0x1C | 22.05\% | $0 \times 3 \mathrm{C}$ | 47.24\% | 0x5C | 72.44\% | 0x7C | 97.64\% |
| 0x1D | 22.83\% | 0x3D | 48.03\% | 0x5D | 73.23\% | 0x7D | 98.43\% |
| $0 \times 1 \mathrm{E}$ | 23.62\% | $0 \times 3 \mathrm{E}$ | 48.82\% | 0x5E | 74.02\% | 0x7E | 99.21\% |
| 0x1F | 24.41\% | 0x3F | 49.61\% | 0x5F | 74.80\% | 0x7F | 100.00\% |

## SIMPLE ENABLE DISABLE WITH PWM CURRENT CONTROL

With bits [7 and 5] of the General Configuration Register set to ' 1 ' the PWM input is enabled as a simple enable/disable. The simple enable/disable feature operates as described in Figure 13. In this mode, when the PWM input is held high (PWM Polarity bit $=0$ ) for $>2 \mathrm{~ms}$ the LM3530 will turn on the LED current at the programmed Full-Scale Current $\times \%$ of Full-Scale Current as set by the code in the Brightness Control Register. When the PWM input is held low for $>2 \mathrm{~ms}$ the device will shut down. With the PWM Polarity bit = 1 the PWM input is configured for active low operation. In this configuration holding PWM low for $>2 \mathrm{~ms}$ will turn on the device at the programmed Full-Scale Current $\times \%$ of Full-Scale Current as set by the code in the Brightness Control Register. Likewise, holding PWM high for $>2 \mathrm{~ms}$ will put the device in shutdown.

Driving the PWM input with a pulsed waveform at a variable duty cycle is also possible in simple enable/Disable mode, so long as the low pulse width is $<2 \mathrm{~ms}$. When a PWM signal is used in this mode the input duty cycle information is internally filtered, and an analog voltage is used to control the LED current. This type of PWM control (PWM to Analog current control) prevents large voltage excursions across the output capacitor that can result in audible noise. Simple Enable/Disable mode can be useful since the default bit setting for the General Configuration Register is 0xCC (Simple Enable bit = 1, PWM Enable = 1, and Full-Scale Current = 19mA). Additionally, the default Brightness Register setting is 0x7F (100\% of Full-Scale current). This gives the LM3530 the ability to turn on after power up (or after reset) without having to do any writes to the $\mathrm{I}^{2} \mathrm{C}$-compatible bus.


FIGURE 13. Simple Enable/Disable Timing

## Example: Simple Enable Disable with PWM Current Control)

As an example, assume that the HWEN input is toggled low then high. This resets the LM3530 and sets all the registers to their default value. When the PWM input is then pulled high for $>2 \mathrm{~ms}$ the LED current becomes:

$$
I_{\text {LED }}=I_{\text {LED_FS }} \times \text { BRT } \times \mathrm{D}=19 \mathrm{~mA} \times 1.00 \times 100 \% \approx 19 \mathrm{~mA} .
$$

where BRT is the \% of $\mathrm{I}_{\text {LED_FS }}$ as set in the Brightness Control Register.
If then the PWM input is fed with a 5 kHz pulsed waveform at $40 \%$ duty cycle the LED current becomes:

$$
I_{\text {LED }}=I_{\text {LED_FS }} \times B R T \times D=19 \mathrm{~mA} \times 1.00 \times 0.4 \approx 7.6 \mathrm{~mA} .
$$

Then, if the Brightness Control Register is loaded with $0 \times 55$ ( $9.6 \%$ of Full-Scale Current) the LED current becomes:

$$
I_{\text {LED }}=I_{\text {LED_FS }} \times B R T \times D=19 \mathrm{~mA} \times 9.65 \times 0.4 \approx 0.73 \mathrm{~mA} .
$$

## AMBIENT LIGHT CURRENT CONTROL

With bits [4:3] of the ALS Configuration Register both set to 1, the LM3530 is configured for Ambient Light Current Control. In this mode the ambient light sensing inputs (ALS1, and/ or ALS2) monitor the outputs of analog output ambient light sensing photo diodes and adjust the LED current depending on the ambient light. The ambient light sensing circuit has 4
configurable Ambient Light Boundaries (ZB0 - ZB3) programmed through the four (8-bit) Zone Boundary Registers. These zone boundaries define 5 ambient brightness zones (Figure 4). Each zone corresponds to a programmable brightness setting which is programmable through the 5 Zone Target Registers (ZOT - Z4T). When the ALS1, and/or ALS2 input (depending on the bit settings of the ALS Input Select bits) detects that the ambient light has crossed to a new zone (as defined by one of the Zone Boundary Registers) the LED current becomes a function of the Brightness Code loaded in the Zone Target Register which corresponds to the new ambient light brightness zone.
On startup the 4 Zone Boundary Registers are pre-loaded with 0x33 (51d), 0x66 (102d), 0x99 (153d), and 0xCC (204d). Each ALS input has a 1V active input voltage range with a 4 mV offset voltage which makes the default Zone Boundaries set at:
Zone Boundary $0=1 \mathrm{~V} \times 51 / 255+4 \mathrm{mV}=204 \mathrm{mV}$
Zone Boundary $1=1 \mathrm{~V} \times 102 / 255+4 \mathrm{mV}=404 \mathrm{mV}$
Zone Boundary $2=1 \mathrm{~V} \times 153 / 255+4 \mathrm{mV}=604 \mathrm{mV}$
Zone Boundary $3=1 \mathrm{~V} \times 204 / 255+4 \mathrm{mV}=804 \mathrm{mV}$
These Zone Boundary Registers are all 8-bit (readable and writable) registers. The first zone (Z0) is defined between 0 and 204 mV , Z1's default is defined between 204 mV and 404 mV , Z2's default is defined between 404 mV and 604 mV , Z3's default is defined between 604 mV and 804 mV , and $\mathrm{Z4}$ 's default is defined between 804 mV and 1.004 V . The default settings for the 5 Zone Target Registers are $0 \times 19$, $0 \times 33$, $0 \times 4 \mathrm{C}, 0 \times 66$, and $0 \times 7 \mathrm{~F}$. This corresponds to LED brightness settings of $0.336 \%, 1.43 \%, 5.781 \%, 24.844 \%$, and $100 \%$ of full-scale current respectively (assuming exponential backlight mapping).

## Example: Ambient Light Control Current

As an example, assume that the APDS-9005 is used as the ambient light sensing photo diode with its output connected to the ALS1 input. The ALS Resistor Select Register is loaded with $0 \times 04$ which configures the ALS1 input for a $2.27 \mathrm{k} \Omega$ internal pull-down resistor (see Table 9). The APDS-9005 has a typical $400 \mathrm{nA} / \mathrm{LUX}$ response. With a $2.27 \mathrm{k} \Omega$ resistor the sensor output would see a 0 to 908 mV swing with a 0 to 1000 LUX change in ambient light. Next, the ALS Configuration Register is programmed with 0x3C. From Table 6, this configures the LM3530's ambient light sensing interface for: ALS1 as the active ALS input (bits $[6: 5]=01$ )

Ambient Light Current Control Enabled (bit $4=1$ )
ALS circuitry Enabled (bit $3=1$ )
Sets the ALS Averaging Time to 512 ms (bits [2:0] = 100)
Next, the General Configuration Register is programmed with $0 \times 19$ which sets the Full-Scale Current to 26mA, selects Exponential Brightness Mapping, and enables the device via the ${ }^{12} \mathrm{C}$-compatible interface.
Now assume that the APDS-9005 ambient light sensor detects a 100 LUX ambient light at its input. This forces the ambient light sensors output (and the ALS1 input) to 87.5 mV corresponding to Zone 0 . Since Zone 0 points to the brightness code programmed in Zone Target Register 0 (loaded with code $0 \times 19$ ), the LED current becomes:

$$
I_{\text {LED }}=I_{\text {LED_FS }} \times \text { ZoneTarget } 0=26 \mathrm{~mA} \times 0.336 \% \approx 87 \mu \mathrm{~A} .
$$

Where the code in Zone Target Register 0 points to the \% of ILED_FS as given by Table 2 or Table 3, depending on whether Exponential or Linear Mapping are selected.
Next, assume that the ambient light changes to 500 LUX (corresponding to an ALS1 voltage of 454 mV ). This moves the ambient light into Zone 2 which corresponds to Zone Target Register 2 (loaded with code 0x4C) the LED current then becomes:

$$
I_{\text {LED }}=I_{\text {LED_FS }} \times \text { ZoneTarget2 }=26 \mathrm{~mA} \times 5.781 \% \approx 1.5 \mathrm{~mA} .
$$

## AMBIENT LIGHT CURRENT CONTROL + PWM

The Ambient Light Current Control can also be a function of the PWM input duty cycle. Assume the LM3530 is configured as described in the above Ambient Light Current Control example, but this time the Enable PWM bit set to ' 1 ' (General Configuration Register bit [5]).

## Example: Ambient Light Current Control + PWM

In this example, the APDS-9005 detects that the ambient light has changed to 1 kLUX. The voltage at ALS1 is now around 908 mV and the ambient light falls within Zone 5. This causes the LED brightness to be a function of Zone Target Register 5 (loaded with 0x7F). Now assume the PWM input is also driven with a $50 \%$ duty cycle pulsed waveform. The LED current now becomes:

$$
I_{\text {LED }}=I_{\text {LED_FS }} \times \text { ZoneTarget5 } \times D=26 \mathrm{~mA} \times 100 \% \times 50 \% \approx 13 \mathrm{~mA} .
$$

## Example: ALS Averaging

As an example, suppose the LM3530's ALS Configuration Register is loaded with $0 \times 3 B$. This configures the device for: ALS1 as the active ALS input (bits [6:5] = 01)
Enables Ambient Light Current Control (bit $4=1$ )
Enables the ALS circuitry (bit $3=1$ )
Sets the ALS Averaging Time to 256ms (bits [2:0] = 011)
Next, the ALS Resistor Select Register is loaded with 0x04. This configures the ALS2 input as high impedance and configures the ALS1 input with a $2.27 \mathrm{k} \Omega$ internal pull-down resistor. The Zone Boundary Registers and Zone Target Registers are left with their default values. The Brightness Ramp Rate Register is loaded with 0x2D. This sets up the LED current ramp rate at $16.384 \mathrm{~ms} / \mathrm{step}$. Finally, the General

Configuration Register is loaded with $0 \times 15$. This sets up the device with:
Simple Enable OFF (bit $7=0$ )
PWM Polarity High (bit $6=0$ )
PWM Input Disabled (bit $5=0$ )
Full-Scale Current $=22.5 \mathrm{~mA}$ (bits [4:2] = 101)
Brightness Mapping Mode as Exponential (bit $1=0$ )
Device Enabled via I2C (bit $0=1$ )
As the device starts up the APDS-9005 ambient light sensor (connected to the ALS1 input) detects 500 LUX. This puts approximately 437.5 mV at ALS1 (see Figure 14). This places the measured ambient light between Zone Boundary Registers 1 and 2, thus corresponding to Zone Target Register 2. The default value for this register is $0 \times 4 \mathrm{C}$. The LED current is programmed to:
$I_{\text {LED }}=I_{\text {LED_FS }} \times$ ZoneTarget2 $=22.5 \mathrm{~mA} \times 5.781 \% \approx 1.3 \mathrm{~mA}$.
Referring to Figure 14, initially the Averager is loaded with Zone 0 so it takes 2 averaging periods for the LM3530 to change to the new zone. After the ALS1 voltage remains at 437.5 mV for two averaging periods (end of period \#2) the LM3530 sees a repeat of Zone 2 and signals the LED current to begin ramping to Zone 2's target beginning at average period \#3. Since the ramp rate is set at $16.384 \mathrm{~ms} /$ step the LED current goes from 0 to 1.3 mA in $76 \times 16.384 \mathrm{~ms}=1.245 \mathrm{~s}$ (approximately 5 average periods).
After the LED current has been at its steady state of 1.3 mA for a while, the ambient light suddenly steps to 900 LUX for 500 ms and then steps back to 500 LUX. In this case the 900 LUX will place the ALS1 voltage at approximately 979 mV corresponding to Zone 4 somewhere during average period \#10 and fall back to 437.5 mV somewhere during average period \#12. The averager output during period \#10 goes to 3 , and
then during period \#11, goes to 4 . Since there have been 2 increases in the average during \#10 and \#11, the beginning of average period \#12 shows a change in the brightness zone to Zone 4. This results in the LED current ramping to the new value of 22.5 mA (Zone 4's target). During period \#12 the ambient light steps back to 500 LUX and forces ALS1 to 437.5 mV (corresponding to Zone 2). After average periods \#12 and \#13 have shown that the averager transitioned lower two times, the brightness zone changes to the new target at the beginning of period \#14. This signals the LED current to ramp down to the zone 2 target of 1.3mA. Looking back at average periods \#12 and \#13, the LED current was only able to ramp up to 7.38 mA due to the ramp rate of $16.384 \mathrm{~ms} / \mathrm{step}$ ( 2 average periods of 256 ms each) before it was instructed to ramp back to Zone 2's target at the start of period \#14. This example demonstrates not only the averaging feature, but how additional filtering of transient events on the ALS inputs can be accomplished by using the LED current ramp rates.


FIGURE 14. ALS Averaging Example

## INTERRUPT OUTPUT

INT is an open-drain output which pulls low when the Ambient Light Sensing circuit has transitioned to a new ambient brightness zone. When a read-back of the ALS Information Register is done INT is reset to the open drain state.

## OVER-VOLTAGE PROTECTION

Over-voltage protection is set at 40 V (minimum) for the LM3530-40 and 23.6 V minimum for the LM3530-25. The 40V version allows typically up to 11 series white LEDs (assuming 3.5 V per LED +400 mV headroom voltage for the current sink $=38.9 \mathrm{~V}$ ). When the OVP threshold is reached the LM3530's switching converter stops switching, allowing the output voltage to discharge. Switching will resume when the output voltage falls to typically 1 V below the OVP threshold. In the event of an LED open circuit the output will be limited to around 40 V with a small amount of voltage ripple. The 25 V version allows up to 6 series white LEDs (assuming 3.5V per

LED +400 mV headroom voltage for the current sink $=21.4 \mathrm{~V}$ ). The 25V OVP option allows for the use of lower voltage and smaller sized $(25 \mathrm{~V})$ output capacitors. The 40 V device would typically require a 50 V output capacitor.

## HARDWARE ENABLE

The HWEN input is an active high hardware enable which must be pulled high to enable the device. Pulling this pin low disables the $\mathrm{I}^{2} \mathrm{C}$-compatible interface, the simple enable/disable input, the PWM input, and resets all registers to their default state (see Table 4).

## THERMAL SHUTDOWN

In the event the die temperature reaches $+140^{\circ} \mathrm{C}$, the LM3530 will stop switching until the die temperature cools by $15^{\circ} \mathrm{C}$. In a thermal shutdown event the device is not placed in reset; therefore, the contents of the registers are left in their current state.

## I2C-Compatible Interface

## START AND STOP CONDITION

The LM3530 is controlled via an ${ }^{2}$ 2 C -compatible interface. START and STOP conditions classify the beginning and the end of the ${ }^{2} \mathrm{C}$ session. A START condition is defined as SDA transitioning from HIGH to LOW while SCL is HIGH. A STOP condition is defined as SDA transitioning from LOW to HIGH while SCL is HIGH. The $I^{2} \mathrm{C}$ master always generates the

START and STOP conditions. The ${ }^{2} \mathrm{C}$ bus is considered busy after a START condition and free after a STOP condition. During data transmission, the ${ }^{2} \mathrm{C}$ master can generate repeated START conditions. A START and a repeated START conditions are equivalent function-wise. The data on SDA must be stable during the HIGH period of the clock signal (SCL). In other words, the state of SDA can only be changed when SCL is LOW.


FIGURE 15. Start and Stop Sequences

## [²C-COMPATIBLE ADDRESS

The 7bit chip address for the LM3530 is ( $0 \times 38$, or $0 \times 39$ ) for the 40 V version and ( $0 \times 36$ ) for the 25 V version. After the START condition, the I ${ }^{2} \mathrm{C}$ master sends the 7 -bit chip address followed by an eighth bit (LSB) read or write (R/W). R/W=0
indicates a WRITE and R/W = 1 indicates a READ. The second byte following the chip address selects the register address to which the data will be written. The third byte contains the data for the selected register.


30086638
FIGURE 16. ${ }^{2} \mathrm{C}$-Compatible Chip Address ( $0 \times 38$ )

I2C Compatible Address
MSB

|  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 1 | 1 | 0 | 1 | 1 | 0 | R/W |
| Bit 7 | Bit 6 | Bit 5 | Bit 4 | Bit 3 | Bit 2 | Bit 1 | Bit 0 |

30086639
FIGURE 17. I2C-Compatible Chip Address (0x36)

## TRANSFERRING DATA

Every byte on the SDA line must be eight bits long, with the most significant bit (MSB) transferred first. Each byte of data must be followed by an acknowledge bit (ACK). The acknowledge related clock pulse (9th clock pulse) is generated by the master. The master then releases SDA (HIGH) during the 9th
clock pulse. The LM3530 pulls down SDA during the 9th clock pulse, signifying an acknowledge. An acknowledge is generated after each byte has been received.
There are fourteen 8-bit registers within the LM3530 as detailed in Table 4.

Register Descriptions
TABLE 4. LM3530 Register Definition

| Register Name | Function | Address | POR Value |
| :---: | :---: | :---: | :---: |
| General Configuration | 1. Simple Interface Enable <br> 2. PWM Polarity <br> 3. PWM enable <br> 4. Full-Scale Current Selection <br> 5. Brightness Mapping Mode Select <br> 6. I2C Device Enable | $0 \times 10$ | $0 x B 0$ |
| ALS Configuration | 1. ALS Current Control Enable <br> 2. ALS Input Enable <br> 3. ALS Input Select <br> 4. ALS Averaging Times | 0x20 | 0x2C |
| Brightness Ramp Rate | Programs the rate of rise and fall of the LED current | $0 \times 30$ | $0 \times 00$ |
| ALS Zone Information | 1. Zone Boundary Change Flag <br> 2. Zone Brightness Information | 0x40 | $0 \times 00$ |
| ALS Resistor Select | Internal ALS1 and ALS2 Resistances | $0 \times 41$ | $0 \times 00$ |
| $\begin{array}{l}\text { Brightness Control } \\ \text { (BRT) }\end{array}$ | Holds the 7 bit Brightness Data | $0 \times A 0$ | 0x7F |
| $\begin{aligned} & \text { Zone Boundary } 0 \\ & \text { (ZBO) } \end{aligned}$ | ALS Zone Boundary \#0 | $0 \times 60$ | $0 \times 33$ |
| $\begin{aligned} & \text { Zone Boundary } 1 \\ & \text { (ZB1) } \end{aligned}$ | ALS Zone Boundary \#1 | $0 \times 61$ | $0 \times 66$ |
| Zone Boundary 2 (ZB2) | ALS Zone Boundary \#2 | $0 \times 62$ | $0 \times 99$ |
| $\begin{aligned} & \hline \text { Zone Boundary } 3 \\ & \text { (ZB3) } \end{aligned}$ | ALS Zone Boundary \#3 | $0 \times 63$ | 0xCC |
| $\begin{aligned} & \text { Zone Target } 0 \\ & \text { (ZOT) } \end{aligned}$ | Zone 0 LED Current Data. The LED Current Source transitions to the brightness code in ZOT when the ALS_ input is less than the zone boundary programmed in ZB0. | 0x70 | 0x19 |
| Zone Target 1 (Z1T) | Zone 1 LED Current Data. The LED Current Source transitions to the brightness code in Z1T when the ALS_ input is between the zone boundaries programmed in ZB1 and ZB0. | 0x71 | $0 \times 33$ |
| Zone Target 2 (Z2T) | Zone 2 LED Current Data. The LED Current Source transitions to the brightness code in Z2T when the ALS_ input is between the zone boundaries programmed in ZB2 and ZB1. | $0 \times 72$ | 0x4C |
| Zone Target 3 (Z3T) | Zone 3 LED Current Data. The LED Current Source transitions to the brightness code in Z3T when the ALS_ input is between the zone boundaries programmed in ZB3 and ZB2. | $0 \times 73$ | $0 \times 66$ |
| Zone Target 4 (Z4T) | Zone 4 LED Current Data. The LED Current Source transitions to the brightness code in Z4T when the ALS_ input is between the zone boundaries programmed in ZB4 and ZB3. | 0x74 | 0x7F |

*Note: Unused bits in the LM3530's Registers default to a logic '1'.

GENERAL CONFIGURATION REGISTER (GP)
The General Configuration Register (address $0 \times 10$ ) is described in Figure 18 and Table 5.

| MSB | General Configuration Register Address 0x10, Default Value 0xB0 |  |  |  |  |  | LSB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bit 7 <br> Simple Interface Enable | Bit 6 <br> PWM <br> Polarity | Bit 5 PWM Enable | Bit 4 Full Scale Current Select | Bit 3 Full Scale Current Select | Bit 2 Full Scale Current Select | Bit 1 <br> Brightness Mapping Mode Select | Bit 0 $12 \mathrm{C}$ <br> Interface Enable |

30086609
FIGURE 18. General Configuration Register

TABLE 5. General Configuration Register Description (0x10)

| Bit 7 <br> (PWM Simple <br> Enable | Bit 6 <br> (PWM <br> Polarity) | Bit 5 (EN_PWM) see Figure 8 | Bit 4 <br> (Full-Scale <br> Current <br> Select) | Bit 3 <br> (Full-Scale <br> Current <br> Select) | Bit 2 <br> (Full-Scale Current Select) | Bit 1 <br> (Mapping <br> Mode Select) | Bit 0 <br> (I2C Device Enable) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 = Simple Interface at PWM Input is Disabled 1 = Simple Interface at PWM Input is Enabled | $0=P W M$ <br> active high $1 \text { = PWM }$ <br> active low | 0 = LED current is not a function of PWM duty cycle 1 = LED current is a function of duty cycle | $000=5 \mathrm{~mA}$ full-scale current $001=8.5 \mathrm{~mA}$ full-scale current $010=12 \mathrm{~mA}$ full-scale current $011=15.5 \mathrm{~mA}$ full-scale current $100=19 \mathrm{~mA}$ full-scale current $101=22.5 \mathrm{~mA}$ full-scale current $110=26 \mathrm{~mA}$ full-scale current $111=29.5 \mathrm{~mA}$ full-scale current |  |  | $0=$ <br> exponential mapping 1 = linear mapping | 0 = Device <br> Disabled <br> 1 = Device <br> Enabled |

## ALS CONFIGURATION REGISTER

The ALS Configuration Register controls the Ambient Light Sensing input functions and is described in Figure 19 and Table 6.


30086610
FIGURE 19. ALS Configuration Register

TABLE 6. ALS Configuration Register Description (0x20)

| Bit 7 | Bit 6 Bit 5 <br> ALS Input ALS Input <br> Select Select | Bit 4 Bit 3 <br> ALS Enable ALS Enable | Bit 2 <br> ALS <br> Averaging <br> Time | Bit 1 <br> ALS <br> Averaging <br> Time | Bit 0 <br> ALS <br> Averaging <br> Time |
| :---: | :---: | :---: | :---: | :---: | :---: |
| N/A | $00=$ The Average of ALS1 and ALS2 is used to control the LED brightness $01=\mathrm{ALS} 1$ is used to control the LED brightness $10=$ ALS2 is used to control the LED brightness 11 = The ALS input with the highest voltage is used to control the LED brightness | 00 or $10=A L S$ is disabled. The Brightness Register is used to determine the LED current. 01 = ALS is enabled. The Brightness Register is used to determine the LED Current. 11 = ALS inputs are enabled. Ambient light determines the LED current. | $\begin{aligned} & 000=32 \mathrm{~ms} \\ & 001=64 \mathrm{~ms} \\ & 010=128 \mathrm{~ms} \\ & 011=256 \mathrm{~ms} \\ & 100=512 \mathrm{~ms} \\ & 101=1024 \mathrm{~ms} \\ & 110=2048 \mathrm{~ms} \\ & 111=4096 \mathrm{~ms} \end{aligned}$ |  |  |

## BRIGHTNESS RAMP RATE REGISTER

The Brightness Ramp Rate Register controls the rate of rise or fall of the LED current. Both the rising rate and falling rate
are independently adjustable Figure 20 and Table 7 describe the bit settings.


FIGURE 20. Brightness Ramp Rate Register

TABLE 7. Brightness Ramp Rate Register Description (0x30)

| Bit 7 | Bit 6 | Bit 5 <br> (BRRI2) | Bit 4 (BRRI1) | Bit 3 (BRRIO) | Bit 2 <br> (BRRD2) | Bit 1 <br> (BRRD1) | Bit 0 <br> (BRRDO) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N/A | N/A | $000=8 \mu \mathrm{~s} / \mathrm{step}$ ( 1.106 ms from 0 to Full Scale) $001=1.024 \mathrm{~ms} / \mathrm{step}$ ( 130 ms from 0 to Full Scale) $010=2.048 \mathrm{~ms} /$ step ( 260 ms from 0 to Full Scale) $011=4.096 \mathrm{~ms} / \mathrm{step}$ ( 520 ms from 0 to Full Scale) $100=8.192 \mathrm{~ms} / \mathrm{step}(1.04 \mathrm{~s}$ from 0 to Full Scale) $101=16.384 \mathrm{~ms} /$ step (2.08s from 0 to Full Scale) $110=32.768 \mathrm{~ms} /$ step ( 4.16 s from 0 to Full Scale) |  |  | $000=8 \mu \mathrm{~s} /$ step (1.106ms from Full Scale to 0) $001=1.024 \mathrm{~ms} / \mathrm{step}(130 \mathrm{~ms}$ from Full Scale to 0 ) $010=2.048 \mathrm{~ms} / \mathrm{step}(260 \mathrm{~ms}$ from Full Scale to 0$)$ $011=4.096 \mathrm{~ms} / \mathrm{step}(520 \mathrm{~ms}$ from Full Scale to 0) $100=8.192 \mathrm{~ms} / \mathrm{step}(1.04 \mathrm{~s}$ from Full Scale to 0) $101=16.384 \mathrm{~ms} /$ step ( 2.08 s from Full Scale to 0 ) $110=32.768 \mathrm{~ms} /$ step ( 4.16 s from Full Scale to 0 ) <br> $111=65.538 \mathrm{~ms} / \mathrm{step}(8.32 \mathrm{~s}$ from Full Scale to 0$)$ |  |  |

## ALS ZONE INFORMATION REGISTER

The ALS Zone Information Register is a read-only register that is updated every time the active ALS input(s) detect that the ambient light has changed to a new zone as programmed in the Zone Boundary Registers. See Zone Boundary Registers description. A new update to the ALS Zone Information

Register is signaled by the INT output going from high to low. A read-back of the ALS Zone Information Register will cause the INT output to go open-drain again. The Zone Change Flag (bit 3) is also updated on a Zone change and cleared on a read back of the ALS Zone Information Register. Figure 21 and Table 8 detail the ALS Zone Information Register.


30086612
FIGURE 21. ALS Zone Information Register

TABLE 8. ALS Zone Information Register Description (0x40)

| Bit 7 | Bit 6 | Bit 5 | Bit 4 | Bit 3 <br> (Zone Boundary Change <br> Flag) | Bit 2 <br> (Z2) | Bit 1 <br> (Z1) |
| :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| N/A | N/A | N/A | N/A | $1=$ the active ALS input has <br> changed to a new ambient <br> (ZO) |  |  |
| light zone as a programmed in |  |  |  |  |  |  |
| the Zone Boundary Registers |  |  |  |  |  |  |
| (ZBO -ZB3) |  |  |  |  |  |  |
| $0=$ no zone change |  |  |  |  |  |  |$\quad$| $000=$ Zone 0 |
| :--- |
| $001=$ Zone 1 |
| $010=$ Zone 2 |
| $011=$ Zone 3 |
| $100=$ Zone 4 |$\quad$.

## ALS RESISTOR SELECT REGISTER

The ALS Resistor Select Register configures the internal resistance from either the ALS1 or ALS2 input to GND. Bits [3:0] program the input resistance at the ALS1 input and bits [7:4]
program the input resistance at the ALS2 input. With bits [3:0] set to all zeroes the ALS1 input is high impedance. With bits [7:4] set to all zeroes the ALS2 input is high impedance.


30086634
FIGURE 22. ALS Resistor Select Register

TABLE 9. ALS Resistor Select Register Description (0x41)

| Bit 7 <br> (ALSR2A | Bit 6 (ALSR2B | Bit 5 <br> (ALSR2C) | Bit 4 | Bit 3 | Bit 2 | $1$ | $0$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 0000=\mathrm{ALS} 2 \text { is high impedance } \\ & 0001=13.531 \mathrm{k} \Omega(73.9 \mu \mathrm{~A} \text { at } 1 \mathrm{~V}) \\ & 0010=9.011 \mathrm{k} \Omega(111 \mu \mathrm{~A} \text { at } 1 \mathrm{~V}) \\ & 0011=5.4116 \mathrm{k} \Omega(185 \mu \mathrm{~A} \text { at } 1 \mathrm{~V}) \\ & 0100=2.271 \mathrm{k} \Omega(440 \mu \mathrm{~A} \text { at } 1 \mathrm{~V}) \\ & 0101=1.946 \mathrm{k} \Omega(514 \mu \mathrm{~A} \text { at } 1 \mathrm{~V}) \\ & 0110=1.815 \mathrm{k} \Omega(551 \mu \mathrm{~A} \text { at } 1 \mathrm{~V}) \\ & 0111=1.6 \mathrm{k} \Omega(625 \mu \mathrm{~A} \text { at } 1 \mathrm{~V}) \\ & 1000=1.138 \mathrm{k} \Omega(879 \mu \mathrm{~A} \text { at } 1 \mathrm{~V}) \\ & 1001=1.05 \mathrm{k} \Omega(952 \mu \mathrm{~A} \text { at } 1 \mathrm{~V}) \\ & 1010=1.011 \mathrm{k} \Omega(989 \mathrm{~A} \text { at } 1 \mathrm{~V}) \\ & 1011=941 \Omega(1.063 \mathrm{~mA} \text { at } 1 \mathrm{~V}) \\ & 1100=759 \Omega(1.318 \mathrm{~mA} \text { at } 1 \mathrm{~V}) \\ & 1101=719 \Omega(1.391 \mathrm{~mA} \text { at } 1 \mathrm{~V}) \\ & 1110=700 \Omega(1.429 \mathrm{~mA} \text { at } 1 \mathrm{~V}) \\ & 1111=667 \Omega(1.499 \mathrm{~mA} \text { at } 1 \mathrm{~V}) \end{aligned}$ |  |  |  | ```0000 = ALS2 is high impedance 0001 = 13.531k\Omega (73.9\muA at 1V) 0010 =9.011k\Omega (111\muA at 1V) 0011 = 5.4116k\Omega (185\muA at 1V) 0100 = 2.271k\Omega (440\muA at 1V) 0101 = 1.946k\Omega (514\muA at 1V) 0110 = 1.815k\Omega (551\muA at 1V) 0111 = 1.6k\Omega (625\muA at 1V) 1000 = 1.138k\Omega (879\muA at 1V) 1001 = 1.05k\Omega (952\muA at 1V) 1010 = 1.011k\Omega (989\muA at 1V) 1011 = 941\Omega (1.063mA at 1V) 1100 = 759\Omega (1.318mA at 1V) 1101 = 719\Omega (1.391mA at 1V) 1110=700\Omega (1.429mA at 1V) 1111 = 667\Omega (1.499mA at 1V)``` |  |  |  |

## BRIGHTNESS CONTROL REGISTER

The Brightness Register (BRT) is an 8-bit register that programs the 127 different LED current levels (Bits [6:0]). The code written to BRT is translated into an LED current as a percentage of $\mathrm{I}_{\text {LED_FULLSCALE }}$ as set via the Full-Scale Current Select bits (General Configuration Register bits [4:2]). The LED current response has a typical 1000:1 dimming ratio at the maximum full-scale current (General Configuration Register bits [4:2] = (111) and using the exponential weighted dimming curve.

There are two selectable LED current profiles. Setting the General Configuration Register bit 1 to 0 selects the exponentially weighted LED current response (see Figure 11). Setting this bit to ' 1 ' selects the linear weighted curve (see Figure 12). Table 2 and Table 3 show the percentage FullScale LED Current at a given Brightness Register Code for both the Exponential and Linear current response.


FIGURE 23. Brightness Control Register

TABLE 10. Brightness Control Register Description (0xA0)

| $\begin{array}{\|l} \hline \text { Bit } 7 \\ \text { N/A } \end{array}$ | Bit 6 <br> Data (MSB) | Bit 5 <br> Data | Bit 4 <br> Data | $\begin{array}{l\|l\|} \hline \text { Bit } 3 \\ \text { Data } \end{array}$ | $\begin{aligned} & \hline \text { Bit } 2 \\ & \text { Data } \end{aligned}$ | Bit 1 <br> Data | Bit 0 <br> Data |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | LED Brightness Data (Bits [6:0] |  |  |  |  |  |  |
|  | Exponential Mapping (see FIX) $0000000 \text { = LEDs Off }$ $0000001=0.08 \% \text { of Full Scale }$ <br> $1111111=100 \%$ of Full Scale |  |  | Linear Mapping (see FIX) $0000000=$ LEDs Off $0000001=0.79 \%$ of Full Scale : <br> $1111111=100 \%$ of Full Scale |  |  |  |

## ZONE BOUNDARY REGISTER

The Zone Boundary Registers are programmed with the ambient light sensing zone boundaries. The default values are set at $20 \%(200 \mathrm{mV}), 40 \%(400 \mathrm{mV}), 60 \%(600 \mathrm{mV})$, and $80 \%$
$(800 \mathrm{mV})$ of the full-scale ALS input voltage range (1V). The necessary conditions for proper ALS operation are that the data in ZB0 < data in ZB1 < data in ZB2 < data in ZB3.
Zone Boundary Register 0 (ZB0)
MSB Address 0x60, Default Value 0x33 LSB

| Bit 7 <br> Data | Bit 6 <br> Data | Bit 5 <br> Data | Bit 4 <br> Data | Bit 3 <br> Data | Bit 2 <br> Data | Bit 1 <br> Data | Bit 0 <br> Data |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| MSB | Zone Boundary Register 1 (ZB1) Address 0x61, Default Value 0x66 |  |  |  |  |  | LSB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bit 7 <br> Data | Bit 6 <br> Data | Bit 5 <br> Data | Bit 4 <br> Data | Bit 3 <br> Data | Bit 2 <br> Data | Bit 1 <br> Data | Bit 0 <br> Data |

Zone Boundary Register 2 (ZB2)
Address 0x62, Default Value 0x99
LSB
MSB

| Bit 7 <br> Data | Bit 6 Data | Bit 5 Data | Bit 4 <br> Data | Bit 3 <br> Data | Bit 2 <br> Data | Bit 1 <br> Data | Bit 0 <br> Data |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |


| MSB | Zone Boundary Register 3 (ZB3) Address 0x63, Default Value 0xCC |  |  |  |  |  | LSB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bit 7 <br> Data | Bit 6 Data | Bit 5 <br> Data | Bit 4 <br> Data | Bit 3 <br> Data | Bit 2 <br> Data | Bit 1 <br> Data | Bit 0 <br> Data |

30086613
FIGURE 24. Zone Boundary Registers

## ZONE TARGET REGISTERS

The Zone Target Registers contain the LED brightness data that corresponds to the current active ALS zone. The default
values for these registers and their corresponding percentage of full-scale current for both linear and exponential brightness is shown in Figure 25 and Table 11.


30086614
FIGURE 25. Zone Target Registers

TABLE 11. Zone Boundary and Zone Target Default Mapping

| Zone Boundary <br> (Default) | Zone Target <br> Register <br> (Default) | Full-Scale <br> Current (Default) | Linear Mapping <br> (Default) | Exponential <br> Mapping <br> (Default) |
| :--- | :--- | :--- | :--- | :--- |
| Boundary 0, <br> Active ALS input is less than 200 <br> mV | $0 x 19$ | 19 mA | $19.69 \%(3.74 \mu \mathrm{~A})$ | $0.336 \%(68.4 \mu \mathrm{~A})$ |
| Boundary 1, <br> Active ALS input is between 200 mV <br> and 400 mV | $0 \times 33$ | 19 mA | $40.16 \%(7.63 \mu \mathrm{~A})$ | $1.43 \%(272 \mu \mathrm{~A})$ |
| Boundary 2, <br> Active ALS input is between 400 mV <br> and 600 mV | $0 \times 4 \mathrm{C}$ | 19 mA | $59.84 \%(11.37$ <br> $\mathrm{mA})$ | $5.78 \%(1.098 \mathrm{~mA})$ |
| Boundary 3, <br> Active ALS input is between 600 mV <br> and 800 mV | $0 \times 66$ | 19 mA | $80.31 \%(15.26$ <br> $\mathrm{mA})$ | $24.84 \%(4.72 \mathrm{~mA})$ |
| Boundary 4, <br> Active ALS input is greater than <br> 800 mV | $0 \times 7 \mathrm{~F}$ | 19 mA | $100 \%(19 \mathrm{~mA})$ | $100 \%(19 \mathrm{~mA})$ |

## Applications Information

## LED CURRENT SETTING/MAXIMUM LED CURRENT

The maximum LED current is restricted by the following factors: the maximum duty cycle that the boost converter can achieve, the peak current limitations, and the maximum output voltage.

## MAXIMUM DUTY CYCLE

The LM3530 can achieve up to typically $94 \%$ maximum duty cycle. Two factors can cause the duty cycle to increase: an increase in the difference between $\mathrm{V}_{\text {OUT }}$ and $\mathrm{V}_{\text {IN }}$ and a decrease in efficiency. This is shown by the following equation:

$$
\mathrm{D}=1-\frac{\mathrm{VIN} \times \eta}{\mathrm{VOUT}}
$$

For a 9-LED configuration $\mathrm{V}_{\text {OUT }}=(3.6 \mathrm{~V} \times 9 \mathrm{LED}+\mathrm{VHR})=33 \mathrm{~V}$ operating with $\eta=70 \%$ from a 3 V battery, the duty cycle requirement would be around $93.6 \%$. Lower efficiency or larger $\mathrm{V}_{\text {Out }}$ to $\mathrm{V}_{\text {IN }}$ differentials can push the duty cycle requirement beyond $94 \%$.

## PEAK CURRENT LIMIT

The LM3530's boost converter has a peak current limit for the internal power switch of 839 mA typical ( 739 mA minimum). When the peak switch current reaches the current limit, the duty cycle is terminated resulting in a limit on the maximum output current and thus the maximum output power the LM3530 can deliver. Calculate the maximum LED current as a function of $\mathrm{V}_{\mathrm{IN}_{\mathrm{N}}}, \mathrm{V}_{\text {OUT }}$, L , efficiency $(\eta)$ and $\mathrm{I}_{\text {PEAK }}$ as:
where $f_{\text {SW }}=500 \mathrm{kHz}$, and $\eta$ and $\mathrm{I}_{\text {PEAK }}$ can be found in the efficiency and $\mathrm{I}_{\text {PEAK }}$ curves in the Typical Performance Characteristics.

## OUTPUT VOLTAGE LIMITATIONS

The LM3530 has a maximum output voltage of 41V typical ( 40 V minimum) for the LM3530-40 version and 24 V typical ( 23.6 V minimum) for the 25 V version. When the output voltage rises above this threshold ( $\mathrm{V}_{\mathrm{ovp}}$ ) the over-voltage protection feature is activated and the duty cycle is terminated. Switching will cease until $\mathrm{V}_{\text {OUT }}$ drops below the hysteresis level (typically 1 V below $\mathrm{V}_{\text {ovp }}$ ). For larger numbers of series connected LEDs the output voltage can reach the OVP threshold at larger LED currents and colder ambient temperatures. Typically white LEDs have a $-3 \mathrm{mV} /{ }^{\circ} \mathrm{C}$ temperature coefficient.

## OUTPUT CAPACITOR SELECTION

The LM3530's output capacitor has two functions: filtering of the boost converters switching ripple, and to ensure feedback loop stability. As a filter, the output capacitor supplies the LED current during the boost converters on time and absorbs the inductor's energy during the switch off time. This causes a sag in the output voltage during the on time and a rise in the output voltage during the off time. Because of this, the output capacitor must be sized large enough to filter the inductor current ripple that could cause the output voltage ripple to become excessive. As a feedback loop component, the output capacitor must be at least $1 \mu \mathrm{~F}$ and have low ESR otherwise the LM3530's boost converter can become unstable. This requires the use of ceramic output capacitors. Table 12 lists part numbers and voltage ratings for different output capacitors that can be used with the LM3530.

$$
\begin{aligned}
& \mathrm{I}_{\text {OUT_MAX }}=\frac{\left(\mathrm{I}_{\text {PEAK }}-\Delta \mathrm{I}_{\mathrm{L}}\right) \times \eta \times \mathrm{V}_{\mathbb{I N}}}{\mathrm{V}_{\text {OUT }}} \\
& \text { where } \Delta \mathrm{I}_{\mathrm{L}}=\frac{\mathrm{V}_{\text {IN }} \times\left(\mathrm{V}_{\text {OUT }}-\mathrm{V}_{\mathbb{N}}\right)}{2 \times \mathrm{f}_{\text {SW }} \times L \times \mathrm{V}_{\text {OUT }}}
\end{aligned}
$$

TABLE 12. Recommended Input/Output Capacitors

| Manufacturer | Part Number | Value | Size | Rating | Description |
| :---: | :--- | :---: | :---: | :---: | :---: |
| Murata | GRM21BR71H105KA12 | $1 \mu \mathrm{~F}$ | 0805 | 50 V | COUT |
| Murata | GRM188B31A225KE33 | $2.2 \mu \mathrm{~F}$ | 0805 | 10 V | CIN |
| TDK | C1608X5R0J225 | $2.2 \mu \mathrm{~F}$ | 0603 | 6.3 V | CIN |

## INDUCTOR SELECTION

The LM3530 is designed to work with a $10 \mu \mathrm{H}$ to $22 \mu \mathrm{H}$ inductor. When selecting the inductor, ensure that the saturation rating for the inductor is high enough to accommodate the peak inductor current. The following equation calculates the peak inductor current based upon LED current, $\mathrm{V}_{\text {IN }}, \mathrm{V}_{\text {OUT }}$, and Efficiency.

$$
I_{\text {PEAK }}=\frac{I_{\text {LED }}}{\eta} \times \frac{V_{\text {OUT }}}{V_{\text {IN }}}+\Delta I_{\mathrm{L}}
$$

where:

$$
\Delta L_{L}=\frac{V_{\text {IN }} \times\left(V_{\text {OUT }}-V_{\text {IN }}\right)}{2 \times f_{\text {SW }} \times L \times V_{\text {OUT }}}
$$

When choosing $L$, the inductance value must also be large enough so that the peak inductor current is kept below the LM3530's switch current limit. This forces a lower limit on L given by the following equation.

$I_{\text {SW_max }}$ is given in the Electrical Table, efficiency $(\eta)$ is shown in the Typical Performance Characteristics, and $\mathrm{f}_{\mathrm{sw}}$ is typically 500 kHz .

TABLE 13. Suggested Inductors

| Manufacturer | Part Number | Value | Size | Rating | DC Resistance |
| :---: | :--- | :---: | :---: | :---: | :---: |
| TDK | VLF3014ST-100MR82 | $10 \mu \mathrm{H}$ | $2.8 \mathrm{~mm} \times 3 \mathrm{~mm} \times 1.4 \mathrm{~mm}$ | 820 mA | $0.25 \Omega$ |
| TDK | VLF3010ST-220MR34 | $22 \mu \mathrm{H}$ | $2.8 \mathrm{~mm} \times 3 \mathrm{~mm} \times 1 \mathrm{~mm}$ | 340 mA | $0.81 \Omega$ |
| TDK | VLF3010ST-100MR53 | $10 \mu \mathrm{H}$ | $2.8 \mathrm{~mm} \times 3 \mathrm{~mm} \times 1 \mathrm{~mm}$ | 530 mA | $0.41 \Omega$ |
| TDK | VLF4010ST-100MR80 | $10 \mu \mathrm{H}$ | $2.8 \mathrm{~mm} \times 3 \mathrm{~mm} \times 1 \mathrm{~mm}$ | 800 mA | $0.25 \Omega$ |
| TDK | VLS252010T-100M | $10 \mu \mathrm{H}$ | $2.5 \mathrm{~mm} \times 2 \mathrm{~mm} \times 1 \mathrm{~mm}$ | 650 mA | $0.71 \Omega$ |
| Coilcraft | LPS3008-103ML | $10 \mu \mathrm{H}$ | $2.95 \mathrm{~mm} \times 2.95 \mathrm{~mm} \times$ <br> 0.8 mm | 520 mA | $0.65 \Omega$ |
| Coilcraft | LPS3008-223ML | $22 \mu \mathrm{H}$ | $2.95 \mathrm{~mm} \times 2.95 \mathrm{~mm} \times$ <br> 0.8 mm | 340 mA | $1.5 \Omega$ |
| Coilcraft | LPS3010-103ML | $10 \mu \mathrm{H}$ | $2.95 \mathrm{~mm} \times 2.95 \mathrm{~mm} \times$ <br> 0.9 mm | 550 mA | $0.54 \Omega$ |
| Coilcraft | LPS3010-223ML | $22 \mu \mathrm{H}$ | $2.95 \mathrm{~mm} \times 2.95 \mathrm{~mm} \times$ <br> 0.9 mm | 360 mA | $1.2 \Omega$ |
| Coilcraft | XPL2010-103ML | $10 \mu \mathrm{H}$ | $1.9 \mathrm{~mm} \times 2 \mathrm{~mm} \times 1 \mathrm{~mm}$ | 610 mA | $0.56 \Omega$ |
| Coilcraft | EPL2010-103ML | $10 \mu \mathrm{H}$ | $2 \mathrm{~mm} \times 2 \mathrm{~mm} \times 1 \mathrm{~mm}$ | 470 mA | $0.91 \Omega$ |
| TOKO | DE2810C-1117AS-100M | $10 \mu \mathrm{H}$ | $3 \mathrm{~mm} \times 3.2 \mathrm{~mm} \times 1 \mathrm{~mm}$ | 600 mA | $0.46 \Omega$ |

DIODE SELECTION
The diode connected between SW and OUT must be a Schottky diode and have a reverse breakdown voltage high enough to handle the maximum output voltage in the application. Ta-
ble 14 lists various diodes that can be used with the LM3530. For 25 V OVP devices a 30 V Schottky is adequate. For 40 V OVP devices, a 40V Schottky diode should be used.

TABLE 14. Suggested Diodes

| Manufacturer | Part Number | Value | Size | Rating |
| :--- | :--- | :--- | :--- | :--- |
| Diodes Inc | B0540WS | Schottky | SOD-323 () | $40 \mathrm{~V} / 500 \mathrm{~mA}$ |
| Diodes Inc | SDM20U40 | Schottky | SOD-523 | $40 \mathrm{~V} / 200 \mathrm{~mA}$ |
|  |  |  | $(1.2 \mathrm{~mm} \times$ |  |
|  |  |  | $0.8 \mathrm{~mm} \times$ |  |
| On Semiconductor | NSR0340V2T1G | Schottky | SOD-523 | $40 \mathrm{~V} / 250 \mathrm{~mA}$ |
|  |  |  | $(1.2 \mathrm{~mm} \times$ |  |
|  |  |  | $0.8 \mathrm{~mm} \times$ |  |
| On Semiconductor | NSR0240V2T1G | Schottky | SOD-523 | $40 \mathrm{~V} / 250 \mathrm{~mA}$ |
|  |  |  | $(1.2 \mathrm{~mm} \times$ |  |
|  |  |  | $0.8 \mathrm{~mm} \times$ |  |
|  |  |  |  |  |
|  |  |  |  |  |

## BOARD LAYOUT GUIDELINES

The LM3530 contains an inductive boost converter which sees a high switched voltage (up to 40V) at the SW pin, and a step current (up to 900 mA ) through the Schottky diode and output capacitor each switching cycle. The high switching voltage can create interference into nearby nodes due to electric field coupling ( $(=\mathrm{CdV} / \mathrm{dt}$ ). The large step current
through the diode and the output capacitor can cause a large voltage spike at the SW pin and the OVP pin due to parasitic inductance in the step current conducting path ( $\mathrm{V}=\mathrm{Ldi} / \mathrm{dt}$ ). Board layout guidelines are geared towards minimizing this electric field coupling and conducted noise. Figure 26 highlights these two noise generating components.


FIGURE 26. LM3530's Boost Converter Showing Pulsed Voltage at SW (High dV/dt) and Current Through Schottky and $\mathrm{C}_{\text {OUT }}$ (High dl/dt)

The following lists the main (layout sensitive) areas of the LM3530 in order of decreasing importance:

Output Capacitor

- Schottky Cathode to $\mathrm{C}_{\text {OUT }}{ }^{+}$
- $\mathrm{C}_{\text {OUT }}$ to GND


## Schottky Diode

- SW Pin to Schottky Anode
- Schottky Cathode to cout+

Inductor

- SW Node PCB capacitance to other traces


## Input Capacitor

- CIN+ to IN pin
- CIN- to GND


## Output Capacitor Placement

The output capacitor is in the path of the inductor current discharge path. As a result $\mathrm{C}_{\text {OUT }}$ sees a high current step from 0 to $I_{\text {PEAK }}$ each time the switch turns off and the Schottky diode turns on. Any inductance along this series path from the cathode of the diode through $\mathrm{C}_{\text {OUT }}$ and back into the LM3530's GND pin will contribute to voltage spikes $\left(V_{\text {SPIKE }}=L_{P_{-}} \times \mathrm{dl} /\right.$ dt ) at SW and OUT which can potentially over-voltage the SW pin, or feed through to GND. To avoid this, $\mathrm{C}_{\mathrm{OUT}^{+}}$must be connected as close as possible to the Cathode of the Schottky diode and $\mathrm{C}_{\text {Out }^{-}}$must be connected as close as possible to the LM3530's GND bump. The best placement for $\mathrm{C}_{\text {OUT }}$ is on the same layer as the LM3530 so as to avoid any vias that can add excessive series inductance (see Figure 28, Figure 29, and Figure 30).

## Schottky Diode Placement

The Schottky diode is in the path of the inductor current discharge. As a result the Schottky diode sees a high current step from 0 to $\mathrm{I}_{\text {PEAK }}$ each time the switch turns off and the diode turns on. Any inductance in series with the diode will cause a voltage spike ( $\mathrm{V}_{\text {SPIKE }}=\mathrm{L}_{\mathrm{P}_{-}} \times \mathrm{dl} / \mathrm{dt}$ ) at SW and OUT which can potentially over-voltage the SW pin, or feed through to $\mathrm{V}_{\text {OUT }}$ and through the output capacitor and into GND. Connecting the anode of the diode as close as possible to the SW pin and the cathode of the diode as close as possible to $\mathrm{C}_{\text {OUt }}$ + will reduce the inductance ( $\mathrm{L}_{\mathrm{P}}$ ) and minimize these voltage spikes (see Figure 28, Figure 29, andFigure 30 ).

## Inductor Placement

The node where the inductor connects to the LM3530's SW bump has 2 issues. First, a large switched voltage ( 0 to $\mathrm{V}_{\text {OUT }}+\mathrm{V}_{\text {F_SснотткY }}$ ) appears on this node every switching cycle. This switched voltage can be capacitively coupled into nearby nodes. Second, there is a relatively large current (input current) on the traces connecting the input supply to the inductor and connecting the inductor to the SW bump. Any resistance in this path can cause large voltage drops that will negatively affect efficiency.
To reduce the capacitively coupled signal from SW into nearby traces, the SW bump to inductor connection must be minimized in area. This limits the PCB capacitance from SW to other traces. Additionally, the other traces need to be routed away from SW and not directly beneath. This is especially true for high impedance nodes that are more susceptible to capacitive coupling such as (SCL, SDA, HWEN, PWM, and possibly ASL1 and ALS2). A GND plane placed directly below SW will dramatically reduce the capacitance from SW into nearby traces
To limit the trace resistance of the VBATT to inductor connection and from the inductor to SW connection, use short, wide traces (see Figure 28, Figure 29, and Figure 30).

## Input Capacitor Selection and Placement

The input bypass capacitor filters the inductor current ripple, and the internal MOSFET driver currents during turn on of the power switch.
The driver current requirement can range from 50 mA at 2.7 V to over 200 mA at 5.5 V with fast durations of approximately 10 ns to 20 ns . This will appear as high di/dt current pulses
coming from the input capacitor each time the switch turns on. Close placement of the input capacitor to the IN pin and to the GND pin is critical since any series inductance between IN and $\mathrm{C}_{\mathrm{IN}^{+}}$or $\mathrm{C}_{\mathrm{IN}^{-}}$and GND can create voltage spikes that could appear on the $\mathrm{V}_{\mathrm{IN}}$ supply line and in the GND plane.
Close placement of the input bypass capacitor at the input side of the inductor is also critical. The source impedance (inductance and resistance) from the input supply, along with the input capacitor of the LM3530, form a series RLC circuit. If the output resistance from the source $\left(\mathrm{R}_{\mathrm{S}}\right)$ is low enough the circuit will be underdamped and will have a resonant frequency (typically the case). Depending on the size of $\mathrm{L}_{\mathrm{S}}$ the resonant frequency could occur below, close to, or above the LM3530's switching frequency. This can cause the supply current ripple to be:

1. Approximately equal to the inductor current ripple when the resonant frequency occurs well above the LM3530's switching frequency;
2. Greater then the inductor current ripple when the resonant frequency occurs near the switching frequency; and
3. Less then the inductor current ripple when the resonant frequency occurs well below the switching frequency. Figure 27 shows the series RLC circuit formed from the output impedance of the supply and the input capacitor. The circuit is re-drawn for the AC case where the $\mathrm{V}_{\text {IN }}$ supply is replaced with a short to GND and the LM3530 + Inductor is replaced with a current source ( $\Delta \mathrm{I}_{\mathrm{L}}$ ).
Equation 1 is the criteria for an underdamped response. Equation 2 is the resonant frequency. Equation 3 is the approximated supply current ripple as a function of $\mathrm{L}_{\mathrm{S}}, \mathrm{R}_{\mathrm{S}}$, and $\mathrm{C}_{\mathrm{IN}}$. As an example, consider a 3.6 V supply with $0.1 \Omega$ of series resistance connected to $\mathrm{C}_{\text {IN }}$ through 50 nH of connecting traces. This results in an underdamped input filter circuit with a resonant frequency of 712 kHz . Since the switching frequency lies near to the resonant frequency of the input RLC network, the supply current is probably larger then the inductor current ripple. In this case using equation 3 from Figure 27 the supply current ripple can be approximated as $1.68 \times$ 's the inductor current ripple. Increasing the series inductance $\left(L_{S}\right)$ to 500 nH causes the resonant frequency to move to around 225 kHz and the supple current ripple to be approximately $0.25 \times$ 's the inductor current ripple.

4. $\frac{1}{\mathrm{~L}_{\mathrm{S}} \times \mathrm{C}_{\mathrm{IN}}}>\frac{\mathrm{R}_{\mathrm{S}}{ }^{2}}{4 \times \mathrm{L}_{\mathrm{S}}{ }^{2}}$
5. $f_{\text {RESONANT }}=\frac{1}{2 \pi \sqrt{L_{S} \times C_{I N}}}$
6. $I_{\text {SUPPLYRIPPLE }} \approx \Delta I_{L} \times \frac{\frac{1}{2 \pi \times 500 \mathrm{kHz} \mathrm{\times C}_{I N}}}{\sqrt{R_{S}{ }^{2}+\left(2 \pi \times 500 k H z \times L_{S}-\frac{1}{\left.2 \pi \times 500 \mathrm{kHz} \mathrm{\times C}_{\mid N}\right)^{2}}\right.}}$
30086628

FIGURE 27. Input RLC Network

Example Layouts
The following three figures show example layouts which apply the required proper layout guidelines. These figures should be used as guides for laying out the LM3530's circuit.


FIGURE 28. Layout Example \#1


300866a2
FIGURE 29. Layout Example \#2


TABLE 15. Application Circuit Component List

| Compon- <br> ent | Manufact- <br> urer | Part Number | Value | Size | Current/Voltage <br> Rating |
| :--- | :--- | :--- | :--- | :---: | :--- |
| L | TDK | VLF3014ST- <br> 100 MR 22 | $10 \mu \mathrm{H}$ | $3 \mathrm{~mm} \times 3 \mathrm{~mm} \times$ <br> 1.4 mm | $\mathrm{I}_{\text {SAT }}=820 \mathrm{~mA}$ |
| COUT | Murata | GRM21BR71 <br> H105KA12 | $1 \mu \mathrm{~F}$ | 0805 | 50 V |
| CIN | Murata | GRM188B31 <br> A225KE33 | $2.2 \mu \mathrm{~F}$ | 0603 | 10 V |
| D1 | Diodes Inc. | B0540WS | Schottky | SOD-323 | $40 \mathrm{~V} / 500 \mathrm{~mA}$ |
| ALS1 | Avago | APDS-9005 | Ambient <br> Light <br> Sensor | $1.6 \mathrm{~mm} \times$ <br> $1.5 \mathrm{~mm} \times$ <br> 0.6 mm | 0 to 1100 Lux |
|  |  |  | Ambient <br> Light | $1.6 \mathrm{~mm} \times$ <br> $1.5 \mathrm{~mm} \times$ <br> Sensor | 0 to 1100 Lux |
| ALS2 | Avago | APDS-9005 |  |  |  |

Physical Dimensions inches (millimeters) unless otherwise noted


## Notes

LM3530 High Efficiency White LED Driver with Programmable Ambient Light Sensing Capability


## Notes

For more National Semiconductor product information and proven design tools, visit the following Web sites at: www.national.com

| Products |  | Design Support |  |
| :--- | :--- | :--- | :--- |
| Amplifiers | www.national.com/amplifiers | WEBENCH® Tools | www.national.com/webench |
| Audio | www.national.com/audio | App Notes | www.national.com/appnotes |
| Clock and Timing | www.national.com/timing | Reference Designs | www.national.com/refdesigns |
| Data Converters | www.national.com/adc | Samples | www.national.com/samples |
| Interface | www.national.com/interface | Eval Boards | www.national.com/evalboards |
| LVDS | www.national.com/lvds | Packaging | www.national.com/packaging |
| Power Management | www.national.com/power | Green Compliance | www.national.com/quality/green |
| Switching Regulators | www.national.com/switchers | Distributors | www.national.com/contacts |
| LDOs | www.national.com/ldo | Quality and Reliability | www.national.com/quality |
| LED Lighting | www.national.com/led | Feedback/Support | www.national.com/feedback |
| Voltage References | www.national.com/vref | Design Made Easy | www.national.com/easy |
| PowerWise® Solutions | www.national.com/powerwise | Applications \& Markets | www.national.com/solutions |
| Serial Digital Interface (SDI) | www.national.com/sdi | Mil/Aero | www.national.com/milaero |
| Temperature Sensors | www.national.com/tempsensors | SolarMagicTM | www.national.com/solarmagic |
| PLL/VCO | www.national.com/wireless | PowerWise® Design <br> University | www.national.com/training |

THE CONTENTS OF THIS DOCUMENT ARE PROVIDED IN CONNECTION WITH NATIONAL SEMICONDUCTOR CORPORATION ("NATIONAL") PRODUCTS. NATIONAL MAKES NO REPRESENTATIONS OR WARRANTIES WITH RESPECT TO THE ACCURACY OR COMPLETENESS OF THE CONTENTS OF THIS PUBLICATION AND RESERVES THE RIGHT TO MAKE CHANGES TO SPECIFICATIONS AND PRODUCT DESCRIPTIONS AT ANY TIME WITHOUT NOTICE. NO LICENSE, WHETHER EXPRESS, IMPLIED, ARISING BY ESTOPPEL OR OTHERWISE, TO ANY INTELLECTUAL PROPERTY RIGHTS IS GRANTED BY THIS DOCUMENT.
TESTING AND OTHER QUALITY CONTROLS ARE USED TO THE EXTENT NATIONAL DEEMS NECESSARY TO SUPPORT NATIONAL'S PRODUCT WARRANTY. EXCEPT WHERE MANDATED BY GOVERNMENT REQUIREMENTS, TESTING OF ALL PARAMETERS OF EACH PRODUCT IS NOT NECESSARILY PERFORMED. NATIONAL ASSUMES NO LIABILITY FOR APPLICATIONS ASSISTANCE OR BUYER PRODUCT DESIGN. BUYERS ARE RESPONSIBLE FOR THEIR PRODUCTS AND APPLICATIONS USING NATIONAL COMPONENTS. PRIOR TO USING OR DISTRIBUTING ANY PRODUCTS THAT INCLUDE NATIONAL COMPONENTS, BUYERS SHOULD PROVIDE ADEQUATE DESIGN, TESTING AND OPERATING SAFEGUARDS.
EXCEPT AS PROVIDED IN NATIONAL'S TERMS AND CONDITIONS OF SALE FOR SUCH PRODUCTS, NATIONAL ASSUMES NO LIABILITY WHATSOEVER, AND NATIONAL DISCLAIMS ANY EXPRESS OR IMPLIED WARRANTY RELATING TO THE SALE AND/OR USE OF NATIONAL PRODUCTS INCLUDING LIABILITY OR WARRANTIES RELATING TO FITNESS FOR A PARTICULAR PURPOSE, MERCHANTABILITY, OR INFRINGEMENT OF ANY PATENT, COPYRIGHT OR OTHER INTELLECTUAL PROPERTY RIGHT.

## LIFE SUPPORT POLICY

NATIONAL'S PRODUCTS ARE NOT AUTHORIZED FOR USE AS CRITICAL COMPONENTS IN LIFE SUPPORT DEVICES OR SYSTEMS WITHOUT THE EXPRESS PRIOR WRITTEN APPROVAL OF THE CHIEF EXECUTIVE OFFICER AND GENERAL COUNSEL OF NATIONAL SEMICONDUCTOR CORPORATION. As used herein:
Life support devices or systems are devices which (a) are intended for surgical implant into the body, or (b) support or sustain life and whose failure to perform when properly used in accordance with instructions for use provided in the labeling can be reasonably expected to result in a significant injury to the user. A critical component is any component in a life support device or system whose failure to perform can be reasonably expected to cause the failure of the life support device or system or to affect its safety or effectiveness.

National Semiconductor and the National Semiconductor logo are registered trademarks of National Semiconductor Corporation. All other brand or product names may be trademarks or registered trademarks of their respective holders.
Copyright® 2011 National Semiconductor Corporation
For the most current product information visit us at www.national.com

| National Semiconductor | National Semiconductor Europe | National Semiconductor Asia | National Semiconductor Japan |
| :--- | :--- | :--- | :--- |
| Americas Technical | Technical Support Center | Pacific Technical Support Center | Technical Support Center |
| Support Center | Email: europe.support@nsc.com | Email: ap.support@nsc.com |  |
| Email: support@nsc.com |  |  |  |
| Tel: $1-800-272-9959$ |  |  |  |

